Protection of Environment

40

PART 63 (§§ 63.1200—End)
Revised as of July 1, 1999

CONTAINING
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AND FUTURE EFFECT
AS OF JULY 1, 1999

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Title 40, Parts 63, (§ 63.1200–End

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To cite the regulations in this volume use title, part and section number. Thus, 40 CFR 63.1211 refers to title 40, part 63, section 1211.
Explanation

The Code of Federal Regulations is a codification of the general and permanent rules published in the Federal Register by the Executive departments and agencies of the Federal Government. The Code is divided into 50 titles which represent broad areas subject to Federal regulation. Each title is divided into chapters which usually bear the name of the issuing agency. Each chapter is further subdivided into parts covering specific regulatory areas.

Each volume of the Code is revised at least once each calendar year and issued on a quarterly basis approximately as follows:
- Title 1 through Title 16: as of January 1
- Title 17 through Title 27: as of April 1
- Title 28 through Title 41: as of July 1
- Title 42 through Title 50: as of October 1

The appropriate revision date is printed on the cover of each volume.

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The Paperwork Reduction Act of 1980 (Pub. L. 96-511) requires Federal agencies to display an OMB control number with their information collection request.
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(b) The matter incorporated is in fact available to the extent necessary to afford fairness and uniformity in the administrative process.

(c) The incorporating document is drafted and submitted for publication in accordance with 1 CFR part 51.

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An index to the text of “Title 3—The President” is carried within that volume.

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RAYMOND A. MOSLEY,
Director,
Office of the Federal Register.

July 1, 1999.
Title 40—Protection of Environment is composed of twenty-four volumes. The parts in these volumes are arranged in the following order: parts 1-49, parts 50-51, part 52 (52.01-52.1018), part 52 (52.1019-End), parts 53-59, part 60, parts 61-62, part 63 (63.1-63.1199), part 63 (63.1200-End), parts 64-71, parts 72-80, parts 81-85, part 86, parts 87-135, parts 136-149, parts 150-189, parts 190-259, parts 260-265, parts 266-299, parts 300-399, parts 400-424, parts 425-699, parts 700-789, and part 790 to End. The contents of these volumes represent all current regulations codified under this title of the CFR as of July 1, 1999.

Chapter I—Environmental Protection Agency appears in all twenty-four volumes. A Pesticide Tolerance Commodity/Chemical Index appears in parts 150-189. A Toxic Substances Chemical—CAS Number Index appears in parts 700-789 and part 790 to End. Redesignation Tables appear in the volumes containing parts 50-51, parts 150-189, and parts 700-789. Regulations issued by the Council on Environmental Quality appear in the volume containing part 790 to End. The OMB control numbers for title 40 appear in §9.1 of this chapter.

For this volume, Ruth Reedy Green was Chief Editor. The Code of Federal Regulations publication program is under the direction of Frances D. McDonald, assisted by Alomha S. Morris.
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Authority: 42 U.S.C. 7401 et seq.

Source: 57 FR 61992, Dec. 29, 1992, unless otherwise noted.

Subpart EEE—National Emission Standards for Hazardous Air Pollutants From Hazardous Waste Combustors

Source: 63 FR 33820, June 19, 1998, unless otherwise noted.

§ § 63.1200–63.1210 [Reserved]

§ 63.1211 Notification requirements.

(a) Notification of Intent To Comply (NIC). (1) All hazardous waste combustors subject to this subpart shall prepare a Notification of Intent to Comply that includes the following information:

(i) General information:
(A) The name and address of the owner/operator and the source;
(B) Whether the source is a major or an area source;
(C) Waste minimization and emission control technique(s) being considered;
(D) Emission control technique(s) being considered;

(E) Waste minimization and emission control technique(s) effectiveness;

(F) A description of the evaluation criteria used or to be used to select waste minimization and/or emission control technique(s); and

(G) A statement that the source intends to comply with this subpart by controlling emissions from the combustion of hazardous waste pursuant to the standards of this subpart.

(ii) Information on key activities and estimated dates for these activities that will bring the source into compliance with emission control requirements of this subpart. The submission of key activities and dates is not intended to be static and may be revised by the source during the period the NIC is in effect. Revisions shall be submitted to the regulatory authority and made available to the public. The following are the key activities and dates that shall be included:

(A) The dates for beginning and completion of engineering studies to evaluate emission control systems or process changes for emissions;

(B) The date by which contracts for emission control systems or process changes for emission control will be awarded, or the date by which orders will be issued for the purchase of component parts to accomplish emission control or process changes;

(C) The date by which construction applications will be submitted;

(D) The date by which on-site construction, installation of emission control equipment, or process change is to be initiated;
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(E) The date by which on-site construction, installation of emission control equipment, or process change is to be completed; and

(F) The date by which final compliance is to be achieved. The individual dates and milestones listed in paragraphs (a)(ii)(A) through (F) of this section as part of the NIC are not requirements and therefore are not enforceable deadlines; the Agency is requiring paragraphs (a)(ii)(A) through (F) of this section as part of the NIC only to inform the public of the source’s intentions towards coming into compliance.

(iii) A summary of the public meeting required under paragraph (b) of this section.

(iv) For any source that does not intend to comply, but will not stop burning hazardous waste as required under paragraph (c) of this section, a certification that the designated source will:

(A) Stop burning hazardous waste on or before the compliance date of the emission standards of this Subpart; and

(B) Be necessary to combust the hazardous waste from another on-site source, during the year prior to the compliance date of the emission standards of this Subpart, because that other source is:

(1) Installing equipment to come into compliance with the emission standards of this Subpart; or

(2) Installing source reduction modifications to eliminate the need for further combustion of wastes.

(2) A draft of the NIC must be made available for public review no later than 30 days prior to the public meeting required under paragraph (b)(1) of this section.

(3) The final NIC must be submitted to the permitting agency no later than one year following the effective date of the emission standards of this subpart.

(b) NIC Public Meeting and Notice. (1) Prior to the submission of the NIC to the permitting agency, and no later than 10 months after the effective date of the emission standards of this subpart, the source shall hold at least one informal meeting with the public to discuss anticipated activities described in the draft NIC for achieving compliance with the MACT standards promulgated in this subpart. The source must post a sign-in sheet or otherwise provide a voluntary opportunity for attendees to provide their names and addresses.

(2) The source shall submit a summary of the meeting, along with the list of attendees and their addresses developed under paragraph (b)(1) of this section, and copies of any written comments or materials submitted at the meeting, to the permitting agency as part of the final NIC, in accordance with paragraph (a)(ii)(A) of this section.

(3) The source must provide public notice of the NIC meeting at least 30 days prior to the meeting. The source shall provide public notice in all of the following forms:

(i) Newspaper advertisement. The source shall publish a notice in a newspaper of general circulation in the county or equivalent jurisdiction of the source. In addition, the source shall publish the notice in newspapers of general circulation in adjacent counties or equivalent jurisdiction where such publication would be necessary to inform the affected public. The notice must be published as a display advertisement.

(ii) Visible and accessible sign. The source shall post a notice on a clearly marked sign at or near the source. The sign must be large enough to be readable from the nearest spot where the public would pass by the source.

(iii) Broadcast media announcement. The source shall broadcast a notice at least once on at least one local radio station or television station.

(iv) Notice to the facility mailing list. The source shall provide a copy of the notice to the facility mailing list in accordance with §124.10(c)(1)(ix) of this chapter.

(4) The notices required under paragraph (b)(3) of this section must include:

(i) The date, time, and location of the meeting;

(ii) A brief description of the purpose of the meeting;

(iii) A brief description of the source and proposed operations, including the address or a map (e.g., a sketched or
§ 63.1212 Progress reports.

(a) General. Not later than two years after the effective date of the emission standards of this subpart, all sources subject to this subpart except those hazardous waste combustion sources that comply with paragraph (b)(2) of this section shall:

(1) Complete engineering design for any physical modifications to the source needed to comply with the emission standards of this subpart;

(2) Submit applicable construction applications to the applicable regulatory authority; and

(3) Enter into a binding contractual commitment to purchase, fabricate, and install any equipment, devices, and ancillary structures needed to comply with the emission requirements of this subpart.

(b) Demonstration. (1) Hazardous waste combustion sources shall submit to the regulatory authority a progress report on or before two years after the effective date of the emission standards of this subpart which contains information demonstrating that the source has met the requirements of paragraph (a) of this section. This information will be used by the regulatory authority to determine if the source has made adequate progress towards compliance with the applicable emission standards.

(2) Sources that intend to come into compliance with the emission standards of this subpart, but can do so without undertaking any of the activities described in paragraph (a) of this section, shall submit documentation either:

(i) Demonstrating that the source, at the time of the progress report, is in compliance with the emissions requirements; or

(ii) Specifying the steps that will be taken to bring the source into compliance, without undertaking any of the activities listed in paragraphs (a)(1) through (3) of this section.

(3) Sources that fail to comply with paragraph (a) above or paragraph (b)(2) of this section shall stop burning hazardous waste on or before the date two years after the effective date of the emission standards of this subpart.

(c) Schedule. (1) The progress report shall contain a detailed schedule that lists key dates for all projects that will bring the source into compliance with the requirements of this subpart (i.e., key dates for the activities required under paragraphs (b)(1)(i) through (iii) of this section). Dates shall cover the time frame from the progress report through the compliance date of the emission standards of this subpart.

(2) The schedule shall contain the following dates:

(i) Bid and award dates for construction contracts and equipment supply contractors;

(ii) Milestones such as ground breaking, completion of drawings and specifications, equipment deliveries, intermediate construction completions, and testing;

(iii) The dates on which applications were submitted for or obtained operating and construction permits or licenses;

(iv) The dates by which approvals of any permits or licenses are anticipated; and
(v) The projected date by which the source will be in compliance with the requirements of this subpart.

(d) Notice of intent to comply. The progress report shall contain a statement that the source intends or does not intend to come into compliance with the applicable emission control requirements of this subpart.

(e) Sources that do not intend to comply.

1) Sources that: indicated in their NIC their intent not to comply with this subpart and stop burning hazardous waste prior to the submittal of a progress report; or meet the requirements of paragraph (a)(1)(iv) of this section are not required to include the requirements of paragraphs (b) and (c) of this section to their progress report, but shall include in their progress report: the date on which the source stopped burning hazardous waste; and the date(s) on which RCRA closure documents were submitted.

2) Those sources that signify in the progress report, submitted not later than two years after the effective date of the emission standards of this subpart, their intention not to comply with the requirements of this subpart must stop burning hazardous waste on or before the date two years after the effective date of the emission standards of this subpart.

§ 63.1214 Extension of the compliance date.

(a) A source that intends to come into compliance with the requirements of this subpart, but due to the installation of controls will not meet the compliance date, may request an extension of the compliance date for one year.

(b) Sources subject to this subpart shall follow the requirements of §63.6(i)(4) or §63.1216 to request an extension of the compliance date.

§ 63.1215 Sources that become affected sources after the effective date of the emission standards of this subpart.

(a) A source that begins to burn hazardous waste after the effective date of the emission standards of this subpart, therefore becoming an affected source, but prior to 9 months after the effective date of the emission standards of this subpart shall comply with all the requirements of §§63.1211 through 63.1213 and associated time frames for public meetings and document submittals.

(b) A source that intends to begin burning hazardous waste more than 9 months after the effective date of the emission standards of this subpart, therefore becoming an affected source, shall meet all the requirements of §§63.1211 through 63.1213 prior to burning hazardous waste.

1) Such sources shall make a draft NIC available, notice their public meeting, hold their public meeting, and submit a final NIC prior to burning hazardous waste.

2) Such sources also shall submit their progress report at the time of the submittal of their final NIC.

§ 63.1216 Extension of the compliance date to install pollution prevention or waste minimization controls.

(a) Applicability. The owner or operator of any source subject to the requirements of this subpart may request from the Administrator or State with an approved Title V program an extension of one year to comply with the emission standards in this subpart, if the owner or operator can reasonably
§ 63.1250 Applicability.

(a) Definition of affected source. The affected source subject to this subpart is the pharmaceutical manufacturing operation, as defined in § 63.1251. Except as specified in paragraph (d) of this section, the provisions of this subpart apply to a pharmaceutical manufacturing operation that was subject to the National Emission Standards for Pharmaceuticals Production, at any time after October 21, 1998, and that is subject to the provisions of this subpart.

(b) Reasonable documentation that the installation of pollution prevention or waste minimization measures will significantly reduce the amount and/or toxicity of hazardous wastes entering the feedstream(s) of the combustion device(s) subject to this subpart, and that the facility could not otherwise install the necessary control measures and comply within three years after the effective date of the emission standards of this subpart.

(b) Requirements for requesting an extension. Requests for a one-year extension must be in writing, must be received not later than 12 months before the affected source’s compliance date, and must contain the following information:

(1) A description of pollution prevention or waste minimization controls that, when installed, will significantly reduce the amount and/or toxicity of hazardous wastes entering the feedstream(s) of the combustion device(s) subject to this subpart. Pollution prevention or waste minimization measures may include: equipment or technology modifications, reformulation or redesign of products, substitution of raw materials, improvements in work practices, maintenance, training, inventory control, or recycling practices conducted as defined in 40 CFR 261.1(c);

(2) A description of other pollution controls to be installed that are necessary to comply with the emission standards;

(3) A reduction goal or estimate of the annual reductions in quantity and/or toxicity of hazardous waste(s) entering the combustion feedstream(s) that will occur by installing the proposed pollution prevention or waste minimization measures;

(4) A comparison of reductions in the amounts and/or toxicity of hazardous wastes combusted after installation of pollution prevention or waste minimization measures to the amounts and/or toxicity of hazardous wastes combusted prior to the installation of these measures; and, if the difference is less than a fifteen percent reduction, a comparison to pollution prevention and waste minimization reductions recorded during the previous five years;

(5) Reasonable documentation that installation of the pollution prevention or waste minimization changes will not result in a net increase (except for documented increases in production) of hazardous constituents released to the environment through other emissions, wastes or effluents;

(6) Reasonable documentation that the design and installation of waste minimization and other measures that are necessary for compliance cannot otherwise be installed within the three year compliance period, and

(7) The information required in 40 CFR 63.6(i)(6)(i)(B) through (D).

(c) Approval of request for extension of compliance. Based on the information provided in any request made under paragraph (a) of this section, the Administrator or State with an approved Title V program may grant an extension of compliance with the emission standards identified in paragraph (a) of this section. The extension will be in writing in accordance with §§ 63.6(i)(10)(i) through 63.6(i)(10)(v)(A). EPA and States must consider the information required in paragraph (a) of this section in approving or denying requests for one-year compliance extensions.

Subpart FFF [Reserved]

Subpart GGG—National Emission Standards for Pharmaceuticals Production

SOURCE: 63 FR 50326, Sept. 21, 1998, unless otherwise noted.

§ 63.1250 Applicability.

(a) Definition of affected source. The affected source subject to this subpart is the pharmaceutical manufacturing operation, as defined in §63.1251. Except as specified in paragraph (d) of this section, the provisions of this subpart...
apply to pharmaceutical manufacturing operations that meet the criteria specified in paragraphs (a)(1) through (a)(3) of this section as follows:

(1) Manufacture a pharmaceutical product, as defined in §63.1251;

(2) Are located at a plant site that is a major source as defined in section 112(a) of the Act; and

(3) Process, use, or produce HAP.

(b) New source applicability. A new affected source subject to this subpart and to which the requirements for new sources apply is an affected source for which construction or reconstruction commenced after April 2, 1997 and the standard was applicable at the time of construction or reconstruction; or a pharmaceutical manufacturing process unit (PMPU), dedicated to manufacturing a single product, that has the potential to emit 10 tons per year of any one HAP or 25 tons per year of combined HAP, for which construction commenced after April 2, 1997.

(c) General Provisions. Table 1 of this subpart specifies the provisions of subpart A of this part that apply to an owner or operator of an affected source subject to this subpart, and clarifies specific provisions in subpart A of this part as necessary for this subpart.

(d) Processes exempted from the affected source. The provisions of this subpart do not apply to research and development facilities.

(e) Storage tank ownership determination. The owner or operator shall follow the procedures specified in paragraphs (e)(1) through (e)(5) of this section to determine to which PMPU a storage tank shall belong.

(1) If a storage tank is dedicated to a single PMPU, the storage tank shall belong to that PMPU.

(2) If a storage tank is shared among PMPU’s, then the storage tank shall belong to that PMPU located on the same plant site as the storage tank that has the greatest annual volume input into or output from the storage tank (i.e., said PMPU has the predominant use of the storage tank).

(3) If predominant use cannot be determined for a storage tank that is shared among PMPU’s and if one of those PMPU’s is subject to this subpart, the storage tank shall belong to said PMPU.

(4) If the predominant use of a storage tank varies from year to year, then predominant use shall be determined based on the utilization that occurred during the year preceding September 21, 1998 for existing affected sources. For new affected sources, predominant use will be based on the first year after initial startup. The determination of predominant use shall be reported in the Notification of Compliance Status required by §63.1260(f). If the predominant use changes, the redetermination of predominant use shall be reported in the next Periodic Report.

(f) Compliance dates. The compliance dates for affected sources are as follows:

(1) An owner or operator of an existing affected source must comply with the provisions of this subpart within 3 years after September 21, 1998.

(2) An owner or operator of a new or reconstructed affected source must comply with the provisions of this subpart on September 21, 1998 or upon startup, whichever is later.

(3) Notwithstanding the requirements of paragraphs (f)(1) and (2) of this section, a new source which commences construction or reconstruction after April 2, 1997 and before September 21, 1998 shall not be required to comply with such promulgated standard until 3 years after September 21, 1998 if:

(i) The promulgated standard is more stringent than the proposed standard; and

(ii) The owner or operator complies with the standard as proposed during the 3-year period immediately after September 21, 1998.
§ 63.1250

(4) Pursuant to section 112(i)(3)(B) of the Act, an owner or operator may request an extension allowing the existing source up to 1 additional year to comply with section 112(d) standards.

(i) For purposes of this subpart, a request for an extension shall be submitted no later than 120 days prior to the compliance dates specified in paragraphs (f)(1) through (3) of this section, except as provided in paragraph (f)(4)(ii) of this section. The dates specified in §63.6(i) for submittal of requests for extensions shall not apply to sources subject to this subpart.

(ii) An owner or operator may submit a compliance extension request after the date specified in paragraph (f)(4)(i) of this section provided the need for the compliance extension arose after that date and before the otherwise applicable compliance date, and the need arose due to circumstances beyond reasonable control of the owner or operator. This request shall include the data described in §63.6(i)(6)(i)(A), (B), (C), and (D).

(g) Applicability of this subpart except during periods of startup, shutdown, and malfunction. (1) Each provision set forth in this subpart shall apply at all times except that emission limitations shall not apply during periods of: startup; shutdown; and malfunction, if the startup, shutdown, and malfunction precludes the ability of a particular emission point of an affected source to comply with one or more specific emission limitations to which it is subject and the owner or operator follows the provisions for periods of startup, shutdown, and malfunction, as specified in §§63.1259(a)(3) and 63.1260(i). Startup, shutdown, and malfunction are defined in §63.1251.

(2) The provisions set forth in §63.1255 of this subpart shall apply at all times except during periods of nonoperation of the PMPU (or specific portion thereof) in which the lines are drained and depressurized resulting in the cessation of the emissions to which §63.1255 of this subpart applies.

(3) The owner or operator shall not shut down items of equipment that are required or utilized for compliance with the emissions limitations of this subpart during times when emissions (or, where applicable, wastewater streams or residuals) are being routed to such items of equipment, if the shutdown would contravene emissions limitations of this subpart applicable to such items of equipment. This paragraph does not apply if the item of equipment is malfunctioning, or if the owner or operator must shut down the equipment to avoid damage due to a malfunction of the PMPU or portion thereof.

(4) During startups, shutdowns, and malfunctions when the emissions limitations of this subpart do not apply pursuant to paragraphs (g)(1) through (3) of this section, the owner or operator shall implement, to the extent reasonably available, measures to prevent or minimize excess emissions to the extent practical. For purposes of this paragraph, “excess emissions” means emissions in excess of those that would have occurred if there were no startup, shutdown, or malfunction and the owner or operator complied with the relevant provisions of this subpart. The measures to be taken shall be identified in the applicable startup, shutdown, and malfunction plan, and may include, but are not limited to, air pollution control technologies, work practices, pollution prevention, monitoring, and/or changes in the manner of operation of the source. Back-up control devices are not required, but may be used if available.

(h) Consistency with other regulations. (1) Consistency with other MACT standards. After the compliance dates specified in this section, an affected source subject to the provisions of this subpart that is also subject to the provisions of any other subpart of 40 CFR parts 63 may elect, to the extent the subparts are consistent, which subpart under which which to maintain records and report to EPA. The affected source shall identify in the Notification of Compliance Status report required by §63.1260(f) under which authority such records will be maintained.

(2) Consistency with 40 CFR parts 264 and 265, subparts AA, BB, and/or CC. After the compliance dates specified in this section, if any affected source subject to this subpart is also subject to monitoring, recordkeeping, and reporting requirements in 40 CFR part 264, subpart AA, BB, or CC, or is subject to
monitoring and recordkeeping requirements in 40 CFR part 265, subpart AA, BB, or CC and the owner or operator complies with the periodic reporting requirements under 40 CFR part 264, subpart AA, BB, or CC that would apply to the device if the facility had final-permitted status, the owner or operator may elect to comply either with the monitoring, recordkeeping, and reporting requirements of this subpart, or with the monitoring, recordkeeping, and reporting requirements in 40 CFR parts 264 and/or 265, as described in this paragraph, which shall constitute compliance with the monitoring, record keeping, and reporting requirements of this subpart. If the owner or operator elects to comply with the monitoring, recordkeeping, and reporting requirements in 40 CFR parts 264 and/or 265, the owner or operator shall report all information required by §63.1260(g). The owner or operator shall identify in the Notification of Compliance Status report required by §63.1260(f) the monitoring, recordkeeping, and reporting authority under which the owner or operator will comply.

(3) Consistency with 40 CFR 60.112b. After the compliance dates specified in this section, a storage tank controlled with a floating roof and in compliance with the provisions of 40 CFR 60.112b, subpart Kb, constitutes compliance with the provisions of this subpart GGG. A storage tank with a fixed roof, closed vent system, and control device in compliance with the provisions of 40 CFR 60.112b, subpart Kb must comply with the monitoring, recordkeeping, and reporting provisions of this subpart GGG. The owner or operator shall identify in the Notification of Compliance Status report required by §63.1260(f) which tanks are in compliance with subpart Kb.

(4) Consistency with subpart I of this part. After the compliance dates specified in this section, for equipment at an affected source subject to this subpart that is also subject to subpart I of this part, an owner or operator may elect to comply with either the provisions of this subpart GGG or the provisions of subpart I of this part. The owner or operator shall identify in the Notification of Compliance Status report required by §63.1260(f) the provisions with which the owner elects to comply.

(5) Consistency with other regulations for wastewater. After the compliance dates specified in this section, the owner or operator of an affected wastewater that is also subject to provisions in 40 CFR parts 260 through 272 shall comply with the more stringent control requirements (e.g., waste management units, numerical treatment standards, etc.) and the more stringent testing, monitoring, recording, and recordkeeping requirements that overlap between the provisions of this subpart and the provisions of 40 CFR parts 260 through 272. The owner or operator shall keep a record of the information used to determine which requirements were the most stringent and shall submit this information if requested by the Administrator.

(i) For the purposes of establishing whether a person is in violation of this subpart, nothing in this subpart shall preclude the use of any credible evidence or information relevant to whether a source would have been in compliance with applicable requirements.

§63.1251 Definitions.

Terms used in this subpart are defined in the Act, in subpart A of this part, or in this section. If the same term is defined in subpart A of this part and in this section, it shall have the meaning given in this section for the purposes of this subpart.

Active ingredient means any component that is intended to furnish pharmacological activity or other direct effect in the diagnosis, cure, mitigation, treatment, or prevention of disease, or to affect the structure or any function of the body of man or other animals. The term includes those components that may undergo chemical change in the manufacture of the pharmaceutical product and be present in the pharmaceutical product in a modified form intended to furnish the specified activity or effect.

Actual HAP emissions means the HAP emitted to the atmosphere from either uncontrolled or controlled emission points.
Air pollution control device or Control device means equipment installed on a process vent, storage tank, wastewater treatment exhaust stack, or combination thereof that reduces the mass of HAP emitted to the air. The equipment may consist of an individual device or a series of devices. Examples include, but are not limited to, incinerators, carbon adsorption units, condensers, flares, boilers, process heaters, and gas absorbers. Process condensers are not considered air pollution control devices or control devices.

Annual average concentration, as used in the wastewater provisions, means the annual average concentration as determined according to the procedures specified in §63.1257(e)(1).

Automated monitoring and recording system means any means of measuring values of monitored parameters and creating a hard copy or computer record of the measured values that does not require manual reading of monitoring instruments and manual transcription of data values. Automated monitoring and recording systems include, but are not limited to, computerized systems and strip charts.

Batch emission episode means a discrete venting episode that may be associated with a single unit operation. A unit operation may have more than one batch emission episode. For example, a displacement of vapor resulting from the charging of a vessel with HAP will result in a discrete emission episode that will last through the duration of the charge and will have an average flowrate equal to the rate of the charge. If the vessel is then heated, there will also be another discrete emission episode resulting from the expulsion of expanded vapor. Both emission episodes may occur in the same vessel or unit operation. There are possibly other emission episodes that may occur from the vessel or other process equipment, depending on process operations.

Batch operation or Batch process means a noncontinuous operation involving intermittent or discontinuous feed into equipment, and, in general, involves the emptying of the equipment after the batch operation ceases and prior to beginning a new operation. Addition of raw material and withdrawal of product do not occur simultaneously in a batch operation.

Bench-scale batch process means a batch process (other than a research and development facility) that is capable of being located on a laboratory bench top. This bench-scale equipment will typically include reagent feed vessels, a small reactor and associated product separator, recovery and holding equipment. These processes are only capable of producing small quantities of product.

Block means a time period that comprises a single batch.

Cleaning operation means routine rinsing, washing, or boil-off of equipment in batch operations between batches.

Closed biological treatment process means a tank or surface impoundment where biological treatment occurs and air emissions from the treatment process are routed to either a control device by means of a closed-vent system or by means of hard-piping. The tank or surface impoundment has a fixed roof, as defined in this section, or a floating flexible membrane cover that meets the requirements specified in §63.1256(c).

Closed-loop system means an enclosed system that returns process fluid to the process and is not vented to the atmosphere except through a closed-vent system.

Closed-purge system means a system or combination of system and portable containers, to capture purged liquids. Containers must be covered or closed when not being filled or emptied.

Closed-vent system means a system that is not open to the atmosphere and is composed of piping, ductwork, connections, and, if necessary, flow inducing devices that transport gas or vapor from an emission point to a control device.

Combustion device means an individual unit of equipment, such as a flare, incinerator, process heater, or boiler, used for the combustion of HAP vapors.

Connector means flanged, screwed, or other joined fittings used to connect
two pipe lines or a pipe line and a piece of equipment. A common connector is a flange. Joined fittings welded completely around the circumference of the interface are not considered connectors for the purpose of this regulation. For the purpose of reporting and recordkeeping, connector means joined fittings that are not inaccessible, ceramic, or ceramic-lined as described in §63.1255(b)(1)(vii) and §63.1255(f)(3).

Construction means the onsite fabrication, erection, or installation of an affected source or a PMPU.

Consumption means the quantity of HAP entering a process that is not used as reactant (makeup). If the same HAP component is generated in the process as well as added as makeup, consumption shall include the quantity generated in the process, as calculated assuming 100 percent stoichiometric conversion. The quantity of material used as reactant is the theoretical amount needed assuming a 100 percent stoichiometric conversion. Makeup is the net amount of material that must be added to the process to replenish losses.

Container, as used in the wastewater provisions, means any portable waste management unit that has a capacity greater than or equal to 0.1 m$^3$ in which a material is stored, transported, treated, or otherwise handled. Examples of containers are drums, barrels, tank trucks, barges, dumpsters, tank cars, dump trucks, and ships.

Continuous process means a process where the inputs and outputs flow continuously throughout the duration of the process. Continuous processes are typically steady state.

Continuous recorder means a data recording device that either records an instantaneous data value at least once every 15 minutes or records 15-minute or more frequent block average values.

Continuous seal means a seal that forms a continuous closure that completely covers the space between the wall of the storage tank and the edge of the floating roof. A continuous seal may be a vapor-mounted, liquid-mounted, or metallic shoe seal.

Control device, for purposes of this §63.1255, means any equipment used for recovering or oxidizing organic hazardous air pollutant vapors. Such equipment includes, but is not limited to, absorbers, carbon adsorbers, condensers, flares, boilers, and process heaters.

Controlled HAP emissions means the quantity of HAP discharged to the atmosphere from an air pollution control device.

Cover, as used in the wastewater provisions, means a device or system which is placed on or over a waste management unit containing wastewater or residuals so that the entire surface area is enclosed to minimize air emissions. A cover may have openings necessary for operation, inspection, and maintenance of the waste management unit such as access hatches, sampling ports, and gauge wells provided that each opening is closed when not in use. Examples of covers include a fixed roof installed on a wastewater tank, a lid installed on a container, and an air-supported enclosure installed over a waste management unit.

Dedicated PMPU means a PMPU that is composed of equipment that is used to manufacture the same product for a continuous period of 6 months or greater. The PMPU includes any shared storage tank(s) that are determined to belong to the PMPU according to the procedures in §63.1250(e).

Double block and bleed system means two block valves connected in series with a bleed valve or line that can vent the line between the two block valves.

Duct work means a conveyance system such as those commonly used for heating and ventilation systems. It is often made of sheet metal and often has sections connected by screws or crimping. Hard-piping is not ductwork.

Enhanced biological treatment system or enhanced biological treatment process means an aerated, thoroughly mixed treatment unit(s) that contains biomass suspended in water followed by a clarifier that removes biomass from the treated water and recycles recovered biomass to the aeration unit. The mixed liquor volatile suspended solids (biomass) is greater than 1 kilogram per cubic meter throughout each aeration unit. The biomass is suspended and aerated in the water of the aeration unit(s) by either submerged air flow or mechanical agitation. A thoroughly mixed treatment unit is a unit
that is designed and operated to approach or achieve uniform biomass distribution and organic compound concentration throughout the aeration unit by quickly dispersing the recycled biomass and the wastewater entering the unit.

Equipment, for purposes of §63.1255, means each pump, compressor, agitator, pressure relief device, sampling connection system, open-ended valve or line, valve, connector, and instrumentation system in organic hazardous air pollutant service; and any control devices or closed-vent systems required by this subpart.

Excipient means any substance other than the active drug or product which have been appropriately evaluated for safety and are included in a drug delivery system to either aid the processing of the drug delivery system during its manufacture; protect, support or enhance stability, bioavailability, or patient acceptability; assist in product identification; or enhance any other attribute of the overall safety and effectiveness of the drug delivery system during storage or use.

External floating roof means a pontoon-type or double-deck type cover that rests on the liquid surface in a storage tank or waste management unit with no fixed roof.

Fill or filling means the introduction of material into a storage tank or the introduction of a wastewater stream or residual into a waste management unit, but not necessarily to complete capacity.

First attempt at repair means to take action for the purpose of stopping or reducing leakage of organic material to the atmosphere.

Fixed roof means a cover that is mounted on a waste management unit or storage tank in a stationary manner and that does not move with fluctuations in liquid level.

Floating roof means a cover consisting of a double deck, pontoon single deck, internal floating cover or covered floating roof, which rests upon and is supported by the liquid being contained, and is equipped with a closure seal or seals to close the space between the roof edge and waste management unit or storage tank wall.

Flow indicator means a device which indicates whether gas flow is, or whether the valve position would allow gas flow to be, present in a line.

Formulation means the process of mixing, blending, or diluting one or more active or inert ingredients with one or more active or inert ingredients, without an intended chemical reaction, to obtain a pharmaceutical dosage form. Formulation operations include mixing, compounding, blending, and tablet coating.

Group of processes means all of the equipment associated with processes in a building, processing area, or facility-wide. For a dedicated process, a group of processes may consist of a single process.

Halogen atoms mean atoms of chlorine or fluorine.

Halogenated compounds means organic HAP compounds that contain halogen atoms.

Halogenated vent stream or Halogenated stream means a process, storage tank, or waste management unit vent determined to have a concentration of halogenated compounds of greater than 20 ppmv, as determined through process knowledge, test results using Method 18 of 40 CFR part 60, appendix A, or test results using any other test method that has been validated according to the procedures in Method 301 of appendix A of this part.

Hard-piping means piping or tubing that is manufactured and properly installed using good engineering judgment and standards, such as ANSI B31.3.

Hydrogen halides and halogens means hydrogen chloride (HCl), chlorine (Cl2), and hydrogen fluoride (HF).

In gas/vapor service means that a piece of equipment in organic hazardous air pollutant service contains a gas or vapor at operating conditions.

In heavy liquid service means that a piece of equipment in organic hazardous air pollutant service is not in gas/vapor service or in light liquid service.

In light liquid service means that a piece of equipment in organic hazardous air pollutant service contains a liquid that meets the following conditions:
(1) The vapor pressure of one or more of the organic compounds is greater than 0.3 kilopascals at 20°C;

(2) The total concentration of the pure organic compounds constituents having a vapor pressure greater than 0.3 kilopascals at 20°C is equal to or greater than 20 percent by weight of the total process stream; and

(3) The fluid is a liquid at operating conditions. (Note: Vapor pressures may be determined by the methods described in 40 CFR 60.485(e)(1).)

In liquid service means that a piece of equipment in organic hazardous air pollutant service is not in gas/vapor service.

In organic hazardous air pollutant or in organic HAP service means that a piece of equipment either contains or contacts a fluid (liquid or gas) that is at least 5 percent by weight of total organic HAP's as determined according to the provisions of §63.180(d). The provisions of §63.180(d) also specify how to determine that a piece of equipment is not in organic HAP service.

In vacuum service means that equipment is operating at an internal pressure which is at least 5 kilopascals below ambient pressure.

In-situ sampling systems means non-extractive samplers or in-line samplers.

Individual drain system means the stationary system used to convey wastewater streams or residuals to a waste management unit. The term includes hard piping; all process drains and junction boxes; and associated sewer lines, other junction boxes, manholes, sumps, and lift stations conveying wastewater streams or residuals. A segregated stormwater sewer system, which is a drain and collection system designed and operated for the sole purpose of collecting rainfall-runoff at a facility, and which is segregated from all other individual drain systems, is excluded from this definition.

Initial startup means the first time a new or reconstructed source begins production. Initial startup does not include operation solely for testing equipment. Initial startup does not include subsequent start ups (as defined in this section) of processes following malfunctions or process shutdowns.

Internal floating roof means a cover that rests or floats on the liquid surface (but not necessarily in complete contact with it) inside a storage tank or waste management unit that has a permanently affixed roof.

Instrumentation system means a group of equipment components used to condition and convey a sample of the process fluid to analyzers and instruments for the purpose of determining process operating conditions (e.g., composition, pressure, flow, etc.). Valves and connectors are the predominant type of equipment used in instrumentation systems; however, other types of equipment may also be included in these systems. Only valves nominally 0.5 inches and smaller, and connectors nominally 0.75 inches and smaller in diameter are considered instrumentation systems for the purposes of this subpart. Valves greater than nominally 0.5 inches and connectors greater than nominally 0.75 inches associated with instrumentation systems are not considered part of instrumentation systems and must be monitored individually.

Junction box means a manhole or access point to a wastewater sewer system line or a lift station.

Large control device means a control device that controls process vents with total emissions of greater than or equal to 10 tons of HAP per year, before control.

Liquid-mounted seal means a foam- or liquid-filled seal mounted in contact with the liquid between the wall of the storage tank or waste management unit and the floating roof. The seal is mounted continuously around the tank or unit.

Liquids dripping means any visible leakage from the seal including dripping, spraying, misting, clouding, and ice formation. Indications of liquid dripping include puddling or new stains that are indicative of an existing evaporated drip.

Malfunction means any sudden, infrequent, and not reasonably preventable failure of air pollution control equipment, emissions monitoring equipment, process equipment, or a process to operate in a normal or usual manner. Failures that are caused all or in
part by poor maintenance or careless operation are not malfunctions.

Maximum true vapor pressure means the equilibrium partial pressure exerted by the total organic HAP in the stored or transferred liquid at the temperature equal to the highest calendar-month average of the liquid storage or transferred temperature for liquids stored or transferred above or below the ambient temperature or at the local maximum monthly average temperature as reported by the National Weather Service for liquids stored or transferred at the ambient temperature, as determined:

1. In accordance with methods described in Chapter 19.2 of the American Petroleum Institute's Manual of Petroleum Measurement Standards, Evaporative Loss From Floating-Roof Tanks (incorporated by reference as specified in §63.14); or
2. As obtained from standard reference texts; or
3. As determined by the American Society for Testing and Materials Method D2879-97, Test Method for Vapor Pressure-Temperature Relationship and Initial Decomposition Temperature of Liquids by Isoteniscope (incorporated by reference as specified in §63.14); or
4. Any other method approved by the Administrator.

Metallic shoe seal or mechanical shoe seal means metal sheets that are held vertically against the wall of the storage tank by springs, weighted levers, or other mechanisms and connected to the floating roof by braces or other means. A flexible coated fabric (envelope) spans the annular space between the metal sheet and the floating roof.

Nondedicated formulation operations means equipment used to formulate numerous products.

Nondedicated recovery device(s) means a recovery device that receives material from more than one PMPU.

Nonrepairable means that it is technically infeasible to repair a piece of equipment from which a leak has been detected without a process shutdown.

Open-ended valve or line means any valve, except pressure relief valves, having one side of the valve seat in contact with process fluid and one side open to atmosphere, either directly or through open piping.

Operating scenario for the purposes of reporting and recordkeeping, means any specific operation of a PMPU and includes for each process:

1. A description of the process and the type of process equipment used;
2. An identification of related process vents and their associated emissions episodes and durations, wastewater PODs, and storage tanks;
3. The applicable control requirements of this subpart, including the level of required control;
4. The control or treatment devices used, as applicable, including a description of operating and/or testing conditions for any associated control device;
5. The process vents, wastewater PODs, and storage tanks (including those from other processes) that are simultaneously routed to the control or treatment device(s);
6. The applicable monitoring requirements of this subpart and any parametric level that assures compliance for all emissions routed to the control or treatment device;
7. Calculations and engineering analyses required to demonstrate compliance; and
8. A verification that the operating conditions for any associated control or treatment device have not been exceeded and that any required calculations and engineering analyses have been performed. For reporting purposes, a change to any of these elements not previously reported, except for paragraph (5) of this definition, shall constitute a new operating scenario.

Partially soluble HAP means a HAP listed in Table 2 of this subpart.

Pharmaceutical manufacturing operations means the facility-wide collection of PMPU's and any other equipment such as heat exchanger systems, or cooling towers that are not associated with an individual PMPU, but that are located at a facility for the purpose of manufacturing pharmaceutical products and are under common control.
Pharmaceutical manufacturing process unit (PMPU) means the process, as defined in this subpart, and any associated storage tanks, equipment identified in §63.1252(f), and components such as pumps, compressors, agitators, pressure relief devices, sampling connection systems, open-ended valves or lines, valves, connectors, and instrumentation systems that are used in the manufacturing of a pharmaceutical product.

Pharmaceutical product means:
(1) Any material described by the standard industrial classification (SIC) code 2833 or 2834;
(2) Any material whose manufacturing process is described by north american industrial classification system (NAICS) code 325411 or 325412;
(3) A finished dosage form of a drug, for example, a tablet, capsule, solution, etc., that contains an active ingredient generally, but not necessarily, in association with inactive ingredients; or
(4) Any component whose intended primary use is to furnish pharmacological activity or other direct effect in the diagnosis, cure, mitigation, treatment, or prevention of disease, or to affect the structure or any function of the body of man or other animals (the term does not include excipients, but includes drug components such as raw starting materials or precursors that undergo chemical change or processing before they become active ingredients).

Plant site means all contiguous or adjoining property that is under common control, including properties that are separated only by a road or other public right-of-way. Common control includes properties that are owned, leased, or operated by the same entity, parent entity, subsidiary, or any combination thereof.

Point of determination (POD) means the point where a wastewater stream exits the process, storage tank, or last recovery device. If soluble and/or partially soluble HAP compounds are not recovered from water before discharge, the discharge point from the process equipment or storage tank is a POD. If water streams are routed to a recovery device, the discharge from the recovery device is a POD. There can be more than 1 POD per process or PMPU.

Pressure release means the emission of materials resulting from the system pressure being greater than the set pressure of the pressure relief device. This release can be one release or a series of releases over a short time period due to a malfunction in the process.

Pressure relief device or valve means a safety device used to prevent operating pressures from exceeding the maximum allowable working pressure of the process equipment. A common pressure relief device is a spring-loaded pressure relief valve. Devices that are actuated either by a pressure of less than or equal to 2.5 psig or by a vacuum are not pressure relief devices.

Primary use means the single largest use of a material.

Process means all equipment which collectively function to produce a pharmaceutical product. A process may consist of one or more unit operations. For the purposes of this subpart, process includes all or a combination of reaction, recovery, separation, purification, or other activity, operation, manufacture, or treatment which are used to produce a pharmaceutical product. Cleaning operations conducted are considered part of the process. The holding of the pharmaceutical product in tanks or other holding equipment for more than 30 consecutive days, or transfer of the pharmaceutical product to containers for shipment, marks the end of a process, and the tanks are considered part of the PMPU that produced the stored material. When material from one unit operation is used as the feedstock for the production of two or more different pharmaceutical products, the unit operation is considered the endpoint of the process that produced the material, and the unit operations into which the material is routed mark the beginning of the other processes. Nondedicated recovery devices located within a contiguous area within the affected source are considered single processes. Nondedicated formulation operations occurring within a contiguous area are considered a single process that is used to formulate numerous materials and/or products. Quality Assurance and Quality Control laboratories are not considered part of any process.
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Process condenser means a condenser whose primary purpose is to recover material as an integral part of a process. The condenser must support a vapor-to-liquid phase change for periods of source equipment operation that are at or above the boiling or bubble point of substance(s) at the liquid surface. Examples of process condensers include distillation condensers, reflux condensers, and condensers used in stripping or flashing operations. In a series of condensers, all condensers up to and including the first condenser with an exit gas temperature below the boiling or bubble point of the substance(s) at the liquid surface are considered to be process condensers. All condensers in line prior to a vacuum source are included in this definition.

Process shutdown means a work practice or operational procedure that stops production from a process or part of a process during which it is technically feasible to clear process material from a process or part of a process consistent with safety constraints and during which repairs can be effected. An unscheduled work practice or operational procedure that stops production from a process or part of a process for less than 24 hours is not a process shutdown. An unscheduled work practice or operational procedure that would stop production from a process or part of a process for a shorter period of time than would be required to clear the process or part of the process of materials and start up the process, and would result in greater emissions than delay of repair of leaking components until the next scheduled process shutdown, is not a process shutdown. The use of spare equipment and technically feasible bypassing of equipment without stopping production are not process shutdowns.

Process tank means a tank that is used to collect material discharged from a feedstock storage tank or unit operation within the process and transfer this material to another unit operation within the process or to a product storage tank. Surge control vessels and bottoms receivers that fit these conditions are considered process tanks.

Process vent means a vent from a unit operation or vents from multiple unit operations within a process that are manifolded together into a common header, through which a HAP-containing gas stream is, or has the potential to be, released to the atmosphere. Examples of process vents include, but are not limited to, vents on condensers used for product recovery, bottom receivers, surge control vessels, reactors, filters, centrifuges, and process tanks. Emission streams that are undiluted and uncontrolled containing less than 50 ppmv HAP, as determined through process knowledge that no HAP are present in the emission stream or using an engineering assessment as discussed in §63.1257(d)(2)(ii), test data using Methods 18 of 40 CFR part 60, appendix A, or any other test method that has been validated according to the procedures in Method 301 of appendix A of this part, are not considered process vents. Process vents do not include vents on storage tanks regulated under §63.1253, vents on wastewater emission sources regulated under §63.1256, or pieces of equipment regulated under §63.1255.

Production-indexed HAP consumption factor is the result of dividing the annual consumption of total HAP by the annual production rate, per process.

A production-indexed volatile organic compound (VOC) consumption factor is the result of dividing the annual consumption of total VOC by the annual production rate, per process.

Publicly owned treatment works (POTW) means any devices and systems used in the storage, treatment, recycling, and reclamation of municipal sewage or industrial wastes of a liquid nature as defined in section 212(2)(A) of the Clean Water Act, as amended [33 U.S.C. §1292(2)(A)]. A POTW includes the treatment works, intercepting sewers, sewage collection systems, pumping, power, and other equipment. The POTW is defined at 40 CFR 403.3(o).

Reactor means a device or vessel in which one or more chemicals or reactants, other than air, are combined or decomposed in such a way that their molecular structures are altered and one or more new organic compounds are formed.

Recovery device, as used in the wastewater provisions, means an individual
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unit of equipment used for the purpose of recovering chemicals for fuel value (i.e., net positive heating value), use, reuse, or for sale for fuel value, use or reuse. Examples of equipment that may be recovery devices include organic removal devices such as decanters, strippers, or thin-film evaporation units. To be a recovery device, a decanter and any other equipment based on the operating principle of gravity separation must receive only two-phase liquid streams.

Repaired means that equipment is adjusted, or otherwise altered, to eliminate a leak as defined in the applicable sections of §63.1255.

Research and development facility means any stationary source whose primary purpose is to conduct research and development into new processes and products, where such source is operated under the close supervision of technically trained personnel, and is not engaged in the manufacture of products for commercial sale in commerce, except in a de minimis manner.

Residual means any HAP-containing liquid or solid material that is removed from a wastewater stream by a waste management unit or treatment process that does not destroy organics (nondestructive unit). Examples of residuals from nondestructive waste management units are: the organic layer and bottom residue removed by a decanter or organic-water separator and the overheads from a steam stripper or air stripper. Examples of materials which are not residuals are: silt; mud; leaves; bottoms from a steam stripper or air stripper; and sludges, ash, or other materials removed from wastewater being treated by destructive devices such as biological treatment units and incinerators.

Safety device means a closure device such as a pressure relief valve, frangible disc, fusible plug, or any other type of device which functions exclusively to prevent physical damage or permanent deformation to a unit or its air emission control equipment by venting gases or vapors directly to the atmosphere during unsafe conditions resulting from an unplanned, accidental, or emergency event. For the purposes of this subpart, a safety device is not used for routine venting of gases or vapors from the vapor headspace underneath a cover such as during filling of the unit or to adjust the pressure in this vapor headspace in response to normal daily diurnal ambient temperature fluctuations. A safety device is designed to remain in a closed position during normal operations and open only when the internal pressure, or another relevant parameter, exceeds the device threshold setting applicable to the air emission control equipment as determined by the owner or operator based on manufacturer recommendations, applicable regulations, fire protection and prevention codes, standard engineering codes and practices, or other requirements for the safe handling of flammable, combustible, explosive, reactive, or hazardous materials.

Sampling connection system means an assembly of equipment within a process unit used during periods of representative operation to take samples of the process fluid. Equipment used to take nonroutine grab samples is not considered a sampling connection system.

Sensor means a device that measures a physical quantity or the change in a physical quantity, such as temperature, pressure, flow rate, pH, or liquid level.

Set pressure means the pressure at which a properly operating pressure relief device begins to open to relieve atypical process system operating pressure.

Sewer line means a lateral, trunk line, branch line, or other conduit including, but not limited to, grates, trenches, etc., used to convey wastewater streams or residuals to a downstream waste management unit.

Shutdown means the cessation of operation of a PMPU or an individual piece of equipment required or used to comply with this part or for emptying and degassing storage tanks. Shutdown occurs for purposes including but not limited to: periodic maintenance, replacement of equipment, or repair. Shutdown does not apply to routine batch operations or the rinsing or washing of equipment in batch operations between batches.

Single-seal system means a floating roof having one continuous seal that completely covers the space between
the wall of the storage tank and the edge of the floating roof. This seal may be a vapor-mounted, liquid-mounted, or metallic shoe seal.

Small control device means a control device that controls process vents with total emissions of less than 10 tons of HAP per year, before control.

Soluble HAP means a HAP listed in Table 3 of this subpart.

Startup means the first time a new or reconstructed source begins production, or, for new equipment added, including equipment used to comply with this subpart, the first time the equipment is put into operation, or for the introduction of a new product/process, the first time the product or process is run in equipment. As used in §63.1255, startup means the setting in operation of a piece of equipment or a control device that is subject to this subpart.

Storage tank means a tank or other vessel that is used to store organic liquids that contain one or more HAP as feedstocks or products of a PMPU. The following are not considered storage tanks for the purposes of this subpart:

1. Vessels permanently attached to motor vehicles such as trucks, railcars, barges, or ships;
2. Pressure vessels designed to operate in excess of 204.9 kilopascals and without emissions to the atmosphere;
3. Vessels storing organic liquids that contain HAP only as impurities;
4. Wastewater storage tanks; and

Surface impoundment means a waste management unit which is a natural topographic depression, manmade excavation, or diked area formed primarily of earthen materials (although it may be lined with manmade materials), which is designed to hold an accumulation of liquid wastes or waste containing free liquids. A surface impoundment is used for the purpose of treating, storing, or disposing of wastewater or residuals, and is not an injection well. Examples of surface impoundments are equalization, settling, and aeration pits, ponds, and lagoons.

Total organic compounds (TOC) means those compounds measured according to the procedures of Method 18 or Method 25A, 40 CFR part 60, appendix A.

Treatment process means a specific technique that removes or destroys the organics in a wastewater or residual stream such as a steam stripping unit, thin-film evaporation unit, waste incinerator, biological treatment unit, or any other process applied to wastewater streams or residuals to comply with §63.1256. Most treatment processes are conducted in tanks. Treatment processes are a subset of waste management units.

Uncontrolled HAP emissions means a gas stream containing HAP which has exited the process (or process condenser, if any), but which has not yet been introduced into an air pollution control device to reduce the mass of HAP in the stream. If the process vent is not routed to an air pollution control device, uncontrolled emissions are those HAP emissions released to the atmosphere.

Unit operation means those processing steps that occur within distinct equipment that are used, among other things, to prepare reactants, facilitate reactions, separate and purify products, and recycle materials. Equipment used for these purposes includes but is not limited to reactors, distillation columns, extraction columns, absorbers, decanters, dryers, condensers, and filtration equipment.

Vapor-mounted seal means a continuous seal that completely covers the annular space between the wall, the storage tank or waste management unit and the edge of the floating roof and is mounted such that there is a vapor space between the stored liquid and the bottom of the seal.

Volatile organic compounds (VOC) means those materials defined in 40 CFR 51.100.

Waste management unit means the equipment, structure(s), and or devices used to convey, store, treat, or dispose of wastewater streams or residuals. Examples of waste management units include wastewater tanks, air flotation units, surface impoundments, containers, oil-water or organic-water separators, individual drain systems, biological wastewater treatment units, waste incinerators, and organic removal devices such as steam and air stripper units, and thin film evaporation units. If such equipment is used
for recovery then it is part of a pharmaceutical process and is not a waste management unit.

Wastewater means any portion of an individual wastewater stream or any aggregation of wastewater streams.

Wastewater stream means water that is discarded from a PMPU through a single POD, that contains an annual average concentration of partially soluble and/or soluble HAP compounds of at least 5 parts per million by weight and a load of at least 0.05 kg/yr, and that is not exempted by the provisions of §63.1256(a)(3). For the purposes of this subpart, noncontact cooling water is not considered a wastewater stream. Wastewater streams are generated by both process operations and maintenance activities.

Wastewater tank means a stationary waste management unit that is designed to contain an accumulation of wastewater or residuals and is constructed primarily of nonearthen materials (e.g., wood, concrete, steel, plastic) which provide structural support. Wastewater tanks used for flow equalization are included in this definition.

Water seal controls means a seal pot, p-leg trap, or other type of trap filled with water (e.g., flooded sewers that maintain water levels adequate to prevent air flow through the system) that creates a water barrier between the sewer line and the atmosphere. The water level of the seal must be maintained in the vertical leg of a drain in order to be considered a water seal.

§ 63.1252 Standards: General.

Each owner or operator of any affected source subject to the provisions of this subpart shall control HAP emissions to the level specified in this section on and after the compliance dates specified in §63.1250(f). Compliance with the emission limits may be demonstrated initially through the provisions of §63.1257 (Test methods and compliance procedures) and continuously through the provisions of §63.1258 (Monitoring requirements).

(a) Opening of a safety device. Opening of a safety device, as defined in §63.1251, is allowed at any time conditions require it to do so to avoid unsafe conditions.

(b) Closed-vent systems. The owner or operator of a closed-vent system that contains bypass lines that could divert a vent stream away from a control device used to comply with the requirements in §§63.1253, 63.1254, and 63.1256 shall comply with the requirements of Table 4 to this subpart and paragraph (b)(1) or (2) of this section. Equipment such as low leg drains, high point bleeds, analyzer vents, open-ended valves or lines, rupture disks and pressure relief valves needed for safety purposes are not subject to this paragraph.

(1) Install, calibrate, maintain, and operate a flow indicator that determines whether vent stream flow is present at least once every 15 minutes. Records shall be maintained as specified in §63.1259(i)(6)(i). The flow indicator shall be installed at the entrance to any bypass line that could divert the vent stream away from the control device to the atmosphere; or

(2) Secure the bypass line valve in the closed position with a car seal or lock and key type configuration. A visual inspection of the seal or closure mechanism shall be performed at least once every month to ensure that the valve is maintained in the closed position and the vent stream is not diverted through the bypass line. Records shall be maintained as specified in §63.1259(i)(6)(ii).

(c) Heat exchange systems. Except as provided in paragraph (c)(2) of this section, owners and operators of affected sources subject to the requirements in paragraph (c)(1) of this section for heat exchange systems that cool process equipment or materials used in pharmaceutical manufacturing operations.

(1) The heat exchange system shall be treated according to the provisions of §63.104, except that the monitoring frequency shall be no less than quarterly.

(2) For identifying leaking equipment, the owner or operator of heat exchange systems on equipment which meet current good manufacturing practice (CGMP) requirements of 21 CFR part 211 may elect to use the physical integrity of the reactor as the surrogate indicator of heat exchange system leaks around the reactor.

(d) Emissions averaging provisions. Except as specified in paragraphs (d)(1)
through (5) of this section, owners or operators of storage tanks or processes subject to the provisions of §§63.1253 and 63.1254 may choose to comply by using emissions averaging requirements specified in §63.1257(g) or (h) for any storage tank or process.

(1) A State may prohibit averaging of HAP emissions and require the owner or operator of an existing source to comply with the provisions in §§63.1253 and 63.1254.

(2) Only emission sources subject to the requirements of §63.1253(b)(1), (c)(1) or §63.1254(a)(2), (a)(3)(ii)(A) or (a)(3)(iii) may be included in any averaging group.

(3) Processes which have been permanently shutdown or storage tanks permanently taken out of HAP service may not be included in any averaging group.

(4) Processes and storage tanks already controlled on or before November 15, 1990 may not be included in an emissions averaging group, except where the level of control is increased after November 15, 1990. In these cases, the uncontrolled emissions shall be the controlled emissions as calculated on November 15, 1990 for the purpose of determining the uncontrolled emissions as specified in §63.1257(g) and (h).

(5) Emission points controlled to comply with a State or Federal rule other than this subpart may not be included in an emissions averaging group, unless the level of control has been increased after November 15, 1990 above what is required by the other State or Federal rule. Only the control above what is required by the other State or Federal rule will be credited. However, if an emission point has been used to generate emissions averaging credit for the purpose of complying with the previously approved average.

(6) Not more than 20 processes subject to §63.1254(a)(2)(i), 20 storage tanks subject to §63.1253(b)(1), and 20 storage tanks subject to §63.1253(c)(1)(i) at an affected source may be included in an emissions averaging group.

(7) Compliance with the emissions standards in §63.1253 shall be satisfied when the annual percent reduction efficiency is greater than or equal to 90 percent for those tanks meeting the requirements of §63.1253(a)(1) and 95 percent for those tanks meeting the requirements of §63.1253(a)(2), as demonstrated using the test methods and compliance procedures specified in §63.1257(g).

(8) Compliance with the emissions standards in §63.1254(a)(2) shall be satisfied when the annual percent reduction efficiency is greater than or equal to 93 percent, as demonstrated using the test methods and compliance procedures specified in §63.1257(h).

(e) Pollution prevention alternative. Except as provided in paragraph (e)(1) of this section, owners and operators may choose to meet the pollution prevention alternative requirement specified in either paragraph (e)(2) or (3) of this section for any PMPU, in lieu of the requirements specified in §§63.1253, 63.1254, 63.1255, and 63.1256. Compliance with paragraphs (e)(2) and (3) of this section shall be demonstrated through the procedures in §63.1257(f).

(1) The HAP that are generated in the PMPU that are not part of the production-indexed consumption factor must be controlled according to the requirements of §§63.1253, 63.1254, 63.1255, and 63.1256. The HAP that are generated as a result of combustion control of emissions must be controlled according to the requirements of paragraph (g) of this section.

(2) The production-indexed HAP consumption factor (kg HAP consumed/kg produced) shall be reduced by at least 75 percent from a 3 year average baseline established no earlier than the 1987 calendar year, or for the time period from startup of the process until the present in which the PMPU was operational and data are available, whichever is the lesser time period. If a time period less than 3 years is used to set the baseline, the data must represent at least 1 year's worth of data. For any reduction in the HAP factor achieved by reducing a HAP that is also a VOC, an equivalent reduction in the VOC factor is also required. For any reduction in the HAP factor that is achieved
by reducing a HAP that is not a VOC, the VOC factor may not be increased.

(3) Both requirements specified in paragraphs (e)(3)(i) and (ii) of this section are met.

(i) The production-indexed HAP consumption factor (kg HAP consumed/kg produced) shall be reduced by at least 50 percent from a 3-year average baseline established no earlier than the 1987 calendar year, or for the time period from startup of the process until the present in which the PMPU was operational and data are available, whichever is less. If a time period less than 3 years is used to set the baseline, the data must represent at least 1 year’s worth of data. For any reduction in the HAP factor achieved by reducing a HAP that is also a VOC, an equivalent reduction in the VOC factor is also required. For any reduction in the HAP factor that is achieved by reducing a HAP that is not a VOC, the VOC factor may not be increased.

(ii) The total PMPU HAP emissions shall be reduced by an amount, in kg/yr, that, when divided by the annual production rate, in kg/yr, and added to the reduction of the production-indexed HAP consumption factor, in kg/kg, yields a value of at least 75 percent of the average baseline HAP production-indexed consumption factor established according to paragraph (e)(3)(i) of this section according to the equation provided in §63.1257(f)(2)(ii)(A). The total PMPU VOC emissions shall be reduced by an amount calculated according to the equation provided in §63.1257(f)(2)(ii)(B). The annual reduction in HAP and VOC air emissions must be due to the use of the following control devices:

(A) Combustion control devices such as incinerators, flares or process heaters.

(B) Control devices such as condensers and carbon adsorbers whose recovered product is destroyed or shipped offsite for destruction.

(C) Any control device that does not ultimately allow for recycling of material back to the PMPU.

(D) Any control device for which the owner or operator can demonstrate that the use of the device in controlling HAP emissions will have no effect on the production-indexed consumption factor for the PMPU.

(f) Control requirements for certain liquid streams in open systems within a PMPU. (1) The owner or operator shall comply with the provisions of Table 5 of this subpart, for each item of equipment meeting all the criteria specified in paragraphs (f)(2) through (4) and either paragraph (f)(5)(i) or (ii) of this section.

(2) The item of equipment is of a type identified in Table 5 of this subpart;

(3) The item of equipment is part of a PMPU, as defined in §63.1251;

(4) The item of equipment is controlled less stringently than in Table 5 of this subpart and the item of equipment is not otherwise exempt from controls by the provisions of this subpart or subpart A of this part; and

(5) The item of equipment:

(i) Is a drain, drain hub, manhole, lift station, trench, pipe, or oil/water separator that conveys water with an annual average concentration greater than or equal to 1,300 parts per million by weight (ppmw) of partially soluble HAP compounds; or an annual average concentration greater than or equal to 5,200 ppmw of partially soluble and/or soluble HAP compounds. The annual average concentration shall be determined according to the procedures in §63.1257(e)(1)(i).

(ii) Is a tank that receives one or more streams that contain water with an annual average concentration greater than or equal to 1,300 ppmw of partially soluble HAP compounds, or greater than or equal to 5,200 ppmw of total partially soluble and/or soluble HAP compounds. The owner or operator of the source shall determine the average concentration of the stream at the inlet to the tank and according to the procedures in §63.1257(e)(1)(ii).

(g) Control requirements for halogenated vent streams that are controlled by combustion devices. If a combustion device is used to comply with the provisions of §§63.1253 (storage tanks), 63.1254 (process vents), 63.1256(h) (wastewater vent streams) for a halogenated vent stream, then the vent stream shall be ducted to a halogen reduction device such as, but not limited to, a scrubber, before it is discharged.
to the atmosphere. The halogen reduction device must reduce emissions by the amounts specified in either paragraph (g)(1) or (2) of this section.

(1) A halogen reduction device after the combustion control device must reduce overall emissions of hydrogen halides and halogens, as defined in §63.1251, by 95 percent or to a concentration less than or equal to 20 ppmv.

(2) A halogen reduction device located before the combustion control device must reduce the halogen atom content of the vent stream to a concentration less than or equal to 20 ppmv.

§ 63.1253 Standards: Storage tanks.

(a) Except as provided in paragraphs (d) and (e) of this section, the owner or operator of a storage tank meeting the criteria of paragraph (a)(1) of this section is subject to the requirements of paragraph (b) of this section. Except as provided in paragraphs (d) and (e) of this section, the owner or operator of a storage tank meeting the criteria of paragraph (a)(2) of this section is subject to the requirements of paragraph (c) of this section. Compliance with the provisions of paragraphs (b) and (c) of this section is demonstrated using the initial compliance procedures in §63.1257(c) and the monitoring requirements in §63.1258.

(1) A storage tank with a design capacity greater than or equal to 38 \( m^3 \) (10,000 gallons [gal]) but less than 75 \( m^3 \) (20,000 gal), and storing a liquid for which the maximum true vapor pressure of total HAP is greater than or equal to 13.1 kPa (1.9 psia).

(2) A storage tank with a design capacity greater than or equal to 75 \( m^3 \) (20,000 gal) storing a liquid for which the maximum true vapor pressure of total HAP is greater than or equal to 13.1 kPa (1.9 psia).

(b) The owner or operator of a storage tank shall equip the affected storage tank with either a fixed roof with internal floating roof, an external floating roof, an external floating roof converted to an internal floating roof, or a closed-vent system meeting the conditions of §63.1252(b) with a control device that meets any of the following conditions:

(1) Reduces inlet emissions of total HAP by 90 percent by weight or greater;

(2) Is an enclosed combustion device that provides a minimum residence time of 0.5 seconds at a minimum temperature of 760 °C;

(3) Is a flare that meets the requirements of §63.11(b); or

(4) Is a control device specified in §63.1257(a)(4).

(c) The owner or operator of a storage tank shall equip the affected storage tank with either a fixed roof with internal floating roof, an external floating roof, an external floating roof converted to an internal floating roof, or a closed-vent system meeting the conditions of §63.1252(b) with a control device that meets any of the following conditions:

(1) Reduces inlet emissions of total HAP as specified in paragraph (c)(1) (i) or (ii) of this section:

(i) By 95 percent by weight or greater; or (ii) If the owner or operator can demonstrate that a control device installed on a storage tank on or before April 2, 1997 is designed to reduce inlet emissions of total HAP by greater than or equal to 90 percent by weight but less than 95 percent by weight, then the control device is required to be operated to reduce inlet emissions of total HAP by 90 percent or greater.

(2) Is an enclosed combustion device that provides a minimum residence time of 0.5 seconds at a minimum temperature of 760 °C;

(3) Is a flare that meets the requirements of §63.11(b); or

(4) Is a control device specified in §63.1257(a)(4).

(d) As an alternative standard, the owner or operator of an existing or new affected source may comply with the storage tank standards by routing storage tank vents to a control device achieving an outlet TOC concentration, as calibrated on methane or the predominant HAP, of 20 ppmv or less, and an outlet concentration of hydrogen halides and halogens of 20 ppmv or less. Compliance with the outlet concentrations shall be determined by the initial compliance procedures of §63.1257(c)(4) and the continuous emission monitoring requirements of §63.1258(b)(5).
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(e) Planned routine maintenance. The specifications and requirements in paragraphs (b) through (d) of this section for control devices do not apply during periods of planned routine maintenance. Periods of planned routine maintenance of the control devices, during which the control device does not meet the specifications of paragraphs (b) through (d) of this section, as applicable, shall not exceed 240 hours per year.

§ 63.1254 Standards: Process vents.

(a) Existing sources. Except as provided in paragraph (c) of this section, the owner or operator of an existing affected source must control the collection of all gas streams originating from processes subject to this standard so as to comply with the requirements in paragraph (a)(1) or the requirements of paragraphs (a)(2) and (a)(3) of this section. If any vent within a process meets the criteria of paragraph (a)(3)(i) of this section, the owner or operator must comply with the provisions in paragraphs (a)(2) and (a)(3) for that process. The requirements of paragraphs (a)(1) and (2) of this section apply to all process vents within a process, as a group, and do not apply to individual vents. An owner or operator may switch from compliance with paragraph (a)(1) of this section to compliance with paragraphs (a)(2) and (a)(3) for that process. The requirements of paragraphs (a)(1) and (2) of this section at any time.

Notification of such a change in the compliance method shall be reported according to the procedures in § 63.1260(h) of this subpart. Compliance with the required emission limits or reductions in paragraphs (a)(1) through (3) of this section may be demonstrated using the initial compliance procedures described in § 63.1257(d) and the monitoring requirements described in § 63.1258.

(1) Except for processes with a vent that meets the conditions in paragraph (a)(3)(i) of this section, actual HAP emissions shall not exceed 900 kilograms (kg) per year [2,000 pounds per year] from the sum of all process vents within a process.

(i) Except as provided in paragraph (a)(1)(iii) of this section, the owner or operator is limited to 7 processes in any 365-day period that can be selected to comply with paragraph (a)(1) of this section.

(ii) The owner or operator may exclude processes with less than 100 lb/yr HAP, on an uncontrolled basis, from the 7-process limit described in paragraph (a)(1)(i) of this section.

(2) Uncontrolled HAP emissions from the sum of all process vents within a process that do not meet the conditions in paragraph (a)(3)(i) of this section or are not controlled according to any of the requirements of paragraphs (a)(2)(i), (a)(2)(ii), (a)(2)(iii), or (c) of this section shall be reduced by 93 percent or greater by weight.

(i) To outlet concentrations less than or equal to 20 ppmv as TOC and less than or equal to 20 ppmv as hydrogen halide and halogens;

(ii) By a flare that meets the requirements of § 63.11(b); or

(iii) By a control device specified in § 63.1257(a)(4).

(3) Except as provided in paragraph (a)(3)(iii) of this section, uncontrolled HAP emissions from each process vent that meets the conditions in paragraph (a)(3)(ii) of this section shall be reduced as specified in paragraph (a)(3)(ii) of this section.

(i) Uncontrolled HAP emissions from a process vent shall be reduced as specified in paragraph (a)(3)(ii) if the vent meets either of the criteria described in paragraph (a)(3)(i)(A) or (B) of this section:

(A) The flow-weighted average flowrate calculated using Equation 1 of this subpart is less than or equal to the flowrate calculated using Equation 2 of this subpart.

\[
FR_{2} = \frac{\sum_{i=1}^{n} (D_{i})(FR_{i})}{\sum_{i=1}^{n} D_{i}}
\]  

(Eq. 1)

\[
FR = 0.02 \times (HL) - 1,000
\]  

(Eq. 2)

Where:
§ 63.1255 Standards: Equipment leaks.

(a) General Equipment Leak Requirements.

(1) The provisions of this section apply to pumps, compressors, agitators, pressure relief devices, sampling connection systems, open-ended valves or lines, valves, connectors, instrumentation systems, control devices, and closed-vent systems required by this subpart that are intended to operate in organic hazardous air pollutant service 300 hours or more during

FR = flow-weighted average flowrate for the vent, scfm

D_i = duration of each emission event, min

FR_i = flowrate of each emission event, scfm

n = number of emission events

FR = flowrate, scfm

HL = annual uncontrolled HAP emissions, lb/yr, as defined in §63.1251

(B) As an alternative to the criteria described in paragraph (a)(3)(i)(A) of this section, uncontrolled HAP emissions from a process vent shall be reduced or controlled as specified in paragraph (a)(3)(ii) of this section if the process vent meets the criteria specified in paragraphs (a)(3)(ii)(B)(1) and (2) of this section or the criteria specified in paragraphs (a)(3)(ii)(B)(1) and (3) of this section.

(i) Uncontrolled HAP emissions from the process vent exceed 25 tons per year.

(ii) The flow-weighted average flowrate for the vent, as calculated in Equation 1 of this section, is less than or equal to 100 scfm.

(iii) The flow weighted average is greater than 100 scfm and less than or equal to the flowrate calculated using Equation 2 of this section.

(A) By 98 percent by weight or greater; or

(B) To outlet concentrations less than or equal to 20 ppmv as TOC and less than or equal to 20 ppmv as hydrogen halides and halogens;

(C) By a flare that meets the requirements of §63.11(b); or

(D) By a control device specified in §63.1257(a)(4).

(iii) If the owner or operator can demonstrate that a control device, installed on a process vent that meets the conditions of paragraph (a)(3)(i) of this section on or before April 2, 1997, was designed to reduce uncontrolled HAP emissions of total HAP by greater than 93 percent by weight, but less than 98 percent by weight, then the control device is required to be operated to reduce inlet emissions of total HAP by 93 percent by weight or greater.

(b) New sources. Uncontrolled HAP emissions from the sum of all process vents within a process at a new affected source that are not controlled according to any of the requirements of paragraphs (b)(1), (2), or (3) of this section or paragraph (c) of this section shall be reduced by 98 percent or greater by weight if the uncontrolled HAP emissions from the sum of all process vents within a process is greater than 180 kg/yr (400 lb/yr). Compliance with the required emission limit or reduction is demonstrated using the initial compliance procedures in §63.1257(d) and the monitoring requirements described in §63.1258.

(1) To outlet concentrations less than or equal to 20 ppmv as TOC and less than or equal to 20 ppmv as hydrogen halides and halogens;

(2) By a flare that meets the requirements of §63.11(b); or

(3) By a control device specified in §63.1257(a)(4).

(c) As an alternative standard, the owner or operator of an existing or new affected source may comply with the process vent standards by routing all vents from a process to a control device achieving an outlet TOC concentration, as calibrated on methane or the predominant HAP, of 20 ppmv or less, and an outlet concentration of hydrogen halides and halogens of 20 ppmv or less. Any process vents within a process that are not routed to this control device must be controlled in accordance with the provisions of paragraphs (a)(2), (a)(3), and (b) of this section, as applicable. Compliance with the outlet concentrations shall be determined by the initial compliance procedures described in §63.1257(d)(1)(iv) and the continuous emission monitoring requirements described in §63.1258(b)(5).

§ 63.1255 Standards: Equipment leaks.
the calendar year within a source subject to the provisions of this subpart.

(2) Consistency with other regulations. After the compliance date for a process, equipment subject to both this section and either of the following will be required to comply only with the provisions of this subpart:

(i) 40 CFR part 60.
(ii) 40 CFR part 61.

(3) [Reserved]

(4) The provisions in §63.1(a)(3) of subpart A of this part do not alter the provisions in paragraph (a)(2) of this section.

(5) Lines and equipment not containing process fluids are not subject to the provisions of this section. Utilities, and other nonprocess lines, such as heating and cooling systems which do not combine their materials with those in the processes they serve, are not considered to be part of a process.

(6) The provisions of this section do not apply to bench-scale processes, regardless of whether the processes are located at the same plant site as a process subject to the provisions of this subpart.

(7) Each piece of equipment to which this section applies shall be identified such that it can be distinguished readily from equipment that is not subject to this section. Identification of the equipment does not require physical tagging of the equipment. For example, the equipment may be identified on a plant site plan, in log entries, or by designation of process boundaries by some form of weatherproof identification. If changes are made to the affected source subject to the leak detection requirements, equipment identification for each type of component shall be updated, if needed, within 30 calendar days of the end of each monitoring period for that component.

(8) Equipment that is in vacuum service is excluded from the requirements of this section.

(9) Equipment that is in organic HAP service, but is in such service less than 300 hours per calendar year, is excluded from the requirements of this section if it is identified as required in paragraph (g)(9) of this section.

(10) When each leak is detected by visual, audible, or olfactory means, or by monitoring as described in §63.180(b) or (c), the following requirements apply:

(i) A weatherproof and readily visible identification, marked with the equipment identification number, shall be attached to the leaking equipment.

(ii) The identification on a valve or connector in light liquid or gas/vapor service may be removed after it has been monitored as specified in paragraph (e)(7)(iii) of this section and §63.174(e), and no leak has been detected during the follow-up monitoring.

(iii) The identification on equipment, except on a valve or connector in light liquid or gas/vapor service, may be removed after it has been repaired.

(b) References. (1) The owner or operator of a source subject to this section shall comply with the following sections of subpart H, except for §63.160, §63.161, §63.162, §63.163, §63.167, §63.168, §63.170, §63.171, §63.172, §63.173, §63.181, and §63.182 of this subpart. In place of §63.160 and §63.162, the owner or operator shall comply with paragraph (a) of this section; in place of §63.161, the owner or operator shall comply with §63.1251 of this subpart; in place of §63.163 and §63.173, the owner or operator shall comply with paragraph (c) of this section; in place of §63.167, the owner or operator shall comply with paragraph (d) of this section; in place of §63.168, the owner or operator shall comply with paragraph (e) of this section; in place of §63.170, the owner or operator shall comply with paragraph (b)(1)(v) of this section; in place of §63.171, the owner or operator shall comply with paragraph (b)(1)(vi) of this section; in place of §63.181, the owner or operator shall comply with paragraph (g) of this section; in place of §63.182, the owner or operator shall comply with paragraph (h) of this section. The term "process unit" as used in subpart H shall be considered to be defined the same as "group of processes" for sources subject to this subpart GGG.

(i) Section 63.164, Compressors;
(ii) Section 63.165, Pressure relief devices in gas/vapor service;
(iii) Section 63.166, Sampling connection systems;
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(iv) Section 63.169, Pumps, valves, connectors, and agitators in heavy liquid service; instrumentation systems; and pressure relief devices in liquid service;

(v) Section 63.171, Delay of repair, shall apply except § 63.171(a) shall not apply. Instead, delay of repair of equipment for which leaks have been detected is allowed if one of the following conditions exist:

(A) The repair is technically infeasible without a process shutdown. Repair of this equipment shall occur by the end of the next scheduled process shutdown.

(B) The owner or operator determines that repair personnel would be exposed to an immediate danger if attempting to repair without a process shutdown. Repair of this equipment shall occur by the end of the next scheduled process shutdown.

(vi) Section 63.172, Closed-vent systems and control devices, for closed-vent systems used to comply with this subpart, and for control devices used to comply with this section only, except

(A) Sections 63.172(k) and (l) shall not apply. In place of § 63.172(k) and (l), the owner or operator shall comply with paragraph (f) of this section.

(B) Owners or operators may, instead of complying with the provisions of § 63.172(f), design a closed-vent system to operate at a pressure below atmospheric pressure. The system shall be equipped with at least one pressure gage or other pressure measurement device that can be read from a readily accessible location to verify that negative pressure is being maintained in the closed-vent system when the associated control device is operating.

(vii) Section 63.174, Connectors, except:

(A) Sections 63.174(f) and (g) shall not apply. In place of § 63.174(f) and (g), the owner or operator shall comply with paragraph (f) of this section.

(B) Days that the connectors are not in organic HAP service shall not be considered part of the 3 month period in § 63.174(e).

(C) Section 63.174(b)(3)(i) shall not apply. Instead, if the percent leaking connectors in the process unit was less than 0.25 percent, during the last required monitoring period, monitoring shall be performed once every 4 years. An owner or operator may comply with the requirements of this paragraph by monitoring at least 40 percent of the connectors in the first 2 years and the remainder of the connectors within the next 2 years. The percent leaking connectors will be calculated for the total of all monitoring performed during the 4 year period.

(D) Section 63.174(b)(3)(iv) shall not apply. Instead, the owner or operator shall increase the monitoring frequency to once every 2 years for the next monitoring period if leaking connectors comprise at least 0.5 percent but less than 1.0 percent of the connectors monitored within the 4 years specified in paragraph (b)(1)(vii)(C) of this section or the first 4 years specified in §63.174(b)(3)(iii). At the end of that 2 year monitoring period, the owner or operator shall monitor once per year while the percent leaking connectors is greater than or equal to 0.5 percent; if the percent leaking connectors is less than 0.5 percent, the owner or operator may return to monitoring once every 4 years or may monitor in accordance with §63.174(b)(3)(iii), if appropriate.

(E) Section 63.174(b)(3)(v) shall not apply. Instead, if an owner or operator complies with the requirements of paragraph (b)(1)(vii)(C) and (D) of this section or §63.174(b)(3)(iii) for a group of processes determines that 1 percent or greater of the connectors are leaking, the owner or operator shall increase the monitoring frequency to one time per year. The owner or operator may again elect to use the provisions of paragraphs (b)(1)(vii)(C) or (D) of this section after a monitoring period in which less than 0.5 percent of the connectors are determined to be leaking.

(F) Section 63.174(b)(3)(iii) shall not apply. Instead, monitoring shall be required once every 8 years, if the percent leaking connectors in the process unit was less than 0.25 percent during the last required monitoring period. An owner or operator shall monitor at least 50 percent of the connectors in the first 4 years and the remainder of the connectors within the next 4 years. If the percent leaking connectors in the first 4 years is equal to or greater
than 0.35 percent, the monitoring program shall revert at that time to the appropriate monitoring frequency specified in paragraphs (b)(1)(vii)(C), (D), or (E) of this section.

(viii) Section 63.177, Alternative means of emission limitation: General;

(ix) Section 63.178, Alternative means of emission limitation: Batch processes, except that § 63.178(b), requirements for pressure testing, shall apply to all processes, not just batch processes;

(x) Section 63.179, Alternative means of emission limitation: Enclosed-ventilated process units;

(xi) Section 63.180, Test methods and procedures, except § 63.180(b)(4)(ii)(A) through (C) shall not apply. Instead calibration gases shall be a mixture of methane and air at a concentration of approximately, but less than, 10,000 parts per million methane for agitators; 2,000 parts per million for pumps; and 500 parts per million for all other equipment, except as provided in section 63.180(b)(4)(iii).

(2) [Reserved]

(c) Standards for Pumps in Light Liquid Service and Agitators in Gas/Vapor Service and in Light Liquid Service. (1) The provisions of this section apply to each pump that is in light organic HAP liquid service, and to each agitator in organic HAP gas/vapor service or in light organic HAP liquid service.

(2)(i) Monitoring. Each pump and agitator subject to this section shall be monitored quarterly to detect leaks by the method specified in § 63.180(b) of subpart H, except as provided in § 63.177 of subpart H, paragraph (f) of this section, and paragraphs (c)(5) through (c)(9) of this section.

(ii) Leak definition. The instrument reading, as determined by the method as specified in § 63.180(b), that defines a leak is:

(A) For agitators, an instrument reading of 10,000 parts per million or greater.

(B) For pumps, an instrument reading of 2,000 parts per million or greater.

(iii) Visual Inspections. Each pump and agitator shall be checked by visual inspection each calendar week for indications of liquids dripping from the pump or agitator seal. If there are indications of liquids dripping from the seal, a leak is detected.

(3) Repair provisions. (i) When a leak is detected, it shall be repaired as soon as practicable, but not later than 15 calendar days after it is detected, except as provided in paragraph (b)(1)(v) of this section.

(ii) A first attempt at repair shall be made no later than 5 calendar days after the leak is detected. First attempts at repair include, but are not limited to, the following practices where practicable:

(A) Tightening of packing gland nuts.

(B) Ensuring that the seal flush is operating at design pressure and temperature.

(4) Calculation of percent leakers. (i) The owner or operator shall decide no later than the end of the first monitoring period what groups of processes will be developed. Once the owner or operator has decided, all subsequent percent calculations shall be made on the same basis.

(ii) If, calculated on a 1 year rolling average, the greater of either 10 percent or three of the pumps in a group of processes leak, the owner or operator shall monitor each pump once per month.

(iii) The number of pumps in a group of processes shall be the sum of all the pumps in organic HAP service, except that pumps found leaking in a continuous process within 1 quarter after startup of the pump shall not count in the percent leaking pumps calculation for that one monitoring period only.

(iv) Percent leaking pumps shall be determined by the following Equation 3:

\[
\%P_L = \frac{(P_L - P_S)}{(P_T - P_S)} \times 100 \text{ (Eq. 3)}
\]

Where:

\%P_L = percent leaking pumps

\(P_L\) = number of pumps found leaking as determined through quarterly monitoring as required in paragraphs (c)(2)(i) and (c)(2)(ii) of this section.

\(P_T\) = total pumps in organic HAP service, including those meeting the criteria in paragraphs (c)(5) and (c)(6) of this section.

\(P_S\) = number of pumps in a continuous process leaking within 1 quarter of startup during the current monitoring period.
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(5) Exemptions. Each pump or agitator equipped with a dual mechanical seal system that includes a barrier fluid system is exempt from the requirements of paragraphs (c)(1) through (c)(4)(iii) of this section, provided the following requirements are met:

(i) Each dual mechanical seal system is:

(A) Operated with the barrier fluid at a pressure that is at all times greater than the pump/agitator stuffing box pressure; or

(B) Equipped with a barrier fluid degassing reservoir that is connected by a closed-vent system to a control device that complies with the requirements of paragraph (b)(1)(vi) of this section, or

(C) Equipped with a closed-loop system that purges the barrier fluid into a process stream.

(ii) The barrier fluid is not in light liquid service.

(iii) Each barrier fluid system is equipped with a sensor that will detect failure of the seal system, the barrier fluid system, or both.

(iv) Each pump/agitator is checked by visual inspection each calendar week for indications of liquids dripping from the pump/agitator seal.

(A) If there are indications of liquids dripping from the pump/agitator seal at the time of the weekly inspection, the pump/agitator shall be monitored as specified in § 63.180(b) to determine if there is a leak of organic HAP in the barrier fluid.

(B) If an instrument reading of 2,000 parts per million or greater is measured for pumps, or 10,000 parts per million or greater is measured for agitators, a leak is detected.

(v) Each sensor as described in paragraph (c)(5)(iii) of this section is observed daily or is equipped with an alarm unless the pump is located within the boundary of an unmanned plant site.

(A) The owner or operator determines, based on design considerations and operating experience, criteria applicable to the presence and frequency of drips and to the sensor that indicate failure of the seal system, the barrier fluid system, or both.

(B) If indications of liquids dripping from the pump/agitator seal exceed the criteria established in paragraph (c)(5)(vi)(A) of this section, or if, based on the criteria established in paragraph (c)(5)(vi)(A) of this section, the sensor indicates failure of the seal system, the barrier fluid system, or both, a leak is detected.

(C) When a leak is detected, it shall be repaired as soon as practicable, but not later than 15 calendar days after it is detected, except as provided in paragraph (b)(1)(v) of this section.

(D) A first attempt at repair shall be made no later than 5 calendar days after each leak is detected.

(6) Any pump/agitator that is designed with no externally actuated shaft penetrating the pump/agitator housing is exempt from the requirements of paragraphs (c)(1) through (c)(4) of this section, except for the requirements of paragraph (c)(2)(iii) and, for pumps, paragraph (c)(4)(iv).

(7) Any pump/agitator equipped with a closed-vent system capable of capturing and transporting any leakage from the seal or seals back to the process or to a control device that complies with the requirements of paragraph (b)(1)(vi) of this section is exempt from the requirements of paragraphs (c)(2) through (c)(5) of this section.

(8) Any pump/agitator that is located within the boundary of an unmanned plant site is exempt from the weekly visual inspection requirement of paragraphs (c)(2)(iii) and (c)(5)(iv) of this section, and the daily requirements of paragraph (c)(5)(v) of this section, provided that each pump/agitator is visually inspected as often as practicable and at least monthly.

(9) If more than 90 percent of the pumps in a group of processes meet the criteria in either paragraph (c)(5) or (c)(6) of this section, the process is exempt from the requirements of paragraph (c)(4) of this section.

(d) Standards: Open-Ended Valves or Lines. (1)(i) Each open-ended valve or line shall be equipped with a cap, blind flange, plug, or a second valve, except as provided in §63.177 and paragraphs (d)(4) through (6) of this section.

(ii) The cap, blind flange, plug, or second valve shall seal the open end at all times except during operations requiring process fluid flow through the open-ended valve or line, or during
maintenance or repair. The cap, blind flange, plug, or second valve shall be in place within 1 hour of cessation of operations requiring process fluid flow through the open-ended valve or line, or within 1 hour of cessation of maintenance or repair.

(2) Each open-ended valve or line equipped with a second valve shall be operated in a manner such that the valve on the process fluid end is closed before the second valve is closed.

(3) When a double block and bleed system is being used, the bleed valve or line may remain open during operations that require venting the line between the block valves, but shall comply with paragraph (d)(1) of this section at all other times.

(4) Open-ended valves or lines in an emergency shutdown system which are designed to open automatically in the event of a process upset are exempt from the requirements of paragraphs (d)(1) through (d)(3) of this section.

(5) Open-ended valves or lines containing materials which would autocatalytically polymerize are exempt from the requirements of paragraphs (d)(1) through (d)(3) of this section.

(e) Standards: Valves in Gas/Vapor Service and in Light Liquid Service. (1) The provisions of this section apply to valves that are either in gas organic HAP service or in light liquid organic HAP service.

(2) For existing and new affected sources, all valves subject to this section shall be monitored, except as provided in paragraph (f) of this section and in §63.177, by no later than 1 year after the compliance date.

(3) Monitoring. The owner or operator of a source subject to this section shall monitor all valves, except as provided in paragraph (f) of this section and in §63.177, at the intervals specified in paragraph (e)(4) of this section and shall comply with all other provisions of this section, except as provided in paragraph (b)(1)(v) of this section, §63.178, and §63.179.

(i) The valves shall be monitored to detect leaks by the method specified in §63.180(b).

(ii) An instrument reading of 500 parts per million or greater defines a leak.

(4) Subsequent monitoring frequencies. After conducting the initial survey required in paragraph (e)(2) of this section, the owner or operator shall monitor valves for leaks at the intervals specified below:

(i) For a group of processes with 2 percent or greater leaking valves, calculated according to paragraph (e)(6) of this section, the owner or operator shall monitor each valve once per month, except as specified in paragraph (e)(9) of this section.

(ii) For a group of processes with less than 2 percent leaking valves, the owner or operator shall monitor each valve once every 4 quarters.

(iii) For a group of processes with less than 1 percent leaking valves, the owner or operator may elect to monitor each valve once every 2 quarters.

(iv) For a group of processes with less than 0.5 percent leaking valves, the owner or operator may elect to monitor each valve once every 4 quarters.

(v) For a group of processes with less than 0.25 percent leaking valves, the owner or operator may elect to monitor each valve once every 2 years.

(5) Calculation of percent leakers. For a group of processes to which this subpart applies, an owner or operator may choose to subdivide the valves in the applicable group of processes and apply the provisions of paragraph (e)(4) of this section to each subgroup. If the owner or operator elects to subdivide the valves in the applicable group of processes, then the provisions of paragraphs (e)(5)(i) through (e)(5)(viii) of this section apply.

(i) The overall performance of total valves in the applicable group of processes must be less than 2 percent leaking valves, as detected according to paragraphs (e)(3)(i) and (ii) of this section and as calculated according to
§63.1255 paragraphs (e)(6) (ii) and (iii) of this section.

(ii) The initial assignment or subsequent reassignment of valves to subgroups shall be governed by the provisions of paragraphs (e)(5)(ii) (A) through (C) of this section.

(A) The owner or operator shall determine which valves are assigned to each subgroup. Valves with less than 1 year of monitoring data or valves not monitored within the last 12 months shall be placed initially into the most frequently monitored subgroup until at least 1 year of monitoring data has been obtained.

(B) Any valve or group of valves can be reassigned from a less frequently monitored subgroup to a more frequently monitored subgroup provided that the valves to be reassigned were monitored during the most recent monitoring period of the less frequently monitored subgroup. The monitoring results must be included with the less frequently monitored subgroup's monitoring event and associated next percent leaking valves calculation for that group.

(C) Any valve or group of valves can be reassigned from a more frequently monitored subgroup to a less frequently monitored subgroup provided that the valves to be reassigned have not leaked for the period of the less frequently monitored subgroup (e.g., for the last 12 months, if the valve or group of valves is to be reassigned to a subgroup being monitored annually). Nonrepairable valves may not be reassigned to a less frequently monitored subgroup.

(iii) The owner or operator shall determine every 6 months if the overall performance of total valves in the applicable group of processes is less than 2 percent leaking valves and so indicate the performance in the next periodic report. If the overall performance of total valves in the applicable group of processes is 2 percent leaking valves or greater, the owner or operator shall revert to the program required in paragraphs (e)(2) through (e)(4) of this section. The overall performance of total valves in the applicable group of processes shall be calculated as a weighted average of the percent leaking valves of each subgroup according to the following Equation 4:

$$\% V_{LO} = \frac{\sum_{i=1}^{n} (\% V_{Li} \times V_i)}{\sum_{i=1}^{n} V_i}$$  

(Eq. 4)

where:

- $\% V_{LO} =$ overall performance of total valves in the applicable process or group of processes
- $\% V_{Li} =$ percent leaking valves in subgroup I, most recent value calculated according to the procedures in paragraphs (e)(6) (ii) and (iii) of this section
- $V_i =$ number of valves in subgroup I
- $n =$ number of subgroups

(iv) Records. In addition to records required by paragraph (g) of this section, the owner or operator shall maintain records specified in paragraphs (e)(5)(iv)(A) through (D) of this section.

(A) Which valves are assigned to each subgroup,

(B) Monitoring results and calculations made for each subgroup for each monitoring period,

(C) Which valves are reassigned and when they were reassigned, and

(D) The results of the semiannual overall performance calculation required in paragraph (e)(5)(iii) of this section.

(v) The owner or operator shall notify the Administrator no later than 30 days prior to the beginning of the next monitoring period of the decision to subgroup valves. The notification shall identify the participating processes and the valves assigned to each subgroup.

(vi) Semiannual reports. In addition to the information required by paragraph (h)(3) of this section, the owner or operator shall submit in the periodic reports the information specified in paragraphs (e)(5)(vi)(A) and (B) of this section.

(A) Valve reassignments occurring during the reporting period, and

(B) Results of the semiannual overall performance calculation required by paragraph (e)(5)(iii) of this section.
(vii) To determine the monitoring frequency for each subgroup, the calculation procedures of paragraph (e)(6)(iii) of this section shall be used.

(viii) Except for the overall performance calculations required by paragraphs (e)(5)(i) and (e)(5)(iii) of this section, each subgroup shall be treated as if it were a process for the purposes of applying the provisions of this section.

(6)(i) The owner or operator shall decide no later than the implementation date of this subpart or upon revision of an operating permit how to group the processes. Once the owner or operator has decided, all subsequent percentage calculations shall be made on the same basis.

(ii) Percent leaking valves for each group of processes or subgroup shall be determined by the following Equation 5:

\[
\% V_L = \frac{V_L}{V_T} \times 100 \quad (\text{Eq. 5})
\]

Where:

\(\% V_L\) = percent leaking valves
\(V_L\) = number of valves found leaking excluding nonrepairables as provided in paragraph (e)(6)(iv)(A) of this section
\(V_T\) = total valves monitored, in a monitoring period excluding valves monitored as required by (e)(7)(iii) of this section

(iii) When determining monitoring frequency for each group of processes or subgroup subject to monthly, quarterly, or semiannual monitoring frequencies, the percent leaking valves shall be the arithmetic average of the percent leaking valves from the last two monitoring periods. When determining monitoring frequency for each group of processes or subgroup subject to annual or biennial (once every 2 years) monitoring frequencies, the percent leaking valves shall be the arithmetic average of the percent leaking valves from the last three monitoring periods.

(iv)(A) Nonrepairable valves shall be included in the calculation of percent leaking valves the first time the valve is identified as leaking and nonrepairable and as required to comply with paragraph (e)(6)(iv)(B) of this section. Otherwise, a number of nonrepairable valves (identified and included in the percent leaking calculation in a previous period) up to a maximum of 1 percent of the total number of valves in organic HAP service at a process may be excluded from calculation of percent leaking valves for subsequent monitoring periods.

(B) If the number of nonrepairable valves exceeds 1 percent of the total number of valves in organic HAP service at a process, the number of nonrepairable valves exceeding 1 percent of the total number of valves in organic HAP service shall be included in the calculation of percent leaking valves.

(7) Repair provisions. (i) When a leak is detected, it shall be repaired as soon as practicable, but no later than 15 calendar days after the leak is detected, except as provided in paragraph (b)(1)(v) of this section.

(ii) A first attempt at repair shall be made no later than 5 calendar days after each leak is detected.

(iii) When a leak is repaired, the valve shall be monitored at least once within the first 3 months after its repair. Days that the valve is not in organic HAP service shall not be considered part of this 3 month period.

(B) First attempts at repair include, but are not limited to, the following practices where practicable:

(i) Tightening of bonnet bolts,
(ii) Replacement of bonnet bolts,
(iii) Tightening of packing gland nuts, and
(iv) Injection of lubricant into lubricated packing.

(8) First attempts at repair include, but are not limited to, the following practices where practicable:

(i) Tightening of bonnet bolts,
(ii) Replacement of bonnet bolts,
(iii) Tightening of packing gland nuts, and
(iv) Injection of lubricant into lubricated packing.

(9) Any equipment located at a plant site with fewer than 250 valves in organic HAP service in the affected source is exempt from the requirements for monthly monitoring specified in paragraph (e)(4)(i) of this section. Instead, the owner or operator shall monitor each valve in organic HAP service for leaks once each quarter, or comply with paragraphs (e)(4)(iii) or (e)(4)(iv) of this section.

(f) Unsafe to Monitor, Difficult to Monitor, and Inaccessible Equipment. (1) Equipment that is designated as unsafe to monitor, difficult to monitor, or inaccessible is exempt from the monitoring requirements specified in paragraphs (f)(1)(i) through (iv) of this section provided the owner or operator meets the requirements specified in paragraph (f)(2), (f)(3), or (f)(4) of this section.
section, as applicable. Ceramic or ceramic-lined connectors are subject to the same requirements as inaccessible connectors.

(i) For pumps and agitators, paragraphs (c)(2), (c)(3), and (c)(4) of this section do not apply.

(ii) For valves, paragraphs (e)(2) through (e)(7) of this section do not apply.

(iii) For closed-vent systems, §63.172(f)(1) and (2), and (g) do not apply.

(iv) For connectors, §63.174(b) through (e) do not apply.

(2) Equipment that is unsafe to monitor.

(i) Equipment may be designated as unsafe to monitor if the owner or operator determines that monitoring personnel would be exposed to an immediate danger as a consequence of complying with the monitoring requirements in paragraphs (f)(1)(i) through (iv) of this section.

(ii) The owner or operator of equipment that is designated as unsafe to monitor must have a written plan that requires monitoring of the equipment as frequently as practicable during safe-to-monitor times, but not more frequently than the periodic monitoring schedule otherwise applicable.

(3) Equipment that is difficult to monitor.

(i) Equipment may be designated as difficult to monitor if the owner or operator determines that the equipment cannot be monitored without elevating the monitoring personnel more than 2 meters above a support surface or it is not accessible at anytime in a safe manner;

(ii) At an existing source, any equipment within a group of processes that meets the criteria of paragraph (f)(3)(i) of this section may be designated as difficult to monitor. At a new affected source, an owner or operator may designate no more than 3 percent of each type of equipment as difficult to monitor.

(iii) The owner or operator of equipment designated as difficult to monitor must follow a written plan that requires monitoring of the equipment at least once per calendar year.

(4) Inaccessible equipment and ceramic or ceramic-lined connectors.

(A) Buried;

(B) Insulated in a manner that prevents access to the equipment by a monitor probe;

(C) Obstructed by equipment or piping that prevents access to the equipment by a monitor probe;

(D) Unable to be reached from a wheeled scissor-lift or hydraulic-type scaffold which would allow access to equipment up to 7.6 meters (25 feet) above the ground; or

(E) Not able to be accessed at any time in a safe manner to perform monitoring. Unsafe access includes, but is not limited to, the use of a wheeled scissor-lift on unstable or uneven terrain, the use of a motorized man-lift basket in areas where an ignition potential exists, or access would require near proximity to hazards such as electrical lines, or would risk damage to equipment.

(ii) At an existing source, any connector, agitator, or valve that meets the criteria of paragraph (f)(4)(i) of this section may be designated as inaccessible. At a new affected source, an owner or operator may designate no more than 3 percent of each type of equipment as inaccessible.

(iii) If any inaccessible equipment or ceramic or ceramic-lined connector is observed by visual, audible, olfactory, or other means to be leaking, the leak shall be repaired as soon as practicable, but no later than 15 calendar days after the leak is detected, except as provided in paragraph (g) of this section.

(g) Recordkeeping Requirements.

(1) An owner or operator of more than one group of processes subject to the provisions of this section may comply with the recordkeeping requirements for the groups of processes in one recordkeeping system if the system identifies with each record the program being implemented (e.g., quarterly monitoring) for each type of equipment. All records and information required by this section shall be maintained in a manner that can be readily accessed at the plant site. This could include physically locating the records at the plant site or accessing the records from a central location by computer at the plant site.
(2) General recordkeeping. Except as provided in paragraph (e) of this section and in paragraph (a)(9) of this section, the following information pertaining to all equipment subject to the requirements in this section shall be recorded:

(i) (A) A list of identification numbers for equipment (except connectors that are not subject to paragraph (f) of this section and instrumentation systems) subject to the requirements of this section. Connectors, except those subject to paragraph (f) of this section, need not be individually identified if all connectors in a designated area or length of pipe subject to the provisions of this section are identified as a group, and the number of subject connectors is indicated. The list for each type of equipment shall be completed no later than the completion of the initial survey required for that component. The list of identification numbers shall be updated, if needed, to incorporate equipment changes within 15 calendar days of the completion of each monitoring survey for the type of equipment component monitored.

(B) A schedule for monitoring connectors subject to the provisions of §63.174(a) and valves subject to the provisions of paragraph (b)(4) of this section.

(C) Physical tagging of the equipment to indicate that it is in organic HAP service is not required. Equipment subject to the provisions of this section may be identified on a plant site plan, in log entries, or by other appropriate methods.

(ii) (A) A list of identification numbers for equipment that the owner or operator elects to equip with a closed-vent system and control device, under the provisions of paragraph (c)(7) of this section.

(B) A list of identification numbers for compressors that the owner or operator elects to designate as operating with an instrument reading of less than 500 parts per million above background, under the provisions of §63.164(i).

(iii) (A) A list of identification numbers for pressure relief devices subject to the provisions in §63.168(a).

(B) A list of identification numbers for pressure relief devices equipped with rupture disks, under the provisions of §63.165(d).

(iv) Identification of instrumentation systems subject to the provisions of this section. Individual components in an instrumentation system need not be identified.

(v) The owner or operator may develop a written procedure that identifies the conditions that justify a delay of repair. The written procedures may be included as part of the startup/shutdown/malfunction plan, required by §63.1260(i), for the source or may be part of a separate document that is maintained at the plant site. Reasons for delay of repair may be documented by citing the relevant sections of the written procedure.

(vi) The following information shall be recorded for each dual mechanical seal system:

(A) Design criteria required by paragraph (c)(5)(vi)(A) of this section and §63.164(e)(2), and an explanation of the design criteria; and

(B) Any changes to these criteria and the reasons for the changes.

(vii) A list of equipment designated as unsafe to monitor, difficult to monitor, or inaccessible under paragraphs (f) or (b)(1)(v)(B) of this section and a copy of the plan for monitoring or inspecting this equipment.

(viii) A list of connectors removed from and added to the process, as described in §63.174(j)(1), and documentation of the integrity of the weld for any removed connectors, as required in §63.174(j). This is not required unless the net credits for removed connectors is expected to be used.

(ix) For batch processes that the owner or operator elects to monitor as provided under §63.178(c), a list of equipment added to batch product processes since the last monitoring period required in §§63.178(c)(3)(ii) and (3)(iii). This list must be completed for each type of equipment within 15 calendar days of the completion of each monitoring survey for the type of equipment monitored.

(3) Records of visual inspections. For visual inspections of equipment subject to the provisions of paragraphs
(c)(2)(iii) and (c)(5)(iv)(A) of this section, the owner or operator shall document that the inspection was conducted and the date of the inspection. The owner or operator shall maintain records as specified in paragraph (g)(4) of this section for leaking equipment identified in this inspection, except as provided in paragraph (g)(5) of this section. These records shall be retained for 2 years.

(4) Monitoring records. When each leak is detected as specified in paragraph (c) of this section and §§63.164, paragraph (e) of this section and §§63.169 and 63.171 of subpart H, the following information shall be recorded and kept for 2 years onsite and 3 years offsite (5 years total):

(i) The instrument and the equipment identification number and the operator name, initials, or identification number.

(ii) The date the leak was detected and the date of the first attempt to repair the leak.

(iii) The date of successful repair of the leak.

(iv) If postrepair monitoring is required, the maximum instrument reading measured by Method 21 of 40 CFR part 60, appendix A after the leak is successfully repaired or determined to be nonrepairable.

(v) “Repair delayed” and the reason for the delay if a leak is not repaired within 15 calendar days after discovery of the leak.

(A) The owner or operator may develop a written procedure that identifies the conditions that justify a delay of repair. In such cases, reasons for delay of repair may be documented by citing the relevant sections of the written procedure.

(B) If delay of repair was caused by depletion of stocked parts, there must be documentation that the spare parts were sufficiently stocked onsite before depletion and the reason for depletion.

(vi) If repairs were delayed, dates of process shutdowns that occur while the equipment is unrepaired.

(vii)(A) If the alternative in §63.174(c)(3)(ii) is not in use for the monitoring period, identification, either by list, location (area or grouping), or tagging of connectors disturbed since the last monitoring period required in §63.174(b), as described in §63.174(c)(1).

(B) The date and results of follow-up monitoring as required in §63.174(c). If identification of disturbed connectors is made by location, then all connectors within the designated location shall be monitored.

(viii) The date and results of the monitoring required in §63.174(c)(3)(i) for equipment added to a batch process since the last monitoring period required in §§63.174(c)(3)(ii) and (c)(3)(iii). If no leaking equipment is found in this monitoring, the owner or operator shall record that the inspection was performed. Records of the actual monitoring results are not required.

(ix) Copies of the periodic reports as specified in paragraph (h)(3) of this section, if records are not maintained on a computerized data base capable of generating summary reports from the records.

(5) Records of pressure tests. The owner or operator who elects to pressure test a process equipment train and supply lines between storage and processing areas to demonstrate compliance with this section is exempt from the requirements of paragraphs (g)(2), (g)(3), (g)(4), and (g)(6) of this section. Instead, the owner or operator shall maintain records of the following information:

(i) The identification of each product, or product code, produced during the calendar year. It is not necessary to identify individual items of equipment in the process equipment train.

(ii) Records demonstrating the proportion of the time during the calendar year the equipment is in use in the process that is subject to the provisions of this subpart. Examples of suitable documentation are records of time in use for individual pieces of equipment or average time in use for the process unit. These records are not required if the owner or operator does not adjust monitoring frequency by the time in use, as provided in §63.174(c)(3)(iii).

(iii) Physical tagging of the equipment to identify that it is in organic HAP service and subject to the provisions of this section is not required.
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identified on a plant site plan, in log entries, or by other appropriate methods.

(iv) The dates of each pressure test required in §63.178(b), the test pressure, and the pressure drop observed during the test.

(v) Records of any visible, audible, or olfactory evidence of fluid loss.

(vi) When a process equipment train does not pass two consecutive pressure tests, the following information shall be recorded in a log and kept for 2 years:

(A) The date of each pressure test and the date of each leak repair attempt.

(B) Repair methods applied in each attempt to repair the leak.

(C) The reason for the delay of repair.

(D) The expected date for delivery of the replacement equipment and the actual date of delivery of the replacement equipment.

(E) The date of successful repair.

(7) Records for closed-vent systems. The owner or operator shall maintain records of the information specified in paragraphs (g)(7)(i) through (g)(7)(iii) of this section for closed-vent systems and control devices subject to the provisions in §§63.165(a) and (b). The results shall include:

(i) The background level measured during each compliance test.

(ii) The maximum instrument reading measured at each piece of equipment during each compliance test.

(8) Records for components in heavy liquid service. Information, data, and analysis used to determine that a piece of equipment or process is in heavy liquid service shall be recorded. Such a determination shall include an analysis or demonstration that the process fluids do not meet the criteria of “in light liquid or gas service.” Examples of information that could document this include, but are not limited to, records of chemicals purchased for the process,
analyses of process stream composition, engineering calculations, or process knowledge.

(9) Records of exempt components. Identification, either by list, location (area or group) of equipment in organic HAP service less than 300 hours per year subject to the provisions of this section.

(10) Records of alternative means of compliance determination. Owners and operators choosing to comply with the requirements of §63.179 shall maintain the following records:

(i) Identification of the process(es) and the organic HAP they handle.

(ii) A schematic of the process, enclosure, and closed-vent system.

(iii) A description of the system used to create a negative pressure in the enclosure to ensure that all emissions are routed to the control device.

(h) Reporting Requirements. (1) Each owner or operator of a source subject to this section shall submit the reports listed in paragraphs (h)(1)(i) through (ii) of this section.

(i) A Notification of Compliance Status Report described in paragraph (h)(2) of this section,

(ii) Periodic Reports described in paragraph (h)(3) of this section, and

(2) Notification of compliance report. Each owner or operator of a source subject to this section shall submit the information specified in paragraphs (h)(2)(i) through (iii) of this section in the Notification of Compliance Status Report described in §63.1260(f).

(i) The notification shall provide the information listed in paragraphs (h)(2)(i)(A) through (C) of this section for each process subject to the requirements of paragraphs (b) through (g) of this section.

(A) Process group identification.

(B) Approximate number of each equipment type (e.g., valves, pumps) in organic HAP service, excluding equipment in vacuum service.

(C) Method of compliance with the standard (for example, “monthly leak detection and repair” or “equipped with dual mechanical seals”).

(ii) The notification shall provide the information listed in paragraphs (h)(2)(ii)(A) and (B) of this section for each process subject to the requirements of paragraph (b)(1)(ix) of this section and §63.178(b).

(A) Products or product codes subject to the provisions of this section, and

(B) Planned schedule for pressure testing when equipment is configured for production of products subject to the provisions of this section.

(iii) The notification shall provide the information listed in paragraphs (h)(2)(iii)(A) and (B) of this section for each process subject to the requirements in §63.179.

(A) Process identification.

(B) A description of the system used to create a negative pressure in the enclosure and the control device used to comply with the requirements of paragraph (b)(1)(vi) of this section.

(iv) Any change in the information submitted under paragraph (h) of this section shall be provided to the Administrator as a part of subsequent Periodic Reports. Section 63.9(j) shall not apply to the Notification of Compliance Status Report described in this paragraph (h)(2) of this section.

(3) Periodic reports. The owner or operator of a source subject to this section shall submit Periodic Reports.

(i) A report containing the information in paragraphs (h)(3)(ii), (h)(3)(iii), and (h)(3)(iv) of this section shall be submitted semiannually starting 6 months after the Notification of Compliance Status Report, as required in paragraph (h)(2) of this section. The first periodic report shall cover the first 6 months after the compliance date specified in §63.1250(e). Each subsequent periodic report shall cover the 6-month period following the preceding period.

(ii) For equipment complying with the provisions of paragraphs (b) through (g) of this section, the summary information listed in paragraphs (h)(3)(ii)(A) through (L) of this section for each monitoring period during the 6-month period.

(A) The number of valves for which leaks were detected as described in paragraph (e)(3) of this section, the percent leakers, and the total number of valves monitored;

(B) The number of valves for which leaks were not repaired as required in
paragraph (e)(7) of this section, identifying the number of those that are determined nonrepairable;

(C) The number of pumps and agitators for which leaks were detected as described in paragraph (c)(2) of this section, the percent leakers, and the total number of pumps and agitators monitored;

(D) The number of pumps and agitators for which leaks were not repaired as required in paragraph (c)(3) of this section;

(E) The number of compressors for which leaks were detected as described in §63.164(f);

(F) The number of compressors for which leaks were not repaired as required in §63.164(g);

(G) The number of connectors for which leaks were detected as described in §63.174(a), the percent of connectors leaking, and the total number of connectors monitored;

(H) The number of connectors for which leaks were not repaired as required in §63.174(d), identifying the number of those that are determined nonrepairable;

(I) The facts that explain any delay of repairs and, where appropriate, why a process shutdown was technically infeasible.

(J) The results of all monitoring to show compliance with §§63.164(i), 63.165(a), and 63.172(f) conducted within the semiannual reporting period.

(K) If applicable, the initiation of a monthly monitoring program under either paragraph (c)(4)(ii) or paragraph (e)(4)(i) of this section.

(L) If applicable, notification of a change in connector monitoring alternatives as described in §63.174(c)(1).

(iii) For owners or operators electing to meet the requirements of §63.178(b), the report shall include the information listed in paragraphs (h)(3)(iii)(A) through (E) of this paragraph for each process.

(A) Product process equipment train identification;

(B) The number of pressure tests conducted;

(C) The number of pressure tests where the equipment train failed either the retest or two consecutive pressure tests;

(D) The facts that explain any delay of repairs; and

(E) The results of all monitoring to determine compliance with §63.172(f) of subpart H.

(iv) Any revisions to items reported in earlier Notification of Compliance Status Report, if the method of compliance has changed since the last report or any other changes to the information reported has occurred.

§63.1256 Standards: Wastewater.

(a) General. Each owner or operator of any affected source (existing or new) shall comply with the general wastewater requirements in paragraphs (a)(1) and (2) of this section.

(1) Identify wastewater that requires control. For each POD, the owner or operator shall comply with the requirements in either paragraph (a)(1)(i), or (ii) of this section to determine whether a wastewater stream is an affected wastewater stream that requires control for soluble and/or partially soluble HAP compounds or to designate the wastewater stream as an affected wastewater stream, respectively. The owner or operator may use a combination of the approaches in paragraphs (a)(1)(i) and (ii) of this section for different affected wastewater generated at the source. The owner or operator shall also comply with the requirements for multiphase discharges in paragraph (a)(4) of this section. Wastewater identified in paragraph (a)(3) of this section is exempt from the provisions of this subpart.

(i) Determine characteristics of a wastewater stream. At new and existing sources, a wastewater stream is an affected wastewater stream if the annual average concentration and annual load exceed any of the criteria specified in paragraph (a)(1)(i)(A) through (C) of this section. At new sources, a wastewater stream is subject to additional control requirements if the annual average concentration and annual load exceed the criteria specified in paragraphs (a)(1)(ii)(D) of this section. The owner or operator shall comply with the provisions of §63.1257(e)(1) to determine the annual average concentrations and annual load of partially soluble and soluble HAP compounds.
(A) The wastewater stream contains partially soluble HAP compounds at an annual average concentration greater than 1,300 ppmw, and the total soluble and partially soluble HAP load in all wastewater from the PMPU exceeds 1 Mg/yr.

(B) The wastewater stream contains partially soluble and/or soluble HAP compounds at an annual average concentration of 5,200 ppmw, and the total soluble and partially soluble HAP load in all wastewater from the PMPU exceeds 1 Mg/yr.

(C) The wastewater stream contains partially soluble and/or soluble HAP at an annual average concentration of greater than 10,000 ppmw, and the total partially soluble and/or soluble HAP load in all wastewater from the affected source is greater than 1 Mg/yr.

(D) The wastewater stream contains soluble HAP compounds at an annual average concentration greater than 110,000 ppmw, and the total soluble and partially soluble HAP load in all wastewater from the PMPU exceeds 1 Mg/yr.

(ii) Designate wastewater as affected wastewater. For existing sources, the owner or operator may elect to designate wastewater streams as meeting the criteria of either paragraphs (a)(1)(i)(A), (B), or (C) of this section. For new sources, the owner or operator may elect to designate wastewater streams meeting the criterion in paragraph (a)(1)(i)(D) or for wastewater known to contain no soluble HAP, as meeting the criterion in paragraph (a)(1)(i)(A) of this section. For designated wastewater the procedures specified in paragraphs (a)(1)(i)(A) and (B) of this section shall be followed, except as specified in paragraphs (g)(8)(i), (g)(9)(i), and (g)(10) of this section. The owner or operator shall comply with all applicable emission suppression requirements specified in paragraphs (b) through (f) of this section.

(B) From the location where the owner or operator designates a wastewater stream as an affected wastewater stream, such wastewater stream shall be managed in accordance with all applicable emission suppression requirements specified in paragraphs (b) through (f) of this section and with the treatment requirements in paragraph (g) of this section.

(iii) Scrubber Effluent. Effluent from a water scrubber that has been used to control Table 2 HAP-containing vent streams that are controlled in order to meet the process vent requirements in §63.1254 of this subpart is considered an affected wastewater stream.

(2) Requirements for affected wastewater. (i) An owner or operator of a facility shall comply with the applicable requirements for wastewater tanks, surface impoundments, containers, individual drain systems, and oil/water separators as specified in paragraphs (b) through (f) of this section, except as provided in paragraph (g)(3) of this section.

(ii) Comply with the applicable requirements for control of soluble and partially soluble compounds as specified in paragraph (g) of this section. Alternatively, the owner or operator may elect to comply with the treatment provisions specified in paragraph (a)(5) of this section.

(iii) Comply with the applicable monitoring and inspection requirements specified in §63.1258.

(iv) Comply with the applicable recordkeeping and reporting requirements specified in §§63.1259 and 63.1260.

(3) Exempt wastewater. The following wastewaters are not subject to the wastewater provisions of this part:

(i) Stormwater from segregated sewers;

(ii) Water from fire-fighting and deluge systems, including testing of such systems;

(iii) Spills; and

(iv) Water from safety showers.

(4) Requirements for multiphase discharges. The owner or operator shall not discharge a separate phase that can be isolated through gravity separation from the aqueous phase to a waste management or treatment unit, unless
the stream is discharged to a treatment unit in compliance with paragraph (g)(13) of this section.

(5) Offsite treatment or onsite treatment not owned or operated by the source. The owner or operator may elect to transfer affected wastewater streams that contain less than 50 ppmw of partially soluble HAP or a residual removed from such affected wastewater to an onsite treatment operation not owned or operated by the owner or operator of the source generating the wastewater or residual, or to an offsite treatment operation, provided that the waste management units up to the activated sludge unit are covered or the owner or operator demonstrates that less than 5 percent of the total soluble HAP is emitted from the these units.

(i) The owner or operator transferring the wastewater or residual shall:

(A) Comply with the provisions specified in paragraphs (b) through (f) of this section for each waste management unit that receives or manages affected wastewater or a residual removed from affected wastewater prior to shipment or transport.

(B) Include a notice with each shipment or transport of affected wastewater or residual removed from affected wastewater. The notice shall state that the affected wastewater or residual contains organic HAP that are to be treated in accordance with the provisions of this subpart. When the transport is continuous or ongoing (for example, discharge to a publicly-owned treatment works), the notice shall be submitted to the treatment operator initially and whenever there is a change in the required treatment. The owner or operator shall keep a record of the notice in accordance with §63.1259(g).

(ii) The owner or operator may not transfer the affected wastewater or residual unless the transferee has submitted to the EPA a written certification that the transferee will manage and treat any affected wastewater or residual removed from affected wastewater received from a source subject to the requirements of this subpart in accordance with the requirements of either:

(A) Paragraphs (b) through (i) of this section; or

(B) Subpart D of this part if alternative emission limitations have been granted the transferor in accordance with those provisions; or

(C) Section 63.6(g).

(iii) The certifying entity may revoke the written certification by sending a written statement to the EPA and the owner or operator giving at least 90 days notice that the certifying entity is rescinding acceptance of responsibility for compliance with the regulatory provisions listed in this paragraph. Upon expiration of the notice period, the owner or operator may not transfer the wastewater stream or residual to the treatment operation.

(iv) By providing this written certification to the EPA, the certifying entity accepts responsibility for compliance with the regulatory provisions listed in paragraph (a)(5)(ii) of this section with respect to any shipment of wastewater or residual covered by the written certification. Failure to abide by any of those provisions with respect to such shipments may result in enforcement action by the EPA against the certifying entity in accordance with the enforcement provisions applicable to violations of these provisions by owners or operators of sources.

(v) Written certifications and revocation statements, to the EPA from the transferees of wastewater or residuals shall be signed by the responsible official of the certifying entity, provide the name and address of the certifying entity, and be sent to the appropriate EPA Regional Office at the addresses listed in §63.13. Such written certifications are not transferable by the treater.

(b) Wastewater tanks. For each wastewater tank that receives, manages, or treats affected wastewater or a residual removed from affected wastewater, the owner or operator shall comply with the requirements of either paragraph (b)(1) or (2) of this section as specified in Table 6 of this subpart.

(1) The owner or operator shall operate and maintain a fixed roof except when the contents of the wastewater tank are heated, treated by means of an exothermic reaction, or sparged, during which time the owner or operator shall comply with the requirements specified in paragraph (b)(2) of
this section. For the purposes of this paragraph, the requirements of paragraph (b)(2) of this section are satisfied by operating and maintaining a fixed roof if the owner or operator demonstrates that the total soluble and partially soluble HAP emissions from the wastewater tank are no more than 5 percent higher than the emissions would be if the contents of the wastewater tank were not heated, treated by an exothermic reaction, or sparged.

(2) The owner or operator shall comply with the requirements in paragraphs (b)(3) through (9) of this section and shall operate and maintain one of the emission control techniques listed in paragraphs (b)(2)(i) through (iii) of this section.

(i) A fixed roof and a closed-vent system that routes the organic HAP vapors vented from the wastewater tank to a control device; or

(ii) A fixed roof and an internal floating roof that meets the requirements specified in §63.119(b), with the differences noted in §63.1257(c)(3)(i) through (iii) for the purposes of this subpart; or

(iii) An external floating roof that meets the requirements specified in §§63.119(c), 63.120(b)(5), and 63.120(b)(6), with the differences noted in §63.1257(c)(3)(i) through (v) for the purposes of this subpart.

(3) If the owner or operator elects to comply with the requirements of paragraph (b)(2)(i) of this section, the fixed roof shall meet the requirements of paragraph (b)(3)(i) of this section, the control device shall meet the requirements of paragraph (b)(3)(ii) of this section, and the closed-vent system shall meet the requirements of paragraph (b)(3)(iii) of this section.

(i) The fixed roof shall meet the following requirements:

(A) Except as provided in paragraph (b)(3)(iv) of this section, the fixed roof and all openings (e.g., access hatches, sampling ports, and gauge wells) shall be maintained in accordance with the requirements specified in §63.1258(h).

(B) Each opening shall be maintained in a closed position (e.g., covered by a lid) at all times that the wastewater tank contains affected wastewater or residual removed from affected wastewater except when it is necessary to use the opening for wastewater sampling, removal, or for equipment inspection, maintenance, or repair.

(ii) The control device shall be designed, operated, and inspected in accordance with the requirements of paragraph (h) of this section.

(iii) Except as provided in paragraph (b)(3)(iv) of this section, the closed-vent system shall be inspected in accordance with the requirements of §63.1258(h).

(iv) For any fixed roof tank and closed-vent system that is operated and maintained under negative pressure, the owner or operator is not required to comply with the requirements specified in §63.1258(h).

(4) If the owner or operator elects to comply with the requirements of paragraph (b)(2)(ii) of this section, the floating roof shall be inspected according to the procedures specified in §63.120(a)(2) and (3), with the differences noted in §63.1257(c)(3)(iv) for the purposes of this subpart.

(5) Except as provided in paragraph (b)(6) of this section, if the owner or operator elects to comply with the requirements of paragraph (b)(2)(iii) of this section, seal gaps shall be measured according to the procedures specified in §63.120(b)(2)(i) through (b)(4) and the wastewater tank shall be inspected to determine compliance with §63.120(b)(5) and (6) according to the schedule specified in §63.120(b)(1)(i) through (iii).

(6) If the owner or operator determines that it is unsafe to perform the seal gap measurements specified in §63.120(b)(2)(i) through (b)(4) or to inspect the wastewater tank to determine compliance with §63.120(b)(5) and (6) because the floating roof appears to be structurally unsound and poses an imminent or potential danger to inspecting personnel, the owner or operator shall comply with the requirements in either paragraph (b)(6)(i) or (ii) of this section.

(i) The owner or operator shall empty and remove the wastewater tank from service within 45 calendar days of determining that the roof is unsafe. If the wastewater tank cannot be emptied within 45 calendar days, the owner or operator may utilize up to two extensions of up to 30 additional
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calendar days each. Documentation of a decision to utilize an extension shall include an explanation of why it was unsafe to perform the inspection or seal gap measurement, shall document that alternate storage capacity is unavailable, and shall specify a schedule of actions that will ensure that the wastewater tank will be emptied as soon as possible.

(7) Except as provided in paragraph (b)(6) of this section, each wastewater tank shall be inspected initially, and semiannually thereafter, for improper work practices in accordance with §63.1258(g). For wastewater tanks, improper work practice includes, but is not limited to, leaving open any access door or other opening when such door or opening is not in use.

(8) Except as provided in paragraph (b)(6) of this section, each wastewater tank shall be inspected for control equipment failures as defined in paragraph (b)(8)(i) of this section according to the schedule in paragraphs (b)(8)(ii) through (H) according to the schedule specified in paragraphs (b)(4) and (5) of this section.

(i) Control equipment failures for wastewater tanks include, but are not limited to, the conditions specified in paragraphs (b)(8)(i)(A) through (H) of this section.

(A) The floating roof is not resting on either the surface of the liquid or on the leg supports.

(B) There is stored liquid on the floating roof.

(C) A rim seal is detached from the floating roof.

(D) There are holes, tears, cracks or gaps in the rim seal or seal fabric of the floating roof.

(E) There are visible gaps between the seal of an internal floating roof and the wall of the wastewater tank.

(F) There are gaps between the metallic shoe seal or the liquid mounted primary seal of an external floating roof and the wall of the wastewater tank that exceed 21.2 square centimeters per meter of tank diameter or the width of any portion of any gap between the primary seal and the tank wall exceeds 1.27 centimeters.

(H) Where a metallic shoe seal is used on an external floating roof, one end of the metallic shoe does not extend into the stored liquid or one end of the metallic shoe does not extend a minimum vertical distance of 61 centimeters above the surface of the stored liquid.

(ii) The owner or operator shall inspect for the control equipment failures in paragraphs (b)(8)(i)(A) through (H) according to the schedule specified in paragraphs (b)(4) and (5) of this section.

(iii) The owner or operator shall inspect for the control equipment failures in paragraph (b)(8)(i)(I) of this section initially, and semiannually thereafter.

(9) Except as provided in paragraph (i) of this section, when an improper work practice or a control equipment failure is identified, first efforts at repair shall be made no later than 5 calendar days after identification and repair shall be completed within 45 calendar days after identification. If a failure that is detected during inspections required by this section cannot be repaired within 45 calendar days and if the tank cannot be emptied within 45 calendar days, the owner or operator may utilize up to two extensions of up to 30 additional calendar days each. Documentation of a decision to utilize an extension shall include a description of the failure, shall document that alternate storage capacity is unavailable, and shall specify a schedule of actions that will ensure that the control equipment will be repaired or the tank will be emptied as soon as practical.

(c) Surface impoundments. For each surface impoundment that receives, manages, or treats affected wastewater or a residual removed from affected wastewater, the owner or operator shall comply with the requirements of paragraphs (c)(1), (2), and (3) of this section.

(1) The owner or operator shall operate and maintain on each surface impoundment either a cover (e.g., air-supported structure or rigid cover) and a
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closed-vent system that routes the organic hazardous air pollutants vapors vented from the surface impoundment to a control device in accordance with paragraphs (c)(1)(i), (iii), (iv), and (v) of this section, or a floating flexible membrane cover as specified in paragraph (c)(1)(ii) of this section.

(i) The cover and all openings shall meet the following requirements:

(A) Except as provided in paragraph (c)(1)(iv) of this section, the cover and all openings (e.g., access hatches, sampling ports, and gauge wells) shall be maintained in accordance with the requirements specified in § 63.1258(h).

(B) Each opening shall be maintained in a closed position (e.g., covered by a lid) at all times that affected wastewater or residual removed from affected wastewater is in the surface impoundment except when it is necessary to use the opening for sampling, removal, or for equipment inspection, maintenance, or repair.

(C) The cover shall be used at all times that affected wastewater or residual removed from affected wastewater is in the surface impoundment except during removal of treatment residuals in accordance with 40 CFR 268.4 or closure of the surface impoundment in accordance with 40 CFR 264.228.

(ii) Floating flexible membrane covers shall meet the requirements specified in paragraphs (c)(1)(ii)(A) through (F) of this section.

(A) The floating flexible cover shall be designed to float on the liquid surface during normal operations, and to form a continuous barrier over the entire surface area of the liquid.

(B) The cover shall be fabricated from a synthetic membrane material that is either:

(1) High density polyethylene (HDPE) with a thickness no less than 2.5 millimeters (100 mils); or

(2) A material or a composite of different materials determined to have both organic permeability properties that are equivalent to those of the material listed in paragraph (c)(1)(ii)(B)(1) of this section, and chemical and physical properties that maintain the material integrity for the intended service life of the material.

(C) The cover shall be installed in a manner such that there are no visible cracks, holes, gaps, or other open spaces between cover section seams or between the interface of the cover edge and its foundation mountings.

(D) Except as provided for in paragraph (c)(1)(ii)(E) of this section, each opening in the floating membrane cover shall be equipped with a closure device designed to operate such that when the closure device is secured in the closed position there are no visible cracks, holes, gaps, or other open spaces in the closure device or between the perimeter of the cover opening and the closure device.

(E) The floating membrane cover may be equipped with one or more emergency cover drains for removal of stormwater. Each emergency cover drain shall be equipped with a slotted membrane fabric cover that covers at least 90 percent of the area of the opening or a flexible fabric sleeve seal.

(F) The closure devices shall be made of suitable materials that will minimize exposure of organic HAP to the atmosphere, to the extent practical, and will maintain the integrity of the equipment throughout its intended service life. Factors to be considered in designing the closure devices shall include: the effects of any contact with the liquid and its vapor managed in the surface impoundment; the effects of outdoor exposure to wind, moisture, and sunlight; and the operating practices used for the surface impoundment on which the floating membrane cover is installed.

(G) Whenever affected wastewater or residual from affected wastewater is in the surface impoundment, the floating membrane cover shall float on the liquid and each closure device shall be secured in the closed position. Opening of closure devices or removal of the cover is allowed to provide access to the surface impoundment for performing routine inspection, maintenance, or other activities needed for normal operations and/or to remove accumulated sludge or other residues from the bottom of the surface impoundment. Openings shall be maintained in accordance with § 63.1258(h).

(iii) The control device shall be designed, operated, and inspected in accordance with paragraph (h) of this section.
(iv) Except as provided in paragraph (c)(1)(v) of this section, the closed-vent system shall be inspected in accordance with §63.1258(h).

(v) For any cover and closed-vent system that is operated and maintained under negative pressure, the owner or operator is not required to comply with the requirements specified in §63.1258(h).

(2) Each surface impoundment shall be inspected initially, and semiannually thereafter, for improper work practices and control equipment failures in accordance with §63.1258(g).

(i) For surface impoundments, improper work practice includes, but is not limited to, leaving open any access hatch or other opening when such hatch or opening is not in use.

(ii) For surface impoundments, control equipment failure includes, but is not limited to, any time a joint, lid, cover, or door has a crack or gap, or is broken.

(3) Except as provided in paragraph (i) of this section, when an improper work practice or a control equipment failure is identified, first efforts at repair shall be made no later than 5 calendar days after identification and repair shall be completed within 45 calendar days after identification.

(d) Containers. For each container that receives, manages, or treats affected wastewater or a residual removed from affected wastewater, the owner or operator shall comply with the requirements of paragraphs (d)(1) through (5) of this section.

(1) The owner or operator shall operate and maintain a cover on each container used to handle, transfer, or store affected wastewater or a residual removed from affected wastewater, the cover and all openings (e.g., bungs, hatches, sampling ports, and pressure relief devices) shall be maintained in accordance with the following requirements:

(i) Except as provided in paragraph (d)(3)(iv) of this section, if the capacity of the container is greater than 0.42 m$^3$, the cover and all openings (e.g., bungs, hatches, sampling ports, and pressure relief devices) shall be maintained in accordance with the requirements specified in §63.1258(h).

(ii) If the capacity of the container is less than or equal to 0.42 m$^3$, the owner or operator shall comply with either paragraph (d)(1)(ii)(A) or (B) of this section.

(A) The container must meet existing Department of Transportation specifications and testing requirements under 49 CFR part 178.

(B) Except as provided in paragraph (d)(3)(iv) of this section, the cover and all openings shall be maintained without leaks as specified in §63.1258(h).

(iii) The cover and all openings shall be maintained in a closed position (e.g., covered by a lid) at all times that affected wastewater or a residual removed from affected wastewater is in the container except when it is necessary to use the opening for filling, removal, inspection, sampling, or pressure relief events related to safety considerations.

(ii) For containers with a capacity greater than or equal to 0.42 m$^3$, either a submerged fill pipe shall be used when a container is being filled by pumping with affected wastewater or a residual removed from affected wastewater or the container shall be located within an enclosure with a closed-vent system that routes the organic HAP vapors vented from the container to a control device.

(i) The submerged fill pipe outlet shall extend to no more than 6 inches or within two fill pipe diameters of the bottom of the container while the container is being filled.

(ii) The cover shall remain in place and all openings shall be maintained in a closed position except for those openings required for the submerged fill pipe and for venting of the container to prevent physical damage or permanent deformation of the container or cover.

(3) During treatment of affected wastewater or a residual removed from affected wastewater, including aeration, thermal or other treatment, in a container, whenever it is necessary for the container to be open, the container shall be located within an enclosure with a closed-vent system that routes the organic HAP vapors vented from the container to a control device.

(i) Except as provided in paragraph (d)(3)(iv) of this section, the enclosure and all openings (e.g., doors, hatches) shall be maintained in accordance with the requirements specified in §63.1258(h).
(ii) The control device shall be designed, operated, and inspected in accordance with paragraph (h) of this section.

(iii) Except as provided in paragraph (d)(3)(iv) of this section, the closed-vent system shall be inspected in accordance with §63.1258(h).

(iv) For any enclosure and closed-vent system that is operated and maintained under negative pressure, the owner or operator is not required to comply with the requirements specified in §63.1258(h).

(4) Each container shall be inspected initially, and semiannually thereafter, for improper work practices and control equipment failures in accordance with §63.1258(g).

(i) For containers, improper work practice includes, but is not limited to, leaving open any access hatch or other opening when such hatch or opening is not in use.

(ii) For containers, control equipment failure includes, but is not limited to, a gap or crack, or is broken.

(5) Except as provided in paragraph (i) of this section, when an improper work practice or a control equipment failure is identified, first efforts at repair shall be made no later than 5 calendar days after identification and repair shall be completed within 15 calendar days after identification.

(e) Individual drain systems. For each individual drain system that receives or manages affected wastewater or a residual removed from affected wastewater, the owner or operator shall comply with the requirements of paragraphs (e)(1), (2), and (3) or with paragraphs (e)(4), (5), and (6) of this section:

(1) If the owner or operator elects to comply with this paragraph, the owner or operator shall operate and maintain on each opening in the individual drain system a cover and if vented, route the vapors to a process or through a closed-vent system to a control device. The owner or operator shall comply with the requirements of paragraphs (e)(1)(i) through (v) of this section.

(i) The cover and all openings shall meet the following requirements:

(A) Except as provided in paragraph (e)(1)(iv) of this section, the cover and all openings (e.g., access hatches, sampling ports) shall be maintained in accordance with the requirements specified in §63.1258(h).

(B) The cover and all openings shall be maintained in a closed position at all times that affected wastewater or a residual removed from affected wastewater is in the drain system except when it is necessary to use the opening for sampling or removal, or for equipment inspection, maintenance, or repair.

(ii) The control device shall be designed, operated, and inspected in accordance with paragraph (h) of this section.

(iii) Except as provided in paragraph (e)(1)(iv) of this section, the closed-vent system shall be inspected in accordance with §63.1258(h).

(iv) For any cover and closed-vent system that is operated and maintained under negative pressure, the owner or operator is not required to comply with the requirements specified in §63.1258(h).

(v) The individual drain system shall be designed and operated to segregate the vapors within the system from other drain systems and the atmosphere.

(2) Each individual drain system shall be inspected initially, and semiannually thereafter, for improper work practices and control equipment failures, in accordance with §63.1258(g).

(i) For individual drain systems, improper work practice includes, but is not limited to, leaving open any access hatch or other opening when such hatch or opening is not in use for sampling or removal, or for equipment inspection, maintenance, or repair.

(ii) For individual drain systems, control equipment failure includes, but is not limited to, a joint, lid, cover, or door has a gap or crack, or is broken.

(3) Except as provided in paragraph (i) of this section, when an improper work practice or a control equipment failure is identified, first efforts at repair shall be made no later than 5 calendar days after identification and repair shall be completed within 15 calendar days after identification.

(4) If the owner or operator elects to comply with this paragraph, the owner
or operator shall comply with the requirements in paragraphs (e)(4)(i) through (iii) of this section:

(i) Each drain shall be equipped with water seal controls or a tightly fitting cap or plug. The owner or operator shall comply with paragraphs (e)(4)(i)(A) and (B) of this section.

(A) For each drain equipped with a water seal, the owner or operator shall ensure that the water seal is maintained. For example, a flow-monitoring device indicating positive flow from a main to a branch water line supplying a trap or water being continuously dripped into the trap by a hose could be used to verify flow of water to the trap. Visual observation is also an acceptable alternative.

(B) If a water seal is used on a drain receiving affected wastewater, the owner or operator shall either extend the pipe discharging the wastewater below the liquid surface in the water seal of the receiving drain, or install a flexible shield (or other enclosure which restricts wind motion across the open area between the pipe and the drain) that encloses the space between the pipe discharging the wastewater to the drain receiving the wastewater. (Water seals which are used on hubs receiving wastewater that is not subject to the provisions of this subpart for the purpose of eliminating cross ventilation to drains carrying affected wastewater are not required to have a flexible cap or extended subsurface discharging pipe.)

(ii) Each junction box shall be equipped with a tightly fitting solid cover (i.e., no visible gaps, cracks, or holes) which shall be kept in place at all times except during inspection and maintenance. If the junction box is vented, the owner or operator shall comply with the requirements in paragraph (e)(4)(ii)(A) or (B) of this section.

(A) The junction box shall be vented to a process or through a closed-vent system to a control device. The closed-vent system shall be inspected in accordance with the requirements of §63.1258(h) and the control device shall be designed, operated, and inspected in accordance with the requirements of paragraph (h) of this section.

(B) If the junction box is filled and emptied by gravity flow (i.e., there is no pump) or is operated with no more than slight fluctuations in the liquid level, the owner or operator may vent the junction box to the atmosphere provided that the junction box complies with the requirements in paragraphs (e)(4)(ii)(B) (1) and (2) of this section.

(1) The vent pipe shall be at least 90 centimeters in length and no greater than 10.2 centimeters in nominal inside diameter.

(2) Water seals shall be installed and maintained at the wastewater entrance(s) to or exit from the junction box restricting ventilation in the individual drain system and between components in the individual drain system. The owner or operator shall demonstrate (e.g., by visual inspection or smoke test) upon request by the Administrator that the junction box water seal is properly designed and restricts ventilation.

(iii) Each sewer line shall not be open to the atmosphere and shall be covered or enclosed in a manner so as to have no visible gaps or cracks in joints, seals, or other emission interfaces. (Note: This provision applies to sewers located inside and outside of buildings.)

(5) Equipment used to comply with paragraphs (e)(4)(i), (ii), or (iii) of this section shall be inspected as follows:

(i) Each drain using a tightly fitting cap or plug shall be visually inspected initially, and semiannually thereafter, to ensure caps or plugs are in place and that there are no gaps, cracks, or other holes in the cap or plug.

(ii) Each junction box shall be visually inspected initially, and semiannually thereafter, to ensure that there are no gaps, cracks, or other holes in the cover.

(iii) The unburied portion of each sewer line shall be visually inspected initially, and semiannually thereafter, for indication of cracks or gaps that could result in air emissions.

(6) Except as provided in paragraph (i) of this section, when a gap, hole, or crack is identified in a joint or cover, first efforts at repair shall be made no later than 5 calendar days after identification, and repair shall be completed
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within 15 calendar days after identification.

(f) Oil-water separators. For each oil-water separator that receives, manages, or treats affected wastewater or a residual removed from affected wastewater, the owner or operator shall comply with the requirements of paragraphs (f)(1) through (6) of this section.

(1) The owner or operator shall maintain one of the following:

(i) A fixed roof and a closed-vent system that routes the organic HAP vapors vented from the oil-water separator to a control device. The fixed roof, closed-vent system, and control device shall meet the requirements specified in paragraph (f)(2) of this section;

(ii) A floating roof that meets the requirements in 40 CFR 60.693-2(a)(1)(i), (a)(1)(ii), (a)(2), (a)(3), and (a)(4). For portions of the oil-water separator where it is infeasible to construct and operate a floating roof, such as over the weir mechanism, the owner or operator shall operate and maintain a fixed roof, closed-vent system, and control device that meet the requirements specified in paragraph (f)(2) of this section.

(2) A fixed roof shall meet the requirements of paragraph (f)(2)(i) of this section, a control device shall meet the requirements of paragraph (f)(2)(ii) of this section, and a closed-vent system shall meet the requirements of (f)(2)(iii) of this section.

(i) The fixed roof shall meet the following requirements:

(A) Except as provided in (f)(2)(iv) of this section, the fixed roof and all openings (e.g., access hatches, sampling ports, and gauge wells) shall be maintained in accordance with the requirements specified in §63.1258(h).

(B) Each opening shall be maintained in a closed, sealed position (e.g., covered by a lid that is gasketed and latched) at all times that the oil-water separator contains affected wastewater or a residual removed from affected wastewater except when it is necessary to use the opening for sampling or removal, or for equipment inspection, maintenance, or repair.

(ii) The control device shall be designed, operated, and inspected in accordance with the requirements of paragraph (h) of this section.

(iii) Except as provided in paragraph (f)(2)(iv) of this section, the closed-vent system shall be inspected in accordance with the requirements of §63.1258(h).

(iv) For any fixed-roof and closed-vent system that is operated and maintained under negative pressure, the owner or operator is not required to comply with the requirements of §63.1258(h).

(3) If the owner or operator elects to comply with the requirements of paragraph (f)(1)(ii) of this section, seal gaps shall be measured according to the procedures specified in 40 CFR part 60, subpart QQQ §60.696(d)(1) and the schedule specified in paragraphs (f)(3)(i) and (ii) of this section.

(i) Measurement of primary seal gaps shall be performed within 60 calendar days after installation of the floating roof and introduction of affected wastewater or a residual removed from affected wastewater and once every 5 years thereafter.

(ii) Measurement of secondary seal gaps shall be performed within 60 calendar days after installation of the floating roof and introduction of affected wastewater or a residual removed from affected wastewater and once every year thereafter.

(4) Each oil-water separator shall be inspected initially, and semiannually thereafter, for improper work practices in accordance with §63.1258(g). For oil-water separators, improper work practice includes, but is not limited to, leaving open or ungasketed any access door or other opening when such door or opening is not in use.

(5) Each oil-water separator shall be inspected for control equipment failures as defined in paragraph (f)(5)(i) of this section according to the schedule specified in paragraphs (f)(5)(ii) and (iii) of this section.

(i) For oil-water separators, control equipment failure includes, but is not limited to, the conditions specified in paragraphs (f)(5)(i)(A) through (G) of this section.

(A) The floating roof is not resting on either the surface of the liquid or on the leg supports.
(B) There is stored liquid on the floating roof.

(C) A rim seal is detached from the floating roof.

(D) There are holes, tears, or other open spaces in the rim seal or seal fabric of the floating roof.

(E) There are gaps between the primary seal and the separator wall that exceed 67 square centimeters per meter of separator wall perimeter or the width of any portion of any gap between the primary seal and the separator wall exceeds 3.8 centimeters.

(F) There are gaps between the secondary seal and the separator wall that exceed 6.7 square centimeters per meter of separator wall perimeter or the width of any portion of any gap between the secondary seal and the separator wall exceeds 1.3 centimeters.

(G) A gasket, joint, lid, cover, or door has a gap or crack, or is broken.

(ii) The owner or operator shall inspect for the control equipment failures in paragraphs (f)(5)(i)(A) through (F) according to the schedule specified in paragraph (f)(3) of this section.

(iii) The owner or operator shall inspect for control equipment failures in paragraph (f)(5)(i)(G) of this section initially, and semiannually thereafter.

(6) Except as provided in paragraph (i) of this section, when an improper work practice or a control equipment failure is identified, first efforts at repair shall be made no later than 5 calendar days after identification and repair shall be completed within 45 calendar days after identification.

(g) Performance standards for treatment processes managing wastewater and/or residuals removed from wastewater. This section specifies the performance standards for treating affected wastewater. The owner or operator shall comply with the requirements as specified in paragraphs (g)(1) through (6) of this section. Where multiple compliance options are provided, the options may be used in combination for different wastewater and/or for different compounds (e.g., soluble versus partially soluble compounds) in the same wastewater, except where otherwise provided in this section. Once affected wastewater or a residual removed from affected wastewater has been treated in accordance with this subpart, it is no longer subject to the requirements of this subpart.

(1) Existing source. For a wastewater stream at an existing source that exceeds or is designated to exceed the concentration and load criteria in paragraph (a)(1)(i)(A) of this section, the owner or operator shall comply with a control option in paragraph (g)(8) of this section. For a wastewater stream at an existing source that exceeds the concentration and load criteria in either paragraph (a)(1)(i)(B) or (C) of this section, the owner or operator shall comply with a control option in paragraph (g)(8) of this section and a control option in paragraph (g)(9) of this section. As an alternative to the control options in paragraphs (g)(8) and (g)(9) of this section, the owner or operator may comply with a control option in either paragraph (g)(10), (11) or (13) of this section, as applicable.

(2) New source. For a wastewater stream at a new source that exceeds or is designated to exceed the concentration and load criteria in paragraph (a)(1)(i)(A) of this section, the owner or operator shall comply with a control option in paragraph (g)(8) of this section. For wastewater at a new source that exceeds the concentration and load criteria in either paragraph (a)(1)(i)(B) or (C) of this section, but does not exceed the criteria in paragraph (a)(1)(i)(D) of this section, the owner or operator shall comply with a control option in paragraph (g)(8) of this section and a control option in paragraph (g)(9) of this section. As an alternative to the control options in paragraphs (g)(8) and/or (9) of this section, the owner or operator may comply with a control option in either paragraph (g)(10), (11), or (13) of this section, as applicable. For a wastewater stream at a new source that exceeds or is designated to exceed the concentration and load criteria in paragraph (a)(1)(i)(D) of this section, the owner or operator shall comply with a control option in paragraph (g)(12) or (13) of this section.

(3) Biological treatment processes. Biological treatment processes in compliance with this section may be either open or closed biological treatment processes as defined in §63.1251. An open biological treatment process in
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compliance with this section need not be covered and vented to a control device. An open or a closed biological treatment process in compliance with this section and using § 63.1257(e)(2)(iii)(E) or (F) to demonstrate compliance is not subject to the requirements of paragraphs (b) and (c) of this section. A closed biological treatment process in compliance with this section and using § 63.1257(e)(2)(iii)(G) to demonstrate compliance shall comply with the requirements of paragraphs (b) and (c) of this section. Waste management units upstream of an open or closed biological treatment process shall meet the requirements of paragraphs (b) through (f) of this section, as applicable.

(4) Performance tests and design evaluations. If the Resource Conservation and Recovery Act (RCRA) option [paragraph (g)(13) of this section] or the enhanced biological treatment process for soluble HAP compounds option [paragraph (g)(10) of this section] is selected to comply with this section, neither a design evaluation nor a performance test is required. For any other nonbiological treatment process, and for closed biological treatment processes as defined in § 63.1251, the owner or operator shall conduct either a design evaluation as specified in § 63.1257(e)(2)(ii) or performance test as specified in § 63.1257(e)(2)(iii). For each open biological treatment process as defined in § 63.1251, the owner or operator shall conduct a performance test as specified in § 63.1257(e)(2)(iii)(E) or (F).

(5) Control device requirements. When gases are vented from the treatment process, the owner or operator shall comply with the applicable control device requirements specified in paragraph (h) of this section and § 63.1257(e)(3), and the applicable leak inspection provisions specified in § 63.1258(h). This requirement is in addition to the requirements for treatment systems specified in paragraphs (g)(8) through (14) of this section. This requirement does not apply to any open biological treatment process that meets the mass removal requirements.

(6) Residuals: general. When residuals result from treating affected wastewater, the owner or operator shall comply with the requirements for residuals specified in paragraph (g)(14) of this section.

(7) Treatment using a series of treatment processes. In all cases where the wastewater provisions in this subpart allow or require the use of a treatment process or control device to comply with emissions limitations, the owner or operator may use multiple treatment processes or control devices, respectively. For combinations of treatment processes where the wastewater stream is conveyed by hard-piping, the owner or operator shall comply with either the requirements of paragraph (g)(7)(ii) or (ii) of this section. For combinations of treatment processes where the wastewater stream is not conveyed by hard-piping, the owner or operator shall comply with the requirements of paragraph (g)(7)(ii) of this section. For combinations of control devices, the owner or operator shall comply with the requirements of paragraph (g)(7)(i) of this section.

(i) Compliance across the combination of all treatment units or control devices in series. (A) For combinations of treatment processes, the wastewater stream shall be conveyed by hard-piping between the treatment processes. For combinations of control devices, the vented gas stream shall be conveyed by hard-piping between the control devices.

(B) For combinations of treatment processes, each treatment process shall meet the applicable requirements of paragraphs (b) through (f) of this section, except as provided in paragraph (g)(3) of this section.

(C) The owner or operator shall identify, and keep a record of, the combination of treatment processes or of control devices, including identification of the first and last treatment process or control device. The owner or operator shall include this information as part of the treatment process description reported in the Notification of Compliance Status.

(D) The performance test or design evaluation shall determine compliance across the combination of treatment processes or control devices. If a performance test is conducted, the “inlet” shall be the point at which the wastewater stream or residual enters the
first treatment process, or the vented gas stream enters the first control device. The “outlet” shall be the point at which the treated wastewater stream exits the last treatment process, or the vented gas stream exits the last control device.

(ii) Compliance across individual units. 
(A) For combinations of treatment processes, each treatment process shall meet the applicable requirements of paragraphs (b) through (f) of this section except as provided in paragraph (g)(3) of this section.
(B) The owner or operator shall identify, and keep a record of, the combination of treatment processes, including identification of the first and last treatment process. The owner or operator shall include this information as part of the treatment process description reported in the Notification of Compliance Status report.
(C) The owner or operator shall determine the mass removed or destroyed by each treatment process. The performance test or design evaluation shall determine compliance for the combination of treatment processes by adding together the mass removed or destroyed by each treatment process and determine the overall control efficiency of the treatment system.

(b) Control options: Wastewater containing partially soluble HAP compounds. The owner or operator shall comply with either paragraph (g)(9)(i) or (ii) of this section for the control of partially soluble HAP compounds at new or existing sources.

(i) 50 ppmw concentration option. The owner or operator shall comply with paragraphs (g)(9)(i)(A) and (B) of this section.
(A) Reduce, by removal or destruction, the concentration of total partially soluble HAP compounds to a level less than 50 ppmw as determined by the procedures specified in §63.1257(e)(2)(iii)(B).
(B) This option shall not be used when the treatment process is a biological treatment process. This option shall not be used when the wastewater is designated as an affected wastewater as specified in paragraph (a)(1)(ii) of this section. Dilution shall not be used to achieve compliance with this option.

(ii) Percent mass removal/destruction option. The owner or operator shall reduce, by removal or destruction, the mass of total partially soluble HAP compounds by 99 percent or more. The removal/destruction efficiency shall be determined by the procedures specified in §63.1257(e)(2)(iii)(C), for noncombustion, nonbiological treatment processes; §63.1257(e)(2)(iii)(D), for combustion processes; and §63.1257(e)(2)(iii)(F) or (G) for biological treatment processes.

(9) Control options: Wastewater containing soluble HAP compounds. The owner or operator shall comply with either paragraph (g)(9)(i) or (ii) of this section for the control of soluble HAP compounds at new or existing sources.

(i) 520 ppmw concentration option. The owner or operator shall comply with paragraphs (g)(9)(i)(A) and (B) of this section.
(A) Reduce, by removal or destruction, the concentration of total soluble HAP compounds to a level less than 520 ppmw as determined in the procedures specified in §63.1257(e)(2)(iii)(B).
(B) This option shall not be used when the treatment process is a biological treatment process. This option shall not be used when the wastewater is designated as an affected wastewater as specified in paragraph (a)(1)(ii) of this section. Dilution shall not be used to achieve compliance with this option.

(ii) Percent mass removal/destruction option. The owner or operator shall reduce, by removal or destruction, the mass of total soluble HAP by 90 percent or more. The removal/destruction efficiency shall be determined by the procedures in §63.1257(e)(2)(iii)(C), for noncombustion, nonbiological treatment processes; §63.1257(e)(2)(iii)(D), for combustion processes; and §63.1257(e)(2)(iii)(F) or (G) for biological treatment processes.

(10) Control option: Enhanced biotreatment for wastewater containing soluble HAP. The owner or operator may elect to treat affected wastewater streams containing soluble HAP and less than 50 ppmw partially soluble HAP in an enhanced biological treatment system, as defined in §63.1251. This option shall not be used when the wastewater is designated as an affected wastewater as specified in paragraph (a)(1)(ii) of
this section. These treatment processes are exempt from the design evaluation or performance tests requirements specified in paragraph (g)(4) of this section.

(11) 95-percent mass reduction option, for biological treatment processes. The owner or operator of a new or existing source using biological treatment for any affected wastewater shall reduce the mass of total soluble and partially soluble HAP sent to that biological treatment unit by at least 95 percent. All wastewater as defined in §63.1251 entering such a biological treatment unit from PMPU’s subject to this subpart shall be included in the demonstration of the 95-percent mass removal. The owner or operator shall comply with paragraphs (g)(11)(i) through (iv) of this section.

(i) Except as provided in paragraph (g)(11)(iv) of this section, the owner or operator shall ensure that all wastewater from PMPU’s subject to this subpart entering a biological treatment unit are treated to destroy at least 95-percent total mass of all soluble and partially soluble HAP compounds.

(ii) For open biological treatment processes, compliance shall be determined using the procedures specified in §63.1257(e)(2)(iii)(E). For closed aerobic biological treatment processes compliance shall be determined using the procedures specified in §63.1257(e)(2)(iii)(G).

(iii) For each treatment process or waste management unit that receives, manages, or treats wastewater subject to this paragraph, from the POD to the biological treatment unit, the owner or operator shall comply with paragraphs (b) through (f) of this section for control of air emissions. When complying with this paragraph, the term affected wastewater in paragraphs (b) through (f) of this section shall mean all wastewater from PMPU’s, not just affected wastewater.

(iv) If wastewater is in compliance with the requirements in paragraph (g)(8), (9), or (12) of this section before entering the biological treatment unit, the hazardous air pollutants mass of that wastewater is not required to be included in the total mass flow rate entering the biological treatment unit for the purpose of demonstrating compliance.

(12) Percent mass removal/destruction option for soluble HAP compounds at new sources. The owner or operator of a new source shall reduce, by removal or destruction, the mass flow rate of total soluble HAP from affected wastewater by 99 percent or more. The removal/destruction efficiency shall be determined by the procedures in §63.1257(e)(2)(iii)(C), for noncombustion, nonbiological treatment processes; §63.1257(e)(2)(iii)(D), for combustion processes; and §63.1257(e)(2)(iii)(F) or (G) for biological treatment processes.

(13) Treatment in a RCRA unit option. The owner or operator shall treat the affected wastewater or residual in a unit identified in, and complying with, paragraph (g)(13)(i), (ii), (iii) of this section. These units are exempt from the design evaluation or performance tests requirements specified in paragraph (g)(4) of this section and §63.1257(e)(2), and from the monitoring requirements specified in paragraph (a)(2)(iii) of this section, as well as recordkeeping and reporting requirements associated with monitoring and performance tests.

(i) The wastewater or residual is discharged to a hazardous waste incinerator for which the owner or operator has been issued a final permit under 40 CFR part 270 and complies with the requirements of 40 CFR part 264, subpart O, or has certified compliance with the interim status requirements of 40 CFR part 265, subpart O;

(ii) The wastewater or residual is discharged to a process heater or boiler burning hazardous waste for which the owner or operator:

(A) Has been issued a final permit under 40 CFR part 270 and complies with the requirements of 40 CFR part 266, subpart H; or

(B) Has certified compliance with the interim status requirements of 40 CFR part 265, subpart O;

(iii) The wastewater or residual is discharged to an underground injection well for which the owner or operator has been issued a final permit under 40 CFR part 270 or 40 CFR part 144 and other applicable hazardous waste injection well regulations.
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complies with the requirements of 40 CFR part 122. The owner or operator shall comply with all applicable requirements of this subpart prior to the point where the wastewater enters the underground portion of the injection well.

(14) Residuals. For each residual removed from affected wastewater, the owner or operator shall control for air emissions by complying with paragraphs (b) through (f) of this section and by complying with one of the provisions in paragraphs (g)(14)(i) through (iv) of this section.

(i) Recycle the residual to a production process or sell the residual for the purpose of recycling. Once a residual is returned to a production process, the residual is no longer subject to this section.

(ii) Return the residual to the treatment process.

(iii) Treat the residual to destroy the total combined mass flow rate of soluble and/or partially soluble HAP compounds by 99 percent or more, as determined by the procedures specified in §63.1257(e)(2)(iii)(C) or (D).

(iv) Comply with the requirements for RCRA treatment options specified in paragraph (g)(13) of this section.

(h) Control devices. For each control device or combination of control devices used to comply with the provisions in paragraphs (b) through (f) and (g)(5) of this section, the owner or operator shall operate and maintain the control device or combination of control devices in accordance with the requirements of paragraphs (h)(1) through (4) of this section.

(1) Whenever organic HAP emissions are vented to a control device which is used to comply with the provisions of this subpart, such control device shall be operating.

(2) The control device shall be designed and operated in accordance with paragraph (h)(2)(i), (ii), (iii), (iv), or (v) of this section, as demonstrated by the procedures specified in §63.1257(e)(3).

(i) An enclosed combustion device (including but not limited to a vapor incinerator, boiler, or process heater) shall meet the conditions in paragraph (h)(2)(i) (A), (B), or (C) of this section, alone or in combination with other control devices. If a boiler or process heater is used as the control device, then the vent stream shall be introduced into the flame zone of the boiler or process heater.

(A) Reduce the organic HAP emissions vented to the control device by 95 percent by weight or greater;

(B) Achieve an outlet TOC concentration of 20 ppmv on a dry basis corrected to 3 percent oxygen. The owner or operator shall use either Method 18 of 40 CFR part 60, appendix A, or any other method or data that has been validated according to the applicable procedures in Method 301 of appendix A of this part; or

(C) Provide a minimum residence time of 0.5 seconds at a minimum temperature of 760°C.

(ii) A vapor recovery system (including but not limited to a carbon adsorption system or condenser), alone or in combination with other control devices, shall reduce the organic HAP emissions vented to the control device by 95 percent by weight or greater or achieve an outlet TOC concentration of 20 ppmv. The 20 ppmv performance standard is not applicable to compliance with the provisions of paragraphs (c) or (d) of this section.

(iii) A flare shall comply with the requirements of §63.11(b).

(iv) A scrubber, alone or in combination with other control devices, shall reduce the organic HAP emissions in such a manner that 95 weight-percent is either removed, or destroyed by chemical reaction with the scrubbing liquid, or achieve an outlet TOC concentration of 20 ppmv. The 20 ppmv performance standard is not applicable to compliance with the provisions of paragraphs (c) or (d) of this section.

(v) Any other control device used shall, alone or in combination with other control devices, reduce the organic HAP emissions vented to the control device by 95 percent by weight or greater or achieve an outlet TOC concentration of 20 ppmv. The 20 ppmv performance standard is not applicable to compliance with the provisions of paragraphs (c) or (d) of this section.

(3) If the control device is a combustion device, the owner or operator shall comply with the requirements in §63.1252(g) to control halogenated vent streams.
§ 63.1257 Test methods and compliance procedures.

(a) General. Except as specified in paragraph (a)(5) of this section, the procedures specified in paragraphs (c), (d), (e), and (f) of this section are required to demonstrate initial compliance with §§63.1253, 63.1254, 63.1256, and 63.1252(e), respectively. The provisions in paragraphs (a) (2) through (3) apply to performance tests that are specified in paragraphs (c), (d), and (e) of this section. The provisions in paragraph (a)(5) of this section are used to demonstrate initial compliance with the alternative standards specified in §§63.1253(d) and 63.1254(c). The provisions in paragraph (a)(6) of this section are used to comply with the outlet concentration requirements specified in §§63.1253(c), 63.1254 (a)(2)(i) and (a)(3)(ii)(B), 63.1254(b)(i) and 63.1256(h)(2).

(1) Design evaluation. To demonstrate that a control device meets the required control efficiency, a design evaluation must address the composition and organic HAP concentration of the vent stream entering the control device. A design evaluation also must address other vent stream characteristics and control device operating parameters as specified in any one of paragraphs (a)(1)(i) through (vi) of this section, depending on the type of control device that is used. If the vent stream is not the only inlet to the control device, the efficiency demonstration also must consider all other vapors, gases, and liquids, other than fuels, received by the control device.

(i) For an enclosed combustion device used to comply with the provisions of 63.1253 (b)(2) or (c)(2), or 63.1256(h)(2)(i)(C) with a minimum residence time of 0.5 seconds and a minimum temperature of 760°F, the design evaluation must document that these conditions exist.

(ii) For a combustion control device that does not satisfy the criteria in paragraph (a)(1)(i) of this section, the design evaluation must document control efficiency and address the following characteristics, depending on the type of control device:

A) For a thermal vapor incinerator, the design evaluation must consider the autoignition temperature of the organic HAP, must consider the vent stream flow rate, and must establish the design minimum and average temperature in the combustion zone.

B) For a catalytic vapor incinerator, the design evaluation shall consider the vent stream flow rate and shall establish the design minimum and average temperatures across the catalyst bed inlet and outlet.

C) For a boiler or process heater, the design evaluation shall consider the vent stream flow rate and shall establish the design minimum and average flame temperature.
zone temperatures and combustion zone residence time; and shall describe the method and location where the vent stream is introduced into the flame zone.

(iii) For a condenser, the design evaluation shall consider the vent stream flow rate, relative humidity, and temperature and shall establish the design outlet organic HAP compound concentration level, design average temperature of the condenser exhaust vent stream, and the design average temperatures of the coolant fluid at the condenser inlet and outlet. The temperature of the gas stream exiting the condenser must be measured and used to establish the outlet organic HAP concentration.

(iv) For a carbon adsorption system that regenerates the carbon bed directly onsite in the control device such as a fixed-bed adsorber, the design evaluation shall consider the vent stream flow rate, relative humidity, and temperature and shall establish the design exhaust vent stream organic compound concentration level, adsorption cycle time, number and capacity of carbon beds, type and working capacity of activated carbon used for carbon beds, design total regeneration stream mass or volumetric flow over the period of each complete carbon bed regeneration cycle, design carbon bed temperature after regeneration, design carbon bed regeneration time, and design service life of carbon. For vacuum desorption, the pressure drop shall be included.

(v) For a carbon adsorption system that does not regenerate the carbon bed directly onsite in the control device such as a carbon canister, the design evaluation shall consider the vent stream mass or volumetric flow rate, relative humidity, and temperature and shall establish the design exhaust vent stream organic compound concentration level, capacity of carbon bed, type and working capacity of activated carbon used for carbon bed, and design carbon replacement interval based on the total carbon working capacity of the control device and source operating schedule.

(vi) For a scrubber, the design evaluation shall consider the vent stream composition; constituent concentrations; liquid-to-vapor ratio; scrubbing liquid flow rate and concentration; temperature; and the reaction kinetics of the constituents with the scrubbing liquid. The design evaluation shall establish the design exhaust vent stream organic compound concentration level and shall include the additional information in paragraphs (a)(ii)(vi)(A) and (B) of this section for trays and a packed column scrubber.

(A) Type and total number of theoretical and actual trays;
(B) Type and total surface area of packing for entire column, and for individual packed sections if column contains more than one packed section.

(2) Calculation of TOC or total organic HAP concentration. The TOC concentration or total organic HAP concentration is the sum of the concentrations of the individual components. If compliance is being determined based on TOC, the owner or operator shall compute TOC for each run using Equation 6 of this subpart. If compliance with the wastewater provisions is being determined based on total organic HAP, the owner or operator shall compute total organic HAP using Equation 6 of this subpart, except that only the organic HAP compounds shall be summed; when determining compliance with paragraph (e)(3)(i) of this section, only the soluble and partially soluble HAP compounds shall be summed.

\[
CG_T = \frac{1}{m} \sum_{j=1}^{m} \left( \sum_{i=1}^{n} CGS_{i,j} \right)
\]

where:

- \( CG_T \) = total concentration of TOC in vented gas stream, average of samples, dry basis, ppmv
- \( CGS_{i,j} \) = concentration of sample components in vented gas stream for sample \( j \), dry basis, ppmv
- \( i \) = identifier for a compound
- \( n \) = number of components in the sample
- \( j \) = identifier for a sample
- \( m \) = number of samples in the sample run

(3) Percent oxygen correction for combustion control devices. If the control device is a combustion device, the TOC or total organic HAP concentrations must be corrected to 3 percent oxygen. The
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integrated sampling and analysis procedures of Method 3B of 40 CFR part 60, appendix A shall be used to determine the actual oxygen concentration \( \%O_{2d} \). The samples shall be taken during the same time that the TOC or total organic HAP samples are taken. The concentration corrected to 3 percent oxygen \( C_c \) shall be computed using Equation 7 of this subpart:

\[
C_c = C_m \left( \frac{17.9}{20.9 - \%O_{2d}} \right) \quad \text{(Eq. 7)}
\]

where:
- \( C_c \) = concentration of TOC or total organic HAP corrected to 3 percent oxygen, dry basis, ppmv
- \( C_m \) = total concentration of TOC in vented gas stream, average of samples, dry basis, ppmv
- \( \%O_{2d} \) = concentration of oxygen measured in vented gas stream, dry basis, percent by volume

(4) Exemptions from compliance demonstrations. An owner or operator using any control device specified in paragraphs (a)(4)(i) through (iv) of this section is exempt from the initial compliance provisions in paragraphs (c), (d), and (e) of this section.

(i) A boiler or process heater with a design heat input capacity of 44 megawatts or greater.

(ii) A boiler or process heater into which the emission stream is introduced with the primary fuel.

(iii) A boiler or process heater burning hazardous waste for which the owner or operator:

(A) Has been issued a final permit under 40 CFR part 270 and complies with the requirements of 40 CFR part 266, subpart H, or

(B) Has certified compliance with the interim status requirements of 40 CFR part 266, subpart H.

(iv) A hazardous waste incinerator for which the owner or operator has been issued a final permit under 40 CFR part 270 and complies with the requirements of 40 CFR part 264, subpart O, or has certified compliance with the interim status requirements of 40 CFR part 265, subpart O.

(5) Initial compliance with alternative standard. Initial compliance with the alternative standards in §§63.1253(d) and 63.1254(c) is demonstrated when the outlet TOC concentration is 20 ppmv or less, and the outlet hydrogen halide and halogen concentration is 20 ppmv or less. To demonstrate initial compliance, the owner or operator shall in compliance with the monitoring provisions in §63.1258(b)(5) on the initial compliance date. The owner or operator shall use Method 18 to determine the predominant organic HAP in the emission stream if the TOC monitor is calibrated on the predominant HAP.

(6) Initial compliance with the 20 ppmv outlet limit. Initial compliance with the 20 ppmv TOC and hydrogen halide and halogen concentration is demonstrated when the outlet TOC concentration is 20 ppmv or less, and the outlet hydrogen halide and halogen concentration is 20 ppmv or less. To demonstrate initial compliance, the owner or operator shall use test methods described in paragraph (b) of this section. The owner or operator shall comply with the monitoring provisions in §63.1258(b)(1) through (5) of this subpart on the initial compliance date.

(b) Test methods. When testing is conducted to measure emissions from an affected source, the test methods specified in paragraphs (b)(1) through (10) of this section shall be used.

(1) EPA Method 1 or 1A of appendix A of part 60 is used for sample and velocity traverses.

(2) EPA Method 2, 2A, 2C, or 2D of appendix A of part 60 is used for velocity and volumetric flow rates.

(3) EPA Method 3 of appendix A of part 60 is used for gas analysis.

(4) EPA Method 4 of appendix A of part 60 is used for stack gas moisture.

(5) [Reserved]

(6) Concentration measurements shall be adjusted to negate the dilution effects of introducing nonaffected gaseous streams into the vent streams prior to control or measurement. The following methods are specified for concentration measurements:

(i) Method 18 may be used to determine HAP concentration in any control device efficiency determination.

(ii) Method 25 of appendix A of part 60 may be used to determine total gaseous nonmethane organic concentration for control efficiency determinations in combustion devices.
(iii) Method 26 of appendix A of part 60 shall be used to determine hydrogen chloride concentrations in control device efficiency determinations or in the 20 ppmv outlet hydrogen halide concentration standard.

(iv) Method 25A of appendix A of part 60 may be used to determine the HAP or TOC concentration for control device efficiency determinations under the conditions specified in Method 25 of appendix A for direct measurement of an effluent with a flame ionization detector, or in demonstrating compliance with the 20 ppmv TOC outlet standard. If Method 25A is used to determine the concentration of TOC for the 20 ppmv standard, the instrument shall be calibrated on methane or the predominant HAP. If calibrating on the predominant HAP, the use of Method 25A shall comply with paragraphs (b)(6)(iv)(A) through (C) of this section.

(A) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A, shall be the single organic HAP representing the largest percent by volume.

(B) The use of Method 25A, 40 CFR part 60, appendix A, is acceptable if the response from the high level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(C) The span value of the analyzer must be less than 100 ppmv.

(7) Testing conditions for continuous processes. Testing of emissions on equipment operating as part of a continuous process will consist of three 1-hour runs. Gas stream volumetric flow rates shall be measured every 15 minutes during each 1-hour run. The HAP concentration shall be determined from samples collected in an integrated sample over the duration of each 1-hour test run, or from grab samples collected simultaneously with the flow rate measurements (every 15 minutes). If an integrated sample is collected for laboratory analysis, the sampling rate shall be adjusted proportionally to reflect variations in flow rate. For continuous gas streams, the emission rate used to determine compliance shall be the average emission rate of the three test runs.

(8) Testing and compliance determination conditions for batch processes. Testing of emissions on equipment where the flow of gaseous emissions is intermittent (batch operations) shall be conducted as specified in paragraphs (b)(8)(i) through (iii) of this section.

(i) Except as provided in paragraph (b)(9) of this section for condensers, testing shall be conducted at absolute worst-case conditions or hypothetical worst-case conditions. Gas stream volumetric flow rates shall be measured at 15-minute intervals. The HAP or TOC concentration shall be determined from samples collected in an integrated sample over the duration of the test, or from grab samples collected simultaneously with the flow rate measurements (every 15 minutes). If an integrated sample is collected for laboratory analysis, the sampling rate shall be adjusted proportionally to reflect variations in flow rate. The absolute worst-case or hypothetical worst-case conditions shall be characterized by the criteria presented in paragraphs (b)(8)(i)(A) and (B) of this section. In all cases, a site-specific plan shall be submitted to the Administrator for approval prior to testing in accordance with §63.7(c) and §63.1250(l). The test plan shall include the emission profile described in paragraph (b)(8)(ii) of this section.

(A) Absolute worst-case conditions are defined by the criteria presented in paragraph (b)(8)(i)(A)(1) or (2) of this section if the maximum load is the most challenging condition for the control device. Otherwise, absolute worst-case conditions are defined by the conditions in paragraph (b)(8)(i)(A)(3) of this section.

(1) The period in which the inlet to the control device will contain at least 50 percent of the maximum HAP load (in lb) capable of being vented to the control device over any 8-hour period. An emission profile as described in paragraph (b)(8)(ii)(A) of this section shall be used to identify the 8-hour period that includes the maximum projected HAP load.

(2) A 1-hour period of time in which the inlet to the control device will contain the highest HAP mass loading rate, in lb/hr, capable of being vented.
to the control device. An emission profile as described in paragraph (b)(8)(ii)(A) of this section shall be used to identify the 1-hour period of maximum HAP loading.

(3) The period of time when the HAP loading or stream composition (including non-HAP) is most challenging for the control device. These conditions include, but are not limited to the following:

(i) Periods when the stream contains the highest combined VOC and HAP load, in lb/hr, described by the emission profiles in (b)(8)(ii);

(ii) Periods when the streams contain HAP constituents that approach limits of solubility for scrubbing media;

(iii) Periods when the streams contain HAP constituents that approach limits of adsorptivity for carbon adsorption systems.

(B) Hypothetical worst-case conditions are simulated test conditions that, at a minimum, contain the highest hourly HAP load of emissions that would be predicted to be vented to the control device from the emissions profile described in paragraph (b)(8)(ii)(B) or (C) of this section.

(ii) Emissions profile. The owner or operator may choose to perform tests only during those periods of the worst-case conditions that the owner or operator selects to control as part of achieving the required emission reduction. The owner or operator must develop an emission profile for the vent to the control device that describes the characteristics of the vent stream at the inlet to the control device under worst case conditions. The emission profile shall be developed based on any one of the procedures described in (b)(8)(ii)(A) through (C) of this section, as required by paragraph (b)(8)(i).

(A) Emission profile by process. The emission profile must consider all emission episodes that could contribute to the vent stack for a period of time that is sufficient to include all processes venting to the stack and shall consider production scheduling. The profile shall describe the HAP load to the device that equals the highest sum of emissions from the episodes that can vent to the control device in any given hour. Emissions per episode shall be calculated using the procedures specified in paragraph (d)(2) of this section. Emissions per episode shall be divided by the duration of the episode only if the duration of the episode is longer than 1 hour.

(B) Emission profile by equipment. The emission profile must consist of emissions that meet or exceed the highest emissions, in lb/hr, that would be expected under actual processing conditions. The profile shall describe equipment configurations used to generate the emission events, volatility of materials processed in the equipment, and the rationale used to identify and characterize the emission events. The emissions may be based on using a compound more volatile than compounds actually used in the process(es), and the emissions may be generated from all equipment in the process(es) or only selected equipment.

(C) Emission profile by capture and control device limitation. The emission profile shall consider the capture and control system limitations and the highest emissions, in lb/hr, that can be routed to the control device, based on maximum flowrate and concentrations possible because of limitations on conveyance and control equipment (e.g., fans, LEL alarms and safety bypasses).

(iii) Three runs, at a minimum of 1 hour each and a maximum of 8 hours each, are required for performance testing. Each run must occur over the same worst-case conditions, as defined in paragraph (b)(8)(i) of this section.

(9) Testing requirements for condensers. For emission streams controlled using condensers, continuous direct measurement of condenser outlet gas temperature to be used in determining concentrations per the design evaluation described in §63.1257(a)(1)(iii) is required.

(10) Wastewater testing. Wastewater analysis shall be conducted in accordance with paragraph (b)(10)(i), (ii), (iii), or (iv) of this section.

(i) Method 305. Use procedures specified in Method 305 of 40 CFR part 63, appendix A and comply with requirements specified in paragraph (b)(10)(v) of this section.

(ii) Method 624, 625, 1624, 1625, or 8270. Use procedures specified in Method 624, 625, 1624, 1625, or 8270 of 40 CFR part 136.
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appendix A and comply with requirements in paragraph (b)(10)(v) of this section.

(iii) Other EPA Methods. Use procedures specified in the method, validate the method using the procedures in paragraph (b)(10)(iii)(A) or (B) of this section, and comply with the procedures in paragraph (b)(10)(v) of this section.

(A) Validate the method according to section 5.1 or 5.3 of Method 301 of 40 CFR part 63, appendix A.

(B) Follow the procedure as specified in ‘Alternative Validation Procedure for EPA Waste Methods’ 40 CFR part 63, appendix D.

(iv) Methods other than an EPA method. Use procedures specified in the method, validate the method using the procedures in paragraph (b)(10)(iii)(A) of this section, and comply with the requirements in paragraph (b)(10)(v) of this section.

(v) Sampling plan. The owner or operator shall prepare a sampling plan. Wastewater samples shall be collected using sampling procedures which minimize loss of organic compounds during sample collection and analysis and maintain sample integrity. The sample plan shall include procedures for determining recovery efficiency of the relevant partially soluble and soluble HAP compounds. An example of an acceptable sampling plan would be one that incorporates similar sampling and sample handling requirements to those of Method 25D of 40 CFR part 60, appendix A. The sampling plan shall be maintained at the facility.

(c) Initial compliance with storage tank provisions. The owner or operator of an affected storage tank shall demonstrate initial compliance with §63.1253(b) or (c), as applicable, by fulfilling the requirements of paragraph (c)(1), (c)(2), or (c)(3) of this section.

(1) Performance test. If this option is chosen to demonstrate initial compliance with the percent reduction requirement of §63.1253(b)(1) or (c)(1)(i), the efficiency of the control device shall be calculated using performance test data as specified in paragraphs (c)(1)(i) through (iii) of this section. Initial compliance with the outlet concentration requirement of §63.1253(b)(2) or (c)(1)(ii) is demonstrated by fulfilling the requirements of paragraph (a)(6) of this section.

(i) Equations 8 and 9 of this subpart shall be used to calculate the mass rate of total HAP reasonably expected maximum filling rate at the inlet and outlet of the control device for standard conditions of 20°C:

\[
E_i = K_2 \left( \sum_{j=1}^{n} C_{ij} M_{ij} Q_i \right) 
\]

(Eq. 8)

\[
E_o = K_2 \left( \sum_{j=1}^{n} C_{oj} M_{oj} Q_o \right) 
\]

(Eq. 9)

where:

\[
C_{ij}, C_{oj} = concentration of sample component j of the gas stream at the inlet and outlet of the control device, respectively, dry basis, ppmv
\]

\[
E_i, E_o = mass rate of total HAP at the inlet and outlet of the control device, respectively, dry basis, kg/hr
\]

\[
M_{ij}, M_{oj} = molecular weight of sample component j of the gas stream at the inlet and outlet of the control device, respectively, gram/gram-mole
\]

\[
Q_i, Q_o = flow rate of gas stream at the inlet and outlet of the control device, respectively, dry standard cubic meter per minute
\]

\[
K_2 = constant, 2.494 \times 10^{-6} \text{ (parts per million) }^{-1} \text{ (gram-mole per standard cubic meter) }^{-1} \text{ (kilogram/gram) }^{-1} \text{ (minute/hour)}, \text{ where standard temperature is } 20°C
\]

\[
n = number of sample components in the gas stream
\]

(ii) The percent reduction in total HAP shall be calculated using Equation 10 of this subpart:

\[
R = \frac{E_i - E_o}{E_i} (100)
\]

(Eq. 10)

where:

\[
R = control efficiency of control device, percent
\]

\[
E_i = mass rate of total HAP at the inlet to the control device as calculated under paragraph (c)(1)(i) of this section, kilograms organic HAP per hour
\]
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E_o = mass rate of total HAP at the outlet of the control device, as calculated under paragraph (c)(1)(i) of this section, kilograms organic HAP per hour.

(iii) A performance test is not required to be conducted if the control device used to comply with §63.1253 (storage tank provisions) is also used to comply with §63.1254 (process vent provisions), and compliance with §63.1254 has been demonstrated in accordance with paragraph (d) of this section.

(2) Design evaluation. If this option is chosen to demonstrate initial compliance with the percent reduction requirement of §63.1253(b) or (c), a design evaluation shall be prepared in accordance with the provisions in paragraph (a)(1) of this section. The design evaluation shall include documentation demonstrating that the control device being used achieves the required control efficiency during reasonably expected maximum filling rate.

(3) Floating roof. If the owner or operator of an affected source chooses to comply with the provisions of §63.1253(b) or (c) by installing a floating roof, the owner or operator shall comply with the procedures described in §§63.119(b), (c), (d), and 63.120(a), (b), and (c), with the differences noted in paragraphs (c)(3)(i) through (v) of this section for the purposes of this subpart.

(i) When the term “storage vessel” is used in §§63.119 and 63.120, the definition of “storage tank” in §63.1251 shall apply for the purposes of this subpart.

(ii) When December 31, 1992 is referred to in §§63.119, April 2, 1997 shall apply instead for the purposes of this subpart.

(iii) When April 22, 1994 is referred to in §§63.119, September 21, 1998 shall apply instead for the purposes of this subpart.

(iv) When the phrase “the compliance date specified in §63.100 of subpart F of this part” is referred to in §63.120, the phrase “the compliance date specified in §63.1250” shall apply for the purposes of this subpart.

(v) When the phrase “the maximum true vapor pressure of the total organic HAP in the stored liquid falls below the values defining Group 1 storage vessels specified in table 5 or table 6 of this subpart” is referred to in §63.120(b)(1)(iv), the phrase “the maximum true vapor pressure of the total organic HAP in the stored liquid falls below 13.1 kPa (1.9 psia)” shall apply for the purposes of this subpart.

(4) Initial compliance with alternative standard. Initial compliance with §63.1253(d) is demonstrated by fulfilling the requirements of paragraph (a)(5) of this section.

(5) Planned maintenance. The owner or operator shall demonstrate compliance with the requirements of §63.1253(e) by including the periods of planned routine maintenance specified by date and time in each Periodic Report required by §63.1260.

(d) Initial compliance with process vent provisions. An owner or operator of an affected source complying with the process vent standards in §63.1254 shall demonstrate compliance using the procedures described in paragraphs (d)(1) through (4) of this section.

(1) Except as provided in paragraph (a)(4) of this section, initial compliance with the process vent standards in §63.1254 shall be demonstrated using the procedures specified in paragraphs (d)(1)(i) through (v), as applicable.

(i) Initial compliance with §63.1254(a)(1)(i) is demonstrated when the actual emissions of HAP from the sum of all process vents within a process that do not meet the criteria specified in §63.1254(a)(3) is less than or equal to 2,000 lb/yr. Initial compliance with §63.1254(a)(1)(ii) is demonstrated when the uncontrolled emissions of HAP from the sum of all process vents within a process is less than or equal to 100 lb/yr. Uncontrolled HAP emissions and controlled HAP emissions shall be determined using the procedures described in paragraphs (d)(2) and (3) of this section.

(ii) Initial compliance with the percent reduction requirements in §§63.1254(a)(2), (a)(3), and (b) is demonstrated by:

(A) Determining controlled HAP emissions using the procedures described in paragraph (d)(3) of this section and uncontrolled HAP emissions.
determined using the procedures described in paragraph (d)(2) of this section and demonstrating that the reductions required by §§ 63.1254(a)(2), (a)(3), and (b) are met; or

(B) Controlling the process vents using a device meeting the criteria specified in paragraph (a)(4) of this section.

(iii) Initial compliance with the outlet concentration requirements in § 63.1254(a)(2)(ii) and (3) is demonstrated when the outlet TOC concentration is 20 ppmv or less and the outlet hydrogen halide and halogen concentration is 20 ppmv or less. The owner or operator shall demonstrate compliance by fulfilling the requirements in paragraph (a)(6) of this section.

(iv) Initial compliance with § 63.1254(c) is demonstrated by fulfilling the requirements of paragraph (a)(5) of this section.

(2) Uncontrolled emissions. An owner or operator of an affected source complying with the emission limitation required by § 63.1254(a)(1), or emissions reductions specified in § 63.1254(a)(2), (a)(3), or (b), for each process vent within a process, shall calculate uncontrolled emissions from all equipment in the process according to the procedures described in paragraph (d)(2)(i) or (ii) of this section, as appropriate.

(i) Emission estimation procedures. Owners or operators shall determine uncontrolled emissions of HAP using measurements and/or calculations for each batch emission episode within each unit operation according to the engineering evaluation methodology in paragraphs (d)(2)(i)(A) through (H) of this section. Except where variations are noted, individual HAP partial pressures in multicomponent systems shall be determined by the following methods: If the components are miscible in one another, use Raoult’s law to calculate partial pressures; if Raoult’s law or Henry’s law are not appropriate or available, use experimentally obtained activity coefficients or models such as the group-contribution models, to predict activity coefficients, or assume the components of the system behave independently and use the summation of all vapor pressures from the HAP as the total HAP partial pressure. Chemical property data can be obtained from standard reference texts.

(A) Vapor displacement. Emissions from vapor displacement due to transfer of material shall be calculated using Equation 11 of this subpart. The individual HAP partial pressures may be calculated using Raoult’s law.

\[ E = \frac{V}{RT} \sum_{i} P_i MW_i \]  

where:

- \( E \) = mass of HAP emitted
- \( V \) = volume of gas displaced from the vessel
- \( R \) = ideal gas law constant
- \( T \) = temperature of the vessel vapor space; absolute
- \( P_i \) = partial pressure of the individual HAP
- \( MW_i \) = molecular weight of the individual HAP
- \( n \) = number of HAP compounds in the emission stream

(B) Purging. Emissions from purging shall be calculated using Equation 12 of this subpart. The partial pressures of individual condensable compounds may be calculated using Raoult’s law, the pressure of the vessel vapor space may be set equal to 760 mmHg, and the partial pressure of HAP shall be assumed to be 25 percent of the saturated value if the purge flow rate is greater than 100 standard cubic feet per minute (scfm).

\[ E = \sum_{i=1}^{n} P_i MW_i \times \frac{(V)(t)}{(R)(T)} \times \frac{P_T}{P_T - \sum_{j=1}^{m} (P_j)} \]  

(Eq. 12)
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Where:
- \( E \) = mass of HAP emitted
- \( V \) = purge flow rate at the temperature and pressure of the vessel vapor space
- \( R \) = ideal gas law constant
- \( T \) = temperature of the vessel vapor space; absolute
- \( P_i \) = partial pressure of the individual HAP
- \( P_j \) = partial pressure of individual condensable VOC compounds (including HAP)
- \( P_T \) = pressure of the vessel vapor space
- \( \text{MW}_i \) = molecular weight of the individual HAP
- \( t \) = time of purge
- \( n \) = number of HAP compounds in the emission stream
- \( i \) = identifier for a HAP compound
- \( j \) = identifier for a condensable compound
- \( m \) = number of condensable compounds (including HAP) in the emission stream

(C) Heating. Emissions caused by the heating of a vessel to a temperature equal to or lower than 10 K below the boiling point shall be calculated using the procedures in either paragraph (d)(2)(i)(C)(1) or (3) of this section. If the contents of a vessel are heated to the boiling point, emissions must be calculated using the procedures in paragraph (d)(2)(i)(C)(4) of this section.

1) This paragraph describes procedures to calculate emissions if the final temperature to which the vessel contents are heated is 10 K below the boiling point of the HAP in the vessel, or lower. The owner or operator shall calculate the mass of HAP emitted per episode using either Equation 13 or 14 of this subpart. The moles of noncondensable gas displaced are calculated using Equation 15 of this subpart. The initial and final pressure of the noncondensable gas in the vessel shall be calculated using Equation 16 of this subpart. The average molecular weight of HAP in the displaced gas shall be calculated using Equation 17 of this subpart.

\[
E = \sum_{i=1}^{n} \left( P_i \right) x_i \times \Delta \eta \times MW_{\text{HAP}} \quad \text{(Eq. 13)}
\]

\[
E = \frac{\sum_{i=1}^{n} \left( P_i \right)_{T_1} + \sum_{i=1}^{n} \left( P_i \right)_{T_2}}{2} \times \Delta \eta \times MW_{\text{HAP}} \quad \text{(Eq. 14)}
\]

\[
\Delta \eta = \frac{V}{R} \left[ \frac{P_{a_1}}{T_1} - \frac{P_{a_2}}{T_2} \right] \quad \text{(Eq. 15)}
\]

\[
P_{a_n} = P_{a_m} - \sum_{j=1}^{m} \left( P_j \right)_{T_n} \quad \text{(Eq. 16)}
\]
MW_{HAP} = \sum_{i=1}^{n} \left( \left( P_i \right)_{T_1} + \left( P_i \right)_{T_2} \right) MW_i \over \sum_{i=1}^{n} \left( \left( P_i \right)_{T_1} + \left( P_i \right)_{T_2} \right) (Eq. 17)

Where:

- $E$ = mass of HAP vapor displaced from the vessel being heated
- $x_i$ = mole fraction of each HAP in the liquid phase
- $x_j$ = mole fraction of each condensable VOC (including HAP) in the liquid phase
- $(P_i^*)$ = vapor pressure of each HAP in the vessel headspace at any temperature between the initial and final heatup temperatures, mmHg
- $(P_j^*)$ = vapor pressure of each condensable VOC (including HAP) in the vessel headspace at any temperature between the initial and final heatup temperatures, mmHg
- 760 = atmospheric pressure, mmHg
- $MW_{HAP}$ = the average molecular weight of HAP present in the displaced gas
- $\Delta\eta$ = number of moles of noncondensable gas displaced
- $V$ = volume of free space in the vessel
- $R$ = ideal gas law constant
- $T_1$ = initial temperature of vessel contents, absolute
- $T_2$ = final temperature of vessel contents, absolute
- $P_{n_{a_{\text{m}}}}$ = partial pressure of noncondensable gas in the vessel headspace at initial (n=1) and final (n=2) temperature
- $P_{n_{a_{\text{m}}}}$ = atmospheric pressure (when $\Delta\eta$ is used in Equation 13 of this subpart, $P_{n_{a_{\text{m}}}}$ may be set equal to 760 mmHg for any vessel)
- $(P_i)_{n_{a_{\text{m}}}}$ = partial pressure of each condensable compound (including HAP) in the vessel headspace at the initial temperature (n=1) and final (n=2) temperature
- $m$ = number of condensable compounds (including HAP) in the displaced vapor
- $j$ = identifier for a condensable compound
- $(P_i)_{n_{a_{\text{m}}}}$ = partial pressure of each HAP in the vessel headspace at initial $(T_i)$ and final $(T_j)$ temperature; [for use in Equation 13, replace $(P_i)_{T_1} + (P_i)_{T_2}$ with $P_i$ at the temperature used to calculate vapor pressure of HAP in Equation 13]
- $MW_i$ = molecular weight of each HAP
- $n$ = number of HAP compounds in the emission stream
- $i$ = identifier for a HAP compound

(2) If the vessel contents are heated to a temperature that is higher than 10 K below the boiling point and less than the boiling point, emissions must be calculated using the procedures in paragraph (d)(2)(i)(C)(i), or (ii), or (iii) of this section.

(i) Use Equation 13 of this subpart. In Equation 13 of this subpart, the HAP vapor pressures must be determined at the temperature 10 K below the boiling point. In the calculation of $\Delta\eta$ for Equation 13 of this subpart, $T_2$ must be the temperature 10 K below the boiling point, and $P_{n_{a_{\text{m}}}}$ must be determined at the temperature 10 K below the boiling point. In the calculation of $MW_{HAP}$, the HAP partial pressures must be determined at the temperature 10 K below the boiling point.

(ii) Use Equation 14 of this subpart. In Equation 14 of this subpart, the HAP partial pressures must be determined at the temperature 10 K below the boiling point. In the calculation of $\Delta\eta$ for Equation 14 of this subpart, $T_2$ must be the temperature 10 K below the boiling point, and $P_{n_{a_{\text{m}}}}$ must be determined at the temperature 10 K below the boiling point. In the calculation of $MW_{HAP}$, the HAP partial pressures must be determined at the temperature 10 K below the boiling point.

(iii) Use Equation 14 of this subpart over specific temperature increments. If the initial temperature is lower than 10 K below the boiling point, emissions must be calculated as the sum over two increments; one increment is from the initial temperature to 10 K below the boiling point, and the second is from 10 K below the boiling point to the lower of either the final temperature or the temperature 5 K below the boiling point.
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point. If the initial temperature is higher than 10 K below the boiling point, emissions are calculated over one increment from the initial temperature to the lower of either the final temperature or the temperature 5 K below the boiling point.

(3)(i) Emissions caused by heating a vessel are calculated using Equation 18 of this subpart.

\[
E = MW_{\text{HAP}} \times \left( N_{\text{avg}} \times \ln \left( \frac{P_T - \sum_{i=1}^{n} (P_{i,1})}{P_T - \sum_{i=1}^{n} (P_{i,2})} \right) \right) - \left( n_{i,2} - n_{i,1} \right) \quad \text{(Eq. 18)}
\]

Where:
- \( E \) = mass of HAP vapor displaced from the vessel being heated
- \( N_{\text{avg}} \) = average gas space molar volume during the heating process
- \( P_T \) = total pressure in the vessel
- \( P_{i,1} \) = partial pressure of the individual HAP compounds at \( T_1 \)
- \( P_{i,2} \) = partial pressure of the individual HAP compounds at \( T_2 \)
- \( MW_{\text{HAP}} \) = average molecular weight of the HAP compounds
- \( n_{i,1} \) = number of moles of condensable in the vessel headspace at \( T_1 \)
- \( n_{i,2} \) = number of moles of condensable in the vessel headspace at \( T_2 \)
- \( n \) = number of HAP compounds in the emission stream

(ii) The average gas space molar volume during the heating process is calculated using Equation 19 of this subpart.

\[
N_{\text{avg}} = \frac{VP_T}{2RT} \left( \frac{1}{T_1} + \frac{1}{T_2} \right) \quad \text{(Eq. 19)}
\]

Where:
- \( N_{\text{avg}} \) = average gas space molar volume during the heating process
- \( V \) = volume of free space in vessel
- \( P_T \) = total pressure in the vessel
- \( R \) = ideal gas law constant
- \( T_1 \) = initial temperature of the vessel
- \( T_2 \) = final temperature of the vessel

(iii) The difference in the number of moles of condensable in the vessel headspace between the initial and final temperatures is calculated using Equation 20 of this subpart.

\[
\left( n_{i,2} - n_{i,1} \right) = \frac{V}{(R)(T_2)} \sum_{i=1}^{n} P_{i,2} - \frac{V}{(R)(T_1)} \sum_{i=1}^{n} P_{i,1} \quad \text{(Eq. 20)}
\]

Where:
- \( V \) = volume of free space in vessel
- \( R \) = ideal gas law constant
- \( T_1 \) = initial temperature in the vessel
- \( T_2 \) = final temperature in the vessel
- \( P_{i,1} \) = partial pressure of the individual HAP compounds at \( T_1 \)
- \( P_{i,2} \) = partial pressure of the individual HAP compounds at \( T_2 \)
- \( n \) = number of HAP compounds in the emission stream

(4) If the vessel contents are heated to the boiling point, emissions must be
calculated using the procedure in paragraphs (d)(2)(i)(c)(4)(i) and (ii) of this section.

(i) Use either of the procedures in paragraph (d)(3)(i)(B)(3) of this section to calculate the emissions from heating to the boiling point (note that \( P_0 = 0 \) in the calculation of; and

(ii) While boiling, the vessel must be operated with a properly operated process condenser. An initial demonstration that a process condenser is properly operated is required for vessels that operate process condensers without secondary condensers that are air pollution control devices. The owner or operator must either measure the condenser exhaust gas temperature and show it is less than the boiling point of the substance(s) in the vessel, or perform a material balance around the vessel and condenser to show that at least 99 percent of the material vaporized while boiling is condensed. Uncontrolled emissions are assumed to be zero under these conditions. The initial demonstration shall be conducted for all appropriate operating scenarios and documented in the Notification of Compliance report described in §63.1260(f).

(D) Depressurization. Emissions from depressurization shall be calculated using the procedures in either paragraphs (d)(2)(i)(D)(1) through (4), paragraphs (d)(2)(i)(D)(5) through (9), or paragraph (d)(2)(i)(D)(10) of this section.

(1) Equations 21 and 22 of this subpart are used to calculate the initial and final volumes of noncondensable gas present in the vessel, adjusted to atmospheric pressure. The HAP partial pressures may be calculated using Raoult’s law.

\[
V_{nc1} = \frac{V_P \cdot P_{nc1}}{760} \quad \text{(Eq. 21)}
\]

\[
V_{nc2} = \frac{V_P \cdot P_{nc2}}{760} \quad \text{(Eq. 22)}
\]

Where:

- \( V_{nc1} \) = initial volume of noncondensable gas in the vessel
- \( V_{nc2} \) = final volume of noncondensable gas in the vessel
- \( V \) = free volume in the vessel being depressurized
- \( P_{nc1} \) = initial partial pressure of the noncondensable gas, as calculated using Equation 23 of this subpart, mmHg
- \( P_{nc2} \) = final partial pressure of the noncondensable gas, as calculated using Equation 24 of this subpart, mmHg
- 760 = atmospheric pressure, mmHg

(2) The initial and final partial pressures of the noncondensable gas in the vessel are determined using Equations 23 and 24 of this subpart:

\[
P_{nc1} = P_1 - \sum_{j=1}^{m} (P_j)(x_j) \quad \text{(Eq. 23)}
\]

\[
P_{nc2} = P_2 - \sum_{j=1}^{m} (P_j)(x_j) \quad \text{(Eq. 24)}
\]

Where:

- \( P_{nc1} \) = initial partial pressure of the noncondensable gas
- \( P_{nc2} \) = final partial pressure of the noncondensable gas
- \( P_1 \) = initial vessel pressure
- \( P_2 \) = final vessel pressure
- \( P_j \) = vapor pressure of each condensable (including HAP) in the emission stream
- \( x_j \) = mole fraction of each condensable (including HAP) in the emission stream
- \( m \) = number of condensable compounds (including HAP) in the emission stream
- \( j \) = identifier for a condensable compound

(3) The average ratio of moles of noncondensable to moles of HAP is calculated using Equation 25 of this subpart:
\[ n_R = \left( \frac{P_{nc1}}{\sum_{i=1}^{n}(P_i^*)(x_i)} + \frac{P_{nc2}}{\sum_{i=1}^{n}(P_i^*)(x_i)} \right) \times \frac{2}{2} \] (Eq. 25)

Where:
- \( n_R \) = average ratio of moles of noncondensable to moles of HAP
- \( P_{nc1} \) = initial partial pressure of the noncondensable gas, as calculated using Equation 23 of this subpart
- \( P_{nc2} \) = final partial pressure of the noncondensable gas, as calculated using Equation 24 of this subpart
- \( P_i^* \) = vapor pressure of each individual HAP
- \( x_i \) = mole fraction of each individual HAP in the liquid phase
- \( n \) = number of HAP compounds
- \( i \) = identifier for a HAP compound

(4) The mass of HAP emitted shall be calculated using Equation 26 of this subpart:

\[ E = \frac{V_{nc1} - V_{nc2}}{n_R} \times \frac{P_{atm}}{RT} \times MW_{HAP} \] (Eq. 26)

Where:
- \( E \) = mass of HAP emitted
- \( V_{nc1} \) = initial volume of noncondensable gas in the vessel, as calculated using Equation 21 of this subpart
- \( V_{nc2} \) = final volume of noncondensable gas in the vessel, as calculated using Equation 22 of this subpart
- \( n_R \) = average ratio of moles of noncondensable to moles of HAP, as calculated using Equation 25 of this subpart
- \( P_{atm} \) = atmospheric pressure, standard
- \( R \) = ideal gas law constant
- \( T \) = vessel temperature, absolute
- \( MW_{HAP} \) = average molecular weight of the HAP, as calculated using Equation 17 of this subpart

(5) The moles of HAP vapor initially in the vessel are calculated using the ideal gas law using Equation 27 of this subpart:

\[ n_{HAP} = \frac{(Y_{HAP})(V)(P_1)}{RT} \] (Eq. 27)

Where:
- \( Y_{HAP} \) = mole fraction of HAP (the sum of the individual HAP fractions, \( \Sigma Y_i \))
- \( V \) = free volume in the vessel being depressurized
- \( P_1 \) = initial vessel pressure
- \( R \) = ideal gas law constant
- \( T \) = vessel temperature, absolute

(6) The initial and final moles of noncondensable gas present in the vessel are calculated using Equations 28 and 29 of this subpart:

\[ n_1 = \frac{VP_{nc1}}{RT} \] (Eq. 28)

\[ n_2 = \frac{VP_{nc2}}{RT} \] (Eq. 29)

Where:
- \( n_1 \) = initial number of moles of noncondensable gas in the vessel
- \( n_2 \) = final number of moles of noncondensable gas in the vessel
- \( V \) = free volume in the vessel being depressurized
- \( P_{nc1} \) = initial partial pressure of the noncondensable gas, as calculated using Equation 23 of this subpart
- \( P_{nc2} \) = final partial pressure of the noncondensable gas, as calculated using Equation 24 of this subpart
- \( R \) = ideal gas law constant
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(7) The initial and final partial pressures of the noncondensable gas in the vessel are determined using Equations 23 and 24 of this subpart.

(8) The moles of HAP emitted during the depressurization are calculated by taking an approximation of the average ratio of moles of HAP to moles of noncondensable and multiplying by the total moles of noncondensables released during the depressurization, using Equation 30 of this subpart:

\[
n_{\text{HAP}} = \left( \frac{n_{\text{HAP},1} + n_{\text{HAP},2}}{n_1 + n_2} \right) \left[ n_1 - n_2 \right] \quad \text{(Eq. 30)}
\]

where:
- \( n_{\text{HAP}} \) = moles of HAP emitted
- \( n_1 \) = initial number of moles of noncondensable gas in the vessel, as calculated using Equation 28 of this subpart
- \( n_2 \) = final number of moles of noncondensable in the vessel, as calculated using Equation 29 of this subpart

(9) The mass of HAP emitted can be calculated using Equation 31 of this subpart:

\[
E = n_{\text{HAP}} \cdot \text{MW}_{\text{HAP}} \quad \text{(Eq. 31)}
\]

where:
- \( E \) = mass of HAP emitted
- \( n_{\text{HAP}} \) = moles of HAP emitted, as calculated using Equation 30 of this subpart
- \( \text{MW}_{\text{HAP}} \) = average molecular weight of the HAP as calculated using Equation 17 of this subpart

(10) Emissions from depressurization may be calculated using Equation 32 of this subpart:

\[
E = \frac{V}{(R)(T)} \times \ln \left( \frac{P_1 - \sum_{i=1}^{n} (P_i)}{P_2 - \sum_{i=1}^{n} (P_i)} \right) \times \sum_{i=1}^{n} (P_i)(\text{MW}_i) \quad \text{(Eq. 32)}
\]

where:
- \( V \) = free volume in vessel being depressurized
- \( R \) = ideal gas law constant
- \( T \) = temperature of the vessel, absolute
- \( P_1 \) = initial pressure in the vessel
- \( P_2 \) = final pressure in the vessel
- \( P_i \) = partial pressure of the individual HAP compounds
- \( \text{MW}_i \) = molecular weight of the individual HAP compounds
- \( n \) = number of HAP compounds in the emission stream
- \( i \) = identifier for a HAP compound

(E) Vacuum systems. Emissions from vacuum systems may be calculated using Equation 33 of this subpart if the air leakage rate is known or can be approximated.

\[
E = \frac{\text{MW}_{\text{HAP}}}{\text{MW}_{\text{nc}}} \left( \frac{P_{\text{system}}}{P_{\text{system}} - P_i^*} - 1 \right) \quad \text{(Eq. 33)}
\]
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where:

\( E \) = mass of HAP emitted

\( P_{\text{system}} \) = absolute pressure of receiving vessel or ejector outlet conditions, if there is no receiver

\( P_{i}^{*} \) = vapor pressure of the HAP at the receiver temperature or the ejector outlet conditions

\( L_{a} \) = total air leak rate in the system, mass/time

\( \text{MW}_{\text{nc}} \) = molecular weight of non-condensable gas

\( t \) = time of vacuum operation

\( \text{MW}_{\text{HAP}} \) = average molecular weight of HAP in the emission stream, as calculated using Equation 17 of this subpart, with HAP partial pressures calculated at the temperature of the receiver or ejector outlet, as appropriate

\( \text{MW}_{g} \) = molecular weight of the evolved gas

(F) Gas evolution. Emissions from gas evolution shall be calculated using Equation 12 of this subpart with \( V \) calculated using Equation 34 of this subpart:

\[
V = \frac{\left( W_{g} \right) (R)(T)}{\left( P_{T}\right) \left( \text{MW}_{g} \right)}
\]  
(Eq. 34)

Where:

\( V \) = volumetric flow rate of gas evolution

\( W_{g} \) = mass flow rate of gas evolution

\( R \) = ideal gas law constant

\( T \) = temperature at the exit, absolute

\( P_{T} \) = vessel pressure

\( \text{MW}_{g} \) = molecular weight of the evolved gas

(G) Air drying. Emissions from air drying shall be calculated using Equation 35 of this subpart:

\[
E = B \times \left( \frac{PS_{1}}{100 - PS_{1}} - \frac{PS_{2}}{100 - PS_{2}} \right)
\]  
(Eq. 35)

Where:

\( E \) = mass of HAP emitted

\( B \) = mass of dry solids

\( PS_{1} \) = HAP in material entering dryer, weight percent

\( PS_{2} \) = HAP in material exiting dryer, weight percent

\( \text{PS}_{1} \) = weight percent of HAP in material entering dryer

\( \text{PS}_{2} \) = weight percent of HAP in material exiting dryer

(H) Empty vessel purging. Emissions from empty vessel purging shall be calculated using Equation (36) of this subpart (Note: The term \(- F t/v\) can be assumed to be 1):

\[
E = \frac{V}{RT} \left( \sum_{i=1}^{n} \left( P_{i} \right) \left( \text{MW}_{i} \right) \left( 1 - e^{-F t/v} \right) \right)
\]  
(Eq. 36)

Where:

\( V \) = volume of empty vessel

\( R \) = ideal gas law constant

\( T \) = temperature of the vessel vapor space; absolute

\( P_{i} \) = partial pressure of the individual HAP at the beginning of the purge

\( \text{MW}_{i} \) = molecular weight of the individual HAP

\( F \) = flowrate of the purge gas

\( t \) = duration of the purge

\( n \) = number of HAP compounds in the emission stream

\( i \) = identifier for a HAP compound
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(ii) Engineering assessments. The owner or operator shall conduct an engineering assessment to calculate uncontrolled HAP emissions for each emission episode that is not due to vapor displacement, purging, heating, depressurization, vacuum operations, gas evolution, or air drying. For emission episodes caused by any of these types of activities, the owner or operator also may calculate uncontrolled HAP emissions based on an engineering assessment if the owner or operator can demonstrate to the Administrator that the methods in paragraph (d)(2)(i) of this section are not appropriate. One criterion the owner or operator could use to demonstrate that the methods in paragraph (d)(2)(i) of this section are not appropriate is if previous test data are available that show a greater than 20 percent discrepancy between the test value and the estimated value. An engineering assessment includes, but is not limited to, the following:

(A) Previous test results, provided the tests are representative of current operating practices at the process unit.
(B) Bench-scale or pilot-scale test data representative of the process under representative operating conditions.
(C) Maximum flow rate, HAP emission rate, concentration, or other relevant parameter specified or implied within a permit limit applicable to the process vent.
(D) Design analysis based on accepted chemical engineering principles, measurable process parameters, or physical or chemical laws or properties. Examples of analytical methods include, but are not limited to:

(1) Use of material balances based on process stoichiometry to estimate maximum organic HAP concentrations.
(2) Estimation of maximum flow rate based on physical equipment design such as pump or blower capacities.
(3) Estimation of HAP concentrations based on saturation conditions.

(E) All data, assumptions, and procedures used in the engineering assessment shall be documented in accordance with §63.1260(e). Data or other information supporting a finding that the emissions estimation equations are inappropriate shall be reported in the Precompliance report.

(3) Controlled emissions. An owner or operator shall determine controlled emissions using the procedures in either paragraph (d)(3)(i) or (ii) of this section. For condensers, controlled emissions shall be calculated using the emission estimation equations described in paragraph (d)(3)(i)(B) of this section.

(i) Small control devices. Except for condensers, controlled emissions for each process vent that is controlled using a small control device shall be determined by using the design evaluation described in paragraph (d)(3)(i)(A) of this section, or conducting a performance test in accordance with paragraph (d)(3)(ii) of this section. Whenever a small control device becomes a large control device, the owner or operator must comply with the provisions in paragraph (d)(3)(ii) of this section and submit the test report in the next Periodic report.

(A) Design evaluation. The design evaluation shall include documentation demonstrating that the control device being used achieves the required control efficiency under worst-case conditions, as determined from the emission profile described in §63.1257(b)(8)(ii). The control efficiency determined from this design evaluation shall be applied to uncontrolled emissions to estimate controlled emissions. The documentation must be conducted in accordance with the provisions in paragraph (a)(1) of this section. The design evaluation shall also include the value(s) and basis for the parameter(s) monitored under §63.1258.

(B) Emission estimation equations. An owner or operator using a condenser as a control device shall determine controlled emissions using exhaust gas temperature measurements and calculations for each batch emission episode within each unit operation according to the engineering methodology in paragraphs (d)(3)(i)(B)(1) through (8) of this section. Individual HAP partial pressures shall be calculated as specified in paragraph (d)(2)(i) of this section.

(1) Emissions from vapor displacement shall be calculated using Equation 11 of this subpart with T set equal to the temperature of the receiver and
the HAP partial pressures determined at the temperature of the receiver.

(2) Emissions from purging shall be calculated using Equation 12 of this subpart with $T$ set equal to the temperature of the receiver and the HAP partial pressures determined at the temperature of the receiver.

(3) Emissions from heating shall be calculated using either Equation 13 of this subpart or Equation 37 of this subpart. In Equation 13, the HAP vapor pressures shall be determined at the temperature of the receiver. In Equations 13 and 37 of this subpart, $\Delta \eta$ is equal to the number of moles of noncondensable displaced from the vessel, as calculated using Equation 15 of this subpart. In Equations 13 and 37 of this subpart, the HAP average molecular weight shall be calculated using Equation 17 with the HAP partial pressures determined at the temperature of the receiver.

(4)(i) Emissions from depressurization shall be calculated using Equation 38 of this subpart.

\[
E = (V_{nc1} - V_{nc2}) \times \frac{\sum_{i=1}^{n} (P_i)}{P_T - \sum_{j=1}^{m} (P_j)} \times \frac{P_T}{RT} \times MW_{HAP} \quad \text{(Eq. 38)}
\]

Where:
- $E$ = mass of HAP vapor emitted
- $V_{nc1}$ = initial volume of noncondensable in the vessel, corrected to the final pressure, as calculated using Equation 39 of this subpart
- $V_{nc2}$ = final volume of noncondensable in the vessel, as calculated using Equation 40 of this subpart
- $P_i$ = partial pressure of each individual HAP at the receiver temperature
- $P_j$ = partial pressure of each condensable (including HAP) at the receiver temperature
- $P_T$ = receiver pressure
- $T$ = temperature of the receiver
- $R$ = ideal gas law constant
- $MW_{HAP}$ = the average molecular weight of HAP calculated using Equation 17 of this subpart with partial pressures determined at the receiver temperature
- $i$ = identifier for a HAP compound
- $n$ = number of HAP compounds in the emission stream
- $m$ = number of condensable compounds (including HAP) in the emission stream
- $j$ = identifier for a condensable compound
(ii) The initial and final volumes of noncondensable gas present in the vessel, adjusted to the pressure of the receiver, are calculated using Equations 39 and 40 of this subpart.

\[
V_{nc1} = \frac{V P_{nc1}}{P_T} \quad \text{(Eq. 39)}
\]

\[
V_{nc2} = \frac{V P_{nc2}}{P_T} \quad \text{(Eq. 40)}
\]

Where:

- \(V_{nc1}\) = initial volume of noncondensable gas in the vessel
- \(V_{nc2}\) = final volume of noncondensable gas in the vessel
- \(V\) = free volume in the vessel being depressurized
- \(P_{nc1}\) = initial partial pressure of the noncondensable gas, as calculated using Equation 41 of this subpart
- \(P_{nc2}\) = final partial pressure of the noncondensable gas, as calculated using Equation 42 of this subpart
- \(P_T\) = pressure of the receiver

(iii) Initial and final partial pressures of the noncondensable gas in the vessel are determined using Equations 41 and 42 of this subpart.

\[
P_{nc1} = P_1 - \sum_{j=1}^{m} P_j \quad \text{(Eq. 41)}
\]

\[
P_{nc2} = P_2 - \sum_{j=1}^{m} P_j \quad \text{(Eq. 42)}
\]

Where:

- \(P_{nc1}\) = initial partial pressure of the noncondensable gas in the vessel
- \(P_{nc2}\) = final partial pressure of the noncondensable gas in the vessel
- \(P_1\) = initial vessel pressure
- \(P_2\) = final vessel pressure
- \(P_j\) = partial pressure of each condensable compound (including HAP) in the vessel
- \(m\) = number of condensable compounds (including HAP) in the emission stream
- \(j\) = identifier for a condensable compound

(5) Emissions from vacuum systems shall be calculated using Equation 33 of this subpart.

(6) Emissions from gas evolution shall be calculated using Equation 12 with \(V\) calculated using Equation 34 of this subpart, \(T\) set equal to the receiver temperature, and the HAP partial pressures determined at the receiver temperature. The term for time, \(t\), in Equation 12 of this subpart is not needed for the purposes of this calculation.

(7) Emissions from air drying shall be calculated using Equation 11 of this subpart with \(V\) equal to the air flow rate and \(P\), determined at the receiver temperature.

(8) Emissions from empty vessel purging shall be calculated using equation 43 of this subpart:

\[
E = \frac{V}{R} \left[ \frac{\sum_{i=1}^{n} (P_i)_{T1} (MW_i)}{T_1} \right] \left[ -e^{-R/V} \right] \left[ \sum_{i=1}^{n} \frac{(P_i)_{T1} (MW_i)}{T_2} \right] \left[ \ln \left( \frac{\sum_{i=1}^{n} (P_i)_{T2}}{\sum_{i=1}^{n} (P_i)_{T1}} + 1 \right) \right] \quad \text{(Eq. 43)}
\]

Where:

- \(V\) = volume of empty vessel
- \(R\) = ideal gas law constant
- \(T_1\) = temperature of the vessel vapor space at beginning of purge
- \(T_2\) = temperature of the receiver, absolute
- \((P_i)_{T1}\) = partial pressure of the individual HAP at the beginning of the purge
- \((P_i)_{T2}\) = partial pressure of the individual HAP at the receiver temperature
MW\textsubscript{i} = molecular weight of the individual HAP

F = flowrate of the purge gas

t = duration of the purge

n = number of HAP compounds in the emission stream

i = identifier for a HAP compound

(ii) Large control devices. Except for condensers, controlled emissions for each process vent that is controlled using a large control device shall be determined by applying the control efficiency of the large control device to the estimated uncontrolled emissions. The control efficiency shall be determined by conducting a performance test on the control device as described in paragraphs (d)(3)(ii)(A) through (C) of this section, or by using the results of a previous performance test as described in paragraph (d)(4) of this section. If the control device is intended to control only hydrogen halides and halogens, the owner or operator may assume the control efficiency of organic HAP is zero percent. If the control device is intended to control only organic HAP, the owner or operator may assume the control efficiency for hydrogen halides and halogen is zero percent. Owners and operators are not required to conduct performance tests for devices described in paragraphs (a)(4) and (d)(4) of this section that are large control devices, as defined in §63.1251.

(A) The performance test shall be conducted by performing emission testing on the inlet and outlet, or, if complying with the provisions of §63.1254(c), on the outlet of the control device, following the test methods and procedures of §63.1257(b). Concentrations shall be calculated from the data obtained through emission testing according to the procedures in paragraph (a)(2) of this section. If the control device is a combustion device that uses supplemental combustion air, the concentrations shall be corrected to 3 percent oxygen according to the procedures in paragraph (a)(3) of this section.

(B) Performance testing shall be conducted under absolute, or hypothetical worst-case conditions, as defined in paragraphs (b)(8)(i)(A) through (B) of this section.

(C) The owner or operator may elect to conduct more than one performance test on the control device for the purpose of establishing more than one operating condition at which the control device achieves the required control efficiency.

(4) An owner or operator is not required to conduct a performance test for the following:

(i) Any control device for which a previous performance test was conducted, provided the test was conducted using the same procedures specified in §63.1257(b) over conditions typical of the appropriate worst-case, as defined in §63.1257(b)(8)(i). The results of the previous performance test shall be used to demonstrate compliance.

(e) Compliance with wastewater provisions. (1) Determining annual average concentration and annual load. To determine the annual average concentration and annual load of partially soluble and/or soluble HAP compounds in a wastewater stream, as required by §63.1256(a)(1), an owner or operator shall comply with the provisions in paragraphs (e)(1)(i) through (iii) of this section. A wastewater stream is exempt from the requirements of §63.1256(a)(2) if the owner or operator determines the annual average concentration and annual load are below all of the applicability cutoffs specified in §63.1256(a)(1)(i) through (iii) of this section. For annual average concentration, only initial rinses are included. Concentration measurements based on Method 305 may not be adjusted by the compound-specific F\textsubscript{m} factor listed in Table 8 of this subpart. Concentration measurements based on methods other than Method 305 shall be adjusted by dividing each concentration by the compound-specific F\textsubscript{m} factor listed in Table 8 of this subpart.

(i) Annual average concentration definition. (A) When complying with §63.1256(a)(1)(i)(A), the annual average concentration means the total mass of partially soluble HAP compounds occurring in the wastewater stream during the calendar year divided by the total mass of the wastewater stream discharged during the same calendar year.

(B) When complying with §63.1256(a)(1)(ii) (B) or (C), the annual
average concentration means the total mass of partially soluble and/or soluble HAP compounds occurring in the wastewater stream during the calendar year divided by the total mass of the wastewater stream discharged during the same calendar year.

(C) When complying with §63.1256(a)(1)(i)(D), the annual average concentration means the total mass of soluble HAP compounds occurring in the wastewater stream during the calendar year divided by the total mass of the wastewater stream discharged during the same calendar year.

(ii) Determination of annual average concentration. An owner or operator shall determine annual average concentrations of partially soluble and/or soluble HAP compounds in accordance with the provisions specified in paragraph (e)(1)(i)(A), (B), or (C) of this section. The owner or operator may determine annual average concentrations by process simulation. Data and other information supporting the simulation shall be reported in the Precompliance Report for approval by the Administrator. The annual average concentration shall be determined either at the POD or downstream of the POD with adjustment for concentration changes made according to paragraph (e)(1)(i)(D) of this section.

(A) Test methods. The concentration of partially soluble HAP, soluble HAP, or total HAP shall be measured using any of the methods described in paragraphs (b)(10)(i) through (iv) of this section.

(B) Knowledge of the wastewater stream. The concentration of partially soluble HAP, soluble HAP, or total HAP shall be calculated based on knowledge of the wastewater stream according to the procedures in paragraphs (e)(1)(i)(B)(1) and (2) of this section. The owner or operator shall document concentrations in the Notification of Compliance Status report described in §63.1260(f).

(1) Mass balance. The owner or operator shall calculate the concentrations of HAP compounds in wastewater considering the total quantity of HAP discharged to the water, the amount of water at the POD, and the amounts of water and HAP lost to other mechanisms such as reactions, air emissions, or uptake in product or other processing materials. The quantities of HAP and water shall be based on batch sheets, manufacturing tickets, or FDA bills of materials. In cases where a chemical reaction occurs that generates or consumes HAP, the amount of HAP remaining after a reaction shall be based on stoichiometry assuming 100 percent theoretical consumption or yield, as applicable.

(2) Published water solubility data. For single components in water, owners and operators may use the water solubilities published in standard reference texts at the POD temperature to determine maximum HAP concentrations. The owner or operator shall also provide documentation describing the testing protocol, and the means by which sample variability and analytical variability were accounted for in the determination of HAP concentrations. Documentation of the bench-scale or pilot-scale test concentration data are representative of actual HAP concentrations.

(C) Bench scale or pilot-scale test data. The concentration of partially soluble HAP, soluble HAP, or total HAP shall be calculated based on bench scale or pilot-scale test data. The owner or operator shall provide sufficient information to demonstrate that the bench-scale or pilot-scale test concentration data are representative of actual HAP concentrations.
on knowledge of the wastewater stream in accordance with paragraphs (e)(1)(ii)(B) of this section. The owner or operator shall maintain records of the total liters of wastewater discharged per year as specified in §63.1259(b).

(2) Compliance with treatment unit control provisions. (i) Performance tests and design evaluations-general. To comply with the control options in §63.1256(g)(10) or (13), neither a design evaluation nor a performance test is required. For any other nonbiological treatment process, the owner or operator shall conduct either a design evaluation as specified in paragraph (e)(2)(ii) of this section, or a performance test as specified in paragraph (e)(2)(iii) of this section to demonstrate that each nonbiological treatment process used to comply with §63.1256(g)(8), (9), and/or (12) achieves the conditions specified for compliance. The owner or operator shall demonstrate by the procedures in either paragraph (e)(2) (ii) or (iii) of this section that each closed biological treatment process used to comply with §63.1256(g)(8), (9), and/or (12) achieves the conditions specified for compliance. If an open biological treatment unit is used to comply with §63.1256(g)(8), (9), and/or (12), the owner or operator shall comply with the performance test requirements in paragraph (e)(2)(iii)(A) of this section.

(ii) Design evaluation. A design evaluation and supporting documentation that addresses the operating characteristics of the treatment process and that is based on operation at a wastewater stream flow rate and a concentration under which it would be most difficult to demonstrate compliance. For closed biological treatment processes, the percent reduction from removal/destruction in the treatment unit and control device shall be determined by a mass balance over the unit. The mass flow rate entering the treatment process minus the mass flow rate exiting the process determines the actual mass removal. Compounds that meet the requirements specified in paragraph (e)(2)(iii)(A)(4) of this section are not required to be included in the design evaluation; the term “performance test” in paragraph (e)(2)(iii)(A)(4) of this section shall mean “design evaluation” for the purposes of this paragraph.

(iii) Performance tests. Performance tests shall be conducted using test methods and procedures that meet the applicable requirements specified in paragraphs (e)(2)(iii)(A) through (G) of this section.

(A) General. This paragraph specifies the general procedures for performance tests that are conducted to demonstrate compliance of a treatment process with the control requirements specified in §63.1256(g).

(1) Representative process unit operating conditions. Compliance shall be demonstrated for representative operating conditions. Operations during periods of malfunction and periods of nonoperation shall not constitute representative conditions. The owner or operator shall record the process information that is necessary to document operating conditions during the test.

(ii) Range of operating conditions. If the treatment process is operating at several different sets of representative operating conditions, the owner or operator shall comply with paragraphs (e)(2)(iii)(A)(2)(i) and (ii) of this section. The owner or operator shall record information that is necessary to document treatment process or control device operating conditions during the test.

(i) Range of operating conditions. If the treatment process will be operating at several different sets of representative operating conditions, performance testing over the entire range is not required. In such cases, the performance test results shall be supplemented with modeling and/or engineering assessments to demonstrate performance over the operating range.
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(ii) Consideration of residence time. If concentration and/or flow rate to the treatment process are not relatively constant (i.e., comparison of inlet and outlet data will not be representative of performance), the owner or operator shall consider residence time, when determining concentration and flow rate.

(3) Testing equipment. All testing equipment shall be prepared and installed as specified in the applicable test methods, or as approved by the Administrator.

(4) Compounds not required to be considered in performance tests. Compounds that meet the requirements specified in (e)(2)(iii)(A)(4)(i), (ii), or (iii) of this section are not required to be included in the performance test. Concentration measurements based on Method 305 shall be adjusted by dividing each concentration by the compound-specific Fm factor listed in Table 8 of this subpart. Concentration measurements based on methods other than Method 305 shall not be adjusted by the compound-specific Fm factor listed in Table 8 of this subpart.

(i) Compounds not used or produced by the PMPU; or

(ii) Compounds with concentrations at the POD that are below 1 ppm; or

(iii) Compounds with concentrations at the POD that are below the lower detection limit where the lower detection limit is greater than 1 ppm. The method shall be an analytical method for wastewater which has the compound of interest as a target analyte.

(5) Treatment using a series of treatment processes. In all cases where the wastewater provisions in this subpart allow or require the use of a treatment process to comply with emissions limitations, the owner or operator may use multiple treatment processes. The owner or operator complying with the requirements of §63.1256(g)(7)(i), when wastewater is conveyed by hard-piping, shall comply with either paragraph (e)(2)(iii)(A)(5)(i) or (ii) of this section. The owner or operator complying with the requirements of §63.1256(g)(7)(ii) shall comply with the requirements of paragraph (e)(2)(iii)(A)(5)(i) of this section.

(i) The owner or operator shall conduct the performance test across each series of treatment processes. For each series of treatment processes, inlet concentration and flow rate shall be measured either where the wastewater enters the first treatment process in a series of treatment processes, or prior to the first treatment process as specified in paragraph (e)(2)(iii)(A)(6) of this section. For each series of treatment processes, outlet concentration and flow rate shall be measured where the wastewater exits the last treatment process in the series of treatment processes, except when the last treatment process is an open or a closed aerobic biological treatment process demonstrating compliance by using the procedures in paragraphs (e)(2)(iii)(E) or (F) of this section. When the last treatment process is either an open or a closed aerobic biological treatment process demonstrating compliance by using the procedures in paragraphs (e)(2)(iii)(E) or (F) of this section, mass flow rate is measured at the inlet and outlet to the series of treatment processes prior to the biological treatment process and at the outlet to the biological treatment process, except as provided in paragraph (e)(2)(iii)(A)(6)(ii) of this section. The mass flow rate destroyed in the biological treatment process for which compliance is demonstrated using paragraphs (e)(2)(iii)(E) or (F) of this section shall be added to the mass flow rate removed or destroyed in the series of treatment units before the biological treatment unit. This sum shall be used to calculate the overall control efficiency.

(ii) The owner or operator shall conduct the performance test across each treatment process in the series of treatment processes. The mass flow rate removed or destroyed by each treatment process shall be added together and the overall control efficiency calculated to determine whether compliance has been demonstrated using paragraphs (e)(2)(iii)(C), (D), (E), (F), or (G) of this section, as applicable. If a biological treatment process is one of the treatment processes in the series of treatment processes, the inlet to the biological treatment process shall be the point at which the wastewater enters the biological treatment process, or the inlet to the equalization tank if
all the criteria of paragraph (e)(2)(iii)(A)(6)(ii) of this section are met.

(6) The owner or operator determining the inlet for purposes of demonstrating compliance with paragraph (e)(2)(iii)(E), or (F) of this section may elect to comply with paragraph (e)(2)(iii)(A)(6)(i) or (ii) of this section.

(i) When wastewater is conveyed exclusively by hard-piping from the point of determination to a treatment process that is either the only treatment process or the first in a series of treatment processes (i.e., no treatment processes or other waste management units are used upstream of this treatment process to store, handle, or convey the wastewater), the inlet to the treatment process shall be at any location from the point of determination to where the wastewater stream enters the treatment process. When samples are taken upstream of the treatment process and before wastewater streams have converged, the owner or operator shall ensure that the mass flow rate of all affected wastewater is accounted for when using §63.1256(g)(9)(ii) or (12) to comply and that the mass flow rate of all wastewater, not just affected wastewater is accounted for when using §63.1256(g)(11) to comply, except as provided in paragraph (e)(2)(iii)(A)(4) of this section.

(ii) The owner or operator may consider the inlet to the equalization tank as the inlet to the biological treatment process if the wastewater is conveyed by hard-piping from either the last previous treatment process or the point of determination to the equalization tank; or the wastewater is conveyed from the equalization tank exclusively by hard-piping to the biological treatment process and no treatment processes or other waste management units are used to store, handle, or convey the wastewater between the equalization tank and the biological treatment process; or the equalization tank is equipped with a fixed roof and a closed-vent system that routes emissions to a control device that meets the requirements of §63.1256(b)(1)(i) through (iv) and §63.1256(b)(2)(i). The outlet from the series of treatment processes prior to the biological treatment process is the point at which the wastewater exits the last treatment process in the series prior to the equalization tank, if the equalization tank and biological treatment process are part of a series of treatment processes. The owner or operator shall ensure that the mass flow rate of all affected wastewater is accounted for when using §63.1256(g)(9)(ii) or (12) to comply and that the mass flow rate of all wastewater, not just affected wastewater is accounted for when using §63.1256(g)(11) to comply, except as provided in paragraph (e)(2)(iii)(A)(4) of this section.

(B) Noncombustion treatment process—concentration limits. This paragraph applies to performance tests that are conducted to demonstrate compliance of a noncombustion treatment process with the ppmw wastewater stream concentration limits at the outlet of the treatment process. This compliance option is specified in §63.1256(g)(8)(i) and (9)(i). Wastewater samples shall be collected using sampling procedures which minimize loss of organic compounds during sample collection and analysis and maintain sample integrity per paragraph (b)(10)(iii) of this section. Samples shall be collected and analyzed using the procedures specified in paragraphs (b)(10)(i), (ii), and (iii) of this section. Samples may be grab samples or composite samples. Samples shall be taken at approximately equally spaced time intervals over a 1-hour period. Each 1-hour period constitutes a run, and the performance test shall consist of a minimum of three runs. Concentration measurements based on methods other than Method 305 may be adjusted by multiplying each concentration by the compound-specific Fm factor listed in Table 8 of this subpart. (For affected wastewater streams that contains both partially soluble and soluble HAP compounds, compliance is demonstrated only if the sum of the concentrations of partially soluble HAP compounds is less than 50 ppmw, and the sum of the concentrations of soluble HAP compounds is less than 520 ppmw.)

(C) Noncombustion, nonbiological treatment process: percent mass removal/destruction option. This paragraph applies to performance tests that are conducted to demonstrate compliance of a
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noncombustion, nonbiological treatment process with the percent mass removal limits specified in §63.1256(g)(8)(ii) and (9)(ii) for partially soluble and soluble HAP compounds, respectively. The owner or operator shall comply with the requirements specified in paragraphs (e)(2)(iii)(C)(1) through (5) of this section.

(1) Concentration. The concentration of partially soluble and/or soluble HAP compounds entering and exiting the treatment process shall be determined as provided in this paragraph. Wastewater samples shall be collected using sampling procedures which minimize loss of organic compounds during sample collection and analysis and maintain sample integrity per paragraph (b)(10)(v) of this section. The method shall be an analytical method for wastewater which has the compound of interest as a target analyte. Samples may be grab samples or composite samples. Samples shall be taken at approximately equally spaced time intervals over a 1-hour period. Each 1-hour period constitutes a run, and the performance test shall consist of a minimum of three runs. Concentration measurements based on Method 305 shall be adjusted by dividing each concentration by the compound-specific Fm factor listed in Table 8 of this subpart. Concentration measurements based on methods other than Method 305 shall not be adjusted by the compound-specific Fm factor listed in Table 8 of this subpart.

(2) Flow rate. The flow rate of the entering and exiting wastewater streams shall be determined using inlet and outlet flow meters, respectively. Where the outlet flow is not greater than the inlet flow, a single flow meter may be used, and may be used at either the inlet or outlet. Flow rate measurements shall be taken at the same time as the concentration measurements.

(3) Calculation of mass flow rate—for noncombustion, nonbiological treatment processes. The mass flow rates of partially soluble and/or soluble HAP compounds entering and exiting the treatment process are calculated using Equations 44 and 45 of this subpart.

\[
\begin{align*}
Q_{MW_a} &= \frac{\rho}{p \times 10^6} \left( \sum_{k=1}^{p} Q_{a,k} \times C_{T,a,k} \right) \quad \text{(Eq. 44)} \\
Q_{MW_b} &= \frac{\rho}{p \times 10^6} \left( \sum_{k=1}^{p} Q_{b,k} \times C_{T,b,k} \right) \quad \text{(Eq. 45)}
\end{align*}
\]

Where:

\(Q_{MW_a}, Q_{MW_b}\) = mass flow rate of partially soluble or soluble HAP compounds, average of all runs, in wastewater entering (\(Q_{MW_a}\)) or exiting (\(Q_{MW_b}\)) the treatment process, kg/hr

\(\rho\) = density of the wastewater, kg/m³

\(Q_{a,k}, Q_{b,k}\) = volumetric flow rate of wastewater entering \((Q_{a,k})\) or exiting \((Q_{b,k})\) the treatment process during each run \(k\), m³/hr

\(C_{T,a,k}, C_{T,b,k}\) = total concentration of partially soluble or soluble HAP compounds in wastewater entering \((C_{T,a,k})\) or exiting \((C_{T,b,k})\) the treatment process during each run \(k\), ppmw

\(p\) = number of runs

\(k\) = identifier for a run

\(10^6\) = conversion factor, mg/kg

(4) Percent removal calculation for mass flow rate. The percent mass removal across the treatment process shall be calculated as follows:

\[
E = \frac{Q_{MW_a} - Q_{MW_b}}{Q_{MW_a}} \times 100 \quad \text{(Eq. 46)}
\]

Where:

\(E\) = removal or destruction efficiency of the treatment process, percent

\(Q_{MW_a}\), \(Q_{MW_b}\) = mass flow rate of partially soluble or soluble HAP compounds in wastewater entering \((Q_{MW_a})\) and exiting \((Q_{MW_b})\) the
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(5) Compare mass removal efficiency to required efficiency. Compare the mass removal efficiency (calculated in Equation 44 of this subpart) to the required efficiency as specified in §63.1256(g)(8)(ii) or (9)(ii). If complying with §63.1256(g)(8)(ii), compliance is demonstrated if the mass removal efficiency is 99 percent or greater. If complying with §63.1256(g)(9)(ii), compliance is demonstrated if the mass removal efficiency is 90 percent or greater.

(D) Combustion treatment processes: percent mass removal/destruction option. This paragraph applies to performance tests that are conducted to demonstrate compliance of a combustion treatment process with the percent mass destruction limits specified in §63.1256(g)(8)(ii) for partially soluble HAP compounds, and/or §63.1256(g)(9)(ii) for soluble HAP compounds. The owner or operator shall comply with the requirements specified in paragraphs (e)(2)(iii)(D)(1) through (8) of this section.

(1) Concentration in wastewater stream entering the combustion treatment process. The concentration of partially soluble and/or soluble HAP compounds entering the treatment process shall be determined as provided in this paragraph. Wastewater samples shall be collected using sampling procedures which minimize loss of organic compounds during sample collection and analysis and maintain sample integrity per paragraph (b)(10)(v) of this section. The method shall be an analytical method for wastewater which has the compound of interest as a target analyte. Samples may be grab samples or composite samples. Samples shall be taken at approximately equally spaced time intervals over a 1-hour period. Each 1-hour period constitutes a run, and the performance test shall consist of a minimum of three runs. Concentration measurements based on Method 305 of appendix A of this part shall be adjusted by dividing each concentration by the compound-specific Fm factor listed in Table 8 of this subpart. Concentration measurements based on methods other than Method 305 shall not be adjusted by the compound-specific Fm factor listed in Table 8 of this subpart.

(2) Flow rate of wastewater entering the combustion treatment process. The flow rate of the wastewater stream entering the combustion treatment process shall be determined using an inlet flow meter. Flow rate measurements shall be taken at the same time as the concentration measurements.

(3) Calculation of mass flow rate in wastewater stream entering combustion treatment processes. The mass flow rate of partially soluble and/or soluble HAP compounds entering the treatment process is calculated as follows:

\[ Q_{MW_a} = \frac{\rho}{\rho_m} \left( \sum_{k=1}^{\rho} Q_{a,k} \ast C_{T,a,k} \right) \]  

(Eq. 47)

Where:

- \( Q_{MW_a} \) = mass flow rate of partially soluble or soluble HAP compounds entering the combustion unit, kg/hr
- \( \rho \) = number of runs
- \( \rho_m \) = density of the wastewater stream, kg/m³
- \( Q_{a,k} \) = volumetric flow rate of wastewater entering the combustion unit during run k, m³/hr
- \( C_{T,a,k} \) = total concentration of partially soluble or soluble HAP compounds in the wastewater stream entering the combustion unit during run k, ppmw

(4) Concentration in vented gas stream exiting the combustion treatment process. The concentration of partially soluble and/or soluble HAP compounds (or TOC) exiting the combustion treatment process in any vented gas stream shall be determined as provided in this section.
Samples may be grab samples or composite samples. Samples shall be taken at approximately equally spaced time intervals over a 1-hour period. Each 1-hour period constitutes a run, and the performance test shall consist of a minimum of three runs. Concentration measurements shall be determined using Method 18 of 40 CFR part 60, appendix A, as appropriate. Volumetric flow rate measurements shall be taken at the same time as the concentration measurements.

(6) Volumetric flow rate of vented gas stream exiting combustion treatment processes. The mass flow rate of partially soluble and/or soluble HAP compounds in a vented gas stream exiting the combustion treatment process shall be calculated as follows:

\[ QMG_b = K_2 \times \left( \sum_{i=1}^{n} \left( CG_{b,i} \times MW_i \right) \right) \times QG_b \]  
\[ \text{Eq. 48} \]

where:

- \( QMG_b \) = mass rate of TOC (minus methane and ethane) or total partially soluble and/or soluble HAP, in vented gas stream, exiting (QMG), the combustion device, dry basis, kg/hr
- \( CG_{b,i} \) = concentration of TOC (minus methane and ethane) or total partially soluble and/or soluble HAP, in vented gas stream, exiting (CG), the combustion device, dry basis, ppmv
- \( MW_i \) = molecular weight of a component, kilogram/kilogram-mole
- \( QG_b \) = flow rate of gas stream exiting the combustion device, dry standard cubic meters per hour
- \( K_2 \) = constant, \( 41.57 \times 10^{-9} \) (parts per million)\(^{-1}\) (gram-mole per standard cubic meter) (kilogram/gram), where standard temperature (gram-mole per standard cubic meter) is 20°C
- \( i \) = identifier for a compound
- \( n \) = number of components in the sample

(7) Destruction efficiency calculation. The destruction efficiency of the combustion unit for partially soluble and/or soluble HAP compounds shall be calculated as follows:

\[ E = \frac{QMW_a - QMG_b}{QMW_a} \times 100 \]  
\[ \text{Eq. 49} \]

Where:

- \( E \) = destruction efficiency of partially soluble or soluble HAP compounds for the combustion unit, percent
- \( QMW_a \) = mass flow rate of partially soluble or soluble HAP compounds entering the combustion unit, kg/hr
- \( QMG_b \) = mass flow rate of TOC (minus methane and ethane) or partially soluble and/or soluble HAP compounds in vented gas stream exiting the combustion treatment process, kg/hr

(8) Compare mass destruction efficiency to required efficiency. Compare the mass destruction efficiency (calculated in Equation 49 of this subpart) to the required efficiency as specified in §63.1256(g)(8)(ii) or (g)(9)(ii). If complying with §63.1256(g)(8)(ii), compliance is demonstrated if the mass destruction efficiency is 99 percent or greater. If complying with §63.1256(g)(9)(ii), compliance is demonstrated if the mass destruction efficiency is 90 percent or greater.

(E) Open or closed aerobic biological treatment processes: 95-percent mass destruction option. This paragraph applies
to performance tests that are conducted for open or closed aerobic biological treatment processes to demonstrate compliance with the 95-percent mass destruction provisions in §63.1256(g)(11) for partially soluble and/or soluble HAP compounds.

(1) Concentration in wastewater stream. The concentration of partially soluble and/or soluble HAP as provided in this paragraph. Concentration measurements to determine E shall be taken as provided in paragraph (e)(2)(iii)(A)(5) of this section for a series of treatment processes. Wastewater samples shall be collected using sampling procedures which minimize loss of organic compounds during sample collection and analysis and maintain sample integrity per paragraph (b)(10)(v) of this section. The method shall be an analytical method for wastewater which has the compound of interest as a target analyte. Samples may be grab samples or composite samples. Samples shall be taken at approximately equally spaced time intervals over a 1-hour period. Each 1-hour period constitutes a run, and the performance test shall consist of a minimum of three runs. Concentration measurements based on Method 305 shall be adjusted by dividing each concentration by the compound-specific Fm factor listed in Table 8 of this subpart. Concentration measurements based on methods other than Method 305 shall not be adjusted by the compound-specific Fm factor listed in Table 8 of this subpart.

(2) Flow rate. Flow rate measurements to determine E shall be taken as provided in paragraph (e)(2)(iii)(A)(5) of this section for a series of treatment processes. Flow rate shall be determined using inlet and outlet flow measurement devices. Where the outlet flow is not greater than the inlet flow, a single flow measurement device may be used, and may be used at either the inlet or outlet. Flow rate measurements shall be taken at the same time as the concentration measurements.

(3) Destruction efficiency. The owner or operator shall comply with the provisions in either paragraph (e)(2)(iii)(E)(3)(i), (ii) or (iii) of this section. Compliance is demonstrated if the destruction efficiency, E, is equal to or greater than 95 percent.

(i) If the performance test is performed across the open or closed biological treatment system only, compliance is demonstrated if E is equal to $F_{bio}$, where E is the destruction efficiency of partially soluble and/or soluble HAP compounds and $F_{bio}$ is the site-specific fraction of partially soluble and/or soluble HAP compounds biodegraded. $F_{bio}$ shall be determined as specified in paragraph (e)(2)(iii)(E)(4) of this section and appendix C of subpart G of this part.

(ii) If compliance is being demonstrated in accordance with paragraphs (e)(2)(iii)(A)(5)(i) or (ii) of this section, the removal efficiency shall be calculated using Equation 49 of this subpart. When complying with paragraph (e)(2)(iii)(A)(5)(ii) of this section, each nonbiological treatment process is a treatment process segment. When complying with paragraph (e)(2)(iii)(A)(5)(iii) of this section, the series of nonbiological treatment processes comprise one treatment process segment.

\[
E = \frac{\text{Nonbiotreatment HAP load removal} + \text{Biotreatment HAP load removal}}{\text{Total influent HAP load}} = \frac{\sum_{i=1}^{n} (QMW_{a,i} - QMW_{b,i}) + QMW_{bio} + F_{bio}}{QMW_{all}} \quad \text{(Eq. 50)}
\]

Where:

- $QMW_{a,i}$ = the soluble and/or partially soluble HAP load entering a treatment process segment
- $QMW_{b,i}$ = the soluble and/or partially soluble HAP load exiting a treatment process segment
- $n$ = the number of treatment process segments
- i = identifier for a treatment process element
- $QMW_{bio}$ = the inlet load of soluble and/or partially soluble HAP to the biological treatment process. The inlet is defined in accordance with
paragraph (e)(2)(iii)(A)(6) of this section. If complying with paragraph (e)(2)(iii)(A)(6)(ii) of this section, QMW\textsubscript{bio} is equal to QMW\textsubscript{all}.

\( F_{\text{bio}} \) = site-specific fraction of soluble and/or partially soluble HAP compounds biodegraded. \( F_{\text{bio}} \) shall be determined as specified in paragraph (e)(2)(iii)(E)(4) of this section and Appendix C of subpart G of this part.

QMW\textsubscript{all} = the total soluble and/or partially soluble HAP load to be treated.

(4) Site-specific fraction biodegraded (\( F_{\text{bio}} \)). The procedures used to determine the compound-specific kinetic parameters for use in calculating \( F_{\text{bio}} \) differ for the compounds listed in Tables 2 and 3 of this subpart. An owner or operator shall calculate \( F_{\text{bio}} \) as specified in either paragraph (e)(2)(iii)(E)(4)(i) or (ii) of this section.

(i) For biological treatment processes that do not meet the definition of “enhanced biological treatment in §63.1251, the owner or operator shall determine the \( F_{\text{bio}} \) for the compounds in Tables 2 and 3 of this subpart using any of the procedures in appendix C to part 63, except procedure 3 (inlet and outlet concentration measurements). (The symbol “\( F_{\text{bio}} \)” represents the site-specific fraction of an individual partially soluble or soluble HAP compound that is biodegraded.)

(ii) If the biological treatment process meets the definition of “enhanced biological treatment process” in §63.1251, the owner or operator shall determine \( F_{\text{bio}} \) for the compounds in Table 2 of this subpart using any of the procedures specified in appendix C to part 63. The owner or operator shall calculate \( F_{\text{bio}} \) for the compounds in Table 3 of this subpart using the defaults for first order biodegradation rate constants (\( K_{\text{f}} \)) in Table 9 of this subpart and follow the procedure explained in Form III of appendix C, 40 CFR part 63, or any of the procedures specified in appendix C of 40 CFR part 63.

(F) Open or closed aerobic biological treatment processes: percent removal for partially soluble or soluble HAP compounds. This paragraph applies to the use of performance tests that are conducted for open or closed aerobic biological treatment processes to demonstrate compliance with the percent removal provisions for either partially soluble HAP compounds in §63.1256(g)(8)(ii) or soluble HAP compounds in §63.1256(g)(9)(ii) or (g)(12). The owner or operator shall comply with the provisions in paragraph (e)(2)(iii)(E) of this section, except that compliance with §63.1256(g)(8)(ii) shall be demonstrated when \( E \) is equal to or greater than 99 percent, compliance with §63.1256(g)(9)(ii) shall be demonstrated when \( E \) is equal to or greater than 90 percent, and compliance with §63.1256(g)(12) shall be demonstrated when \( E \) is equal to or greater than 99 percent.

(G) Closed biological treatment processes: percent mass removal option. This paragraph applies to the use of performance tests that are conducted for closed biological treatment processes to demonstrate compliance with the percent removal provisions in §§63.1256(g)(8)(ii), (g)(9)(ii), (g)(11), or (g)(12). The owner or operator shall comply with the requirements specified in paragraphs (e)(2)(iii)(G)(1) through (4) of this section.

(1) Comply with the procedures specified in paragraphs (e)(2)(iii)(C)(1) through (3) of this section to determine characteristics of the wastewater entering the biological treatment unit, except that the term “partially soluble and/or soluble HAP” shall mean “soluble HAP” for the purposes of this section if the owner or operator is complying with §63.1256(g)(9)(ii) or (g)(12), and it shall mean “partially soluble HAP” if the owner or operator is complying with §63.1256(g)(8)(ii).

(2) Comply with the procedures specified in paragraphs (e)(2)(iii)(D)(4) through (6) of this section to determine the characteristics of gas vent streams exiting a control device, with the differences noted in paragraphs (e)(2)(iii)(G)(3)(i) and (ii) of this section.

(i) The term “partially soluble and/or soluble HAP” shall mean “soluble HAP” for the purposes of this section if the owner or operator is complying with §63.1256(g)(9)(ii) or (g)(12), and it shall mean “partially soluble HAP” if the owner or operator is complying with §63.1256(g)(8)(ii).
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(ii) The term "combustion treatment process" shall mean "control device" for the purposes of this section.

(3) Percent removal/destruction calculation. The percent removal and destruction across the treatment unit and any control device(s) shall be calculated using Equation 51 of this subpart:

$$E = \frac{QMW_a - (QMW_b + QMG_b)}{QMW_a}$$  \hspace{1cm} \text{(Eq. 51)}

Where:

\(E\) = removal and destruction efficiency of the treatment unit and control device(s), percent

\(QMW_a\), \(QMW_b\) = mass flow rate of partially soluble or soluble HAP compounds in wastewater entering (\(QMW_a\)) and exiting (\(QMW_b\)) the treatment process, kilograms per hour (as calculated using Equations WW1 and WW2)

\(QMG_b\) = mass flow rate of partially soluble or soluble HAP compounds in vented gas stream exiting the combustion treatment process, kg/hr

(4) Compare mass removal/destruction efficiency to required efficiency. Compare the mass removal/destruction efficiency (calculated using Equation 51 of this subpart) to the required efficiency as specified in §63.1256(h)(2). If complying with the 95-percent reduction efficiency requirement, comply with the requirements specified in paragraphs (e)(3)(ii) (A) through (J) of this section.

(i) Performance test for control devices other than flares. This paragraph applies to performance tests that are conducted to demonstrate compliance of a control device with the efficiency limits specified in §63.1256(h)(2). If complying with the 95-percent reduction efficiency requirement, comply with the requirements specified in paragraphs (e)(3)(ii) (A) through (J) of this section.

(A) General. The owner or operator shall comply with the general performance test provisions in paragraphs (e)(2)(iii)(A) through (G) of this section, except that the term "treatment unit" shall mean "control device" for the purposes of this section.

(B) Sampling sites. Sampling sites shall be selected using Method 1 or 1A of 40 CFR part 60, appendix A, as appropriate. For determination of compliance with the 95 percent reduction requirement, sampling sites shall be located at the inlet and the outlet of the control device. For determination of compliance with the 20 ppmv limit, the sampling site shall be located at the outlet of the control device.

(C) Concentration in gas stream entering or exiting the control device. The concentration of total organic HAP or TOC in a gas stream shall be determined as provided in this paragraph. Samples may be grab samples or composite samples (i.e., integrated samples). Samples shall be taken at approximately equally spaced time intervals over a 1-hour period. Each 1-hour
period constitutes a run, and the performance test shall consist of a minimum of three runs. Concentration measurements shall be determined using Method 18 of 40 CFR part 60, appendix A. Alternatively, any other test method validated according to the procedures in Method 301 of appendix A of this part may be used.

(D) Volumetric flow rate of gas stream entering or exiting the control device. The volumetric flow rate of the gas stream shall be determined using Method 2, 2A, 2C, or 2D of 40 CFR part 60, appendix A, as appropriate. Volumetric flow rate measurements shall be taken at the same time as the concentration measurements.

(E) Calculation of TOC concentration. The owner or operator shall compute TOC in accordance with the procedures in paragraph (a)(2) of this section.

(F) Calculation of total organic HAP concentration. The owner or operator determining compliance based on total organic HAP concentration shall compute the total organic HAP concentration in accordance with the provisions in paragraph (a)(2) of this section.

(G) Requirements for combustion control devices. If the control device is a combustion device, the owner or operator shall correct TOC and organic HAP concentrations to 3 percent oxygen in accordance with the provisions in paragraph (a)(3) of this section, and demonstrate initial compliance with the requirements for halogenated streams in accordance with paragraph (a)(6) of this section.

(H) Mass rate calculation. The mass rate of either TOC (minus methane and ethane) or total organic HAP for each sample run shall be calculated using the following equations. Where the mass rate of TOC is being calculated, all organic compounds (minus methane and ethane) measured by methods specified in paragraph (e)(3)(i)(C) of this section are summed using Equations 52 and 53 of this subpart. Where the mass rate of total organic HAP is being calculated, only soluble and partially soluble HAP compounds shall be summed using Equations 52 and 53.

\[
\begin{align*}
QMG_a &= K_2 \left( \sum_{i=1}^{n} \left( CG_{a,i} \right) * \left( MW_i \right) \right) * QG_a \quad \text{(Eq. 52)} \\
QMG_b &= K_2 \left( \sum_{i=1}^{n} \left( CG_{b,i} \right) * \left( MW_i \right) \right) * QG_b \quad \text{(Eq. 53)}
\end{align*}
\]

Where:

- \( CG_{a,i} \), \( CG_{b,i} \) = concentration of TOC or total organic HAP, in vented gas stream, entering (\( CG_{a,i} \)) and exiting (\( CG_{b,i} \)) the control device, dry basis, ppmv
- \( QMG_a \), \( QMG_b \) = mass rate of TOC or total organic HAP, in vented gas stream, entering (\( QMG_a \)) and exiting (\( QMG_b \)) the control device, dry basis, kg/hr
- \( MW_i \) = molecular weight of a component, kilogram/kilogram-mole
- \( QG_a \), \( QG_b \) = flow rate of gas stream entering (\( QG_a \)) and exiting (\( QG_b \)) the control device, dry standard cubic meters per hour
- \( K_2 \) = constant, \( 41.57 \times 10^{-9} \) (parts per million)-1 (gram-mole per standard cubic meter) (kilogram/gram), where standard temperature (gram-mole per standard cubic meter) is 20°C
- \( i \) = identifier for a compound
- \( n \) = number of components in the sample

(I) Percent reduction calculation. The percent reduction in TOC or total organic HAP for each sample run shall be calculated using Equation 54 of this subpart:

\[
E = \frac{QMG_a - QMG_b}{QMG_a} \times 100\% \quad \text{(Eq. 54)}
\]
where:
E = destruction efficiency of control device, percent
QMG
a
, QMG
b
= mass rate of TOC or total organic HAP, in vented gas stream entering and exiting (QMG
a
) the control device, dry basis, kilograms per hour

(i) Compare mass destruction efficiency to required efficiency. If complying with the 95-percent reduction efficiency requirement, compliance is demonstrated if the mass destruction efficiency (calculated in Equation 51 of this subpart) is 95 percent or greater. If complying with the 20 ppmv limit, compliance is demonstrated if the outlet TOC concentration is 20 ppmv, or less.

(ii) Design evaluation. A design evaluation conducted in accordance with the provisions in paragraph (a)(1) of this section. Compounds that meet the requirements specified in paragraph (e)(2)(iii)(A)(4) of this section are not required to be included in the design evaluation.

(iii) Compliance demonstration for flares. When a flare is used to comply with §63.1256(h), the owner or operator shall comply with the flare provisions in §63.11(b). An owner or operator is not required to conduct a performance test to determine percent emission reduction or outlet organic HAP or TOC concentration when a flare is used.

(iv) Exemptions from compliance demonstrations. An owner or operator using any control device specified in paragraph (a)(4) of this section is exempt from the requirements in paragraphs (e)(3)(i) through (e)(3)(iii) of this section and from the requirements in §63.6(f).

(f) Pollution prevention alternative standard. The owner or operator shall demonstrate compliance with §63.1252(e)(2) using the procedures described in paragraph (f)(1) and (f)(3) of this section. The owner or operator shall demonstrate compliance with §63.1252(e)(3) using the procedures described in paragraphs (f)(2) and (f)(3) of this section.

(1) Compliance is demonstrated when the annual kg/kg factor, calculated according to the procedure in paragraphs (f)(1)(i) and (ii) of this section, is reduced by at least 75 percent of the baseline factor calculated according to the procedure in paragraph (f)(1)(i) and (ii) of this section.

(i) The production-indexed HAP consumption factors shall be calculated by dividing annual consumption of total HAP by the annual production rate, per process. The production-indexed total VOC consumption factor shall be calculated by dividing annual consumption of total VOC by the annual production rate, per process.

(ii) The baseline factor is calculated from yearly production and consumption data for the first 3-year period in which the PMPU was operational, beginning no earlier than the 1987 calendar year, or for a minimum period of 12 months from startup of the process until the present in which the PMPU was operational and data are available, beginning no earlier than the 1987 calendar year.

(iii) The annual factor is calculated on the following bases:
(A) For continuous processes, the annual factor shall be calculated every 30 days for the 12-month period preceding the 30th day (30-day rolling average).
(B) For batch processes, the annual factor shall be calculated every 10 batches for the 12-month period preceding the 10th batch (10-batch rolling average). The annual factor shall be calculated every 5 batches if the number of batches is less than 10 for the 12-month period preceding the 10th batch and shall be calculated every year if the number of batches is less than 5 for the 12-month period preceding the 5th batch.

(2) Compliance is demonstrated when the requirements of paragraphs (f)(2)(i) through (iv) of this section are met.

(i) The annual kg/kg factor, calculated according to the procedure in paragraphs (f)(1)(i) and (f)(1)(iii) of this section, is reduced to a value equal to or less than 50 percent of the baseline factor calculated according to the procedure in paragraphs (f)(1)(i) and (ii) of this section.

(ii) The yearly reductions associated with add-on controls that meet the criteria of §§63.1252(h)(3)(ii)(A) through (D) must be equal to or greater than the amounts calculated in paragraphs (f)(2)(ii)(A) and (B) of this section:
(A) The mass of HAP calculated using Equation 55 of this subpart:
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\[
[kg \text{ reduced}]_a = [kg/kg]_b (0.75 - P_R)[kg \text{ produced}]_a \quad (E \text{q. } 55)
\]

Where:
- \([kg/kg]_b\) = the baseline production-indexed HAP consumption factor, in kg/kg
- \([kg \text{ produced}]_a\) = the annual HAP production rate, in kg/yr
- \([kg \text{ reduced}]_a\) = the annual reduction required by add-on controls, in kg/yr
- \(P_R\) = the fractional reduction in the annual kg/kg factor achieved using pollution prevention where \(P_R\) is \(\geq 0.5\)

(B) The mass of VOC calculated using Equation 56 of this subpart:

\[
VOC_{\text{reduced}} = (VF_{\text{base}} - VF_P - VF_{\text{annual}}) \times M_{\text{prod}} \quad (E \text{q. 56})
\]

Where:
- \(VOC_{\text{reduced}}\) = required VOC emission reduction from add-on controls, kg/yr
- \(VF_{\text{base}}\) = baseline VOC factor, kg VOC emitted/kg production
- \(VF_P\) = reduction in VOC factor achieved by pollution prevention, kg VOC emitted/kg production
- \(VF_{\text{annual}}\) = target annual VOC factor, kg VOC emitted/kg production
- \(M_{\text{prod}}\) = production rate, kg/yr

(iii) Demonstration that the criteria in §63.1252(e)(3)(ii)(A) through (D) are met shall be accomplished through a description of the control device and of the material streams entering and exiting the control device.

(iv) The annual reduction achieved by the add-on control shall be quantified using the methods described in §63.1257(d).

(3) Each owner or operator of a PMPU complying with the P2 standard shall prepare a P2 demonstration summary that shall contain, at a minimum, the following information:

(i) Descriptions of the methodologies and forms used to measure and record daily consumption of HAP compounds reduced as part of the P2 standard.

(ii) Descriptions of the methodologies and forms used to measure and record daily production of products which are included in the P2 standard.

(iii) Supporting documentation for the descriptions provided in paragraphs (f)(3)(i) and (ii) including, but not limited to, operator log sheets and copies of daily, monthly, and annual inventories of materials and products.

(g) Compliance with storage tank provisions by using emissions averaging. An owner or operator with two or more affected storage tanks may demonstrate compliance with §63.1253, as applicable, by fulfilling the requirements of paragraphs (g)(1) through (4) of this section.

(1) The owner or operator shall develop and submit for approval an Implementation Plan containing all the information required in §63.1259(e) 6 months prior to the compliance date of the standard. The Administrator shall have 90 days to approve or disapprove the emissions averaging plan after which time the plan shall be considered approved.

(2) The annual mass rate of total organic HAP \((E^T_i, E^T_o)\) shall be calculated for each storage tank included in the emissions average using the procedures specified in paragraph (c)(1), (2), or (3) of this section.

(3) Equations 57 and 58 of this subpart shall be used to calculate total HAP emissions for those tanks subject to §63.1253(b) or (c):

\[
E_T^i = \sum_{j=1}^{n} E_{o_j} \quad (E \text{q. 57})
\]

\[
E_T^o = \sum_{j=1}^{n} E_{i_j} \quad (E \text{q. 58})
\]

Where:
- \(E_{o_j}\) = yearly mass rate of total HAP at the outlet of the control device for tank \(j\)  
- \(E_{i_j}\) = yearly mass rate of total HAP at the inlet of the control device for tank \(j\)  
- \(E_T^i\) = total yearly uncontrolled HAP emissions  
- \(E_T^o\) = total yearly actual HAP emissions  
- \(n\) = number of tanks included in the emissions average

(4) The overall percent reduction efficiency shall be calculated as follows:

\[
R = \frac{E_T^i - D E_T^o}{E_T^i} \times 100\% 
\]

where:
- \(D\) =
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R = overall percent reduction efficiency
D = discount factor = 1.1 for all controlled storage tanks

(h) Compliance with process vent provisions by using emissions averaging. An owner or operator with two or more affected processes complying with §63.1254 by using emissions averaging shall demonstrate compliance with paragraphs (h)(1), (2) and (3) of this section.

(1) The owner or operator shall develop and submit for approval an Implementation Plan at least 6 months prior to the compliance date of the standard containing all the information required in §63.1259(e). The Administrator shall have 90 days to approve or disapprove the emissions averaging plan. The plan shall be considered approved if the Administrator either approves the plan in writing, or fails to disapprove the plan in writing. The 90-day period shall begin when the Administrator receives the request. If the request is denied, the owner or operator must still be in compliance with the standard by the compliance date.

(2) Owners or operators shall calculate uncontrolled and controlled emissions of HAP by using the methods specified in paragraph (d)(2) and (3) of this section for each process included in the emissions average.

(i) Equations 60 and 61 of this subpart shall be used to calculate total HAP emissions:

\[ E_{TU} = \sum_{j=1}^{n} E_{Ui} \]  \hspace{1cm} (Eq. 60)

where:

- \( E_{Ui} \) = yearly uncontrolled emissions from process \( i \)
- \( E_{Ci} \) = yearly actual emissions for process \( i \)
- \( E_{TU} \) = total yearly uncontrolled emissions
- \( E_{TC} \) = total yearly actual emissions
- \( n \) = number of processes included in the emissions average

(3) The overall percent reduction efficiency shall be calculated using Equation 62 of this subpart:

\[ R = \frac{E_{TU} - D E_{TC}}{E_{TU}} \times 100\% \]  \hspace{1cm} (Eq. 62)

where:

- \( R \) = overall percent reduction efficiency
- \( D \) = discount factor = 1.1 for all controlled emission points

§ 63.1258 Monitoring Requirements.

(a) The owner or operator of any existing, new, or reconstructed affected source shall provide evidence of continued compliance with the standard as specified in this section. During the initial compliance demonstration, maximum or minimum operating parameter levels, as appropriate, shall be established for emission sources that will indicate the source is in compliance. Test data, calculations, or information from the evaluation of the control device design shall be used to establish the operating parameter level.

(b) Monitoring for control devices. (1) Parameters to monitor. Except as specified in paragraph (b)(1)(i) of this section, for each control device, the owner or operator shall install and operate monitoring devices and operate within the established parameter levels to ensure continued compliance with the standard. Monitoring parameters are specified for control scenarios in Table 4 of this subpart and in paragraphs (b)(1)(ii) through (xi) of this section.

(i) Periodic verification. For control devices that control vent streams totaling less than 1 ton/yr HAP emissions, before control, monitoring shall consist of a daily verification that the device is operating properly. If the control device is used to control batch process vents alone or in combination with other streams, the verification may be on a per batch basis. This verification shall include, but not be limited to, a daily or per batch demonstration that the unit is working as designed and may include the daily measurements of the parameters described in (b)(1)(ii) through (x) of this section. This demonstration shall be included in the Precompliance report,
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to be submitted 6 months prior to the compliance date of the standard.

(ii) Scrubbers. For affected sources using liquid scrubbers, the owner or operator shall establish a minimum scrubber liquid flow rate or pressure drop as a site-specific operating parameter which must be measured and recorded every 15 minutes during the period in which the scrubber is functioning in achieving the HAP removal required by this subpart. If the scrubber uses a caustic solution to remove acid emissions, the owner or operator shall establish a minimum pH of the effluent scrubber liquid as a site-specific operating parameter which must be measured at least once a day. The minimum scrubber flow rate or pressure drop shall be based on the conditions anticipated under worst-case conditions, as defined in §63.1257(b)(8)(i).

(A) The monitoring device used to determine the pressure drop shall be certified by the manufacturer to be accurate to within ±10 percent of the maximum pressure drop measured.

(B) The monitoring device used for measurement of scrubber liquid flow rate shall be certified by the manufacturer to be accurate within ±10 percent of the design scrubber liquid flow rate.

(C) The monitoring device shall be calibrated annually.

(iii) Condensers. For each condenser, the owner or operator shall establish the maximum condenser outlet gas temperature as a site-specific operating parameter which must be measured and recorded at least every 15 minutes during the period in which the condenser is functioning in achieving the HAP removal required by this subpart.

(A) The temperature monitoring device must be accurate to within ±2 percent of the temperature measured in degrees Celsius or ±2.5 °C, whichever is greater.

(B) The temperature monitoring device must be calibrated annually.

(iv) Regenerative carbon adsorbers. For each regenerative carbon adsorber, the owner or operator shall comply with the provisions in paragraphs (b)(1)(iv)(A) through (F) of this section.

(A) Establish the regeneration cycle characteristics specified in paragraphs (b)(1)(iv)(A)(1) through (4) of this section under worst-case conditions, as defined in §63.1257(b)(8)(i).

(1) Minimum regeneration frequency (i.e., operating time since last regeneration);

(2) Minimum temperature to which the bed is heated during regeneration;

(3) Maximum temperature to which the bed is cooled, measured within 15 minutes of completing the cooling phase; and

(4) Minimum regeneration stream flow.

(B) Monitor and record the regeneration cycle characteristics specified in paragraphs (b)(1)(iv)(B)(1) through (4) of this section for each regeneration cycle.

(1) Regeneration frequency (operating time since end of last regeneration);

(2) Temperature to which the bed is heated during regeneration;

(3) Temperature to which the bed is cooled, measured within 15 minutes of the completion of the cooling phase; and

(4) Regeneration stream flow.

(C) Use a temperature monitoring device that is accurate to within ±2 percent of the temperature measured in degrees Celsius or ±2.5 °C, whichever is greater.

(D) Use a regeneration stream flow monitoring device capable of recording the total regeneration stream flow to within ±10 percent of the established value (i.e., accurate to within ±10 percent of the reading).

(E) Calibrate the temperature and flow monitoring devices annually.

(F) Conduct an annual check for bed poisoning in accordance with manufacturer’s specifications.

(v) Nonregenerative carbon adsorbers. For each nonregenerative carbon adsorber, the owner or operator shall establish and monitor the maximum time interval between replacement based on the conditions anticipated under worst-case, as defined in §63.1257(b)(8)(i).

(vi) Flares. For each flare, the presence of the pilot flame shall be monitored every 15 minutes during the period in which the flare is functioning in
achieving the HAP removal required by this subpart.

(vii) Thermal incinerators. For each thermal incinerator, the owner or operator shall establish the minimum temperature of the gases exiting the combustion chamber as the site-specific operating parameter which must be measured and recorded at least once every 15 minutes during the period in which the combustion device is functioning in achieving the HAP removal required by this subpart.

(A) The temperature monitoring device must be accurate to within ±0.75 percent of the temperature measured in degrees Celsius or ±2.5°C, whichever is greater.

(B) The temperature monitoring device must be calibrated annually.

(viii) Catalytic incinerators. For each catalytic incinerator, the owner or operator shall establish the minimum temperature of the gases exiting the combustion chamber as the site-specific operating parameter which must be measured and recorded at least once every 15 minutes during the period in which the catalytic incinerator is functioning in achieving the HAP removal required by this subpart.

(A) The temperature monitoring device must be accurate to within ±0.75 percent of the temperature measured in degrees Celsius or ±2.5°C, whichever is greater.

(B) The temperature monitoring device must be calibrated annually.

(ix) Process heaters and boilers. (A) Except as specified in paragraph (b)(1)(ix)(B) of this section, for each boiler or process heater, the owner or operator shall establish the minimum temperature of the gases exiting the combustion chamber as the site-specific operating parameter which must be measured and recorded at least once every 15 minutes during the period in which the boiler or process heater is functioning in achieving the HAP removal required by this subpart.

(i) The temperature monitoring device must be accurate to within ±0.75 percent of the temperature measured in degrees Celsius or ±2.5°C, whichever is greater.

(ii) The temperature monitoring device must be calibrated annually.

(B) The owner or operator is exempt from the monitoring requirements specified in paragraph (b)(1)(ix)(A) of this section if either:

(1) All vent streams are introduced with primary fuel; or

(2) The design heat input capacity of the boiler or process heater is 44 megawatts or greater.

(x) Continuous emission monitor. As an alternative to the parameters specified in paragraphs (b)(1)(ii) through (ix) of this section, an owner or operator may monitor and record the outlet HAP concentration or both the outlet TOC concentration and outlet hydrogen halide and halogen concentration every 15 minutes during the period in which the control device is functioning in achieving the HAP removal required by this subpart. The owner or operator need not monitor the hydrogen halide and halogen concentration if, based on process knowledge, the owner or operator determines that the emission stream does not contain hydrogen halides or halogens. The HAP or TOC monitor must meet the requirements of Performance Specification 8 or 9 of appendix B of part 60 and must be installed, calibrated, and maintained, according to §63.8. As part of the QA/QC Plan, calibration of the device must include, at a minimum, quarterly cylinder gas audits.

(xi) CVS visual inspections. The owner or operator shall perform monthly visual inspections of each closed vent system as specified in §63.1252(b).

(2) Averaging periods. Averaging periods for parametric monitoring levels shall be established according to paragraphs (b)(2)(i) through (iii) of this section.

(i) Except as provided in paragraph (b)(2)(iii) of this section, a daily (24-hour) or block average shall be calculated as the average of all values for a monitored parameter level set according to the procedures in (b)(3)(iii) of this section recorded during the operating day or block.
(ii) The operating day or block shall be defined in the Notification of Compliance Status report. The daily average may be from midnight to midnight or another continuous 24-hour period. The block average is limited to a period of time that is, at a maximum, equal to the time from the beginning to end of a batch process.

(iii) Monitoring values taken during periods in which the control devices are not functioning in controlling emissions, as indicated by periods of no flow, shall not be considered in the averages. Where flow to the device could be intermittent, the owner or operator shall install, calibrate and operate a flow indicator at the inlet or outlet of the control device to identify periods of no flow.

(3) Procedures for setting parameter levels for control devices used to control emissions from process vents. (i) Small control devices. Except as provided in paragraph (b)(1)(i) of this section, for devices controlling less than 10 tons per year of HAP for which a performance test is not required, the parametric levels shall be set based on the design evaluation required in §63.1257(d)(3)(i). If a performance test is conducted, the monitoring parameter level shall be established according to the procedures in (b)(3)(iii) of this section.

(ii) Large control devices. For devices controlling greater than 10 tons per year of HAP for which a performance test is required, the parameter level must be established as follows:

(A) If the operating parameter level to be established is a maximum, it must be based on the average of the values from each of the three test runs.

(B) If the operating parameter level to be established is a minimum, it must be based on the average of the values from each of the three test runs.

(C) The owner or operator may establish the parametric monitoring level(s) based on the performance test supplemented by engineering assessments and manufacturer's recommendations. Performance testing is not required to be conducted over the entire range of expected parameter values. The rationale for the specific level for each parameter, including any data and calculations used to develop the level(s) and a description of why the level indicates proper operation of the control device shall be provided in the Precompliance report. The procedures specified in this section have not been approved by the Administrator and determination of the parametric monitoring level using these procedures is subject to review and approval by the Administrator.

(iii) Parameters for control devices controlling batch process vents. For devices controlling batch process vents alone or in combination with other streams, the parameter level(s) shall be established in accordance with paragraph (b)(3)(iii)(A) or (B) of this section.

(A) If more than one batch emission episode has been selected to be controlled, a single level for the batch process(es) shall be determined from the initial compliance demonstration.

(B) Instead of establishing a single level for the batch process(es), as described in paragraph (b)(3)(iii)(A) of this section, an owner or operator may establish separate levels for each batch emission episode, selected to be controlled. If separate monitoring levels are established, the owner or operator must provide a record indicating at what point in the daily schedule or log of processes required to be recorded per the requirements of §63.1259(b)(9) the parameter being monitored changes levels and must record at least one reading of the new parameter level, even if the duration of monitoring for the new parameter is less than 15-minutes.

(4) Request approval to monitor alternative parameters. An owner or operator may request approval to monitor parameters other than those required by paragraphs (b)(1)(ii) through (ix) of this section. The request shall be submitted according to the procedures specified in §63.8(f) or included in the Precompliance report.

(5) Monitoring for the alternative standards. For control devices that are used to comply with the provisions of §63.1253(d) or 63.1254(c), the owner or operator shall monitor and record the outlet TOC concentration and the outlet hydrogen halide and halogen concentration every 15 minutes during the period in which the device is functioning in achieving the HAP removal
required by this subpart. A TOC monitor meeting the requirements of Performance Specification 8 or 9 of appendix B of part 60 shall be installed, calibrated, and maintained, according to §63.8. The owner or operator need not monitor the hydrogen halide and halogen concentration if, based on process knowledge, the owner or operator determines that the emission stream does not contain hydrogen halides or halogens.

(6) Exceedances of operating parameters. An exceedance of an operating parameter is defined as one of the following:

(i) If the parameter, averaged over the operating day or block, is below a minimum value established during the initial compliance demonstration.

(ii) If the parameter, averaged over the operating day or block, is above the maximum value established during the initial compliance demonstration.

(iii) Each loss of pilot flame for flares.

(7) Excursions. Excursions are defined by either of the two cases listed in paragraphs (b)(7)(i) or (ii) of this section.

(i) When the period of control device operation is 4 hours or greater in an operating day and monitoring data are insufficient to constitute a valid hour of data, as defined in paragraph (b)(7)(iii) of this section, for at least 75 percent of the operating hours.

(ii) When the period of control device operation is less than 4 hours in an operating day and more than one of the hours during the period of operation does not constitute a valid hour of data due to insufficient monitoring data.

(iii) Monitoring data are insufficient to constitute a valid hour of data, as used in paragraphs (b)(7)(i) and (ii) of this section, if measured values are unavailable for any of the required 15-minute periods within the hour.

(8) Violations. Exceedances of parameters monitored according to the provisions of paragraphs (b)(3)(ii) and (iv) through (ix) of this section or excursions as defined by paragraphs (b)(7)(i) through (iii) of this section constitute violations of the operating limit according to paragraphs (b)(8)(i), (ii), and (iv) of this section. Exceedances of the outlet concentrations monitored according to the provisions of paragraph (b)(5) of this section constitute violations of the emission limit according to the provisions of paragraphs (b)(8)(iii) and (iv) of this section.

(i) Except as provided in paragraph (b)(8)(iv) of this section, for episodes occurring more than once per day, exceedances of established parameter limits or excursions will result in no more than one violation per operating day for each monitored item of equipment utilized in the process.

(ii) Except as provided in paragraph (b)(8)(iv) of this section, for control devices used for more than one process in the course of an operating day, exceedances or excursions will result in no more than one violation per operating day, per control device, for each process for which the control device is in service.

(iii) Except as provided in paragraph (b)(8)(iv) of this section, exceedances of the 20 ppmv TOC outlet emission limit, averaged over the operating day, will result in no more than one violation per day per control device. Except as provided in paragraph (b)(8)(iv) of this section, exceedances of the 20 ppmv hydrogen halide or halogen outlet emission limit, averaged over the operating day, will result in no more than one violation per day per control device.

(iv) Periods of time when monitoring measurements exceed the parameter values as well as periods of inadequate monitoring data do not constitute a violation if they occur during a startup, shutdown, or malfunction, and the facility follows its startup, shutdown, and malfunction plan.

(c) Monitoring for emission limits. The owner or operator of any affected source complying with the provisions of §63.1254(a)(1) shall demonstrate continuous compliance with the 2,000 lb/yr emission limits by calculating daily a 365-day rolling summation of emissions. For owners and operators opting
to switch compliance strategy from the 93 percent control requirement to the 2,000 lb/yr compliance method, as described in §63.1254(a), the rolling average must include emissions from the past 365 days. Each day that the total emissions per process exceeds 2,000 lb/yr will be considered a violation of the emission limit.

(d) Monitoring for equipment leaks. The owner or operator of any affected source complying with the requirements of §63.1255 of this subpart shall meet the monitoring requirements described §63.1255 of this subpart.

(e) Pollution prevention. The owner or operator of any affected source that chooses to comply with the requirements of §§63.1252(e)(2) and (3) shall calculate a yearly rolling average of kg HAP consumption per kg production and kg VOC consumption per kg production every month or every 10 batches. Each rolling average kg/kg factor that exceeds the value established in §63.1257(f)(1)(ii) will be considered a violation of the emission limit.

(f) Emissions averaging. The owner or operator of any affected source that chooses to comply with the requirements of §63.1252(d) shall meet all monitoring requirements specified in paragraphs (b)(1) and (3) of this section, as applicable, for all processes and storage tanks included in the emissions average.

(g) Inspection and monitoring of waste management units and treatment processes. (1) For each wastewater tank, surface impoundment, container, individual drain system, and oil-water separator that receives, manages, or treats wastewater, a residual removed from wastewater, a recycled wastewater, or a recycled residual removed from wastewater, the owner or operator shall comply with the inspection requirements specified in Table 7 of this subpart.

(2) For each biological treatment unit used to comply with §63.1256(g), the owner or operator shall monitor TSS, BOD, and the biomass concentration at a frequency approved by the permitting authority and using methods approved by the permitting authority. The owner or operator may request approval to monitor other parameters. The request shall be submitted in the Precompliance report according to the procedures specified in §63.1260(e), and shall include a description of planned reporting and recordkeeping procedures. The Administrator shall specify appropriate reporting and recordkeeping requirements as part of the review of the permit application or by other appropriate means.

(h) Leak inspection provisions for vapor suppression equipment. (1) Except as provided in paragraph (h)(9) of this section, for each vapor collection system, closed-vent system, fixed roof, cover, or enclosure required to comply with this section, the owner or operator shall comply with the requirements of paragraphs (h)(2) through (8) of this section.

(2) Except as provided in paragraphs (h)(6) and (7) of this section, each vapor collection system and closed-vent system shall be inspected according to the procedures and schedule specified in paragraphs (h)(2)(i) and (ii) of this section and each fixed roof, cover, and enclosure shall be inspected according to the procedures and schedule specified in paragraph (h)(2)(iii) of this section.

(i) If the vapor collection system or closed-vent system is constructed of hard-piping, the owner or operator shall:

(A) Conduct an initial inspection according to the procedures in paragraph (h)(3) of this section, and

(B) Conduct annual visual inspections for visible, audible, or olfactory indications of leaks.
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(ii) If the vapor collection system or closed-vent system is constructed of ductwork, the owner or operator shall:

(A) Conduct an initial inspection according to the procedures in paragraph (h)(3) of this section, and

(B) Conduct annual inspections according to the procedures in paragraph (h)(3) of this section.

(C) Conduct annual visual inspections for visible, audible, or olfactory indications of leaks.

(iii) For each fixed roof, cover, and enclosure, the owner or operator shall:

(A) Conduct an initial inspection according to the procedures in paragraph (h)(3) of this section, and

(B) Conduct semiannual visual inspections for visible, audible, or olfactory indications of leaks.

(3) Each vapor collection system, closed-vent system, fixed roof, cover, and enclosure shall be inspected according to the procedures specified in paragraphs (h)(3)(i) through (v) of this section.

(i) Inspections shall be conducted in accordance with Method 21 of 40 CFR part 60, appendix A.

(ii) Detection instrument performance criteria. (A) Except as provided in paragraph (h)(3)(ii)(B) of this section, the detection instrument shall meet the performance criteria of Method 21 of 40 CFR part 60, appendix A, except the instrument response factor criteria in section 3.1.2(a) of Method 21 shall be for the average composition of the process fluid not each individual VOC in the stream. For process streams that contain nitrogen, air, or other inerts which are not organic HAP or VOC, the average stream response factor shall be calculated on an inert-free basis.

(B) If no instrument is available at the plant site that will meet the performance criteria specified in paragraph (h)(3)(ii)(A) of this section, the instrument readings may be adjusted by multiplying by the average response factor of the process fluid, calculated on an inert-free basis as described in paragraph (h)(3)(ii)(A) of this section.

(iii) The detection instrument shall be calibrated before use on each day of its use by the procedures specified in Method 21 of 40 CFR part 60, appendix A.

(iv) Calibration gases shall be as follows:

(A) Zero air (less than 10 parts per million hydrocarbon in air); and

(B) Mixtures of methane in air at a concentration less than 10,000 parts per million. A calibration gas other than methane in air may be used if the instrument does not respond to methane or if the instrument does not meet the performance criteria specified in paragraph (h)(2)(ii)(A) of this section. In such cases, the calibration gas may be a mixture of one or more of the compounds to be measured in air.

(v) An owner or operator may elect to adjust or not adjust instrument readings for background. If an owner or operator elects to not adjust readings for background, all such instrument readings shall be compared directly to the applicable leak definition to determine whether there is a leak. If an owner or operator elects to adjust instrument readings for background, the owner or operator shall measure background concentration using the procedures in § 63.180(b) and (c). The owner or operator shall subtract background reading from the maximum concentration indicated by the instrument.

(vi) The background level shall be determined according to the procedures in Method 21 of 40 CFR part 60 appendix A.

(vii) The arithmetic difference between the maximum concentration indicated by the instrument and the background level shall be compared with 500 parts per million for determining compliance.

(4) Leaks, as indicated by an instrument reading greater than 500 parts per million above background or by visual inspections, shall be repaired as soon as practicable, except as provided in paragraph (h)(5) of this section.

(i) A first attempt at repair shall be made no later than 5 calendar days after the leak is detected.

(ii) Repair shall be completed no later than 15 calendar days after the leak is detected, except as provided in paragraph (h)(4)(iii) of this section.

(iii) For leaks found in vapor collection systems used for transfer operations, repairs shall be completed no later than 15 calendar days after the leak is detected or at the beginning of
(5) Delay of repair of a vapor collection system, closed-vent system, fixed roof, cover, or enclosure for which leaks have been detected is allowed if the repair is technically infeasible without a shutdown, as defined in §63.1251, or if the owner or operator determines that emissions resulting from immediate repair would be greater than the fugitive emissions likely to result from delay of repair. Repair of such equipment shall be complete by the end of the next shutdown.

(6) Any parts of the vapor collection system, closed-vent system, fixed roof, cover, or enclosure that are designated, as described in paragraph (h)(8)(i) of this section, as unsafe to inspect are exempt from the inspection requirements of paragraphs (h)(2)(i), (ii), and (iii) of this section if:

(i) The owner or operator determines that the equipment is unsafe to inspect because inspecting personnel would be exposed to an imminent or potential danger as a consequence of complying with paragraphs (h)(2)(i), (ii), or (iii) of this section; and

(ii) The owner or operator has a written plan that requires inspection of the equipment as frequently as practicable during safe-to-inspect times.

(7) Any parts of the vapor collection system, closed-vent system, fixed roof, cover, or enclosure that are designated, as described in paragraph (h)(8)(ii) of this section, as difficult to inspect are exempt from the inspection requirements of paragraphs (h)(2)(i), (ii), and (iii)(A) of this section if:

(i) The owner or operator determines that the equipment cannot be inspected without elevating the inspecting personnel more than 2 meters above a support surface; and

(ii) The owner or operator has a written plan that requires inspection of the equipment at least once every 5 years.

(8) Records shall be maintained as specified in §63.1259(1) through (9).

(9) If a closed-vent system subject to this section is also subject to the equipment leak provisions of §63.1255, the owner or operator shall comply with the provisions of §63.1255 and is exempt from the requirements of this section.

§63.1259 Recordkeeping requirements.

(a) Requirements of subpart A of this part. The owner or operator of an affected source shall comply with the recordkeeping requirements in subpart A of this part as specified in Table 1 of this subpart and in paragraphs (a)(1) through (5) of this section.

(1) Data retention. Each owner or operator of an affected source shall keep copies of all records and reports required by this subpart for at least 5 years, as specified in §63.10(b)(1).

(2) Records of applicability determinations. The owner or operator of a stationary source that is not subject to this subpart shall keep a record of the applicability determination, as specified in §63.10(b)(3).

(3) Startup, shutdown, and malfunction plan. The owner or operator of an affected source shall develop and implement a written startup, shutdown, and malfunction plan as specified in §63.6(e)(3). This plan shall describe, in detail, procedures for operating and maintaining the affected source during periods of startup, shutdown, and malfunction and a program for corrective action for malfunctioning process, air pollution control, and monitoring equipment used to comply with this subpart. The owner or operator of an affected source shall keep the current and superseded versions of this plan onsite, as specified in §63.6(e)(3)(v). The owner or operator shall keep the startup, shutdown, and malfunction records specified in paragraphs (b)(3)(i) through (iii) of this section. Reports related to the plan shall be submitted as specified in §63.1260(i).

(i) The owner or operator shall record the occurrence and duration of each malfunction of air pollution control equipment used to comply with this subpart, as specified in §63.6(e)(3)(iii).

(ii) The owner or operator shall record the occurrence and duration of each malfunction of continuous monitoring systems used to comply with this subpart.

(iii) For each startup, shutdown, or malfunction, the owner or operator shall record all information necessary to demonstrate that the procedures specified in the affected source's startup, shutdown, and malfunction plan were followed, as specified in
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(4) Recordkeeping requirements for sources with continuous monitoring systems. The owner or operator of an affected source who elects to install a continuous monitoring system shall maintain records specified in § 63.10(c)(1) through (14).

(5) Application for approval of construction or reconstruction. For new affected sources, each owner or operator shall comply with the provisions in § 63.5 regarding construction and reconstruction, excluding the provisions specified in § 63.5(d)(1)(ii)(H), (d)(2), and (d)(3)(ii).

(b) Records of equipment operation. The owner or operator must keep the following records up-to-date and readily accessible:

(1) Each measurement of a control device operating parameter monitored in accordance with § 63.1258 and each measurement of a treatment process parameter monitored in accordance with § 63.1258(g)(2) and (3).

(2) For processes subject to § 63.1252(e), records of consumption, production, and the rolling average values of the production-indexed HAP and VOC consumption factors.

(3) For each continuous monitoring system used to comply with this subpart, records documenting the completion of calibration checks and maintenance of continuous monitoring systems.

(4) For processes in compliance with the 2,000 lb/yr emission limit of § 63.1254(a)(1), records of the rolling annual total emissions.

(5) Records of the following, as appropriate:

(i) The number of batches per year for each batch process.

(ii) The operating hours per year for continuous processes.

(6) Uncontrolled and controlled emissions per batch for each process.

(7) Wastewater concentration per POD or process.

(8) Number of storage tank turnovers per year, if used in an emissions average.

(9) Daily schedule or log of each operating scenario prior to its operation.

(10) Description of worst-case operating conditions as determined using the procedures described in § 63.1257(b)(8) for control devices.

(11) Periods of planned routine maintenance as described in § 63.1257(c)(5).

(c) Records of operating scenarios. The owner or operator of an affected source shall keep records of each operating scenario which demonstrates compliance with this subpart.

(d) Records of equipment leak detection and repair programs. The owner or operator of any affected source implementing the leak detection and repair (LDAR) program specified in § 63.1255 of this subpart, shall implement the recordkeeping requirements in § 63.1255 of this subpart.

(e) Records of emissions averaging. The owner or operator of any affected source that chooses to comply with the requirements of § 63.1252(d) shall maintain up-to-date records of the following information:

(1) An Implementation Plan which shall include in the plan, for all process vents and storage tanks included in each of the averages, the information listed in paragraphs (e)(1)(i) through (v) of this section.

(i) The identification of all process vents and storage tanks in each emissions average.

(ii) The uncontrolled and controlled emissions of HAP and the overall percent reduction efficiency as determined in §§ 63.1257(g)(1) through (4) or 63.1257(h)(1) through (3) as applicable.

(iii) The calculations used to obtain the uncontrolled and controlled HAP emissions and the overall percent reduction efficiency.

(iv) The estimated values for all parameters required to be monitored under § 63.1258(f) for each process and storage tank included in an average.

(v) A statement that the compliance demonstration, monitoring, inspection, recordkeeping and reporting provisions in §§ 63.1257(g) and (h), 63.1258(f), and 63.1260(k) that are applicable to each emission point in the emissions average will be implemented beginning on the date of compliance.

(2) The Implementation Plan must demonstrate that the emissions from the processes and storage tanks proposed to be included in the average will
not result in greater hazard or, at the option of the operating permit authority, greater risk to human health or the environment than if the storage tanks and process vents were controlled according to the provisions in §§ 63.1253 and 63.1254, respectively.

(i) This demonstration of hazard or risk equivalency shall be made to the satisfaction of the operating permit authority.

(A) The Administrator may require owners and operators to use specific methodologies and procedures for making a hazard or risk determination.

(B) The demonstration and approval of hazard or risk equivalency shall be made according to any guidance that the Administrator makes available for use or any other technically sound information or methods.

(ii) An emissions averaging plan that does not demonstrate hazard or risk equivalency to the satisfaction of the Administrator shall not be approved. The Administrator may require such adjustments to the emissions averaging plan as are necessary in order to ensure that the average will not result in greater hazard or risk to human health or the environment than would result if the emission points were controlled according to §§ 63.1253 and 63.1254.

(iii) A hazard or risk equivalency demonstration must:

(A) Be a quantitative, comparative chemical hazard or risk assessment;

(B) Account for differences between averaging and non-averaging options in chemical hazard or risk to human health or the environment; and

(C) Meet any requirements set by the Administrator for such demonstrations.

(3) Records as specified in paragraphs (a), (b) and (d) of this section.

(4) A rolling quarterly calculation of the annual percent reduction efficiency as specified in §63.1257(g) and (h).

(f) Records of delay of repair. Documentation of a decision to use a delay of repair due to unavailability of parts, as specified in §63.1256(i), shall include a description of the failure, the reason additional time was necessary (including a statement of why replacement parts were not kept onsite and when delivery from the manufacturer is scheduled), and the date when the repair was completed.

(g) Record of wastewater stream or residual transfer. The owner or operator transferring an affected wastewater stream or residual removed from an affected wastewater stream in accordance with §63.1256(a)(5) shall keep a record of the notice sent to the treatment operator stating that the wastewater stream or residual contains organic HAP which are required to be managed and treated in accordance with the provisions of this subpart.

(h) Records of extensions. The owner or operator shall keep documentation of a decision to use an extension, as specified in §63.1256(b)(6)(ii) or (b)(9), in a readily accessible location. The documentation shall include a description of the failure, documentation that alternate storage capacity is unavailable, and specification of a schedule of actions that will ensure that the control equipment will be repaired and the tank will be emptied as soon as practical.

(i) Records of inspections. The owner or operator shall keep records specified in paragraphs (i)(1) through (9) of this section.

(1) A record that each waste management unit inspection required by §63.1256(b) through (f) was performed.

(2) A record that each inspection for control devices required by §63.1256(h) was performed.

(3) A record of the results of each seal gap measurement required by §63.1256(b)(5) and (f)(3). The records shall include the date of measurement, the raw data obtained in the measurement, and the calculations described in §63.120(b)(2) through (4).

(4) Records identifying all parts of the vapor collection system, closed-vent system, fixed roof, cover, or enclosure that are designated as unsafe to inspect in accordance with §63.1258(h)(6), an explanation of why the equipment is unsafe to inspect, and the plan for inspecting the equipment.

(5) Records identifying all parts of the vapor collection system, closed-vent system, fixed roof, cover, or enclosure that are designated as difficult to inspect in accordance with §63.1258(h)(7), an explanation of why the equipment is difficult to inspect,
and the plan for inspecting the equipment.

(6) For each vapor collection system or closed-vent system that contains bypass lines that could divert a vent stream away from the control device and to the atmosphere, the owner or operator shall keep a record of the information specified in either paragraph (i)(6)(i) or (ii) of this section.

(i) Hourly records of whether the flow indicator specified under §63.1252(b)(1) was operating and whether a diversion was detected at any time during the hour, as well as records of the times and durations of all periods when the vent stream is diverted from the control device or the flow indicator is not operating.

(ii) Where a seal mechanism is used to comply with §63.1252(b)(2), hourly records of flow are not required. In such cases, the owner or operator shall record that the monthly visual inspection of the seals or closure mechanisms has been done, and shall record the occurrence of all periods when the seal mechanism is broken, the bypass line valve position has changed, or the key for a lock-and-key type lock has been checked out, and records of any car-seal that has broken.

(7) For each inspection conducted in accordance with §63.1258(h)(2) and (3) during which a leak is detected, a record of the information specified in paragraphs (i)(7)(i) through (viii) of this section.

(i) The instrument identification numbers; operator name or initials; and identification of the equipment.

(ii) The date the leak was detected and the date of the first attempt to repair the leak.

(iii) Maximum instrument reading measured by the method specified in §63.1258(h)(4) after the leak is successfully repaired or determined to be non-repairable.

(iv) “Repair delayed” and the reason for the delay if a leak is not repaired within 15 calendar days after discovery of the leak.

(v) The name, initials, or other form of identification of the owner or operator (or designee) whose decision it was that repair could not be effected without a shutdown.

(vi) The expected date of successful repair of the leak if a leak is not repaired within 15 calendar days.

(vii) Dates of shutdowns that occur while the equipment is unrepairable.

(viii) The date of successful repair of the leak.

(8) For each inspection conducted in accordance with §63.1258(h)(3) during which no leaks are detected, a record that the inspection was performed, the date of the inspection, and a statement that no leaks were detected.

(9) For each visual inspection conducted in accordance with §63.1258(h)(2)(i)(B) or (h)(2)(iii)(B) of this section during which no leaks are detected, a record that the inspection was performed, the date of the inspection, and a statement that no leaks were detected.

\[\text{§63.1260 Reporting requirements.}\]

(a) The owner or operator of an affected source shall comply with the reporting requirements of paragraphs (b) through (l) of this section. Applicable reporting requirements of §§63.9 and 63.10 are also summarized in Table 1 of this subpart.

(b) Initial notification. The owner or operator shall submit the applicable initial notification in accordance with §63.9(b) or (d).

(c) Application for approval of construction or reconstruction. An owner or operator who is subject to §63.5(b)(3) shall submit to the Administrator an application for approval of the construction of a new major affected source, the reconstruction of a major affected source, or the reconstruction of a major source such that the source becomes a major affected source subject to the standards. The application shall be prepared in accordance with §63.5(d).

(d) Notification of CMS performance evaluation. An owner or operator who is required by the Administrator to conduct a performance evaluation for a continuous monitoring system shall notify the Administrator of the date of the performance evaluation as specified in §63.8(e)(2).

(e) Precompliance report. The Precompliance report shall be submitted at least 6 months prior to the compliance date of the standard. For
new sources, the Precompliance report shall be submitted to the Administrator with the application for approval of construction or reconstruction. The Administrator shall have 90 days to approve or disapprove the plan. The plan shall be considered approved if the Administrator either approves the plan in writing, or fails to disapprove the plan in writing. The 90 day period shall begin when the Administrator receives the request. If the request is denied, the owner or operator shall notify the Administrator of the compliance with the standard by the compliance date. To change any of the information submitted in the report, the owner or operator shall notify the Administrator 90 days before the planned change is to be implemented; the change shall be considered approved if the Administrator either approves the change in writing, or fails to disapprove the change in writing. The Precompliance report shall include:

(1) Requests for approval to use alternative monitoring parameters or requests to set monitoring parameters according to §63.1258(b)(4).

(2) Descriptions of the daily or per batch demonstrations to verify that control devices subject to §63.1258(b)(1)(i) are operating as designed.

(3) A description of test conditions, and the corresponding monitoring parameter values for parameters that are set according to §63.1258(b)(3)(ii)(C).

(4) For owners and operators complying with the requirements of §63.1252(e), the P2 demonstration summary required in §63.1257(f).

(5) Data and rationale used to support an engineering assessment to calculate uncontrolled emissions from process vents as required in §63.1257(d)(2)(ii).

(f) Notification of Compliance Status report. The Notification of Compliance Status report required under §63.9 shall be submitted no later than 150 days after the compliance date and shall include:

(1) The results of any applicability determinations, emission calculations, or analyses used to identify and quantify HAP emissions from the affected source.

(2) The results of emissions profiles, performance tests, engineering analyses, design evaluations, or calculations used to demonstrate compliance. For performance tests, results should include descriptions of sampling and analysis procedures and quality assurance procedures.

(3) Descriptions of monitoring devices, monitoring frequencies, and the values of monitored parameters established during the initial compliance determinations, including data and calculations to support the levels established.

(4) Listing of all operating scenarios.

(5) Descriptions of worst-case operating and/or testing conditions for control devices.

(6) Identification of emission points subject to overlapping requirements described in §63.1250(h) and the authority under which the owner or operator will comply.

(g) Periodic reports. An owner or operator shall prepare Periodic reports in accordance with paragraphs (g)(1) and (2) of this section and submit them to the Administrator.

(1) Submittal schedule. Except as provided in (g)(1) (i), (ii) and (iii) of this section, an owner or operator shall submit Periodic reports semiannually, beginning 60 operating days after the end of the applicable reporting period. The first report shall be submitted no later than 240 days after the date the Notification of Compliance Status is due and shall cover the 6-month period beginning on the date the Notification of Compliance Status is due.

(i) When the Administrator determines on a case-by-case basis that more frequent reporting is necessary to accurately assess the compliance status of the affected source; or

(ii) When the monitoring data are used directly for compliance determination and the source experience excess emissions, in which case quarterly reports shall be submitted. Once an affected source reports excess emissions, the affected source shall follow a quarterly reporting format until a request to reduce reporting frequency is approved. If an owner or operator submits a request to reduce the frequency of reporting, the provisions in §63.10(e)(3)(i) and (ii) shall apply, except that the
term “excess emissions and continuous monitoring system performance report and/or summary report” shall mean “Periodic report” for the purposes of this section.

(iii) When a new operating scenario has been operated since the last report, in which case quarterly reports shall be submitted.

(2) Content of Periodic report. The owner or operator shall include the information in paragraphs (g)(2)(i) through (vii) of this section, as applicable.

(i) Each Periodic report must include the information in §63.10(e)(3)(vi)(A) through (I) and (K) through (M). For each continuous monitoring system, the Periodic report must also include the information in §63.10(e)(3)(vi)(J).

(ii) If the total duration of excess emissions, parameter exceedances, or excursions for the reporting period is 1 percent or greater of the total operating time for the reporting period, or the total continuous monitoring system downtime for the reporting period is 5 percent or greater of the total operating time for the reporting period, the Periodic report must include the information in paragraphs (g)(2)(ii)(A) through (D) of this section.

(A) Monitoring data, including 15-minute monitoring values as well as daily average values of monitored parameters, for all operating days when the average values were outside the ranges established in the Notification of Compliance Status report or operating permit.

(B) Duration of excursions, as defined in §63.1258(b)(7).

(C) Operating logs and operating scenarios for all operating days when the values are outside the levels established in the Notification of Compliance Status report or operating permit.

(D) When a continuous monitoring system is used, the information required in §63.10(c)(5) through (13).

(iii) For each inspection conducted in accordance with §63.1258(h)(2) or (3) during which a leak is detected, the records specified in §63.1259(i)(7) must be included in the next Periodic report.

(iv) For each vapor collection system or closed vent system with a bypass line subject to §63.1252(b)(1), records required under §63.1259(i)(6)(ii) of all periods when the vent stream is diverted from the control device through a bypass line. For each vapor collection system or closed vent system with a bypass line subject to §63.1252(b)(2), records required under §63.1259(i)(6)(ii) of all periods in which the seal mechanism is broken, the bypass valve position has changed, or the key to unlock the bypass line valve was checked out.

(v) The information in paragraphs (g)(2)(iv)(A) through (D) of this section shall be stated in the Periodic report, when applicable.

(A) No excess emissions.

(B) No exceedances of a parameter.

(C) No excursions.

(D) No continuous monitoring system has been inoperative, out of control, repaired, or adjusted.

(vi) For each tank subject to control requirements, periods of planned routine maintenance during which the control device does not meet the specifications of §63.1253(b) through (d).

(vii) Each new operating scenario which has been operated since the time period covered by the last Periodic report. For the initial Periodic report, each operating scenario for each process operated since the compliance date shall be submitted.

(h) Notification of process change.

(1) Except as specified in paragraph (h)(2) of this section, whenever a process change is made, or a change in any of the information submitted in the Notification of Compliance Status Report, the owner or operator shall submit a report quarterly. The report may be submitted as part of the next Periodic report required under paragraph (g) of this section. The report shall include:

(i) A brief description of the process change.

(ii) A description of any modifications to standard procedures or quality assurance procedures.

(iii) Revisions to any of the information reported in the original Notification of Compliance Status Report under paragraph (f) of this section.

(iv) Information required by the Notification of Compliance Status Report under paragraph (f) of this section for changes involving the addition of processes or equipment.
(2) An owner or operator must submit a report 60 days before the scheduled implementation date of either of the following:
(i) Any change in the activity covered by the Precompliance report.
(ii) A change in the status of a control device from small to large.
(i) Reports of startup, shutdown, and malfunction. For the purposes of this subpart, the startup, shutdown, and malfunction reports shall be submitted on the same schedule as the periodic reports required under paragraph (g) of this section instead of the schedule specified in §63.10(d)(5)(i). These reports shall include the information specified in §63.1259(a)(3)(i) through (iii) and shall contain the name, title, and signature of the owner or operator or other responsible official who is certifying its accuracy. Reports are only required if a startup, shutdown, or malfunction occurred during the reporting period. Any time an owner or operator takes an action that is not consistent with the procedures specified in the affected source’s startup, shutdown, and malfunction plan, the owner or operator shall submit an immediate startup, shutdown, and malfunction report as specified in §63.10(d)(4)(iii).
(j) Reports of LDAR programs. The owner or operator of any affected source implementing the LDAR program specified in §63.1255 of this subpart shall implement the reporting requirements in §63.1255 of this subpart. Copies of all reports shall be retained as records for a period of 5 years, in accordance with the requirements of §63.10(b)(1).
(k) Reports of emissions averaging. The owner or operator of any affected source that chooses to comply with the requirements of §63.1252(d) shall submit the implementation plan described in §63.1259(e) 6 months prior to the compliance date of the standard and the following information in the periodic reports:
(1) The records specified in §63.1259(e) for each process or storage tank included in the emissions average;
(2) All information as specified in paragraph (g) of this section for each process or storage tank included in the emissions average;
(3) Any changes of the processes or storage tanks included in the average;
(4) The calculation of the overall percent reduction efficiency for the reporting period;
(5) Changes to the Implementation Plan which affect the calculation methodology of uncontrolled or controlled emissions or the hazard or risk equivalency determination.
(6) Every second semiannual or fourth quarterly report, as appropriate, shall include the results according to §63.1259(e)(4) to demonstrate the emissions averaging provisions of §§63.1252(d), 63.1257(g) and (h), 63.1258(f), and 63.1259(f) are satisfied.
(l) Notification of performance test and test plan. The owner or operator of an affected source shall notify the Administrator of the planned date of a performance test at least 60 days before the test in accordance with §63.7(b). The owner or operator also must submit the test plan required by §63.7(c) and the emission profile required by §63.1257(b)(8)(ii) with the notification of the performance test.
(m) Request for extension of compliance. An owner or operator may submit to the Administrator a request for an extension of compliance in accordance with §63.1250(f)(4).

§63.1261 Delegation of authority.
(a) In delegating implementation and enforcement authority to a State under §112(d) of the Clean Air Act, the authorities contained in paragraph (b) of this section shall be retained by the Administrator and not transferred to a State.
(b) The authority conferred in §63.177; the authority to approve applications for determination of equivalent means of emission limitation; and the authority to approve alternative test methods shall not be delegated to any State.
**Table 1 To Subpart GGG—General Provisions Applicability To Subpart GGG**

<table>
<thead>
<tr>
<th>General provisions reference</th>
<th>Summary of requirements</th>
<th>Applies to subpart GGG</th>
<th>Comments</th>
</tr>
</thead>
<tbody>
<tr>
<td>63.1(a)(1)</td>
<td>General applicability of the General Provisions</td>
<td>Yes</td>
<td>Additional terms defined in §63.1251; when overlap between subparts A and GGG of this part, subpart GGG takes precedence.</td>
</tr>
<tr>
<td>63.1(a)(2–7)</td>
<td>Initial applicability determination</td>
<td>Yes</td>
<td>No discussions stated.</td>
</tr>
<tr>
<td>63.1(a)(8)</td>
<td>Title V operating permit—see part 70</td>
<td>Yes</td>
<td>All major affected sources are required to obtain a Title V permit.</td>
</tr>
<tr>
<td>63.1(a)(9–14)</td>
<td>Record of the applicability determination</td>
<td>Yes</td>
<td>All affected sources are subject to subpart GGG according to the applicability definition of subpart GGG.</td>
</tr>
<tr>
<td>63.1(c)(1)</td>
<td>Applicability after standards are set</td>
<td>Yes</td>
<td>Subpart GGG clarifies the applicability of each paragraph of subpart A to sources subject to subpart GGG.</td>
</tr>
<tr>
<td>63.1(c)(2)</td>
<td>Title V permit requirement</td>
<td>No</td>
<td>No discussions stated.</td>
</tr>
<tr>
<td>63.1(c)(3)</td>
<td>Requirements for existing source that obtains an extension of compliance</td>
<td>No</td>
<td>Area sources are not subject to subpart GGG.</td>
</tr>
<tr>
<td>63.1(c)(4)</td>
<td>[Reserved]</td>
<td>Yes</td>
<td>For certain provisions identified in §63.1259(a)(5)</td>
</tr>
<tr>
<td>63.2</td>
<td>Definitions</td>
<td>Yes</td>
<td>Except replace the terms “source” and “stationary source” with “affected source”.</td>
</tr>
<tr>
<td>63.3</td>
<td>Units and abbreviations</td>
<td>Yes</td>
<td>Except replace the terms “source” and “stationary source” with “affected source”.</td>
</tr>
<tr>
<td>63.4</td>
<td>Prohibited activities</td>
<td>Yes</td>
<td>Except replace the terms “source” and “stationary source” with “affected source”.</td>
</tr>
<tr>
<td>63.5(a)</td>
<td>Construction and reconstruction—applicability</td>
<td>Yes</td>
<td>For certain provisions identified in §63.1259(a)(5)</td>
</tr>
<tr>
<td>63.5(b)(1)</td>
<td>Upon construction, relevant standards for new sources</td>
<td>Yes</td>
<td>For certain provisions identified in §63.1259(a)(5)</td>
</tr>
<tr>
<td>63.5(b)(2)</td>
<td>New construction/reconstruction</td>
<td>Yes</td>
<td>For certain provisions identified in §63.1259(a)(5)</td>
</tr>
<tr>
<td>63.5(b)(3)</td>
<td>Construction/reconstruction notification</td>
<td>Yes</td>
<td>For certain provisions identified in §63.1259(a)(5)</td>
</tr>
<tr>
<td>63.5(b)(4)</td>
<td>Construction/reconstruction compliance</td>
<td>Yes</td>
<td>For certain provisions identified in §63.1259(a)(5)</td>
</tr>
<tr>
<td>63.5(b)(5)</td>
<td>Equipment addition or process change</td>
<td>Yes</td>
<td>For certain provisions identified in §63.1259(a)(5)</td>
</tr>
<tr>
<td>63.5(c)</td>
<td>Application for approval of construction/reconstruction</td>
<td>Yes</td>
<td>For certain provisions identified in §63.1259(a)(5)</td>
</tr>
<tr>
<td>63.5(f)</td>
<td>Construction/reconstruction approval based on prior State review</td>
<td>Yes</td>
<td>For certain provisions identified in §63.1259(a)(5)</td>
</tr>
<tr>
<td>Section</td>
<td>Compliance with standards and maintenance requirements</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>---------</td>
<td>--------------------------------------------------------</td>
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<td>----</td>
</tr>
<tr>
<td>63.6(a)(1)</td>
<td>Requirements for area sources that increases emissions to become major.</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.6(b)(1)</td>
<td>Compliance dates for new and reconstructed sources</td>
<td>No</td>
<td>Yes</td>
</tr>
<tr>
<td>63.6(b)(2)</td>
<td>Compliance dates for new and reconstructed sources</td>
<td>No</td>
<td>Yes</td>
</tr>
<tr>
<td>63.6(b)(7)</td>
<td>Compliance dates for sources resulting from new unaffected area sources becoming subject to standards.</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.6(c)</td>
<td>Compliance dates for existing sources</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.6(e)</td>
<td>Operation and maintenance requirements</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.6(f)-(g)</td>
<td>Compliance with non opacity and alternative opacity emission standards</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.6(h)</td>
<td>Opacity and visible emission standards</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.6(i)</td>
<td>Extension of compliance with emission standards</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.6(j)</td>
<td>Exemption from compliance with emission standards</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.7(a)</td>
<td>Performance testing requirements.</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.7(a)(1)</td>
<td>Notification of performance test</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.7(a)(2)</td>
<td>Notification of delay in conducting a scheduled performance test</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.7(b)</td>
<td>Quality assurance program</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.7(d)</td>
<td>Performance testing facilities.</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.7(e)</td>
<td>Conduct of performance tests.</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.7(f)</td>
<td>Use of alternative test method</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.7(g)</td>
<td>Data analysis, record-keeping, and reporting</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.7(h)</td>
<td>Waiver of performance tests</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(a)</td>
<td>Monitoring requirements</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(b)(1)</td>
<td>Conduct of monitoring</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(b)(2)</td>
<td>CMS and combined effluents</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(b)(3)</td>
<td>CMS requirements</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(c)(1)</td>
<td>OMS requirements</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(c)(2)</td>
<td>CMS operation requirements</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(c)(3)</td>
<td>CMS calibration and malfunction provisions</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(d)</td>
<td>CMS quality control program</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(e)(1)</td>
<td>Performance evaluations of CMS</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(e)(2)</td>
<td>Notification of performance evaluation</td>
<td>Yes</td>
<td>No</td>
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<tr>
<td>63.8(e)(3)</td>
<td>CMS requirements/alternatives</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(e)(4)</td>
<td>Reporting performance evaluation results</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(e)(5)</td>
<td>Results of COMS performance evaluation</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.8(f)-(g)</td>
<td>Alternative monitoring method/reduction of monitoring data</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.9(a)</td>
<td>Notification requirements—Applicability and general information</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.9(b)</td>
<td>Notification of performance test</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.9(e)</td>
<td>Notification of opacity and visible emissions observations</td>
<td>Yes</td>
<td>No</td>
</tr>
<tr>
<td>63.9(g)(1)</td>
<td>Additional notification requirements for sources with CMS</td>
<td>Yes</td>
<td>No</td>
</tr>
</tbody>
</table>

Subpart GGG specifies compliance dates.
Subpart GGG specifies NS applicability and compliance dates.
Subpart GGG specifies performance test conditions.
Subpart GGG does not contain any opacity or visible emission standards.
§ 63.1250(f)(4) specifies provisions for compliance extensions.
Subpart GGG specifies required testing and compliance procedures.
Subpart GGG also contains test methods and procedures specific to pharmaceutical sources.

See § 63.1258.

See §.

Subpart GGG does not contain any opacity or visible emission standards.
<table>
<thead>
<tr>
<th>General provisions reference</th>
<th>Summary of requirements</th>
<th>Applies to subpart GGG</th>
<th>Comments</th>
</tr>
</thead>
<tbody>
<tr>
<td>63.9(g)(2)</td>
<td>Notification of compliance with opacity emission standard</td>
<td>No</td>
<td>Subpart GGG does not contain any opacity or visible emission standards.</td>
</tr>
<tr>
<td>63.9(g)(3)</td>
<td>Notification that criterion to continue use of alternative to relative accuracy testing has been exceeded</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.9(h)</td>
<td>Notification of compliance status</td>
<td>Yes</td>
<td>Due 150 days after compliance date.</td>
</tr>
<tr>
<td>63.9(i)</td>
<td>Adjustment to time periods or postmark deadlines for submittal and review of required communications</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.9(j)</td>
<td>Change in information provided</td>
<td>Yes</td>
<td>See §</td>
</tr>
<tr>
<td>63.10(a)</td>
<td>Recordkeeping requirements</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.10(b)(1)</td>
<td>Records retention</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.10(b)(2)</td>
<td>Information and documentation to support notifications</td>
<td>No</td>
<td>Subpart GGG specifies recordkeeping requirements.</td>
</tr>
<tr>
<td>63.10(b)(3)</td>
<td>Records retention for sources not subject to relevant standard</td>
<td>Yes</td>
<td>Applicability requirements are given in § 63.1250.</td>
</tr>
<tr>
<td>63.10(c)-(d)(2)</td>
<td>Other recordkeeping and reporting provisions</td>
<td>Yes</td>
<td>Subpart GGG does not include any opacity or visible emission standards.</td>
</tr>
<tr>
<td>63.10(d)(3)</td>
<td>Reporting results of opacity or visible emissions observations</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.10(d)(4-5)</td>
<td>Other recordkeeping and reporting provisions</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.10(e)</td>
<td>Additional CMS reporting requirements</td>
<td>Yes</td>
<td></td>
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<tr>
<td>63.10(f)</td>
<td>Waiver of recordkeeping or reporting requirements</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.11</td>
<td>Control device requirements for flares</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.12</td>
<td>State authority and delegations</td>
<td>Yes</td>
<td>See § 63.1261.</td>
</tr>
<tr>
<td>63.13</td>
<td>Addresses of State air pollution control agencies</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.14</td>
<td>Incorporations by reference</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.15</td>
<td>Availability of information and confidentiality</td>
<td>Yes</td>
<td></td>
</tr>
</tbody>
</table>
### TABLE 2 TO SUBPART GGG.—PARTIALLY SOLUBLE HAP

<table>
<thead>
<tr>
<th>Compound</th>
<th>Used as</th>
</tr>
</thead>
<tbody>
<tr>
<td>1,1,1-Trichloroethane (methyl chloroform)</td>
<td></td>
</tr>
<tr>
<td>1,1,2,2-Tetrachloroethane</td>
<td></td>
</tr>
<tr>
<td>1,1,2-Trichloroethane</td>
<td></td>
</tr>
<tr>
<td>1,1-Dichloroethylene (vinylidene chloride)</td>
<td></td>
</tr>
<tr>
<td>1,2-Dibromoethane</td>
<td></td>
</tr>
<tr>
<td>1,2-Dichloroethane (ethylene dichloride)</td>
<td></td>
</tr>
<tr>
<td>1,2-Dichloropropane</td>
<td></td>
</tr>
<tr>
<td>1,3-Dichloropropene</td>
<td></td>
</tr>
<tr>
<td>2,4,5-Trichlorophenol</td>
<td></td>
</tr>
<tr>
<td>2-Butanone (mek)</td>
<td></td>
</tr>
<tr>
<td>1,4-Dichlorobenzene</td>
<td></td>
</tr>
<tr>
<td>Acrone</td>
<td></td>
</tr>
<tr>
<td>Acrylonitrile</td>
<td></td>
</tr>
<tr>
<td>Allyl chloride</td>
<td></td>
</tr>
<tr>
<td>Benzene</td>
<td></td>
</tr>
<tr>
<td>Benzyl chloride</td>
<td></td>
</tr>
<tr>
<td>Biphenyl</td>
<td></td>
</tr>
<tr>
<td>Bromoform (tribromomethane)</td>
<td></td>
</tr>
<tr>
<td>Bromomethane</td>
<td></td>
</tr>
<tr>
<td>Butadiene</td>
<td></td>
</tr>
<tr>
<td>Carbon disulfide</td>
<td></td>
</tr>
<tr>
<td>Chlorobenzene</td>
<td></td>
</tr>
<tr>
<td>Chloroethane (ethyl chloride)</td>
<td></td>
</tr>
<tr>
<td>Chloroform</td>
<td></td>
</tr>
<tr>
<td>Chloromethane</td>
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</tr>
<tr>
<td>Chloroprene</td>
<td></td>
</tr>
<tr>
<td>Cumene</td>
<td></td>
</tr>
<tr>
<td>Dichloroethyl ether</td>
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</tr>
<tr>
<td>Dinitrophenol</td>
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<tr>
<td>Epichlorohydrin</td>
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</tr>
<tr>
<td>Ethyl acrylate</td>
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</tr>
<tr>
<td>Ethylene oxide</td>
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</tr>
<tr>
<td>Hexachlorobenzene</td>
<td></td>
</tr>
<tr>
<td>Hexachlorobutadiene</td>
<td></td>
</tr>
<tr>
<td>Hexachloroethane</td>
<td></td>
</tr>
<tr>
<td>Methyl methacrylate</td>
<td></td>
</tr>
<tr>
<td>Methyl-t-butyl ether</td>
<td></td>
</tr>
<tr>
<td>Methylene chloride</td>
<td></td>
</tr>
<tr>
<td>N,N-dimethylaniline</td>
<td></td>
</tr>
<tr>
<td>Propionaldehyde</td>
<td></td>
</tr>
<tr>
<td>Propylene oxide</td>
<td></td>
</tr>
<tr>
<td>Styrene</td>
<td></td>
</tr>
<tr>
<td>Tetrachloroethene (perchloroethylene)</td>
<td></td>
</tr>
<tr>
<td>Tetrachloromethane (carbon tetrachloride)</td>
<td></td>
</tr>
<tr>
<td>Toluene</td>
<td></td>
</tr>
<tr>
<td>Trichlorobenzene (1,2,4-)</td>
<td></td>
</tr>
<tr>
<td>Trichloroethylene</td>
<td></td>
</tr>
<tr>
<td>Triethylamine</td>
<td></td>
</tr>
<tr>
<td>Trimethylpentane</td>
<td></td>
</tr>
<tr>
<td>Vinyl acetate</td>
<td></td>
</tr>
<tr>
<td>Vinyl chloride</td>
<td></td>
</tr>
<tr>
<td>Xylene (m)</td>
<td></td>
</tr>
<tr>
<td>Xylene (o)</td>
<td></td>
</tr>
<tr>
<td>Xylene (p)</td>
<td></td>
</tr>
<tr>
<td>N-hexane</td>
<td></td>
</tr>
</tbody>
</table>

### TABLE 3 TO SUBPART GGG.—SOLUBLE HAP

<table>
<thead>
<tr>
<th>Compound</th>
<th>Used as</th>
</tr>
</thead>
<tbody>
<tr>
<td>1,1-Dimethylhydrazine</td>
<td></td>
</tr>
<tr>
<td>1,4-Dioxane</td>
<td></td>
</tr>
<tr>
<td>Acetone</td>
<td></td>
</tr>
<tr>
<td>Acetophenone</td>
<td></td>
</tr>
<tr>
<td>Diethyl sulfate</td>
<td></td>
</tr>
<tr>
<td>Dimethyl sulfate</td>
<td></td>
</tr>
<tr>
<td>Dinitrotoluene</td>
<td></td>
</tr>
<tr>
<td>Ethylene glycol dimethyl ether</td>
<td></td>
</tr>
<tr>
<td>Ethylene glycol monobutyl ether acetate</td>
<td></td>
</tr>
<tr>
<td>Ethylene glycol monomethyl ether acetate</td>
<td></td>
</tr>
<tr>
<td>Isophorone</td>
<td></td>
</tr>
<tr>
<td>Methanol (methyl alcohol)</td>
<td></td>
</tr>
<tr>
<td>Nitrobenzene</td>
<td></td>
</tr>
<tr>
<td>Toluene</td>
<td></td>
</tr>
<tr>
<td>Control device</td>
<td>Monitoring equipment required</td>
</tr>
<tr>
<td>----------------</td>
<td>-------------------------------</td>
</tr>
<tr>
<td>All control devices</td>
<td>1. Flow indicator installed at all bypass lines to the atmosphere and equipped with continuous recorder or. 2. Valves sealed closed with car-seal or lock-and-key configuration.</td>
</tr>
<tr>
<td>Scrubber</td>
<td>Liquid flow rate or pressure drop mounting device. Also a pH monitor if the scrubber is used to control acid emissions.</td>
</tr>
<tr>
<td>Thermal incinerator</td>
<td>Temperature monitoring device installed in firebox or in ductwork immediately downstream of firebox.</td>
</tr>
<tr>
<td>Catalytic incinerator</td>
<td>Temperature monitoring device installed in gas stream immediately before and after catalyst bed.</td>
</tr>
<tr>
<td>Boiler or process heater &lt;44 mega watts and vent stream is not mixed with the primary fuel</td>
<td>Temperature monitoring device installed at condenser exit.</td>
</tr>
<tr>
<td>Condenser</td>
<td>None</td>
</tr>
<tr>
<td>Carbon adsorber (nonregenerative)</td>
<td>Stream flow monitoring device, and Carbon bed temperature monitoring device.</td>
</tr>
<tr>
<td>Carbon adsorber (regenerative)</td>
<td>None</td>
</tr>
</tbody>
</table>

*As an alternative to the monitoring requirements specified in this table, the owner or operator may use a CEM meeting the requirements of Performance Specifications 8 or 9 of appendix B of part 60 to monitor TOC every 15 minutes.

*Monitor may be installed in the firebox or in the ductwork immediately downstream of the firebox before any substantial heat exchange is encountered.
## Table 5 to Subpart GGG.—Control Requirements for Items of Equipment That Meet the Criteria of §63.1252(f)

<table>
<thead>
<tr>
<th>Item of equipment</th>
<th>Control requirement *</th>
</tr>
</thead>
<tbody>
<tr>
<td>Drain or drain hub</td>
<td>(a) Tightly fitting solid cover (TFSC); or</td>
</tr>
<tr>
<td></td>
<td>(b) TFSC with a vent to either a process, or to a fuel gas system, or to a control device meeting the requirements of §63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(c) Water seal with submerged discharge or barrier to protect discharge from wind.</td>
</tr>
<tr>
<td>Manhole</td>
<td>(a) TFSC; or</td>
</tr>
<tr>
<td></td>
<td>(b) TFSC with a vent to either a process, or to a fuel gas system, or to a control device meeting the requirements of §63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(c) If the item is vented to the atmosphere, use a TFSC with a properly operating water seal at the entrance or exit to the item to restrict ventilation in the collection system. The vent pipe shall be at least 90 cm in length and not exceeding 10.2 cm in nominal inside diameter.</td>
</tr>
<tr>
<td>Lift station</td>
<td>(a) TFSC; or</td>
</tr>
<tr>
<td></td>
<td>(b) TFSC with a vent to either a process, or to a fuel gas system, or to a control device meeting the requirements of §63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(c) If the lift station is vented to the atmosphere, use a TFSC with a properly operating water seal at the entrance or exit to the item to restrict ventilation in the collection system. The vent pipe shall be at least 90 cm in length and not exceeding 10.2 cm in nominal inside diameter. The lift station shall be level controlled to minimize changes in the liquid level.</td>
</tr>
<tr>
<td>Trench</td>
<td>(a) TFSC; or</td>
</tr>
<tr>
<td></td>
<td>(b) TFSC with a vent to either a process, or to a fuel gas system, or to a control device meeting the requirements of §63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(c) If the item is vented to the atmosphere, use a TFSC with a properly operating water seal at the entrance or exit to the item to restrict ventilation in the collection system. The vent pipe shall be at least 90 cm in length and not exceeding 10.2 cm in nominal inside diameter.</td>
</tr>
<tr>
<td>Pipe</td>
<td>Each pipe shall have no visible gaps in joints, seals, or other emission interfaces</td>
</tr>
<tr>
<td>Oil/Water separator</td>
<td>(a) Equip with a fixed roof and route vapors to a process or to a fuel gas system, or equip with a closed-vent system that routes vapors to a control device meeting the requirements of §63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(b) Equip with a floating roof that meets the equipment specifications of §60.693 (a)(1)(i), (a)(1)(ii), (a)(2), (a)(3), and (a)(4).</td>
</tr>
<tr>
<td>Tank</td>
<td>Maintain a fixed roof. If the tank is sparged or used for heating or treating by means of an exothermic reaction, a fixed roof and a system shall be maintained that routes the organic hazardous air pollutants vapors to other process equipment or a fuel gas system, or a closed-vent system that routes vapors to a control device that meets the requirements of 40 CFR §63.119 (e)(1) or (e)(2).</td>
</tr>
</tbody>
</table>

AAA: Where a tightly fitting solid cover is required, it shall be maintained with no visible gaps or openings, except during periods of sampling, inspection, or maintenance.

AAA: Manhole includes sumps and other points of access to a conveyance system.

AAA: A fixed roof may have openings necessary for proper venting of the tank, such as pressure/vacuum vent, j-pipe vent.

AAA: The liquid in the tank is agitated by injecting compressed air or gas.

## Table 6 to Subpart GGG.—Wastewater—Compliance Options for Wastewater Tanks

<table>
<thead>
<tr>
<th>Capacity, m³</th>
<th>Maximum true vapor pressure, kPa</th>
<th>Control requirements</th>
</tr>
</thead>
<tbody>
<tr>
<td>&lt;75</td>
<td></td>
<td>§63.1256(b)(1).</td>
</tr>
<tr>
<td>&gt;75 and &lt;151</td>
<td></td>
<td>§63.1256(b)(1).</td>
</tr>
<tr>
<td>&gt;151</td>
<td></td>
<td>§63.1256(b)(2).</td>
</tr>
<tr>
<td>To comply with</td>
<td>Inspection or monitoring requirement</td>
<td>Frequency of inspection or monitoring</td>
</tr>
<tr>
<td>---------------</td>
<td>--------------------------------------</td>
<td>--------------------------------------</td>
</tr>
<tr>
<td>TANKS:</td>
<td></td>
<td></td>
</tr>
<tr>
<td>63.1256(b)(3)(i)</td>
<td>Inspect fixed roof and all openings for leaks.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>63.1256(b)(3)(ii)</td>
<td>Inspect floating roof in accordance with §§63.120(a)(2) and (a)(3).</td>
<td>See §§63.120(a)(2) and (a)(3).</td>
</tr>
<tr>
<td>63.1256(b)(5)</td>
<td>Measure floating roof seal gaps in accordance with §§63.120(b)(2)(i) through (b)(4).</td>
<td>See §63.120(b)(2)(i) through (b)(4).</td>
</tr>
<tr>
<td></td>
<td>—Primary seal gaps</td>
<td>Initially Once every 5 years (annually if no secondary seal).</td>
</tr>
<tr>
<td></td>
<td>—Secondary seal gaps</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>SURFACE IMPOUNDMENTS:</td>
<td>Inspect wastewater tank for control equipment failures and improper work practices.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>CONTAINERS:</td>
<td>Inspect cover and all openings for leaks.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>63.1256(d)(1)(i)</td>
<td>Inspect surface impoundment for control equipment failures and improper work practices.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>INDIVIDUAL DRAIN SYSTEMS:</td>
<td>Inspect cover and all openings to ensure there are no gaps, cracks, or holes.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>63.1256(e)(1)(i)</td>
<td>Inspect individual drain system for control equipment failures and improper work practices.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>63.1256(e)(1)(ii)</td>
<td>Verify that sufficient water is present to properly maintain integrity of water seals.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>63.1256(e)(4)(i)</td>
<td>Inspect all drains using tightly-fitted caps or plugs to ensure caps and plugs are in place and properly installed.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>63.1256(e)(5)(i)</td>
<td>Inspect all junction boxes to ensure covers are in place and have no visible gaps, cracks, or holes.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>63.1256(e)(5)(ii)</td>
<td>Inspect unburied portion of all sewer lines for cracks and gaps.</td>
<td>Initially Semiannually</td>
</tr>
<tr>
<td>------------------</td>
<td>------------------------------------------------</td>
<td>-----------------------</td>
</tr>
<tr>
<td>63.1256(f)(3)</td>
<td>Primary seal gaps</td>
<td>Once every 5 years.</td>
</tr>
<tr>
<td>63.1256(f)(3)</td>
<td>Secondary seal gaps</td>
<td>Initially</td>
</tr>
<tr>
<td>63.1256(f)(4)</td>
<td>Inspect oil-water separator for control equipment failures and improper work practices.</td>
<td>Initially Semiannually</td>
</tr>
</tbody>
</table>

* As specified in §63.1256(e), the owner or operator shall comply with either the requirements of §63.1256(e)(1) and (2) or §63.1256(e)(4) and (5).
* Within 60 days of installation as specified in §63.1256(f)(3).
<table>
<thead>
<tr>
<th>Chemical name</th>
<th>CAS No.</th>
<th>Fr_m</th>
</tr>
</thead>
<tbody>
<tr>
<td>Acetaldehyde</td>
<td>75070</td>
<td>1.00</td>
</tr>
<tr>
<td>Acetonitrile</td>
<td>75059</td>
<td>0.99</td>
</tr>
<tr>
<td>Acetophenone</td>
<td>98862</td>
<td>0.31</td>
</tr>
<tr>
<td>Acrolein</td>
<td>107028</td>
<td>1.00</td>
</tr>
<tr>
<td>Acrylonitrile</td>
<td>107131</td>
<td>1.00</td>
</tr>
<tr>
<td>Allyl chloride</td>
<td>107051</td>
<td>1.00</td>
</tr>
<tr>
<td>Benzene</td>
<td>71432</td>
<td>1.00</td>
</tr>
<tr>
<td>Benzylic chloride</td>
<td>100447</td>
<td>1.00</td>
</tr>
<tr>
<td>Biphenyl</td>
<td>92524</td>
<td>0.86</td>
</tr>
<tr>
<td>Bromoform</td>
<td>75252</td>
<td>1.00</td>
</tr>
<tr>
<td>Butadiene (1,3-)</td>
<td>106990</td>
<td>1.00</td>
</tr>
<tr>
<td>Carbon disulfide</td>
<td>75150</td>
<td>1.00</td>
</tr>
<tr>
<td>Carbon tetrachloride</td>
<td>56235</td>
<td>1.00</td>
</tr>
<tr>
<td>Chlorobenzene</td>
<td>108907</td>
<td>0.96</td>
</tr>
<tr>
<td>Chloroform</td>
<td>67663</td>
<td>1.00</td>
</tr>
<tr>
<td>Chloroprene (2-Chloro-1,3-butadiene)</td>
<td>126998</td>
<td>1.00</td>
</tr>
<tr>
<td>Cumene</td>
<td>98828</td>
<td>1.00</td>
</tr>
<tr>
<td>Dichlorobenzene (p-1,4-)</td>
<td>106467</td>
<td>1.00</td>
</tr>
<tr>
<td>Dichloroethane (1,2-) (Ethylene dichloride)</td>
<td>107062</td>
<td>1.00</td>
</tr>
<tr>
<td>Dichloroethyether (bis(2-chloroethyl ether))</td>
<td>111444</td>
<td>0.76</td>
</tr>
<tr>
<td>Dichloropropene (1,3-)</td>
<td>542756</td>
<td>1.00</td>
</tr>
<tr>
<td>Diethyl sulfate</td>
<td>68675</td>
<td>0.0025</td>
</tr>
<tr>
<td>Dimethyl sulfate</td>
<td>77781</td>
<td>0.086</td>
</tr>
<tr>
<td>Dimethylamine (N,N)</td>
<td>121697</td>
<td>0.00080</td>
</tr>
<tr>
<td>Dimethyloxazine (1,1-)</td>
<td>57147</td>
<td>0.38</td>
</tr>
<tr>
<td>Dinitrophenol (2,4-)</td>
<td>51285</td>
<td>0.0077</td>
</tr>
<tr>
<td>Dinitrofluorobenzene</td>
<td>121142</td>
<td>0.085</td>
</tr>
<tr>
<td>Dioxane (1,4-) (1,4-Diethyleneglycol)</td>
<td>123911</td>
<td>0.87</td>
</tr>
<tr>
<td>Epichlorohydrin (1-Chloro-3,2-epoxypropane)</td>
<td>106898</td>
<td>0.94</td>
</tr>
<tr>
<td>Ethyl acrylate</td>
<td>140865</td>
<td>1.00</td>
</tr>
<tr>
<td>Ethylbenzene</td>
<td>106414</td>
<td>1.00</td>
</tr>
<tr>
<td>Ethyl chloride (Chloroethane)</td>
<td>75003</td>
<td>1.00</td>
</tr>
<tr>
<td>Ethylene dibromide (Dibromomethane)</td>
<td>106934</td>
<td>1.00</td>
</tr>
<tr>
<td>Ethylene glycol dimethyl ether</td>
<td>110714</td>
<td>0.86</td>
</tr>
<tr>
<td>Ethylene glycol monobutyl ether acetate</td>
<td>112072</td>
<td>0.043</td>
</tr>
<tr>
<td>Ethylene glycol monomethyl ether acetate</td>
<td>110946</td>
<td>0.0053</td>
</tr>
<tr>
<td>Ethylene oxide</td>
<td>75218</td>
<td>1.00</td>
</tr>
<tr>
<td>Ethyldiene dichloride (1,1-Dichloroethane)</td>
<td>75343</td>
<td>1.00</td>
</tr>
<tr>
<td>Hexachlorobenzene</td>
<td>118741</td>
<td>0.97</td>
</tr>
<tr>
<td>Hexachlorobutadiene</td>
<td>87683</td>
<td>0.88</td>
</tr>
<tr>
<td>Hexachloroethane</td>
<td>67721</td>
<td>0.50</td>
</tr>
<tr>
<td>Hexane</td>
<td>110543</td>
<td>1.00</td>
</tr>
<tr>
<td>Isophorone</td>
<td>78591</td>
<td>0.47</td>
</tr>
<tr>
<td>Methanol</td>
<td>67561</td>
<td>0.85</td>
</tr>
<tr>
<td>Methyl bromide (Bromomethane)</td>
<td>74839</td>
<td>1.00</td>
</tr>
<tr>
<td>Methyl chloride (Chloromethane)</td>
<td>74873</td>
<td>1.00</td>
</tr>
<tr>
<td>Methyl ethyl ketone (2-Butanone)</td>
<td>78930</td>
<td>0.99</td>
</tr>
<tr>
<td>Methyl isobutyl ketone (Hexone)</td>
<td>108101</td>
<td>0.98</td>
</tr>
<tr>
<td>Methyl methacrylate</td>
<td>80626</td>
<td>1.00</td>
</tr>
<tr>
<td>Methyl tert-butyl ether</td>
<td>162404</td>
<td>1.00</td>
</tr>
<tr>
<td>Methylenedioxyethane (Dichloromethane)</td>
<td>75092</td>
<td>1.00</td>
</tr>
<tr>
<td>Naphthalene</td>
<td>91203</td>
<td>0.99</td>
</tr>
<tr>
<td>Nitrobenzene</td>
<td>99453</td>
<td>0.39</td>
</tr>
<tr>
<td>Nitropropane (2-)</td>
<td>79469</td>
<td>0.99</td>
</tr>
<tr>
<td>Phosgene</td>
<td>75445</td>
<td>1.00</td>
</tr>
<tr>
<td>Propionaldehyde</td>
<td>123396</td>
<td>1.00</td>
</tr>
<tr>
<td>Propylene dichloride (1,2-Dichloropropane)</td>
<td>78875</td>
<td>1.00</td>
</tr>
<tr>
<td>Propylene oxide</td>
<td>75569</td>
<td>1.00</td>
</tr>
<tr>
<td>Styrene</td>
<td>100425</td>
<td>1.00</td>
</tr>
<tr>
<td>Tetrachloroethane (1,1,2,2-)</td>
<td>79345</td>
<td>1.00</td>
</tr>
<tr>
<td>Tetrachloroethylenesulfone (Perchloroethylene)</td>
<td>127184</td>
<td>1.00</td>
</tr>
<tr>
<td>Toluene</td>
<td>108883</td>
<td>1.00</td>
</tr>
<tr>
<td>Toluene (c-t)</td>
<td>95534</td>
<td>0.15</td>
</tr>
<tr>
<td>Trichlorobenzene (1,2,4-)</td>
<td>120621</td>
<td>1.00</td>
</tr>
<tr>
<td>Trichloroethylene (1,1,1-) (Methyl chloroform)</td>
<td>71556</td>
<td>1.00</td>
</tr>
<tr>
<td>Trichloroethylene (1,1,2-) (Vinyl Trichloride)</td>
<td>79005</td>
<td>0.98</td>
</tr>
<tr>
<td>Trichloroethylene</td>
<td>79016</td>
<td>1.00</td>
</tr>
<tr>
<td>Trichlorophenol (2,4,5-)</td>
<td>95994</td>
<td>1.00</td>
</tr>
<tr>
<td>Triethylamine</td>
<td>121448</td>
<td>1.00</td>
</tr>
<tr>
<td>Triethylamine monobutyl ether acetate</td>
<td>542841</td>
<td>1.00</td>
</tr>
<tr>
<td>Vinyl acetate</td>
<td>108054</td>
<td>1.00</td>
</tr>
</tbody>
</table>
Subpart HHH—National Emission Standards for Hazardous Air Pollutants From Natural Gas Transmission and Storage Facilities

SOURCE: 64 FR 32648, June 17, 1999, unless otherwise noted.

§ 63.1270 Applicability and designation of affected source.

(a) This subpart applies to owners and operators of natural gas transmission and storage facilities that transport or store natural gas prior to entering the pipeline to a local distribution company or to a final end user (if there is no local distribution company), and that are major sources of hazardous air pollutants (HAP) emissions as determined using the maximum natural gas throughput calculated as specified in either paragraph (a)(1) or (a)(2) of this section and paragraphs (a)(3) and (a)(4) of this section. A compressor station that transports natural gas prior to the point of custody transfer, or to a natural gas processing plant (if present) is considered a part of the oil and natural gas production source category. A facility that is determined to be an area source, based on emission estimates using the maximum natural gas throughput calculated as specified in paragraph (a)(1) or (a)(2) of this section, but subsequently increases emissions or potential to emit above the major source levels (without first obtaining and complying with other limitations that keep its potential to emit HAP below major source levels, becomes a major source and must comply thereafter with all applicable provisions of this subpart starting on the applicable compliance date specified in paragraph (d) of this section. Nothing in this paragraph is intended to preclude a source from limiting its potential to emit through other appropriate mechanisms that may be available through the permitting authority.

(1) Facilities that store, transport, or distribute natural gas shall determine major source status using the maximum annual facility natural gas throughput calculated according to paragraphs...
§ 63.1270  

(a)(1)(i) through (a)(1)(iv) of this section.  

(i) The owner or operator shall determine the number of hours to complete the storage cycle for the facility. The storage cycle is the number of hours for the injection cycle, calculated according to the equation in paragraph (a)(1)(i)(A) of this section, plus the number of hours for the withdrawal cycle, calculated according to the equation in paragraph (a)(1)(i)(B) of this section.  

(A) The hours for the facility injection cycle are determined according to the following equation:

\[
 IC = \frac{WGC}{IR_{\text{max}}} 
\]

Where:

- \( IC \) = Facility injection cycle in hours/cycle.  
- \( WGC \) = Working gas capacity in cubic meters. The working gas capacity is defined as the maximum storage capacity minus the FERC cushion (as defined in §63.1271).  
- \( IR_{\text{max}} \) = Maximum facility injection rate in cubic meters per hour.  

(B) The hours for the facility withdrawal cycle are determined according to the following equation:

\[
 WC = \frac{WGC}{WR_{\text{max}}} 
\]

Where:

- \( WC \) = Facility withdrawal cycle, hours/cycle.  
- \( WGC \) = Working gas capacity, cubic meters. The working gas capacity is defined as the maximum storage capacity minus the FERC cushion (as defined in §63.1271) and shall be the same value as used in paragraph (a)(1)(i)(A) of this section.  
- \( WR_{\text{max}} \) = Maximum facility withdrawal rate in cubic meters per hour.  

(ii) The owner or operator shall calculate the number of storage cycles for the facility per year according to the following equation:

\[
 \text{Cycle} = \frac{8760 \text{ hr/yr}}{IC + WC} 
\]

Where:

- \( \text{Cycle} \) = Number of storage cycles for the facility per year.  
- \( IC \) = Number of hours for a facility injection cycle, hours/cycle, as calculated in paragraph (a)(1)(i)(A) of this section.  
- \( WC \) = Number of hours for a facility withdrawal cycle, hours/cycle, as calculated in paragraph (a)(1)(i)(B) of this section.  

(iii) The owner or operator shall calculate the facilitywide maximum annual glycol dehydration unit hours of operation based on the following equation:

\[
 \text{Operation} = \text{Cycles} \times WC 
\]

Where:

- \( \text{Operation} \) = Facilitywide maximum annual glycol dehydration unit hours of operation (hr/yr).  
- \( \text{Cycles} \) = Number of storage cycles for the facility per year, as calculated in paragraph (a)(1)(i)(ii) of this section.  
- \( WC \) = Number of hours for a facility withdrawal cycle, hours/cycle, as calculated in paragraph (a)(1)(i)(B) of this section.  

(iv) The owner or operator shall calculate the maximum facilitywide natural gas throughput based on the following equation:

\[
 \text{Throughput} = \text{Operation} \times WR_{\text{max}} 
\]

Where:

- \( \text{Throughput} \) = Maximum facilitywide natural gas throughput in cubic meters per year.  
- \( \text{Operation} \) = Maximum facilitywide annual glycol dehydration unit hours of operation in hours per year, as calculated in paragraph (a)(1)(i)(iii) of this section.  
- \( WR_{\text{max}} \) = Maximum facility withdrawal rate in cubic meters per hour.  

(2) Facilities that only transport natural gas shall calculate the maximum natural gas throughput as the highest annual natural gas throughput over the 5 years prior to June 17, 1999, multiplied by a factor of 1.2.  

(3) The owner or operator shall maintain records of the annual facility natural gas throughput each year and upon request, submit such records to the Administrator. If the facility annual natural gas throughput increases above the maximum natural gas throughput calculated in paragraph (a)(1) or (a)(2) of this section, the maximum natural gas throughput must be recalculated using the higher throughput multiplied by a factor of 1.2.  

(4) The owner or operator shall determine the maximum values for other parameters used to calculate potential emissions as the maximum over the same period for which maximum throughput is determined as specified in paragraph (a)(1) or (a)(2) of this section. These parameters shall be based...
§ 63.1271 Definitions.

All terms used in this subpart shall have the meaning given to them in the Clean Air Act, subpart A of this part (General Provisions), and in this section. If the same term is defined in subpart A and in this section, it shall have the meaning given in this section for purposes of this subpart.

Boiler means an enclosed device using controlled flame combustion and having the primary purpose of recovering and exporting thermal energy in the form of steam or hot water. Boiler also means any industrial furnace as defined in 40 CFR 260.10.

Closed-vent system means a system that is not open to the atmosphere and is composed of piping, ductwork, connections, and if necessary, flow inducing devices that transport gas or vapor from an emission point to one or more control devices. If gas or vapor from regulated equipment is routed to a process (e.g., to a fuel gas system), the conveyance system shall not be considered a closed-vent system and is not subject to closed-vent system standards.

Combustion device means an individual unit of equipment, such as a flare, incinerator, process heater, or boiler, used for the combustion of organic HAP emissions.

Compressor station means any permanent combination of compressors that move natural gas at increased pressure from fields, in transmission pipelines, or into storage.

Continuous recorder means a data recording device that either records an instantaneous data value at least once every hour or records hourly or more frequent block average values.

Control device means any equipment used for recovering or oxidizing HAP or volatile organic compounds (VOC) vapors. Such equipment includes, but is not limited to, absorbers, carbon adsorbers, condensers, incinerators, flares, boilers, and process heaters. For the purposes of this subpart, if gas or vapor from regulated equipment is used, reused (i.e., injected into the flame zone of a combustion device), returned back to the process, or sold,
then the recovery system used, including piping, connections, and flow inducing devices, is not considered to be control devices or closed-vent systems.

Custody transfer means the transfer of hydrocarbon liquids or natural gas:

(1) After processing and/or treatment in the producing operations; or

(2) From storage vessels or automatic transfer facilities, or other equipment, including product loading racks, to pipelines or any other forms of transportation.

Facility means any grouping of equipment where natural gas is processed, compressed, or stored prior to entering a pipeline to a local distribution company or (if there is no local distribution company) to a final end user. Examples of a facility for this source category are: an underground natural gas storage operation; or a natural gas compressor station that receives natural gas via pipeline, from an underground natural gas storage operation, or from a natural gas processing plant. The emission points associated with these phases include, but are not limited to, process vents. Processes that may have vents include, but are not limited to, dehydration and compressor station engines.

Facility, for the purpose of a major source determination, means natural gas transmission and storage equipment that is located inside the boundaries of an individual surface site (as defined in this section) and is connected by ancillary equipment, such as gas flow lines or power lines. Equipment that is part of a facility will typically be located within close proximity to other equipment located at the same facility. Natural gas transmission and storage equipment or groupings of equipment located on different gas leases, mineral fee tracts, lease tracts, subsurface unit areas, surface fee tracts, or surface lease tracts shall not be considered part of the same facility.

Federal Energy Regulatory Commission Cushion or FERC Cushion means the minimum natural gas capacity of a storage field as determined by the Federal Energy Regulatory Commission.

Flame zone means the portion of the combustion chamber in a combustion device occupied by the flame envelope.

Flash tank. See the definition for gas-condensate-glycol (GCG) separator.

Flow indicator means a device which indicates whether gas flow is present in a line or whether the valve position would allow gas flow to be present in a line.

Gas-condensate-glycol (GCG) separator means a two- or three-phase separator through which the “rich” glycol stream of a glycol dehydration unit is passed to remove entrained gas and hydrocarbon liquid. The GCG separator is commonly referred to as a flash separator or flash tank.

Glycol dehydration unit means a device in which a liquid glycol (including, but not limited to, ethylene glycol, diethylene glycol, or triethylene glycol) absorbent directly contacts a natural gas stream and absorbs water in a contact tower or absorption column (absorber). The glycol contacts and absorbs water vapor and other gas stream constituents from the natural gas and becomes “rich” glycol. This glycol is then regenerated in the glycol dehydration unit reboiler. The “lean” glycol is then recycled.

Glycol dehydration unit baseline operations means operations representative of the glycol dehydration unit operations as of June 17, 1999. For the purposes of this subpart, for determining the percentage of overall HAP emission reduction attributable to process modifications, glycol dehydration unit baseline operations shall be parameter values (including, but not limited to, glycol circulation rate or glycol-HAP absorbency) that represent actual long-term conditions (i.e., at least 1 year). Glycol dehydration units in operation for less than 1 year shall document that the parameter values represent expected long-term operating conditions had process modifications not been made.

Glycol dehydration unit process vent means either the glycol dehydration unit reboiler vent and the vent from the GCG separator (flash tank), if present.

Glycol dehydration unit reboiler vent means the vent through which exhaust from the reboiler of a glycol dehydration unit passes from the reboiler to the atmosphere or to a control device.
Hazardous air pollutants or HAP means the chemical compounds listed in section 112(b) of the Clean Air Act (Act). All chemical compounds listed in section 112(b) of the Act need to be considered when making a major source determination. Only the HAP compounds listed in Table 1 of this subpart need to be considered when determining compliance.

Incinerator means an enclosed combustion device that is used for destroying organic compounds. Auxiliary fuel may be used to heat waste gas to combustion temperatures. Any energy recovery section is not physically formed into one manufactured or assembled unit with the combustion section; rather, the energy recovery section is a separate section following the combustion section and the two are joined by ducts or connections carrying flue gas. The above energy recovery section limitation does not apply to an energy recovery section used solely to preheat the incoming vent stream or combustion air.

Initial startup means the first time a new or reconstructed source begins production. For the purposes of this subpart, initial startup does not include subsequent startups (as defined in this section) of equipment, for example, following malfunctions or shutdowns.

Major source, as used in this subpart, shall have the same meaning as in §63.2, except that:

(1) Emissions from any pipeline compressor station or pump station shall not be aggregated with emissions from other similar units, whether or not such units are in a contiguous area or under common control; and

(2) Emissions from processes, operations, and equipment that are not part of the same facility, as defined in this section, shall not be aggregated.

Natural gas means a naturally occurring mixture of hydrocarbon and non-hydrocarbon gases found in geologic formations beneath the earth's surface. The principal hydrocarbon constituent is methane.

Natural gas transmission means the pipelines used for the long distance transport of natural gas (excluding processing). Specific equipment used in natural gas transmission includes the land, mains, valves, meters, boosters, regulators, storage vessels, dehydrators, compressors, and their driving units and appurtenances, and equipment used for transporting gas from a production plant, delivery point of purchased gas, gathering system, storage area, or other wholesale source of gas to one or more distribution area(s).

No detectable emissions means no escape of HAP from a device or system to the atmosphere as determined by:

(1) Instrument monitoring results in accordance with the requirements of §63.1282(b); and

(2) The absence of visible openings or defects in the device or system, such as rips, tears, or gaps.

Operating parameter value means a minimum or maximum value established for a control device or process parameter which, if achieved by itself or in combination with one or more other operating parameter values, indicates that an owner or operator has complied with an applicable operating parameter limitation, over the appropriate averaging period as specified in §63.1282(e) and (f).

Operating permit means a permit required by 40 CFR part 70 or part 71.

Organic monitoring device means an instrument used to indicate the concentration level of organic compounds exiting a control device based on a detection principle such as infra-red, photoionization, or thermal conductivity.

Primary fuel means the fuel that provides the principal heat input (i.e., more than 50 percent) to the device. To be considered primary, the fuel must be able to sustain operation without the addition of other fuels.

Process heater means an enclosed device using a controlled flame, the primary purpose of which is to transfer heat to a process fluid or process material that is not a fluid, or to a heat transfer material for use in a process (rather than for steam generation).

Safety device means a device that meets both of the following conditions: the device is not used for planned or routine venting of liquids, gases, or fumes from the unit or equipment on which the device is installed; and the
§ 63.1272 Startups, shutdowns, and malfunctions.

(a) The provisions set forth in this subpart shall apply at all times except during startups or shutdowns, during malfunctions, and during periods of non-operation of the affected sources (or specific portion thereof) resulting in cessation of the emissions to which this subpart applies. However, during the startup, shutdown, malfunction, or period of non-operation of one portion of an affected source, all emission points which can comply with the specific provisions to which they are subject must do so during the startup, shutdown, malfunction, or period of non-operation.

(b) The owner or operator shall not shut down items of equipment that are required or utilized for compliance with the provisions of this subpart during times when emissions are being routed to such items of equipment, if the shutdown would contravene requirements of this subpart applicable to such items of equipment. This paragraph does not apply if the item of equipment is malfunctioning, or if the owner or operator must shut down the equipment to avoid damage due to a contemporaneous startup, shutdown, or malfunction of the affected source or a portion thereof.

(c) During startups, shutdowns, and malfunctions when the requirements of this subpart do not apply pursuant to paragraphs (a) and (b) of this section, the owner or operator shall implement, to the extent reasonably available, measures to prevent or minimize excess emissions to the maximum extent practical. For purposes of this paragraph, the term “excess emissions” means emissions in excess of those that would have occurred if there were no startup, shutdown, or malfunction, and

device remains in a closed, sealed position at all times except when an unplanned event requires that the device open for the purpose of preventing physical damage or permanent deformation of the unit or equipment on which the device is installed in accordance with good engineering and safety practices for handling flammable, combustible, explosive, or other hazardous materials. Examples of unplanned events which may require a safety device to open include failure of an essential equipment component or a sudden power outage.

Shutdown means for purposes including, but not limited to, periodic maintenance, replacement of equipment, or repair, the cessation of operation of a glycol dehydration unit, or other affected source under this subpart, or equipment required or used solely to comply with this subpart.

Startup means the setting into operation of a glycol dehydration unit, or other affected equipment under this subpart, or equipment required or used to comply with this subpart. Startup includes initial startup and operation solely for the purpose of testing equipment.

Storage vessel means a tank or other vessel that is designed to contain an accumulation of crude oil, condensate, intermediate hydrocarbon liquids, produced water, or other liquid, and is constructed primarily of non-earthed materials (e.g., wood, concrete, steel, plastic) that provide structural support.

Surface site means any combination of one or more graded pad sites, gravel pad sites, foundations, platforms, or the immediate physical location upon which equipment is physically affixed.

Temperature monitoring device means an instrument used to monitor temperature and having a minimum accuracy of ±2 percent of the temperature being monitored expressed in °C, or ±2.5 °C, whichever is greater. The temperature monitoring device may measure temperature in degrees Fahrenheit or degrees Celsius, or both.

Total organic compounds or TOC, as used in this subpart, means those compounds which can be measured according to the procedures of Method 18, 40 CFR part 60, appendix A.

Underground storage means the subsurface facilities utilized for storing natural gas that has been transferred from its original location for the primary purpose of load balancing, which is the process of equalizing the receipt and delivery of natural gas. Processes and operations that may be located at an underground storage facility include, but are not limited to, compression and dehydration.
the owner or operator complied with the relevant provisions of this subpart. The measures to be taken shall be identified in the applicable startup, shutdown, and malfunction plan, and may include, but are not limited to, air pollution control technologies, recovery technologies, work practices, pollution prevention, monitoring, and/or changes in the manner of operation of the source. Back-up control devices are not required, but may be used if available.

(d) The owner or operator shall prepare a startup, shutdown, or malfunction plan as required in § 63.6(e)(3) except that the plan is not required to be incorporated by reference into the source's Title V permit as specified in § 63.6(e)(3)(i). Instead, the owner or operator shall keep the plan on record as required by § 63.6(e)(3)(v). The failure of the plan to adequately minimize emissions during the startup, shutdown, or malfunction does not shield an owner or operator from enforcement actions.

§ 63.1273 [Reserved]

§ 63.1274 General standards.

(a) Table 2 of this subpart specifies the provisions of subpart A (General Provisions) that apply and those that do not apply to owners and operators of affected sources subject to this subpart.

(b) All reports required under this subpart shall be sent to the Administrator at the appropriate address listed in § 63.13. Reports may be submitted on electronic media.

(c) Except as specified in paragraph (d) of this section, the owner or operator of an affected source (i.e., glycol dehydration unit) located at an existing or new major source of HAP emissions shall comply with the requirements in this subpart as follows:

(1) The control requirements for glycol dehydration unit process vents specified in § 63.1275;

(2) The monitoring requirements specified in § 63.1283; and

(3) The recordkeeping and reporting requirements specified in §§ 63.1284 and 63.1285.

(d) Exemptions. The owner or operator is exempt from the requirements of paragraphs (c)(1) and (c)(2) of this section if the criteria listed in paragraph (d)(1) or (d)(2) of this section are met. Records of the determination of these criteria must be maintained as required in § 63.1284(d) of this subpart.

(1) The actual annual average flow of gas to the glycol dehydration unit is less than 283 thousand standard cubic meters per day, as determined by the procedures specified in § 63.1282(a)(1) of this subpart; or

(2) The actual average emissions of benzene from the glycol dehydration unit process vents to the atmosphere are less than 0.90 megagrams per year as determined by the procedures specified in § 63.1282(a)(2) of this subpart.

(e) Each owner or operator of a major HAP source subject to this subpart is required to apply for a part 70 or part 71 operating permit from the appropriate permitting authority. If the Administrator has approved a State operating permit program under part 70, the permit shall be obtained from the State authority. If a State operating permit program has not been approved, the owner or operator shall apply to the EPA Regional Office pursuant to part 71.

(f) [Reserved]

(g) In all cases where the provisions of this subpart require an owner or operator to repair leaks by a specified time after the leak is detected, it is a violation of this standard to fail to take action to repair the leak(s) within the specified time. If action is taken to repair the leak(s) within the specified time, failure of that action to successfully repair the leak(s) is not a violation of this standard. However, if the repairs are unsuccessful, a leak is detected and the owner or operator shall take further action as required by the applicable provisions of this subpart.

§ 63.1275 Glycol dehydration unit process vent standards.

(a) This section applies to each glycol dehydration unit, subject to this subpart, with an actual annual average natural gas flowrate equal to or greater than 283 thousand standard cubic meters per day and with actual average benzene glycol dehydration unit process vent emissions equal to or greater than 0.90 megagrams per year.

(b) Except as provided in paragraph (c) of this section, an owner or operator
of a glycol dehydration unit process vent shall comply with the requirements specified in paragraphs (b)(1) and (b)(2) of this section.

(1) For each glycol dehydration unit process vent, the owner or operator shall control air emissions by either paragraph (b)(1)(i) or (b)(1)(ii) of this section.

(i) The owner or operator shall connect the process vent to a control device or a combination of control devices through a closed-vent system. The closed-vent system shall be designed and operated in accordance with the requirements of §63.1281(c). The control device(s) shall be designed and operated in accordance with the requirements of §63.1281(d).

(ii) The owner or operator shall connect the process vent to a control device or a combination of control devices through a closed-vent system and the outlet benzene emissions from the control device(s) shall be less than 0.90 megagrams per year. The closed-vent system shall be designed and operated in accordance with the requirements of §63.1281(c). The control device(s) shall be designed and operated in accordance with the requirements of §63.1281(d), except that the performance requirements specified in §63.1281(d)(i) and (ii) do not apply.

(2) One or more safety devices that vent directly to the atmosphere may be used on the air emission control equipment installed to comply with paragraph (b)(1) of this section.

(c) As an alternative to the requirements of paragraph (b) of this section, the owner or operator may comply with one of the following:

(1) The owner or operator shall control air emissions by connecting the process vent to a process natural gas line.

(2) The owner or operator shall demonstrate, to the Administrator’s satisfaction, that the total HAP emissions to the atmosphere from the glycol dehydration unit process vent are reduced by 95.0 percent through process modifications or a combination of process modifications and one or more control devices, in accordance with the requirements specified in §63.1281(e).

(3) Control of HAP emissions from a GCG separator (flash tank) vent is not required if the owner or operator demonstrates, to the Administrator’s satisfaction, that total emissions to the atmosphere from the glycol dehydration unit process vent are reduced by one of the levels specified in paragraphs (c)(3)(i) through (c)(3)(ii), through the installation and operation of controls as specified in paragraph (b)(1) of this section.

(i) HAP emissions are reduced by 95.0 percent or more.

(ii) Benzene emissions are reduced to a level less than 0.90 megagrams per year.

§§ 63.1276–63.1280 [Reserved]

§ 63.1281 Control equipment requirements.

(a) This section applies to each closed-vent system and control device installed and operated by the owner or operator to control air emissions as required by the provisions of this subpart. Compliance with paragraphs (c) and (d) of this section will be determined by review of the records required by §63.1284, the reports required by §63.1285, by review of performance test results, and by inspections.

(b) [Reserved]

(c) Closed-vent system requirements.

(1) The closed-vent system shall route all gases, vapors, and fumes emitted from the material in a HAP emissions unit to a control device that meets the requirements specified in paragraph (d) of this section.

(2) The closed-vent system shall be designed and operated with no detectable emissions.

(3) If the closed-vent system contains one or more bypass devices that could be used to divert all or a portion of the gases, vapors, or fumes from entering the control device, the owner or operator shall meet the requirements specified in paragraphs (c)(3)(i) and (c)(3)(ii) of this section.

(i) For each bypass device, except as provided for in paragraph (c)(3)(ii) of this section, the owner or operator shall either:

(A) Properly install, calibrate, maintain, and operate a flow indicator at the inlet to the bypass device that could divert the stream away from the control device to the atmosphere that
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takes a reading at least once every 15 minutes, and that sounds an alarm when the bypass device is open such that the stream is being, or could be, diverted away from the control device to the atmosphere; or

(B) Secure the bypass device valve installed at the inlet to the bypass device in the non-diverting position using a car-seal or a lock-and-key type configuration. The owner or operator shall visually inspect the seal or closure mechanism at least once every month to verify that the valve is maintained in the non-diverting position and the vent stream is not diverted through the bypass device.

(ii) Low leg drains, high point bleeds, analyzer vents, open-ended valves or lines, and safety devices are not subject to the requirements of paragraph (c)(3)(i) of this section.

(d) Control device requirements. (1) The control device used to reduce HAP emissions in accordance with the standards of this subpart shall be one of the control devices specified in paragraphs (d)(1)(i) through (iii) of this section.

(i) An enclosed combustion device (e.g., thermal vapor incinerator, catalytic vapor incinerator, boiler, or process heater) that is designed and operated in accordance with one of the following performance requirements:

(A) Reduces the mass content of either TOC or total HAP in the gases vented to the device by 95.0 percent by weight or greater, as determined in accordance with the requirements of §63.1282(d);

(B) Reduces the concentration of either TOC or total HAP in the exhaust gases at the outlet to the device to a level equal to or less than 20 parts per million by volume on a dry basis corrected to 3 percent oxygen as determined in accordance with the requirements of §63.1282(d);

(C) Operates at a minimum residence time of 0.5 second at a minimum temperature of 760 °C.

(D) If a boiler or process heater is used as the control device, then the vent stream shall be introduced into the flame zone of the boiler or process heater.

(ii) A vapor recovery device (e.g., carbon adsorption system or condenser) or other control device that is designed and operated to reduce the mass content of either TOC or total HAP in the gases vented to the device by 95.0 percent by weight or greater as determined in accordance with the requirements of §63.1282(d).

(iii) A flare that is designed and operated in accordance with the requirements of §63.11(b).

(2) [Reserved]

(3) The owner or operator shall demonstrate that a control device achieves the performance requirements of paragraph (d)(1) of this section by following the procedures specified in §63.1282(d).

(4) The owner or operator shall operate each control device in accordance with the requirements specified in paragraphs (d)(4)(i) and (ii) of this section.

(i) Each control device used to comply with this subpart shall be operating at all times when gases, vapors, and fumes are vented from the emissions unit or units through the closed-vent system to the control device, as required under §63.1275, except when maintenance or repair of a unit cannot be completed without a shutdown of the control device. An owner or operator may vent more than one unit to a control device used to comply with this subpart.

(ii) For each control device monitored in accordance with the requirements of §63.1283(d), the owner or operator shall demonstrate compliance according to the requirements of §63.1282(e), or (f) as applicable.

(5) For each carbon adsorption system used as a control device to meet the requirements of paragraph (d)(1) of this section, the owner or operator shall manage the carbon as follows:

(i) Following the initial startup of the control device, all carbon in the control device shall be replaced with fresh carbon on a regular, predetermined time interval that is no longer than the carbon service life established for the carbon adsorption system.

(ii) The spent carbon removed from the carbon adsorption system shall be either regenerated, reactivated, or burned in one of the units specified in paragraphs (d)(5)(ii)(A) through (d)(5)(ii)(G) of this section.
(A) Regenerated or reactivated in a thermal treatment unit for which the owner or operator has been issued a final permit under 40 CFR part 270 that implements the requirements of 40 CFR part 264, subpart X.

(B) Regenerated or reactivated in a thermal treatment unit equipped with and operating organic air emission controls in accordance with this section.

(C) Regenerated or reactivated in a thermal treatment unit equipped with and operating organic air emission controls in accordance with a national emissions standard for HAP under another subpart in 40 CFR part 61 or this part.

(D) Burned in a hazardous waste incinerator for which the owner or operator has been issued a final permit under 40 CFR part 270 that implements the requirements of 40 CFR part 264, subpart O.

(E) Burned in a hazardous waste incinerator which the owner or operator has designed and operates in accordance with the requirements of 40 CFR part 265, subpart O.

(F) Burned in a boiler or industrial furnace for which the owner or operator has been issued a final permit under 40 CFR part 270 that implements the requirements of 40 CFR part 266, subpart H.

(G) Burned in a boiler or industrial furnace which the owner or operator has designed and operates in accordance with the interim status requirements of 40 CFR part 266, subpart H.

(e) Process modification requirements. Each owner or operator that chooses to comply with §63.1275(c)(2) shall meet the requirements specified in paragraphs (e)(1) through (e)(3) of this section.

(1) The owner or operator shall determine glycol dehydration unit baseline operations (as defined in §63.1271). Records of glycol dehydration unit baseline operations shall be retained as required under §63.1274(b)(1).

(2) The owner or operator shall document, to the Administrator’s satisfaction, the conditions for which the glycol dehydration unit baseline operations shall be modified to achieve the 95.0 percent overall HAP emission reduction, either through process modifications or through a combination of process modifications and one or more control devices. If a combination of process modifications and one or more control devices is used, the owner or operator shall also establish the percent HAP reduction to be achieved by the control device to achieve an overall HAP emission reduction of 95.0 percent for the glycol dehydration unit process vent. Only modifications in glycol dehydration unit operations directly related to process changes, including, but not limited to, changes in glycol circulation rate or glycol-HAP absorbency, shall be allowed. Changes in the inlet gas characteristics or natural gas throughput rate shall not be considered in determining the overall HAP emission reduction.

(3) The owner or operator that achieves a 95.0 percent HAP emission reduction using process modifications alone shall comply with paragraph (e)(3)(i) of this section. The owner or operator that achieves a 95.0 percent HAP emission reduction using a combination of process modifications and one or more control devices shall comply with paragraphs (e)(3)(i) and (e)(3)(ii) of this section.

(i) The owner or operator shall maintain records, as required in §63.1274(b)(10), that the facility continues to operate in accordance with the conditions specified under paragraph (e)(2) of this section.

(ii) The owner or operator shall comply with the control device requirements specified in paragraph (d) of this section, except that the emission reduction achieved shall be the emission reduction specified in paragraph (e)(2) of this section.

§63.1282 Test methods, compliance procedures, and compliance demonstrations.

(a) Determination of glycol dehydration unit flowrate or benzene emissions. The procedures of this paragraph shall be used by an owner or operator to determine glycol dehydration unit natural gas flowrate or benzene emissions to meet the criteria for the exemption from control requirements under §63.1274(d).

(1) The determination of actual flowrate of natural gas to a glycol dehydration unit shall be made using the
procedures of either paragraph (a)(1)(i) or (a)(1)(ii) of this section.

(i) The owner or operator shall install and operate a monitoring instrument that directly measures natural gas flowrate to the glycol dehydration unit with an accuracy of plus or minus 2 percent or better. The owner or operator shall convert the annual natural gas flowrate to a daily average by dividing the annual flowrate by the number of days per year the glycol dehydration unit processed natural gas.

(ii) The owner or operator shall document, to the Administrator's satisfaction, that the actual annual average natural gas flowrate to the glycol dehydration unit is less than 85 thousand standard cubic meters per day.

(2) The determination of actual average benzene emissions from a glycol dehydration unit shall be made using the procedures of either paragraph (a)(2)(i) or (a)(2)(ii) of this section.

Emissions shall be determined either uncontrolled or with federally enforceable controls in place.

(i) The owner or operator shall determine actual average benzene emissions using the model GRI-GLYCalc\textsuperscript{TM}, Version 3.0 or higher, and the procedures presented in the associated GRI-GLYCalc\textsuperscript{TM} Technical Reference Manual. Inputs to the model shall be representative of actual operating conditions of the glycol dehydration unit and may be determined using the procedures documented in the Gas Research Institute (GRI) report entitled “Atmospheric Rich/Lean Method for Determining Glycol Dehydrator Emissions” (GRI-95/0368.1); or

(ii) The owner or operator shall determine an average mass rate of benzene emissions in kilograms per hour through direct measurement by performing three runs of Method 18 in 40 CFR part 60, appendix A (or an equivalent method), and averaging the results of the three runs. Annual emissions in kilograms per year shall be determined by multiplying the mass rate by the number of hours the unit is operated per year. This result shall be converted to megagrams per year.

(b) No detectable emissions test procedure. (1) The procedure shall be conducted in accordance with Method 21, 40 CFR part 60, appendix A.

(2) The detection instrument shall meet the performance criteria of Method 21, 40 CFR part 60, appendix A, except the instrument response factor criteria in section 3.1.2(a) of Method 21 shall be for the average composition of the fluid, and not for each individual organic compound in the stream.

(3) The detection instrument shall be calibrated before use on each day of its use by the procedures specified in Method 21, 40 CFR part 60, appendix A.

(4) Calibration gases shall be as follows:

(i) Zero air (less than 10 parts per million by volume hydrocarbon in air); and

(ii) A mixture of methane in air at a methane concentration of less than 10,000 parts per million by volume.

(5) An owner or operator may choose to adjust or not adjust the detection instrument readings to account for the background organic concentration level. If an owner or operator chooses to adjust the instrument readings for the background level, the background level value must be determined according to the procedures in Method 21 of 40 CFR part 60, appendix A.

(6)(i) Except as provided in paragraph (b)(6)(ii) of this section, the detection instrument shall meet the performance criteria of Method 21 of 40 CFR part 60, appendix A, except the instrument response factor criteria in section 3.1.2(a) of Method 21 shall be for the average composition of the process fluid not each individual volatile organic compound in the stream. For process streams that contain nitrogen, air, or other inerts which are not organic hazardous air pollutants or volatile organic compounds, the average stream response factor shall be calculated on an inert-free basis.

(ii) If no instrument is available at the facility that will meet the performance criteria specified in paragraph (b)(6)(ii) of this section, the instrument readings may be adjusted by multiplying by the average response factor of the process fluid, calculated on an inert-free basis as described in paragraph (b)(6)(i) of this section.

(7) An owner or operator must determine if a potential leak interface operates with no detectable emissions using the applicable procedure specified in
paragraph (b)(7)(i) or (b)(7)(ii) of this section.

(i) If an owner or operator chooses not to adjust the detection instrument readings for the background organic concentration level, then the maximum organic concentration value measured by the detection instrument is compared directly to the applicable value for the potential leak interface as specified in paragraph (b)(8) of this section.

(ii) If an owner or operator chooses to adjust the detection instrument readings for the background organic concentration level, the value of the arithmetic difference between the maximum organic concentration value measured by the instrument and the background organic concentration value as determined in paragraph (b)(5) of this section is compared with the applicable value for the potential leak interface as specified in paragraph (b)(8) of this section.

(8) A potential leak interface is determined to operate with no detectable organic emissions if the organic concentration value determined in paragraph (b)(7) is less than 500 parts per million by volume.

(c) [Reserved]

d) Control device performance test procedures. This paragraph applies to the performance testing of control devices. The owners or operators shall demonstrate that a control device achieves the performance requirements of §63.1281(d)(1) or (e)(3)(ii) using either a performance test as specified in paragraph (d)(3) of this section or a design analysis as specified in paragraph (d)(4) of this section. The owner or operator may elect to use the alternative procedures in paragraph (d)(5) of this section for performance testing of a condenser used to control emissions from a glycol dehydration unit process vent.

(1) The following control devices are exempt from the requirements to conduct performance tests and design analyses under this section:

(i) A flare that is designed and operated in accordance with §63.11(b);

(ii) A boiler or process heater with a design heat input capacity of 44 megawatts or greater;

(iii) A boiler or process heater into which the vent stream is introduced with the primary fuel or is used as the primary fuel;

(iv) A boiler or process heater burning hazardous waste for which the owner or operator has either been issued a final permit under 40 CFR part 270 and complies with the requirements of 40 CFR part 266, subpart H, or has certified compliance with the interim status requirements of 40 CFR part 266, subpart H;

(v) A hazardous waste incinerator for which the owner or operator has been issued a final permit under 40 CFR part 270 and complies with the requirements of 40 CFR part 264, subpart O, or has certified compliance with the interim status requirements of 40 CFR part 265, subpart O.

(vi) A control device for which a performance test was conducted for determining compliance with a regulation promulgated by the EPA, and the test was conducted using the same methods specified in this section, and either no process changes have been made since the test, or the owner or operator can demonstrate that the results of the performance test, with or without adjustments, reliably demonstrate compliance despite process changes.

(2) An owner or operator shall design and operate each flare in accordance with the requirements specified in §63.11(b) and in paragraphs (d)(2)(i) and (d)(2)(ii) of this section.

(i) The compliance determination shall be conducted using Method 22 of 40 CFR part 60, appendix A, to determine visible emissions.

(ii) An owner or operator is not required to conduct a performance test to determine percent emission reduction or outlet organic HAP or TOC concentration when a flare is used.

(3) For a performance test conducted to demonstrate that a control device meets the requirements of §63.1281(d)(1) or (e)(3)(i), the owner or operator shall use the test methods and procedures specified in paragraphs (d)(3)(i) through (d)(3)(iv) of this section. The performance test shall be conducted according to the schedule specified in §63.7(a)(2), and the results of the performance test shall be submitted in the Notification of Compliance Status Report as required in §63.1285(d)(1)(ii).
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(i) Method 1 or 1A, 40 CFR part 60, appendix A, as appropriate, shall be used for selection of the sampling sites specified in paragraphs (d)(3)(i)(A) and (B) of this section. Any references to particulate mentioned in Methods 1 and 1A do not apply to this section.

(A) To determine compliance with the control device percent reduction requirements specified in § 63.1281(d)(1)(i)(A), (d)(1)(ii), or (e)(3)(ii), sampling sites shall be located at the inlet of the first control device and at the outlet of the final control device.

(B) To determine compliance with the enclosed combustion device total HAP concentration limit specified in § 63.1281(d)(1)(i)(B), the sampling site shall be located at the outlet of the control device.

(ii) The gas volumetric flowrate shall be determined using Method 2, 2A, 2C, or 2D, 40 CFR part 60, appendix A, as appropriate.

(iii) To determine compliance with the control device percent reduction performance requirement in § 63.1281(d)(1)(i)(A), 63.1281(d)(1)(ii), or 63.1281(e)(3)(ii), the owner or operator shall use either Method 18, 40 CFR part 60, appendix A, or Method 25A, 40 CFR part 60, appendix A; alternatively, any other method or data that have been validated according to the applicable procedures in Method 301 of appendix A of this part may be used. The following procedures shall be used to calculate the percentage of reduction:

(A) The minimum sampling time for each run shall be 1 hour in which either an integrated sample or a minimum of four grab samples shall be taken. If grab sampling is used, then the samples shall be taken at approximately equal intervals in time, such as 15-minute intervals during the run.

(B) The mass rate of either TOC (minus methane and ethane) or total HAP (Ei, Eo) shall be calculated.

1. The following equations shall be used:

\[ E_i = K_2 \left( \sum_{j=1}^{n} C_{ij} M_{ij} \right) Q_i \]

Where:

\[ C_{ij}, C_{oj} = \text{Concentration of sample component } j \text{ of the gas stream at the inlet and outlet of the control device, respectively, dry basis, parts per million by volume.} \]

\[ E_i, E_o = \text{Mass rate of TOC (minus methane and ethane) or total HAP at the inlet and outlet of the control device, respectively, dry basis, kilogram per hour.} \]

\[ M_{ij}, M_{oj} = \text{Molecular weight of sample component } j \text{ of the gas stream at the inlet and outlet of the control device, respectively, gram/gram-mole.} \]

\[ Q_i, Q_o = \text{Flowrate of gas stream at the inlet and outlet of the control device, respectively, dry standard cubic meter per minute.} \]

\[ K_2 = \text{Constant, } 2.494 \times 10^{-6} \text{ (parts per million)} \cdot \text{gram-mole per standard cubic liter)} \cdot \text{gram/gram}) \cdot \text{minute/hour), where standard temperature is } 20^\circ \text{C.} \]

(B) When the TOC mass rate is calculated, all organic compounds (minus methane and ethane) measured by Method 18, of 40 CFR part 60, appendix A; or Method 25A, 40 CFR part 60, appendix A, shall be summed using the equations in paragraph (d)(3)(iii)(B)(1) of this section.

(C) When the total HAP mass rate is calculated, only HAP chemicals listed in Table 1 of this subpart shall be summed using the equations in paragraph (d)(3)(iii)(B)(1) of this section.

(C) The percentage of reduction in TOC (minus methane and ethane) or total HAP shall be calculated as follows:

\[ R_{cd} = \frac{E_i - E_o}{E_i} \times 100\% \]

Where:

\[ R_{cd} = \text{Control efficiency of control device, percent.} \]

\[ E_i, E_o = \text{Mass rate of TOC (minus methane and ethane) or total HAP at the inlet to the control device as calculated under paragraph (d)(3)(iii)(B) of this section, kilograms TOC per hour or kilograms HAP per hour.} \]

\[ E_o = \text{Mass rate of TOC (minus methane and ethane) or total HAP at the outlet of the control device, as calculated under paragraph (d)(3)(iii)(B) of this section, kilograms TOC per hour or kilograms HAP per hour.} \]
(D) If the vent stream entering a boiler or process heater with a design capacity less than 44 megawatts is introduced with the combustion air or as a secondary fuel, the weight-percentage of reduction of total HAP or TOC (minus methane and ethane) across the device shall be determined by comparing the TOC (minus methane and ethane) or total HAP in all combusted vent streams and primary and secondary fuels with the TOC (minus methane and ethane) or total HAP exiting the device, respectively.

(iv) To determine compliance with the enclosed combustion device total HAP concentration limit specified in §63.1281(d)(1)(i)(B), the owner or operator shall use either Method 18, 40 CFR part 60, appendix A; or Method 25A, 40 CFR part 60, appendix A, to measure either TOC (minus methane and ethane) or total HAP. Alternatively, any other method or data that have been validated according to Method 301 of appendix A of this part, may be used. The following procedures shall be used to calculate parts per million by volume concentration, corrected to 3 percent oxygen:

(A) The minimum sampling time for each run shall be 1 hour in which either an integrated sample or a minimum of four grab samples shall be taken. If grab sampling is used, then the samples shall be taken at approximately equal intervals in time, such as 15-minute intervals during the run.

(B) The TOC concentration or total HAP concentration shall be calculated according to paragraph (d)(3)(iv)(B)(1) or (d)(3)(iv)(B)(2) of this section.

(1) The TOC concentration (C_{TOC}) is the sum of the concentrations of the individual components and shall be computed for each run using the following equation:

\[ C_{TOC} = \frac{\sum_{j=1}^{n} C_{ji}}{x} \]

Where:

\( C_{TOC} \) = Concentration of total organic compounds minus methane and ethane, dry basis, parts per million by volume.

\( C_{ji} \) = Concentration of sample components j of sample i, dry basis, parts per million by volume.

\( n \) = Number of components in the sample.

\( x \) = Number of samples in the sample run.

(2) The total HAP concentration (C_{HAP}) shall be computed according to the equation in paragraph (d)(3)(iv)(B)(1) of this section, except that only HAP chemicals listed in Table 1 of this subpart shall be summed.

(C) The TOC concentration or total HAP concentration shall be corrected to 3 percent oxygen as follows:

(1) The emission rate correction factor for excess air, integrated sampling and analysis procedures of Method 3B, 40 CFR part 60, appendix A, shall be used to determine the oxygen concentration (%O_{2d}). The samples shall be taken during the same time that the samples are taken for determining TOC concentration or total HAP concentration.

(2) The concentration corrected to 3 percent oxygen (C_{c}) shall be computed using the following equation:

\[ C_{c} = C_{m} \left( \frac{17.9}{20.9 - \%O_{2d}} \right) \]

Where:

\( C_{c} \) = TOC concentration of total HAP concentration corrected to 3 percent oxygen, dry basis, parts per million by volume.

\( C_{m} \) = TOC concentration or total HAP concentration, dry basis, parts per million by volume.

\( \%O_{2d} \) = Concentration of oxygen, dry basis, percent by volume.

(4) For a design analysis conducted to meet the requirements of §63.1281(d)(1) or (e)(3)(ii), the owner or operator shall meet the requirements specified in paragraphs (d)(4)(i) and (d)(4)(ii) of this section. Documentation of the design analysis shall be submitted as a part of the Notification of Compliance Status Report as required in §63.1285(d)(1)(i).

(i) The design analysis shall include analysis of the vent stream characteristics and control device operating parameters for the applicable control device as specified in paragraphs (d)(4)(i) (A) through (F) of this section.

(A) For a thermal vapor incinerator, the design analysis shall include the vent stream composition, constituent
concentrations, and flowrate and shall establish the design minimum and average temperatures in the combustion zone and the combustion zone residence time.

(B) For a catalytic vapor incinerator, the design analysis shall include the vent stream composition, constituent concentrations, and flowrate and shall establish the design minimum and average temperatures across the catalyst bed inlet and outlet, and the design service life of the catalyst.

(C) For a boiler or process heater, the design analysis shall include the vent stream composition, constituent concentrations, and flowrate; shall establish the design minimum and average flame zone temperatures and combustion zone residence time; and shall describe the method and location where the vent stream is introduced into the flame zone.

(D) For a condenser, the design analysis shall include the vent stream composition, constituent concentrations, flowrate, relative humidity, and temperature, and shall establish the design outlet organic compound concentration level, design average temperature of the condenser exhaust vent stream, and the design average temperatures of the coolant fluid at the condenser inlet and outlet. As an alternative to the design analysis, an owner or operator may elect to use the procedures specified in paragraph (d)(5) of this section.

(E) For a regenerable carbon adsorption, the design analysis shall include the vent stream composition, constituent concentrations, flowrate, relative humidity, and temperature, and shall establish the design exhaust vent stream organic compound concentration level, adsorption cycle time, number and capacity of carbon beds, type and working capacity of activated carbon used for the carbon bed, design total regeneration stream flow over the period of each complete carbon bed regeneration cycle, design carbon bed temperature after regeneration, design carbon bed regeneration time, and design service life of the carbon.

(F) For a nonregenerable carbon adsorption system, such as a carbon canister, the design analysis shall include the vent stream composition, constituent concentrations, flowrate, relative humidity, and temperature, and shall establish the design exhaust vent stream organic compound concentration level, capacity of the carbon bed, type and working capacity of activated carbon used for the carbon bed, and design carbon replacement interval based on the total carbon working capacity of the control device and source operating schedule. In addition, these systems will incorporate dual carbon canisters in case of emission breakthrough occurring in one canister.

(ii) If the owner or operator and the Administrator do not agree on a demonstration of control device performance using a design analysis, then the disagreement shall be resolved using the results of a performance test performed by the owner or operator in accordance with the requirements of paragraph (d)(3) of this section. The Administrator may choose to have an authorized representative observe the performance test.

(5) As an alternative to the procedures in paragraphs (d)(3) and (d)(4)(i)(D) of this section, an owner or operator may elect to use the procedures documented in the GRI report entitled, “Atmospheric Rich/Lean Method for Determining Glycol Dehydrator Emissions,” (GRI-95/0368.1) as inputs for the model GRI-GLYCalc™, Version 3.0 or higher, to determine condenser performance.

(e) Compliance demonstration for control devices performance requirements. This paragraph applies to the demonstration of compliance with the control device performance requirements specified in § 63.1281(d)(1) and (e)(3)(ii). Compliance shall be demonstrated using the requirements in paragraphs (e)(1) through (e)(3) of this section. As an alternative, an owner or operator that installs a condenser as the control device to achieve the requirements specified in § 63.1281(d)(2)(ii) or § 63.1275(c)(2), may demonstrate compliance according to paragraph (f) of this section. An owner or operator may switch between compliance with paragraph (e) of this section and compliance with paragraph (f) of this section only after at least 1 year of operation in compliance with the selected approach. Notification of such a change
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Compliance with percent reduction performance requirements—condensers.

(1) The owner or operator shall establish a site-specific condenser performance curve according to the procedures specified in 40 CFR 63.1283(d)(5)(ii).

(2) Compliance with the percent reduction requirement in 40 CFR 63.1281(d)(1)(ii) or 63.1275(c)(2) shall be demonstrated by the procedures in paragraphs (f)(2)(i) through (f)(2)(iii) of this section.

(i) The owner or operator must calculate the daily average condenser outlet temperature in accordance with 40 CFR 63.1283(d)(4).

(ii) The owner or operator shall determine the condenser efficiency for the current operating day using the daily average condenser outlet temperature calculated in paragraph (f)(2)(i) of this section and the condenser performance curve established in paragraph (f)(1) of this section.

(iii) Except as provided in paragraphs (f)(2)(iii) (A), (B), and (D) of this section, at the end of each operating day the owner or operator shall calculate the 30-day average HAP emission reduction from the condenser efficiencies determined in paragraph (f)(2)(ii) of this section for the preceding 30 operating days. If the owner or operator uses a combination of process modifications and a condenser in accordance with the requirements of 40 CFR 63.1275(c)(2), the 30-day average HAP emission reduction shall be calculated using the emission reduction achieved through process modifications and the condenser efficiency determined in paragraph (f)(2)(ii) of this section, both for the preceding 30 operating days.

(A) After the compliance date specified in 40 CFR 63.1270(f), an owner or operator of a facility that stores natural gas that has less than 30 days of data for determining the average HAP emission reduction, shall calculate the cumulative average at the end of the withdrawal season, each season, until 30 days of condenser operating data are accumulated. For a facility that does not store natural gas, the owner or operator that has less than 30 days of data for determining average HAP emission reduction, shall calculate the cumulative average at the end of the calendar year, each year, until 30 days of condenser operating data are accumulated.

(B) After the compliance date specified in 40 CFR 63.1270(f), an owner or operator that has less than 30 days of data for determining average HAP emission reduction, shall calculate the cumulative average at the end of the withdrawal season, each season, until 30 days of condenser operating data are accumulated. For a facility that does not store natural gas, the owner or operator that has less than 30 days of data for determining average HAP emission reduction, shall calculate the cumulative average at the end of the calendar year, each year, until 30 days of condenser operating data are accumulated.

(C) For the purposes of this subpart, a withdrawal season begins the first time gas is withdrawn from the storage field after July 1 of the calendar year and ends on June 30 of the next calendar year.

(D) Glycol dehydration units that are operated continuously have the option of complying with the requirements specified in 40 CFR 63.772(g).

(3) Compliance is achieved with the emission limitation specified in 40 CFR 63.1281(d)(1)(ii) or 63.1275(c)(2) if the average HAP emission reduction calculated in paragraph (f)(2)(iii)(A) of this section, is equal to or greater than 95.0 percent.
(a) This section applies to an owner or operator using air emission controls in accordance with the requirements of §63.1275.

(b) [Reserved]

(c) Closed-vent system inspection and monitoring requirements. (1) For each closed-vent system required to comply with this section, the owner or operator shall comply with the requirements of paragraphs (c)(2) through (7) of this section.

(2) Except as provided in paragraphs (c) (5) and (6) of this section, each closed-vent system shall be inspected according to the procedures and schedule specified in paragraphs (c)(2)(i) and (ii) of this section.

(i) For each closed-vent system joints, seams, or other connections that are permanently or semi-permanently sealed (e.g., a welded joint between two sections of hard piping or a bolted or gasketed ducting flange), the owner or operator shall:

(A) Conduct an initial inspection according to the procedures specified in §63.1282(b) to demonstrate that the closed-vent system operates with no detectable emissions.

(B) Conduct annual visual inspections for defects that could result in air emissions. Defects include, but are not limited to, visible cracks, holes, or gaps in ductwork; loose connections; or broken or missing caps or other closure devices. The owner or operator shall monitor a component or connection using the procedures specified in §63.1282(b) to demonstrate that it operates with no detectable emissions following any time the component or connection is repaired or replaced or the connection is unsealed.

(ii) For closed-vent system components other than those specified in paragraph (c)(2)(i) of this section, the owner or operator shall:

(A) Conduct an initial inspection according to the procedures specified in §63.1282(b) to demonstrate that the closed-vent system operates with no detectable emissions.

(B) Conduct annual inspections according to the procedures specified in §63.1282(b) to demonstrate that the components or connections operate with no detectable emissions.

(C) Conduct annual visual inspections for defects that could result in air emissions. Defects include, but are not limited to, visible cracks, holes, or gaps in ductwork; loose connections; or broken or missing caps or other closure devices.

(3) In the event that a leak or defect is detected, the owner or operator shall repair the leak or defect as soon as practicable, except as provided in paragraph (c)(4) of this section.

(i) A first attempt at repair shall be made no later than 5 calendar days after the leak is detected.

(ii) Repair shall be completed no later than 15 calendar days after the leak is detected.

(4) Delay of repair of a closed-vent system for which leaks or defects have been detected is allowed if the repair is technically infeasible without a shutdown, as defined in §63.1271, or if the owner or operator determines that emissions resulting from immediate repair would be greater than the fugitive emissions likely to result from delay of repair. Repair of such equipment shall be completed by the end of the next shutdown.

(5) Any parts of the closed-vent system or cover that are designated, as described in paragraphs (c)(5) (i) and (ii) of this section, as unsafe to inspect are exempt from the inspection requirements of paragraphs (c)(2) (i) and (ii) of this section if:

(i) The owner or operator determines that the equipment is unsafe to inspect because inspecting personnel would be exposed to an imminent or potential danger as a consequence of complying with paragraph (c)(2) (i) or (ii) of this section; and

(ii) The owner or operator has a written plan that requires inspection of the equipment as frequently as practicable during safe-to-inspect times.

(6) Any parts of the closed-vent system or cover that are designated, as described in paragraphs (c)(6) (i) and (ii) of this section, as difficult to inspect are exempt from the inspection requirements of paragraphs (c)(2) (i) and (ii) of this section if:
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(i) The owner or operator determines that the equipment cannot be inspected without elevating the inspecting personnel more than 2 meters above a support surface; and

(ii) The owner or operator has a written plan that requires inspection of the equipment at least once every 5 years.

(7) Records shall be maintained as specified in §63.1284(d)(5) through (8).

(d) Control device monitoring requirements.

(1) For each control device except as provided for in paragraph (d)(2) of this section, the owner or operator shall install and operate a continuous parameter monitoring system in accordance with the requirements of paragraphs (d)(3) through (9) of this section that will allow a determination to be made whether the control device is achieving the applicable performance requirements of §63.1281(d) or (e)(3). The continuous parameter monitoring system must meet the following specifications and requirements:

(i) Each continuous parameter monitoring system shall measure data values at least once every hour and record either:

(A) Each measured data value; or
(B) Each block average value for each 1-hour period or shorter periods calculated from all measured data values during each period. If values are measured more frequently than once per minute, a single value for each minute may be used to calculate the hourly (or shorter period) block average instead of all measured values.

(ii) The monitoring system must be installed, calibrated, operated, and maintained in accordance with the manufacturer's specifications or other written procedures that provide reasonable assurance that the monitoring equipment is operating properly.

(2) An owner or operator is exempted from the monitoring requirements specified in paragraphs (d)(3) through (9) of this section for the following types of control devices:

(i) A boiler or process heater in which all vent streams are introduced with the primary fuel or are used as the primary fuel;

(ii) A boiler or process heater with a design heat input capacity equal to or greater than 44 megawatts.

(3) The owner or operator shall install, calibrate, operate, and maintain a device equipped with a continuous recorder to measure the values of operating parameters appropriate for the control device as specified in either paragraph (d)(3)(i), (d)(3)(ii), or (d)(3)(iii) of this section.

(i) A continuous monitoring system that measures the following operating parameters as applicable:

(A) For a thermal vapor incinerator, a temperature monitoring device equipped with a continuous recorder. The monitoring device shall have a minimum accuracy of ±2 percent of the temperature being monitored in °C, or ±2.5 °C, whichever value is greater. The temperature sensor shall be installed at a location in the combustion chamber downstream of the combustion zone.

(B) For a catalytic vapor incinerator, a temperature monitoring device equipped with a continuous recorder. The device shall be capable of monitoring temperatures at two locations and have a minimum accuracy of ±2 percent of the temperatures being monitored in °C, or ±2.5 °C, whichever value is greater. One temperature sensor shall be installed in the vent stream at the nearest feasible point to the catalyst bed inlet and a second temperature sensor shall be installed in the vent stream at the nearest feasible point to the catalyst bed outlet.

(C) For a flare, a heat sensing monitoring device equipped with a continuous recorder that indicates the continuous ignition of the pilot flame.

(D) For a boiler or process heater with a design heat input capacity of less than 44 megawatts, a temperature monitoring device equipped with a continuous recorder. The temperature monitoring device shall have a minimum accuracy of ±2 percent of the temperature being monitored in °C, or ±2.5 °C, whichever value is greater. The temperature sensor shall be installed at a location in the combustion chamber downstream of the combustion zone.

(E) For a condenser, a temperature monitoring device equipped with a continuous recorder. The temperature monitoring device shall have a minimum accuracy of ±2 percent of the
temperature being monitored in °C, or ±2.5 °C, whichever value is greater. The temperature sensor shall be installed at a location in the exhaust vent stream from the condenser.

(F) For a regenerative-type carbon adsorption system:

(1) A continuous parameter monitoring system to measure and record the average total regeneration stream mass flow or volumetric flow during each carbon bed regeneration cycle. The integrating regenerating stream flow monitoring device must have an accuracy of ±10 percent; and

(2) A continuous parameter monitoring system to measure and record the average carbon bed temperature for the duration of the carbon bed steaming cycle and to measure the actual carbon bed temperature after regeneration and within 15 minutes of completing the cooling cycle. The temperature monitoring device shall have a minimum accuracy of ±2 percent of the temperature being monitored in °C, or ±2.5 °C, whichever value is greater.

(G) For a nonregenerative-type carbon adsorption system, the owner or operator shall monitor the design carbon replacement interval established using a performance test performed in accordance with §63.1282(d)(3) or a design analysis in accordance with §63.1282(d)(4)(i)(F) and shall be based on the total carbon working capacity of the control device and source operating schedule.

(ii) A continuous monitoring system that measures the concentration level of organic compounds in the exhaust vent stream from the control device using an organic monitoring device equipped with a continuous recorder. The monitor must meet the requirements of Performance Specification 8 or 9 of appendix B of 40 CFR part 60 and must be installed, calibrated, and maintained according to the manufacturer’s specifications.

(iii) A continuous monitoring system that measures alternative operating parameters other than those specified in paragraph (d)(3)(i) or (d)(3)(ii) of this section upon approval of the Administrator as specified in §63.8(f)(1) through (5).

(4) Using the data recorded by the monitoring system, the owner or operator must calculate the daily average value for each monitored operating parameter for each operating day. If HAP emissions unit operation is continuous, the operating day is a 24-hour period. If the HAP emissions unit operation is not continuous, the operating day is the total number of hours of control device operation per 24-hour period. Valid data points must be available for 75 percent of the operating hours in an operating day to compute the daily average.

(5) For each operating parameter monitored in accordance with the requirements of paragraph (d)(3) of this section, the owner or operator shall comply with paragraph (d)(5)(i) of this section for all control devices, and when condensers are installed, the owner or operator shall also comply with paragraph (d)(5)(ii) of this section for condensers.

(i) The owner or operator shall establish a minimum operating parameter value or a maximum operating parameter value, as appropriate for the control device, to define the conditions at which the control device must be operated to continuously achieve the applicable performance requirements of §63.1284(d)(1) or (e)(3)(ii). Each minimum or maximum operating parameter value shall be established as follows:

(A) If the owner or operator conducts performance tests in accordance with the requirements of §63.1282(d)(3) to demonstrate that the control device achieves the applicable performance requirements specified in §63.1281(d)(1) or (e)(3)(ii), then the minimum operating parameter value or the maximum operating parameter value shall be established based on values measured during the performance test and supplemented, as necessary, by control device design analysis or control device manufacturer’s recommendations or a combination of both.

(B) If the owner or operator uses a control device design analysis in accordance with the requirements of §63.1282(d)(4) to demonstrate that the control device achieves the applicable performance requirements specified in §63.1281(d)(1) or (e)(3)(ii), then the minimum operating parameter value or the maximum operating parameter value is...
§ 63.1283

shall be established based on the control device design analysis and may be supplemented by the control device manufacturer’s recommendations.

(ii) The owner or operator shall establish a condenser performance curve showing the relationship between condenser outlet temperature and condenser control efficiency. The curve shall be established as follows:

(A) If the owner or operator conducts a performance test in accordance with the requirements of §63.1282(d)(3) to demonstrate that the condenser achieves the applicable performance requirements in §63.1281(d)(1) or (e)(3)(ii), then the condenser performance curve shall be based on values measured during the performance test and supplemented as necessary by control device design analysis, or control device manufacturer’s recommendations, or a combination of both.

(B) If the owner or operator uses a control device design analysis in accordance with the requirements of §63.1282(d)(4)(i)(D) to demonstrate that the condenser achieves the applicable performance requirements specified in §63.1281(d)(1) or (e)(3)(ii), then the condenser performance curve shall be based on the condenser design analysis and may be supplemented by the control device manufacturer’s recommendations.

(C) As an alternative to paragraphs (d)(5)(ii)(A) and (B) of this section, the owner or operator may elect to use the procedures documented in the GRI report entitled, “Atmospheric Rich/Learn Method for Determining Glycol Dehydrator Emissions” (GRI-950368.1) as inputs for the model GRI-GLYCalc™, Version 3.0 or higher, to generate a condenser performance curve.

(6) An excursion for a given control device is determined to have occurred when the monitoring data or lack of monitoring data result in any one of the criteria specified in paragraphs (d)(6)(i) through (d)(6)(iv) of this section being met. When multiple operating parameters are monitored for the same control device and during the same operating day, and more than one of these operating parameters meets an excursion criterion specified in paragraphs (d)(6)(i) through (d)(6)(iv) of this section, then a single excursion is determined to have occurred for the control device for that operating day.

(i) An excursion occurs when the daily average value of a monitored operating parameter is less than the minimum operating parameter limit (or, if applicable, greater than the maximum operating parameter limit) established for the operating parameter in accordance with the requirements of paragraph (d)(5)(i) of this section.

(ii) An excursion occurs when average condenser efficiency calculated according to the requirements specified in §63.1282(f)(3) is less than 95.0 percent, as specified in §63.1282(f)(3).

(iii) An excursion occurs when the monitoring data are not available for at least 75 percent of the operating hours.

(iv) If the closed-vent system contains one or more bypass devices that could be used to divert all or a portion of the gases, vapors, or fumes from entering the control device, an excursion occurs when:

(A) For each bypass line subject to §63.1281(c)(3)(i)(A) the flow indicator indicates that flow has been detected and that the stream has been diverted away from the control device to the atmosphere.

(B) For each bypass line subject to §63.1281(c)(3)(i)(B), if the seal or closure mechanism has been broken, the bypass line valve position has changed, the key for the lock-and-key type lock has been checked out, or the car-seal has broken.

(7) For each excursion, except as provided for in paragraph (d)(8) of this section, the owner or operator shall be deemed to have failed to have applied control in a manner that achieves the required operating parameter limits. Failure to achieve the required operating parameter limits is a violation of this standard.

(8) An excursion is not a violation of the operating parameter limit as specified in paragraphs (d)(8)(i) and (d)(8)(ii) of this section.

(i) An excursion does not count toward the number of excused excursions allowed under paragraph (d)(8)(ii) of this section when the excursion occurs during any one of the following periods:
(A) During a period of startup, shutdown, or malfunction when the affected facility is operated during such period in accordance with the facility's startup, shutdown, and malfunction plan; or
(B) During periods of non-operation of the unit or the process that is vented to the control device (resulting in cessation of HAP emissions to which the monitoring applies).

(ii) For each control device, or combinations of control devices, installed on the same HAP emissions unit, one excused excursion is allowed per semiannual period for any reason. The initial semiannual period is the 6-month reporting period addressed by the first Periodic Report submitted by the owner or operator in accordance with §63.1285(e) of this subpart.

§ 63.1284 Recordkeeping requirements.

(a) The recordkeeping provisions of subpart A of this part, that apply and those that do not apply to owners and operators of facilities subject to this subpart are listed in Table 2 of this subpart.

(b) Except as specified in paragraphs (c) and (d) of this section, each owner or operator of a facility subject to this subpart shall maintain the records specified in paragraphs (b)(1) through (b)(10) of this section:

(i) The owner or operator of an affected source subject to the provisions of this subpart shall maintain files of all information (including all reports and notifications) required by this subpart. The files shall be retained for at least 5 years following the date of each occurrence, measurement, maintenance, corrective action, report or period.

(ii) All applicable records shall be maintained in such a manner that they can be readily accessed.

(iii) The most recent 12 months of records shall be retained on site or shall be accessible from a central location by computer or other means that provides access within 2 hours after a request.

(iv) Records may be maintained in hard copy or computer-readable form including, but not limited to, on paper, microfilm, computer, floppy disk, magnetic tape, or microfiche.

(2) Records specified in §63.10(b)(2);
(3) Records specified in §63.10(c) for each monitoring system operated by the owner or operator in accordance with the requirements of §63.1283(d).

Nothing in paragraphs (d)(1) through (d)(8) of this section shall be construed to allow or excuse a monitoring parameter excursion caused by any activity that violates other applicable provisions of this subpart.

§ 63.1284 Recordkeeping requirements.

(a) The recordkeeping provisions of subpart A of this part, that apply and those that do not apply to owners and operators of facilities subject to this subpart are listed in Table 2 of this subpart.

(b) Except as specified in paragraphs (c) and (d) of this section, each owner or operator of a facility subject to this subpart shall maintain the records specified in paragraphs (b)(1) through (b)(10) of this section:

(i) The owner or operator of an affected source subject to the provisions of this subpart shall maintain files of all information (including all reports and notifications) required by this subpart. The files shall be retained for at least 5 years following the date of each occurrence, measurement, maintenance, corrective action, report or period.

(ii) All applicable records shall be maintained in such a manner that they can be readily accessed.

(iii) The most recent 12 months of records shall be retained on site or shall be accessible from a central location by computer or other means that provides access within 2 hours after a request.

(iv) Records may be maintained in hard copy or computer-readable form including, but not limited to, on paper, microfilm, computer, floppy disk, magnetic tape, or microfiche.

(2) Records specified in §63.10(b)(2);
(3) Records specified in §63.10(c) for each monitoring system operated by the owner or operator in accordance with the requirements of §63.1283(d).

Nothing in paragraphs (d)(1) through (d)(8) of this section shall be construed to allow or excuse a monitoring parameter excursion caused by any activity that violates other applicable provisions of this subpart.
which all pilot flames are absent shall be kept rather than daily averages.

(iii) Hourly records of whether the flow indicator specified under § 63.1281(c)(3)(i)(A) was operating and whether flow was detected at any time during the hour, as well as records of the times and durations of all periods when the vent stream is diverted from the control device or the monitor is not operating.

(iv) Where a seal or closure mechanism is used to comply with § 63.1281(c)(3)(i)(B), hourly records of flow are not required. In such cases, the owner or operator shall record that the monthly visual inspection of the seals or closure mechanism has been done, and shall record the duration of all periods when the seal mechanism is broken, the bypass line valve position has changed, or the key for a lock-and-key type lock has been checked out, and records of any car-seal that has broken.

(5) Records identifying all parts of the closed-vent system that are designated as unsafe to inspect in accordance with § 63.1283(c)(5), an explanation of why the equipment is unsafe to inspect, and the plan for inspecting the equipment.

(6) Records identifying all parts of the closed-vent system that are designated as difficult to inspect in accordance with § 63.1283(c)(6), an explanation of why the equipment is difficult to inspect, and the plan for inspecting the equipment.

(7) For each inspection conducted in accordance with § 63.1283(c), during which a leak or defect is detected, a record of the information specified in paragraphs (b)(7)(i) through (b)(7)(viii) of this section.

(i) The instrument identification numbers, operator name or initials, and identification of the equipment.

(ii) The date the leak or defect was detected and the date of the first attempt to repair the leak or defect.

(iii) Maximum instrument reading measured by the method specified in § 63.1283(c)(3) after the leak or defect is successfully repaired or determined to be nonrepairable.

(iv) “Repair delayed” and the reason for the delay if a leak or defect is not repaired within 15 calendar days after discovery of the leak or defect.

(v) The name, initials, or other form of identification of the owner or operator (or designee) whose decision it was that repair could not be effected without a shutdown.

(vi) The expected date of successful repair of the leak or defect if a leak or defect is not repaired within 15 calendar days.

(vii) Dates of shutdowns that occur while the equipment is unrepaired.

(viii) The date of successful repair of the leak or defect.

(8) For each inspection conducted in accordance with § 63.1283(c) during which no leaks or defects are detected, a record that the inspection was performed, the date of the inspection, and a statement that no leaks or defects were detected.

(9) Records of glycol dehydration unit baseline operations calculated as required under § 63.1281(e)(1).

(10) Records required in § 63.1281(e)(3)(i) documenting that the facility continues to operate under the conditions specified in § 63.1281(e)(2).

(c) An owner or operator that elects to comply with the benzene emission limit specified in § 63.1275(b)(1)(ii) shall document, to the Administrator’s satisfaction, the following items:

(1) The method used for achieving compliance and the basis for using this compliance method; and

(2) The method used for demonstrating compliance with 0.90 megagrams per year of benzene.

(3) Any information necessary to demonstrate compliance as required in the methods specified in paragraphs (c)(3) and (c)(2) of this section.

(d) An owner or operator that is exempt from control requirements under § 63.1274(d) shall maintain the records specified in paragraph (d)(1) or (d)(2) of this section, as appropriate, for each glycol dehydration unit that is not controlled according to the requirements of § 63.1274(c).

(1) The actual annual average natural gas throughput (in terms of natural gas flowrate to the glycol dehydration unit per day), as determined in accordance with § 63.1282(a)(1); or

(2) The actual average benzene emissions (in terms of benzene emissions
§ 63.1285 Reporting requirements.

(a) The reporting provisions of subpart A of this part that apply and those that do not apply to owners and operators of facilities subject to this subpart are listed in Table 2 of this subpart.

(b) Each owner or operator of a facility subject to this subpart shall submit the information listed in paragraphs (b)(1) through (b)(6) of this section, except as provided in paragraph (b)(7) of this section.

(1) The initial notifications required for existing affected sources under § 63.9(b)(2) shall be submitted by 1 year after an affected source becomes subject to the provisions of this subpart or by June 17, 2000, whichever is later. Affected sources that are major sources on or before June 17, 2000 and plan to be area sources by June 17, 2002 shall include in this notification a brief, non-binding description of a schedule for the action(s) that are planned to achieve area source status.

(2) The date of the performance evaluation as specified in § 63.8(e)(2), required only if the owner or operator is requested by the Administrator to conduct a performance evaluation for a continuous monitoring system. A separate notification of the performance evaluation is not required if it is included in the initial notification submitted in accordance with paragraph (b)(1) of this section.

(3) The planned date of a performance test at least 60 days before the test in accordance with § 63.7(b). Unless requested by the Administrator, a site-specific test plan is not required by this subpart. If requested by the Administrator, the owner or operator must also submit the site-specific test plan required by § 63.7(c) with the notification of the performance test. A separate notification of the performance test is not required if it is included in the initial notification submitted in accordance with paragraph (b)(1) of this section.

(4) A Notification of Compliance Status Report as described in paragraph (d) of this section;

(5) Periodic Reports as described in paragraph (e) of this section;

(6) Startup, shutdown, and malfunction reports, as specified in § 63.10(d)(5), shall be submitted as required. Separate startup, shutdown, or malfunction reports as described in § 63.10(d)(5)(i) are not required if the information is included in the Periodic Report specified in paragraph (e) of this section.

(7) Each owner or operator of a glycol dehydration unit subject to this subpart that is exempt from the control requirements for glycol dehydration unit process vents in § 63.1275, is exempt from all reporting requirements for major sources in this subpart for that unit.

(c) [Reserved]

(d) Each owner or operator of a source subject to this subpart shall submit a Notification of Compliance Status Report as required under § 63.9(h) within 180 days after the compliance date specified in § 63.1270(d). In addition to the information required under § 63.9(h), the Notification of Compliance Status Report shall include the information specified in paragraphs (d)(1) through (d)(10) of this section. This information may be submitted in an operating permit application, in an amendment to an operating permit application, in a separate submittal, or in any combination of the three. If all of the information required under this paragraph have been submitted at any time prior to 180 days after the applicable compliance dates specified in § 63.1270(d), a separate Notification of Compliance Status Report is not required. If an owner or operator submits the information specified in paragraphs (d)(1) through (d)(9) of this section at different times, and/or different submittals, later submittals may refer to
earlier submittals instead of duplicating and resubmitting the previously submitted information.

(1) If a closed-vent system and a control device other than a flare are used to comply with §63.1274, the owner or operator shall submit:

(i) The design analysis documentation specified in §63.1282(d)(4) of this subpart if the owner or operator elects to prepare a design analysis; or

(ii) If the owner or operator elects to conduct a performance test, the performance test results including the information specified in paragraphs (d)(1)(ii)(A) and (B) of this section. Results of a performance test conducted prior to the compliance date of this subpart can be used provided that the test was conducted using the methods specified in §63.1282(d)(3), and that the test conditions are representative of current operating conditions.

(A) The percent reduction of HAP or TOC, or the outlet concentration of HAP or TOC (parts per million by volume on a dry basis), determined as specified in §63.1282(d)(3) of this subpart; and

(B) The value of the monitored parameters specified in §63.1283(d) of this subpart, or a site-specific parameter approved by the permitting agency, averaged over the full period of the performance test.

(2) If a closed-vent system and a flare are used to comply with §63.1274, the owner or operator shall submit performance test results including the information in paragraphs (d)(2)(i) and (ii) of this section.

(i) All visible emission readings, heat content determinations, flowrate measurements, and exit velocity determinations made during the compliance determination required by §63.1282(d)(2) of this subpart, and

(ii) A statement of whether a flame was present at the pilot light over the full period of the compliance determination.

(3) The owner or operator shall submit one complete test report for each test method used for a particular source.

(i) For additional tests performed using the same test method, the results specified in paragraph (d)(1)(ii) of this section shall be submitted, but a complete test report is not required.

(ii) A complete test report shall include a sampling site description, description of sampling and analysis procedures and any modifications to standard procedures, quality assurance procedures, record of operating conditions during the test, record of preparation of standards, record of calibrations, raw data sheets for field sampling, raw data sheets for field and laboratory analyses, documentation of calculations, and any other information required by the test method.

(4) For each control device other than a flare used to meet the requirements of §63.1274, the owner or operator shall submit the information specified in paragraphs (d)(4)(i) through (iii) of this section for each operating parameter required to be monitored in accordance with the requirements of §63.1283(d).

(i) The minimum operating parameter value or maximum operating parameter value, as appropriate for the control device, established by the owner or operator to define the conditions at which the control device must be operated to continuously achieve the applicable performance requirements of §63.1281(d)(1) or (e)(3)(ii).

(ii) An explanation of the rationale for why the owner or operator selected each of the operating parameter values established in §63.1283(d)(5) of this subpart. This explanation shall include any data and calculations used to develop the value, and a description of why the chosen value indicates that the control device is operating in accordance with the applicable requirements of §63.1281(d)(1) or (e)(3)(ii).

(iii) A definition of the source’s operating day for purposes of determining daily average values of monitored parameters. The definition shall specify the times at which an operating day begins and ends.

(5) Results of any continuous monitoring system performance evaluations shall be included in the Notification of Compliance Status Report.

(6) After a title V permit has been issued to the owner or operator of an affected source, the owner or operator
of such source shall comply with all requirements for compliance status reports contained in the source's title V permit, including reports required under this subpart. After a title V permit has been issued to the owner or operator of an affected source, and each time a notification of compliance status is required under this subpart, the owner or operator of such source shall submit the notification of compliance status to the appropriate permitting authority following completion of the relevant compliance demonstration activity specified in this subpart.

(7) The owner or operator that elects to comply with the requirements of §63.1275(b)(1)(ii) shall submit the records required under §63.1284(c).

(8) The owner or operator shall submit an analysis demonstrating whether an affected source is a major source using the maximum throughput calculated according to §63.1270(a).

(9) The owner or operator shall submit a statement as to whether the source has complied with the requirements of this subpart.

(10) The owner or operator shall submit the analysis prepared under §63.1281(e)(2) to demonstrate that the conditions by which the facility will be operated to achieve an overall HAP emission reduction of 95.0 percent through process modifications or a combination of process modifications and one or more control devices.

(e) Periodic Reports. An owner or operator shall prepare Periodic Reports in accordance with paragraphs (e)(1) and (2) of this section and submit them to the Administrator.

(1) An owner or operator shall submit Periodic Reports semiannually, beginning 60 operating days after the end of the applicable reporting period. The first report shall be submitted no later than 240 days after the date the Notification of Compliance Status Report is due and shall cover the 6-month period ending on the date the Notification of Compliance Status Report is due.

(2) The owner or operator shall include the information specified in paragraphs (e)(2)(i) through (viii) of this section, as applicable.

(i) The information required under §63.10(e)(3). For the purposes of this subpart and the information required under §63.10(e)(3), excursions (as defined in §63.1283(d)(6)) shall be considered excess emissions.

(ii) A description of all excursions as defined in §63.1283(d)(6) of this subpart that have occurred during the 6-month reporting period.

(A) For each excursion caused when the daily average value of a monitored operating parameter is less than the minimum operating parameter limit (or, if applicable, greater than the maximum operating parameter limit), as specified in §63.1283(d)(6)(i), the report must include the daily average values of the monitored parameter, the applicable operating parameter limit, and the date and duration of the period that the excursion occurred.

(B) For each excursion caused when the 30-day average condenser control efficiency is less than 95.0 percent, as specified in §63.1283(d)(6)(ii), the report must include the 30-day average values of the condenser control efficiency, and the date and duration of the period that the excursion occurred.

(C) For each excursion caused by lack of monitoring data, as specified in §63.1283(d)(6)(iii), the report must include the date and duration of period when the monitoring data were not collected and the reason why the data were not collected.

(iii) For each inspection conducted in accordance with §63.1283(c) during which a leak or defect is detected, the records specified in §63.1284(b)(7) must be included in the next Periodic Report.

(iv) For each closed-vent system with a bypass line subject to §63.1281(c)(3)(i)(A), records required under §63.1284(b)(4)(iii) of all periods when the vent stream is diverted from the control device through a bypass line. For each closed-vent system with a bypass line subject to §63.1281(c)(3)(i)(B), records required under §63.1284(b)(4)(iv) of all periods in which the seal or closure mechanism is broken, the bypass valve position has changed, or the key to unlock the bypass line valve was checked out.

(v) If an owner or operator elects to comply with §63.1275(b)(1)(ii), the records required under §63.1284(c)(3).
be stated in the Periodic Report, when applicable.

(A) No excursions.

(B) No continuous monitoring system has been inoperative, out of control, repaired, or adjusted.

(vii) Any change in compliance methods as specified in §63.1275(b).

(viii) If the owner or operator elects to comply with §63.1275(c)(2), the records required under §63.1284(b)(10).

(f) Notification of process change. Whenever a process change is made, or a change in any of the information submitted in the Notification of Compliance Status Report, the owner or operator shall submit a report within 180 days after the process change is made or as a part of the next Periodic Report as required under paragraph (e) of this section, whichever is sooner. The report shall include:

(1) A brief description of the process change;

(2) A description of any modification to standard procedures or quality assurance procedures;

(3) Revisions to any of the information reported in the original Notification of Compliance Status Report under paragraph (d) of this section; and

(4) Information required by the Notification of Compliance Status Report under paragraph (d) of this section for changes involving the addition of processes or equipment.

§ 63.1286 Delegation of authority.

(a) In delegating implementation and enforcement authority to a State under section 112(l) of the Act, the authorities contained in paragraph (b) of this section shall be retained by the Administrator and not transferred to a State.

(b) Authorities will not be delegated to States for §§63.1282 and 63.1287 of this subpart.

§ 63.1287 Alternative means of emission limitation.

(a) If, in the judgment of the Administrator, an alternative means of emission limitation will achieve a reduction in HAP emissions at least equivalent to the reduction in HAP emissions from that source achieved under the applicable requirements in §§63.1274 through 63.1281, the Administrator will publish a notice in the FEDERAL REGISTER permitting the use of the alternative means for purposes of compliance with that requirement. The notice may condition the permission on requirements related to the operation and maintenance of the alternative means.

(b) Any notice under paragraph (a) of this section shall be published only after public notice and an opportunity for a hearing.

(c) Any person seeking permission to use an alternative means of compliance under this section shall collect, verify, and submit to the Administrator information showing that this means achieves equivalent emission reductions.

§§ 63.1288–63.1289 [Reserved]

APPENDIX TO SUBPART HHH—TABLES

Table 1.—List of Hazardous Air Pollutants (HAP) for Subpart HHH

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<thead>
<tr>
<th>CAS Number</th>
<th>Chemical name</th>
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<tr>
<td>75070</td>
<td>Acetaldehyde</td>
</tr>
<tr>
<td>71432</td>
<td>Benzene (includes benzene in gasoline)</td>
</tr>
<tr>
<td>75150</td>
<td>Carbon disulfide</td>
</tr>
<tr>
<td>403581</td>
<td>Carbonyl sulfide</td>
</tr>
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<td>100414</td>
<td>Ethyl benzene</td>
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<td>107211</td>
<td>Ethylene glycol</td>
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<td>1330207</td>
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<td>106443</td>
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*CAS numbers refer to the Chemical Abstracts Services registry number assigned to specific compounds, isomers, or mixtures of compounds.
### TABLE 2 TO SUBPART HHH.—APPLICABILITY OF 40 CFR PART 63 GENERAL PROVISIONS TO SUBPART HHH

<table>
<thead>
<tr>
<th>General provisions reference</th>
<th>Applicable to subpart HHH</th>
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§ 63.1290 Applicability.

(a) The provisions of this subpart apply to each new and existing flexible polyurethane foam or rebond foam process that meets the criteria listed in paragraphs (a)(1) through (3) of this section.

(1) Produces flexible polyurethane or rebond foam;

(2) Emitted a HAP, except as provided in paragraph (c)(2) of this section; and

(3) Is located at a plant site that is a major source, as defined in § 63.2 of subpart A.

(b) For the purpose of this subpart, an affected source includes all processes meeting the criteria in paragraphs (a)(1) through (a)(3) of this section that are located at a contiguous plant site, with the exception of those processes listed in paragraph (c) of this section.

(c) A process meeting one of the following criteria listed in paragraphs (c)(1) through (3) of this section shall not be subject to the provisions of this subpart:

(1) A process exclusively dedicated to the fabrication of flexible polyurethane foam;

(2) A research and development process; or

(3) A slabstock flexible polyurethane foam process at a plant site where the total amount of HAP, excluding disocyanate reactants, used for slabstock foam production and foam fabrication is less than or equal to five tons per year, provided that slabstock foam production and foam fabrication processes are the only processes at the plant site that emit HAP. The amount of non-disocyanate HAP used, HAP\text{used}, shall be calculated using Equation 1. Owners or operators of slabstock foam processes exempt from the regulation in accordance with this paragraph shall maintain records to verify that total non-disocyanate HAP use at the plant site is less than 5 tons per year (4.5 megagrams per year).

\[
\text{HAP}\text{used} = \sum_{i=m}^{m} (\text{VOL}_{ABA,i}) \times \text{D}_{ABA,i} \times \sum_{j=n}^{n} (\text{VOL}_{clean,j}) \times \text{D}_{clean,j} \times \text{WT}_{HAP\text{clean},j} + \sum_{k=o}^{o} (\text{VOL}_{adh,k}) \times \text{D}_{adh,k} \times \text{WT}_{HAP\text{adh},k} \div 2000
\]

(Equation 1)

Where,

- \text{HAP}\text{used} = \text{amount of HAP, excluding disocyanate reactants, used at the plant site for slabstock foam production and foam fabrication, tons per year}
- \text{VOL}_{ABA,i} = \text{volume of HAP ABA} \ i \ \text{used at the facility, gallons per year}
- \text{D}_{ABA,i} = \text{density of HAP ABA} \ i \ \text{, pounds per gallon}
- m = \text{number of HAP ABA} \text{s used}
- \text{VOL}_{clean,j} = \text{volume of HAP used as an equipment cleaner, gallons per year}
- \text{D}_{clean,j} = \text{density of HAP equipment cleaner} \ j \ \text{, pounds per gallon}
- n = \text{number of HAP equipment cleaners used}
- \text{WT}_{HAP\text{clean},j} = \text{HAP content of equipment cleaner} \ j \ \text{, weight percent}
- \text{VOL}_{adh,k} = \text{volume of adhesive} \ k \ \text{, gallons per year}
- \text{D}_{adh,k} = \text{density of adhesive} \ k \ \text{, pounds per gallon}
- \text{WT}_{HAP\text{adh},k} = \text{HAP content of adhesive} \ k \ \text{, weight percent}
- o = \text{number of adhesives used}

§ 63.1291 Compliance schedule.

(a) Existing affected sources shall be in compliance with all provisions of this subpart no later than October 8, 2001.

(b) New or reconstructed affected sources shall be in compliance with all provisions of this subpart upon initial startup.
All terms used in this subpart shall have the meaning given them in the Act, in subpart A of this part, and in this section. If a term is defined in subpart A and in this section, it shall have the meaning given in this section for purposes of this subpart.

Auxiliary blowing agent, or ABA, means a low-boiling point liquid added to assist foaming by generating gas beyond that resulting from the isocyanate-water reaction.

Breakthrough means that point in the adsorption step when the mass transfer zone (i.e., the section of the carbon bed where the HAP is removed from the carrier gas stream) first reaches the carbon bed outlet as the mass transfer zone moves down the bed in the direction of flow. The breakthrough point is characterized by the beginning of a sharp increase in the outlet HAP or organic compound concentration.

Calibrate means to verify the accuracy of a measurement device against a known standard. For the purpose of this subpart, there are two levels of calibration. The initial calibration includes the verification of the accuracy of the device over the entire operating range of the device. Subsequent calibrations can be conducted for a point or several points in a limited range of operation that represents the most common operation of the device.

Canned motor pump means a pump with interconnected cavity housings, motor rotors, and pump casing. In a canned motor pump, the motor bearings run in the process liquid and all seals are eliminated.

Carbon adsorption system means a system consisting of a tank or container that contains a specific quantity of activated carbon. For the purposes of this subpart, a carbon adsorption system is used as a control device for storage vessels. Typically, the spent carbon bed does not undergo regeneration, but is replaced.

Connector means flanged, screwed, or other joined fittings used to connect two pipe lines or a pipe line and a piece of equipment. A common connector is a flange. Joined fittings welded completely around the circumference of the interface are not considered to be connectors for the purposes of this subpart.

Cured foam means flexible polyurethane foam with fully developed physical properties. A period of 12 to 24 hours from pour is typically required to completely cure foam, although mechanical or other devices are sometimes used to accelerate the curing process.

Curing area means the area in a slabstock foam production facility where foam buns are allowed to fully develop physical properties.

Diaphragm pump means a pump where the driving member is a flexible diaphragm made of metal, rubber, or plastic. In a diaphragm pump, there is no packing or seals that are exposed to the process liquid.

Diisocyanate means a compound containing two isocyanate groups per molecule. The most common diisocyanate compounds used in the flexible polyurethane foam industry are toluene disiocyanate (TDI) and methylene diphenyl disiocyanate (MDI).

Flexible polyurethane foam means a flexible cellular polymer containing urea and carbamate linkages in the chain backbone produced by reacting a diisocyanate, polyol, and water. Flexible polyurethane foams are open-celled, permit the passage of air through the foam, and possess the strength and flexibility to allow repeated distortion or compression under stress with essentially complete recovery upon removal of the stress.

Flexible polyurethane foam process means the equipment used to produce a flexible polyurethane foam product.

Foam fabrication process means an operation for cutting or bonding flexible polyurethane foam pieces together or to other substrates.

Grade of foam means foam with a distinct combination of indentation force deflection (IFD) and density values.

HAP ABA means methylene chloride, or any other HAP compound used as an auxiliary blowing agent.
§ 63.1292  

HAP-based means to contain 5 percent (by weight) or more of HAP. This applies to equipment cleaners (and mixhead flushes) and mold release agents. The concentration of HAP may be determined using EPA test method 18, material safety data sheets, or engineering calculations.

High-pressure mixhead means a mixhead where mixing is achieved by impingement of the high pressure streams within the mixhead.

Indentation Force Deflection (IFD) means a measure of the load bearing capacity of flexible polyurethane foam. IFD is generally measured as the force (in pounds) required to compress a 50 square inch circular indentor foot into a four inch thick sample, typically 15 inches square or larger, to 25 percent of the sample's initial height.

In diisocyanate service means a piece of equipment that contains or contacts a diisocyanate.

In HAP ABA service means a piece of equipment that contains or contacts a HAP ABA.

Initial startup means the first time a new or reconstructed affected source begins production of flexible polyurethane foam.

Isocyanate means a reactive chemical grouping composed of a nitrogen atom bonded to a carbon atom bonded to an oxygen atom; or a chemical compound, usually organic, containing one or more isocyanate groups.

Magnetic drive pump means a pump where an externally-mounted magnet coupled to the pump motor drives the impeller in the pump casing. In a magnetic drive pump, no seals contact the process fluid.

Metering pump means a pump used to deliver reactants, ABA, or additives to the mixhead.

Mixhead means a device that mixes two or more component streams before dispensing foam producing mixture to the desired container.

Molded flexible polyurethane foam means a flexible polyurethane foam that is produced by shooting the foam mixture into a mold of the desired shape and size.

Mold release agent means any material which, when applied to the mold surface, serves to prevent sticking of the foam part to the mold.

Plant site means all contiguous or adjoining property that is under common control, including properties that are separated only by a road or other public right-of-way. Common control includes properties that are owned, leased, or otherwise operated by the same entity, parent entity, subsidiary, or any combination thereof.

Polyol, for the purpose of this subpart, means a polyether or polyester polymer with more than one reactive hydroxyl group attached to the molecule.

Rebond foam means the foam resulting from a process of adhering small particles of foam (usually scrap or recycled foam) together to make a usable cushioning product. Various adhesives and bonding processes are used. A typical application for rebond foam is for carpet underlay.

Rebound foam process means the equipment used to produce a rebond foam product. For the purpose of this subpart, the rebound foam process includes raw material storage; production equipment and associated piping, ductwork, etc.; and curing and storage areas.

Reconstructed source means an affected source undergoing reconstruction, as defined in subpart A. For the purposes of this subpart, process modifications made to reduce HAP ABA emissions to meet the existing source requirements of this subpart shall not be counted in determining whether or not a change or replacement meets the definition of reconstruction.

Recovery device means an individual unit of equipment capable of and used for the purpose of recovering chemicals for use, reuse, or sale. Recovery devices include, but are not limited to, carbon adsorbers, absorbers, and condensers.

Research and development process means a laboratory or pilot plant operation whose primary purpose is to conduct research and development into new processes and products, where the operations are under the close supervision of technically trained personnel, and which is not engaged in the manufacture of products for commercial sale except in a de minimis manner.

Run of foam means a continuous production of foam, which may consist of several grades of foam.
Environmental Protection Agency § 63.1294

Sealless pump means a canned-motor pump, diaphragm pump, or magnetic drive pump, as defined in this section.

Slabstock flexible polyurethane foam means flexible polyurethane foam that is produced in large continuous buns that are then cut into the desired size and shape.

Slabstock flexible polyurethane foam production line includes all portions of the flexible polyurethane foam process from the mixhead to the point in the process where the foam is completely cured.

Storage vessel means a tank or other vessel that is used to store diisocyanate or HAP ABA for use in the production of flexible polyurethane foam. Storage vessels do not include vessels with capacities smaller than 38 cubic meters (or 10,000 gallons).

Transfer pump means all pumps used to transport diisocyanate or HAP ABA that are not metering pumps.

Transfer vehicle means a railcar, tank truck, or other vehicle used to transport HAP ABA to the flexible polyurethane foam facility.

§ 63.1293 Standards for slabstock flexible polyurethane foam production.

Each owner or operator of a new or existing slabstock affected source shall comply with § 63.1294 and either paragraph (a) or (b) of this section:

(a) The emission point specific limitations in §§ 63.1295 through 63.1298; or

(b) For sources that use no more than one HAP as an ABA and an equipment cleaner, the source-wide emission limitation in § 63.1299.

§ 63.1294 Standards for slabstock flexible polyurethane foam production—diisocyanate emissions.

Each new and existing slabstock affected source shall comply with the provisions of this section.

(a) Diisocyanate storage vessels. Diisocyanate storage vessels shall be equipped with either a system meeting the requirements in paragraph (a)(1) of this section, or a carbon adsorption system meeting the requirements of paragraph (a)(2) of this section.

(1) The storage vessel shall be equipped with a vapor return line from the storage vessel to the tank truck or rail car that is connected during unloading.

(i) During each unloading event, the vapor return line shall be inspected for leaks by visual, audible, or any other detection method.

(ii) When a leak is detected, it shall be repaired as soon as practicable, but not later than the subsequent unloading event.

(2) The storage vessel shall be equipped with a carbon adsorption system, meeting the monitoring requirements of § 63.1303(a), that routes displaced vapors through activated carbon before being discharged to the atmosphere. The owner or operator shall replace the existing carbon with fresh carbon upon indication of breakthrough before the next unloading event.

(b) Transfer pumps in diisocyanate service. Each transfer pump in diisocyanate service shall meet the requirements of paragraph (b)(1) or (b)(2) of this section.

(1) The pump shall be a sealless pump; or

(2) The pump shall be a submerged pump system meeting the requirements in paragraphs (b)(2)(i) through (iii) of this section.

(i) The pump shall be completely immersed in bis(2-ethylhexyl)phthalate (DEHP, CAS # 118-81-7), 2(methyloctyl)phthalate (DINP, CAS # 68515-48-0), or another neutral oil.

(ii) The pump shall be visually monitored weekly to detect leaks.

(iii) When a leak is detected, it shall be repaired in accordance with the procedures in paragraphs (b)(2)(iii)(A) and (B) of this section, except as provided in paragraph (d) of this section.

(A) The leak shall be repaired as soon as practicable, but not later than 15 calendar days after it is detected.

(B) A first attempt at repair shall be made no later than 5 calendar days after the leak is detected. First attempts at repair include, but are not limited to, the following practices where practicable:

(1) Tightening of packing gland nuts.

(2) Ensuring that the seal flush is operating at design pressure and temperature.

(c) Other components in diisocyanate service. If evidence of a leak is found by
§ 63.1295 Standards for slabstock flexible polyurethane foam production—HAP ABA storage vessels.

Each owner or operator of a new or existing slabstock affected source complying with the emission point specific limitation option provided in § 63.1293(a) shall control HAP ABA storage vessels in accordance with the provisions of this section.

(a) Each HAP ABA storage vessel shall be equipped with either a vapor balance system meeting the requirements in paragraph (b) of this section, or a carbon adsorption system meeting the requirements of paragraph (c) of this section.

(b) The storage vessel shall be equipped with a vapor balance system. The owner or operator shall ensure that the vapor return line from the storage vessel to the tank truck or rail car is connected during unloading.

(c) The storage vessel shall be equipped with a carbon adsorption system, meeting the monitoring requirements of § 63.1303(a), that routes displaced vapors through activated carbon before discharging to the atmosphere. The owner or operator shall replace the existing carbon with fresh carbon upon indication of breakthrough before the next unloading event.

§ 63.1296 Standards for slabstock flexible polyurethane foam production—HAP ABA equipment leaks.

Each owner or operator of a new or existing slabstock affected source complying with the emission point specific limitation option provided in § 63.1293(a) shall control HAP ABA emissions from leaks from transfer pumps, valves, connectors, pressure-relief valves, and open-ended lines in accordance with the provisions in this section.

(a) Pumps. Each pump in HAP ABA service shall be controlled in accordance with either paragraph (a)(1) or (a)(2) of this section.

(1) The pump shall be a sealless pump, or

(2) Each pump shall be monitored for leaks in accordance with paragraphs (a)(2)(i) and (ii) of this section. Leaks shall be repaired in accordance with paragraph (a)(2)(iii) of this section.

(i) Each pump shall be monitored quarterly to detect leaks by the method specified in § 63.1304(a). If an instrument reading of 10,000 parts per million (ppm) or greater is measured, a leak is detected.

(ii) Each pump shall be checked by visual inspection each calendar week for indications of liquids dripping from the pump seal. If there are indications of liquids dripping from the pump seal, a leak is detected.

(iii) When a leak is detected, it shall be repaired in accordance with the procedures in paragraphs (a)(2)(iii)(A) and (B) of this section, except as provided in paragraph (f) of this section.
(A) The leak shall be repaired as soon as practicable, but not later than 15 calendar days after it is detected.

(B) A first attempt at repair shall be made no later than 5 calendar days after the leak is detected. First attempts at repair include, but are not limited to, the following practices, where practicable:

(1) Tightening of packing gland nuts.

(2) Ensuring that the seal flush is operating at design pressure and temperature.

(b) Valves. Each valve in HAP ABA service shall be monitored for leaks in accordance with paragraph (b)(1) of this section, except as provided in paragraphs (b)(3) and (4) of this section. Leaks shall be repaired in accordance with paragraph (b)(2) of this section.

(1) Each valve shall be monitored quarterly to detect leaks by the method specified in §63.1304(a). If an instrument reading of 10,000 parts per million or greater is measured, a leak is detected.

(2) When a leak is detected, the owner or operator shall repair the leak in accordance with the procedures in paragraphs (b)(2)(i) and (ii) of this section, except as provided in paragraph (f) of this section.

(i) The leak shall be repaired as soon as practicable, but not later than 15 calendar days after it is detected.

(ii) A first attempt at repair shall be made no later than 5 calendar days after the leak is detected. First attempts at repair include, but are not limited to, the following practices where practicable:

(A) Tightening of bonnet bolts;

(B) Replacement of bonnet bolts;

(C) Tightening of packing gland nuts; and

(D) Injection of lubricant into lubricated packing.

(3) Any valve that is designated as an unsafe-to-monitor valve is exempt from the requirements of paragraphs (b)(1) and (2) of this section if:

(i) The owner or operator of the valve has a written plan that requires monitoring of the valve as frequently as practicable during safe-to-monitor times. The plan shall also include requirements for repairing leaks as soon as possible after detection.

(ii) The owner or operator shall monitor the unsafe-to-monitor valve in accordance with the written plan, and

(iv) The owner or operator shall repair leaks in accordance with the written plan.

(4) Any valve that is designated as a difficult-to-monitor valve is exempt from the requirements of paragraphs (b)(1) and (2) of this section if:

(i) The owner or operator of the valve determines that the valve cannot be monitored without elevating the monitoring personnel more than 2 meters above a support surface or it is not accessible at any time in a safe manner;

(ii) The process within which the valve is located is an existing source, or the process within which the valve is located is a new source that has less than 3 percent of the total number of valves designated as difficult to monitor; and

(iii) The owner or operator of the valve develops a written plan that requires monitoring of the valve at least once per calendar year. The plan shall also include requirements for repairing leaks as soon as possible after detection.

(iv) The owner or operator shall monitor the difficult-to-monitor valve in accordance with the written plan, and

(v) The owner or operator shall repair leaks in accordance with the written plan.

(c) Connectors. Each connector in HAP ABA service shall be monitored for leaks in accordance with paragraph (c)(1) of this section, except as provided in paragraph (c)(3) of this section. Leaks shall be repaired in accordance with paragraph (c)(2) of this section, except as provided in paragraph (c)(4) of this section.

(1) Connectors shall be monitored at the times specified in paragraphs (c)(1)(i) through (iii) of this section to detect leaks by the method specified in §63.1304(a). If an instrument reading of 10,000 ppm or greater is measured, a leak is detected.
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(i) Each connector shall be monitored annually, and

(ii) Each connector that has been opened or has otherwise had the seal broken shall be monitored for leaks within the first 3 months after being returned to HAP ABA service.

(iii) If a leak is detected, the connector shall be monitored for leaks in accordance with paragraph (c)(1) of this section within the first 3 months after its repair.

(2) When a leak is detected, it shall be repaired in accordance with the procedures in paragraphs (c)(2)(i) and (ii) of this section, except as provided in paragraph (c)(4) and paragraph (f) of this section.

(i) The leak shall be repaired as soon as practicable, but no later than 15 calendar days after the leak is detected.

(ii) A first attempt at repair shall be made no later than 5 calendar days after the leak is detected.

(3) Any connector that is designated as an unsafe-to-monitor connector is exempt from the requirements of paragraph (c)(1) of this section if:

(i) The owner or operator determines that the connector is unsafe to monitor because personnel would be exposed to an immediate danger as a result of complying with paragraph (c)(1) of this section; and

(ii) The owner or operator has a written plan that requires monitoring of the connector as frequently as practicable during safe-to-monitor periods.

(4) Any connector that is designated as an unsafe-to-repair connector is exempt from the requirements of paragraph (c)(2) of this section if:

(i) The owner or operator determines that repair personnel would be exposed to an immediate danger as a consequence of complying with paragraph (c)(2) of this section; and

(ii) The connector will be repaired as soon as practicable, but not later than 6 months after the leak was detected.

(5) Pressure-relief devices. Each pressure-relief device in HAP ABA service shall be monitored for leaks in accordance with paragraph (d)(1) of this section. Leaks shall be repaired in accordance with paragraph (d)(2) of this section.

(1) Each pressure-relief device in HAP ABA service shall be monitored within 5 calendar days by the method specified in §63.1304(a) if evidence of a potential leak is found by visual, audible, olfactory, or any other detection method. If an instrument reading of 10,000 ppm or greater is measured, a leak is detected.

(2) When a leak is detected, the leak shall be repaired as soon as practicable, but not later than 15 calendar days after it is detected, except as provided in paragraph (f) of this section. The owner or operator shall make a first attempt at repair no later than 5 calendar days after the leak is detected.

(6) Open-ended valves or lines. (1)(i) Each open-ended valve or line in HAP ABA service shall be equipped with a cap, blind flange, plug, or a second valve, except as provided in paragraph (e)(4) of this section.

(ii) The cap, blind flange, plug, or second valve shall seal the open end at all times except during operations requiring process fluid flow through the open-ended valve or line, or during maintenance or repair.

(2) Each open-ended valve or line equipped with a second valve shall be operated in a manner such that the valve on the process fluid end is closed before the second valve is closed.

(3) When a double block and bleed system is being used, the bleed valve or line may remain open during operations that require venting the line between the block valves but shall comply with paragraph (e)(1) of this section at all other times.

(4) Open-ended valves or lines in an emergency shutdown system which are designed to open automatically in the event of a process upset are exempt from the requirements of paragraphs (e)(1), (2), and (3) of this section.

(f) Delay of repair. (1) Delay of repair of equipment for which leaks have been detected is allowed for equipment that is isolated from the process and that does not remain in HAP ABA service.

(2) Delay of repair for valves and connectors is also allowed if:

(i) The owner or operator determines that emissions of purged material resulting from immediate repair are greater than the fugitive emissions likely to result from delay of repair, and
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§ 63.1297 Standards for slabstock flexible polyurethane foam production—HAP ABA emissions from the production line.

(a) Each owner or operator of a new or existing slabstock affected source complying with the emission point specific limitation option provided in §63.1293(a)(1) shall control HAP ABA emissions from the slabstock polyurethane foam production line in accordance with the provisions in this section. Compliance shall be determined on a rolling annual basis as described in paragraph (a)(1) of this section. As an alternative, the owner or operator can determine compliance on a monthly basis, as described in paragraph (a)(2) of this section.

(1) Rolling annual compliance. In determining compliance on a rolling annual basis, actual HAP ABA emissions shall be compared to allowable HAP ABA emissions for each consecutive 12-month period. The allowable HAP ABA emission level shall be calculated based on the production for the 12-month period, resulting in a potentially different allowable level each month. The requirements for this monthly compliance alternative are provided in paragraph (c) of this section.

(3) Each owner or operator electing to change between the compliance methods described under paragraphs (a)(1) and (a)(2) of this section shall notify the Administrator no later than 180 calendar days prior to the change.

(b) Rolling annual compliance. At each slabstock foam production source complying with the rolling annual compliance provisions described in paragraph (a)(1) of this section, actual HAP ABA emissions shall not exceed the allowable HAP ABA emission level for a consecutive 12-month period. The actual HAP ABA emission level for a consecutive 12-month period shall be determined using the procedures in paragraph (b)(1) of this section, and the allowable HAP ABA emission level for the corresponding 12-month period shall be calculated in accordance with paragraph (b)(2) of this section.

(1) The actual HAP ABA emissions for a 12-month period shall be calculated as the sum of actual monthly HAP ABA emissions for each of the individual 12 months in the period. Actual monthly HAP ABA emissions shall be equal to the amount of HAP ABA added to the slabstock foam production line at the mixhead, determined in accordance with §63.1303(b), unless a recovery device is used. Slabstock foam production sources using recovery devices to reduce HAP ABA emissions shall determine actual monthly HAP ABA emissions using the procedures in paragraph (e) of this section.

(2) Monthly compliance alternative. As an alternative to determining compliance on a rolling annual basis, an owner or operator can determine compliance by comparing actual HAP ABA emissions to allowable HAP ABA emissions for each month. The allowable HAP ABA emission level shall be calculated based on the production for the month, resulting in a potentially different allowable level each month. The requirements for this monthly compliance alternative are provided in paragraph (c) of this section.

(3) Each owner or operator electing to change between the compliance methods described under paragraphs (a)(1) and (a)(2) of this section shall notify the Administrator no later than 180 calendar days prior to the change.

(c) Monthly compliance alternative. As an alternative to determining compliance on a rolling annual basis, an owner or operator can determine compliance by comparing actual HAP ABA emissions to allowable HAP ABA emissions for each month. The allowable HAP ABA emission level shall be calculated based on the production for the month, resulting in a potentially different allowable level each month. The requirements for this monthly compliance alternative are provided in paragraph (c) of this section.

(3) Each owner or operator electing to change between the compliance methods described under paragraphs (a)(1) and (a)(2) of this section shall notify the Administrator no later than 180 calendar days prior to the change.

\[
\text{emiss} \text{allow, month} = \sum_{j=1}^{m} \left( \sum_{i=1}^{\text{limit}_{i}} \left( \frac{\text{polyol}_{i}}{100} \right) \right) j \quad \text{(Equation 2)}
\]
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Where:

\[ \text{emiss}_{\text{allow}, \text{month}} = \text{Allowable HAP ABA emissions from the slabstock foam production source for the month, pounds.} \]

\[ m = \text{Number of slabstock foam production lines.} \]

\[ \text{polyol}_i = \text{Amount of polyol used in the month in the production of foam grade } i \text{ on foam production line } j, \text{ determined in accordance with paragraph (b)(3) of this section, pounds.} \]

\[ n = \text{Number of foam grades produced in the month on foam production line } j. \]

\[ \text{limit}_i = \text{HAP ABA formulation limit for foam grade } i \text{ on foam production line } j, \text{ determined in accordance with paragraph (d) of this section.} \]

(3) The amount of polyol used for specific foam grades shall be based on the amount of polyol added to the slabstock foam production line at the mixhead, determined in accordance with the provisions of §63.1303(b).

(c) Monthly compliance alternative. At each slabstock foam production source complying with the monthly compliance alternative described in paragraph (a)(2) of this section, actual HAP ABA emissions shall not exceed the corresponding allowable HAP ABA emission level for the same month. The actual monthly HAP ABA emission level shall be determined using the procedures in paragraph (c)(1) of this section, and the allowable monthly HAP ABA emission level shall be calculated in accordance with paragraph (c)(2) of this section.

(1) The actual monthly HAP ABA emissions shall be equal to the amount of HAP ABA added to the slabstock foam production line at the mixhead, determined in accordance with §63.1303(b), unless a recovery device is used. Slabstock foam production sources using recovery devices to reduce HAP ABA emissions shall determine actual monthly HAP ABA emissions using the procedures in paragraph (e) of this section.

(2) The allowable HAP ABA emissions for the month shall be determined in accordance with Equation 2 of this section.

(d) HAP ABA formulation limitations. For each grade, the HAP ABA formulation limitation shall be determined in accordance with paragraphs (d)(1) through (d)(3) of this section. For any grade, the owner or operator may designate zero as the HAP ABA formulation limitation and not determine the HAP ABA formulation limitation in accordance with paragraphs (d)(1) through (d)(3) of this section.

(1) For existing sources, the HAP ABA formulation limitation for each grade of slabstock foam produced shall be determined using Equation 3 of this section. Zero shall be the formulation limitation for any grade of foam where the result of the formulation limitation equation (Equation 3) is negative (i.e., less than zero).

\[
\text{ABA}_{\text{limit}} = -0.25(\text{IFD}) - 19.1 \left( \frac{1}{\text{IFD}} \right) - 16.2(\text{DEN}) - 7.56 \left( \frac{1}{\text{DEN}} \right) + 36.5
\]  (Equation 3)

Where:

\[ \text{ABA}_{\text{limit}} = \text{HAP ABA formulation limitation, parts HAP ABA allowed per hundred parts polyol (pph).} \]

\[ \text{IFD} = \text{Indentation force deflection, pounds.} \]

\[ \text{DEN} = \text{Density, pounds per cubic foot.} \]

(2) For new sources, the HAP ABA formulation limitation for each grade of slabstock foam produced shall be determined as described in paragraphs (d)(2)(i) through (d)(2)(iv) of this section and in Table 1 of this subpart.

(i) For each foam grade with a density of 0.95 pounds per cubic foot or less, the HAP ABA formulation limitation shall be determined using Equation 3. Zero shall be the formulation limitation for any grade of foam where the result of the formulation limitation equation (Equation 3 of this section) is negative (i.e., less than zero).
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(ii) For each foam grade with a density of 1.4 pounds per cubic foot or less, and an IFD of 15 pounds or less, the HAP ABA formulation limitation shall be determined using Equation 3.

(iii) For each foam grade with a density greater than 0.95 pounds per cubic foot and an IFD greater than 15 pounds, the HAP ABA formulation limitation shall be zero.

(iv) For each foam grade with a density greater than 1.40 pounds per cubic foot, the HAP ABA formulation limitation shall be zero.

(3) With the exception of those grades for which the owner or operator has designated zero as the HAP ABA formulation limitation, the IFD and density for each foam grade shall be determined in accordance with §63.1304(b) and recorded in accordance with §63.1307(c)(1)(ii)(B) or §63.1307(c)(2)(i)(B) within 10 working days of the production of the foam.

(e) Compliance using recovery devices. If a recovery device is used to comply with paragraphs (b) or (c) of this section, the owner or operator shall determine the allowable HAP ABA emissions for each month using Equation 2 in paragraph (b)(2) of this section, and the actual monthly HAP ABA emissions in accordance with paragraph (e)(3) of this section. The owner or operator shall also comply with the provisions of paragraph (e)(2) of this section.

(1) The actual monthly HAP ABA emissions shall be determined using Equation 4:

\[ E_{\text{actual}} = E_{\text{unc}} - \text{HAPABA}_{\text{recovered}} \]  

(Equation 4)

Where:

- \( E_{\text{actual}} \) = Actual HAP ABA emissions after control, pounds/month.
- \( E_{\text{unc}} \) = Uncontrolled HAP ABA emissions, pounds/month, determined in accordance with paragraph (b)(1) of this section.
- HAPABA_{recovered} = HAP ABA recovered, pounds/month, determined in accordance with paragraph (e)(2) of this section.

(2) The amount of HAP ABA recovered shall be determined in accordance with §63.1303(c).

§ 63.1298 Standards for slabstock flexible polyurethane foam production—HAP emissions from equipment cleaning.

Each owner or operator of a new or existing slabstock affected source complying with the emission point specific limitation option provided in §63.1293(a)(1) shall not use a HAP or a HAP-based material as an equipment cleaner.

§ 63.1299 Standards for slabstock flexible polyurethane foam production—source-wide emission limitation.

Each owner or operator of a new or existing slabstock affected source complying with the source-wide emission limitation option provided in §63.1293(b) shall control HAP ABA storage and equipment leak emissions, HAP ABA emissions from the production line, and equipment cleaning HAP emissions in accordance with the provisions in this section. Compliance shall be determined on a rolling annual basis in accordance with paragraph (a) of this section. As an alternative, the owner or operator can determine compliance monthly, as described in paragraph (b) of this section.

(a) Rolling annual compliance. Under the rolling annual compliance provisions, actual source-wide HAP ABA storage and equipment leak emissions, HAP ABA emissions from the production line, and equipment cleaning HAP emissions are compared to allowable source-wide emissions for each consecutive 12-month period. The allowable source-wide HAP emission level is calculated based on the production for the 12-month period, resulting in a potentially different allowable level for each 12-month period. While compliance is on an annual basis, compliance shall be determined monthly for the preceding 12-month period. The actual source-wide HAP emission level for a consecutive 12-month period shall be determined using the procedures in
paragraphs (c)(1) through (4) of this section, unless a recovery device is used. Slabstock foam production sources using recovery devices shall determine actual source-wide HAP emissions in accordance with paragraph (e) of this section. The allowable HAP emission level for a consecutive 12-month period shall be determined using the procedures in paragraph (d) of this section.

(b) Monthly compliance alternative. As an alternative to determining compliance on a rolling annual basis, an owner or operator can determine compliance by comparing actual HAP emissions to allowable HAP emissions for each month. The allowable source-wide emission level is calculated based on the production for the month, resulting in a potentially different allowable level each month. The actual monthly emission level shall be determined using the procedures in paragraphs (c)(1) through (3) of this section, unless a recovery device is used. Slabstock foam production sources using recovery devices shall determine actual source-wide HAP emissions in accordance with paragraph (e) of this section. The allowable monthly HAP ABA emission level shall be determined in accordance with Equation 6.

(c) Procedures for determining actual source-wide HAP emissions. The actual source-wide HAP ABA storage and equipment leak emissions, HAP ABA emissions from the production line, and equipment cleaning HAP emissions shall be determined using the procedures in this section. Actual source-wide HAP emissions for each individual month shall be determined using the procedures specified in paragraphs (c)(1) through (3) of this section.

(1) Actual source-wide HAP emissions for a month shall be determined using Equation 5 and the information determined in accordance with paragraphs (c)(2) and (3) of this section.

\[
PWE_{\text{actual}} = \sum_{i=1}^{n} \left( ST_{i, \text{begin}} - ST_{i, \text{end}} + ADD_{i} \right) \quad \text{(Equation 5)}
\]

Where:
- \( PWE_{\text{actual}} \) = Actual source-wide HAP ABA and equipment cleaning HAP emissions for a month, pounds/month.
- \( n \) = Number of HAP ABA storage vessels.
- \( ST_{i, \text{begin}} \) = Amount of HAP ABA in storage vessel \( i \) at the beginning of the month, pounds, determined in accordance with the procedures listed in paragraph (c)(2) of this section.
- \( ST_{i, \text{end}} \) = Amount of HAP ABA in storage vessel \( i \) at the end of the month, pounds, determined in accordance with the procedures listed in paragraph (c)(2) of this section.
- \( ADD_{i} \) = Amount of HAP ABA added to storage vessel \( i \) during the month, pounds, determined in accordance with the procedures listed in paragraph (c)(3) of this section.

(2) The amount of HAP ABA in a storage vessel shall be determined by monitoring the HAP ABA level in the storage vessel in accordance with §63.1303(d).

(3) The amount of HAP ABA added to a storage vessel for a given month shall be the sum of the amounts of all individual HAP ABA deliveries that occur during the month. The amount of each individual HAP ABA delivery shall be determined in accordance with §63.1303(e).

(4) Actual source-wide HAP emissions for each consecutive 12-month period shall be calculated as the sum of actual monthly source-wide HAP emissions for each of the individual 12 months in the period, calculated in accordance with paragraphs (c)(1) through (3) of this section.

(d) Allowable source-wide HAP emissions for a consecutive 12-month period shall be calculated as the sum of allowable monthly source-wide HAP emissions for each of the individual 12 months in the period.
source-wide HAP emissions for each individual month shall be calculated using Equation 6.

\[
\text{emiss}_{\text{allow}, \text{month}} = \sum_{j=1}^{m} \left( \sum_{i=1}^{n} \left( \frac{\text{limit}_i \cdot \text{polyol}_i}{100} \right) \right) \quad \text{(Equation 6)}
\]

Where:
- \( \text{emiss}_{\text{allow}, \text{month}} \) = Allowable HAP ABA storage and equipment leak emissions, HAP ABA emissions from the production line, and equipment cleaning HAP emissions from the slabstock foam production source for the month, pounds.
- \( m \) = Number of slabstock foam production lines.
- \( \text{polyol}_i \) = Amount of polyol used in the month in the production of foam grade \( i \) on foam production line \( j \), determined in accordance with §63.1303(b), pounds.
- \( n \) = Number of foam grades produced in the month on foam production line \( j \).
- \( \text{limit}_i \) = HAP ABA formulation limit for foam grade \( i \), parts HAP ABA per 100 parts polyol. The HAP ABA formulation limits are determined in accordance with §63.1297(d).

(e) Compliance using recovery devices.

If a recovery device is used to comply with paragraphs (a) or (b) of this section, the owner or operator shall determine the allowable source-wide HAP emissions for each month using Equation 6 in paragraph (d) of this section, and the actual monthly source-wide HAP emissions in accordance with paragraph (e)(1) of this section. The owner or operator shall also comply with the provisions of paragraph (e)(2) of this section.

(1) Actual monthly source-wide HAP emissions shall be determined using Equation 7.

\[
E_{\text{actual}} = E_{\text{unc}} - \text{HAPABA}_{\text{recovered}} \quad \text{(Equation 7)}
\]

Where:
- \( E_{\text{actual}} \) = Actual source-wide HAP emissions after control, pounds/month.
- \( E_{\text{unc}} \) = Uncontrolled source-wide HAP emissions, pounds/month, determined in accordance with paragraph (c) (1) through (3) of this section.
- \( \text{HAPABA}_{\text{recovered}} \) = HAP ABA recovered, pounds/month, determined in accordance with paragraph (e)(2) of this section.

(2) The amount of HAP ABA recovered shall be determined in accordance with §63.1303(c).

§63.1300 Standards for molded flexible polyurethane foam production.

Each owner or operator of a new or existing molded affected source shall comply with the provisions in paragraphs (a) and (b) of this section.

(a) A HAP or HAP-based material shall not be used as an equipment cleaner to flush the mixhead, nor shall it be used elsewhere as an equipment cleaner in a molded flexible polyurethane foam process, with the following exception. Diisocyanates may be used to flush the mixhead and associated piping during periods of startup or maintenance, provided that the diisocyanate compounds are contained in a closed-loop system and are re-used in production.

(b) A HAP-based mold release agent shall not be used in a molded flexible polyurethane foam source process.

§63.1301 Standards for rebond foam production.

Each owner or operator of a new or existing rebond foam affected source
shall comply with the provisions in paragraphs (a) and (b) of this section.
(a) A HAP or HAP-based material shall not be used as an equipment cleaner at a rebond foam source.
(b) A HAP-based mold release agent shall not be used in a rebond foam source.

§ 63.1302 Applicability of subpart A requirements.
The owner or operator of an affected source shall comply with the applicable requirements of subpart A of this part, as specified in Table 2 of this subpart.

§ 63.1303 Monitoring requirements.
Owners and operators of affected sources shall comply with each applicable monitoring provision in this section.
(a) Monitoring requirements for storage vessel carbon adsorption systems. Each owner or operator using a carbon adsorption system to meet the requirements of §63.1294(a) or §63.1295 shall monitor the concentration level of the HAP or the organic compounds in the exhaust vent stream (or outlet stream exhaust) from the carbon adsorption system at the frequency specified in (a)(1) or (2) of this section in accordance with either (a)(3) or (4) of this section.

(i) The concentration level of HAP or organic compounds shall be monitored during each unloading event, or once per month during an unloading event if multiple unloading events occur in a month.
(ii) As an alternative to monthly monitoring, the owner or operator can set the monitoring frequency at an interval no greater than 20 percent of the carbon replacement interval, which is established using a design analysis described below in paragraphs (a)(1)(i) through (iii) of this section.

(ii) The design analysis shall consider the vent stream composition, constituent concentration, flow rate, relative humidity, and temperature.

(iii) The design analysis shall establish the carbon replacement interval based on the total carbon working capacity of the carbon adsorption system and the schedule for filling the storage vessel.

(b) Monitoring for HAP ABA and polyol added to the foam production line at the mixhead.

(i) Owners or operators of all slabstock affected sources shall continuously monitor the amount of polyol added at the mixhead when foam is being poured, in accordance with paragraphs (b)(2) through (4) of this section.

(ii) Owners or operators of slabstock foam affected sources using the emission point specific limitation option provided in §63.1293(a)(1) shall continuously monitor the amount of HAP ABA added at the mixhead when foam is being poured, in accordance with paragraphs (b)(2)(ii), (b)(3), and (b)(4) of this section.

(ii) The device used to monitor the parameter from paragraph (b)(2) shall have an accuracy to within +/− 2.0 percent of the HAP ABA being measured, and shall be calibrated initially, and periodically, in accordance with paragraph (b)(3)(i) or (ii) of this section.

(i) For polyol pumps, the device shall be calibrated at least once each 6 months.
(ii) For HAP ABA pumps, the device shall be calibrated at least once each month.

(4) Measurements must be recorded at the beginning and end of the production of each grade of foam within a run of foam.

(5) As an alternative to the monitoring described in paragraphs (b)(2) through (4) of this section, the owner or operator may develop an alternative monitoring program. Alternative monitoring programs must be submitted to the Administrator for approval in the Precompliance Report as specified in §63.1306(c)(4) for existing sources or in the Application for approval of construction or reconstruction for new sources. If an owner or operator wishes to develop an alternative monitoring program after the compliance date, the program shall be submitted to the Administrator for approval before the owner or operator wishes to begin using the alternative program. If the Administrator does not notify the owner or operator of objections to the program within 45 days after its receipt, the program shall be deemed approved.

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Recovered HAP ABA monitoring.
The owner or operator of each slabstock affected source using a recovery device to reduce HAP ABA emissions shall develop and comply with a recovered HAP ABA monitoring and recordkeeping program. The components of these plans shall include, at a minimum, the items listed in paragraphs (c)(1) through (5) of this section. These plans must be submitted for approval in accordance with paragraph (c)(6) of this section.

(1) A device, installed, calibrated, maintained, and operated according to the manufacturer’s specifications, that indicates the cumulative amount of HAP ABA recovered by the solvent recovery device over each 1-month period. The device shall be certified by the manufacturer to be accurate to within $\pm 2.0\%$.

(2) The location where the monitoring will occur shall ensure that the measurements are taken after HAP ABA has been fully recovered (i.e., after separation from water introduced into the HAP ABA during regeneration).

(3) A description of the parameter to be monitored, and the times the parameter will be monitored.

(4) Data demonstrating that the monitoring device is accurate to within $\pm 2.0\%$.

(5) Procedures to ensure that the accuracy of the parameter monitoring results is maintained. These procedures shall, at a minimum, consist of periodic calibration of all monitoring devices.

(6) Recovered HAP ABA monitoring and recordkeeping programs must be submitted to the Administrator for approval in the Precompliance Report as specified in §63.1306(c)(8) for existing sources or in the Application for approval of construction or reconstruction for new sources. If an owner or operator wishes to develop a recovered HAP ABA monitoring program after the compliance date, the program shall be submitted to the Administrator for approval before the owner or operator wishes to begin using the program. If the Administrator does not notify the owner or operator of objections to the program within 45 days after its receipt, the program shall be deemed approved. Until the program is approved, the owner or operator of an affected
source remains subject to the requirements of this subpart.

(d) Monitoring of HAP ABA in a storage vessel. The amount of HAP ABA in a storage vessel shall be determined weekly by monitoring the HAP ABA level in the storage vessel using a level measurement device that meets the criteria described in paragraphs (d)(1) and either (d)(2) or (d)(3) of this section.

(1) The level measurement device must be calibrated initially and at least once per year thereafter.

(2) With the exception of visually-read level measurement devices (i.e., gauge glass), the device must have either a digital or printed output.

(3) If the level measurement device is a visually-read device, the device must be equipped with permanent graduated markings to indicate HAP ABA level in the storage tank.

(e) Monitoring of HAP ABA added to a storage vessel. The amount of HAP ABA added to a storage vessel during a delivery shall be determined in accordance with either paragraphs (e)(1), (2), (3), or (4) of this section.

(1) The volume of HAP ABA added to the storage vessel shall be determined by recording the volume in the storage vessel prior to the delivery and the volume after the delivery, provided that the storage tank level measurement device used to determine the levels meets the criteria in (d) of this section.

(2) The volume of HAP ABA added to the storage vessel shall be determined by monitoring the flow rate using a device with an accuracy of ±2.0 percent, and calibrated initially and at least once each six months thereafter.

(3) The weight of HAP ABA added to the storage vessel shall be calculated as the difference of the full weight of the transfer vehicle prior to unloading into the storage vessel and the empty weight of the transfer vehicle after unloading into the storage vessel. The weight shall be determined using a scale meeting the requirements of either paragraph (e)(2)(i) or (ii) of this section.

(i) A description of the parameter to be monitored to determine the amount of HAP ABA added to the storage vessel during a delivery,

(ii) A description of how the results will be recorded, and how the results will be converted into the amount of HAP ABA added to the storage vessel during a delivery,

(iii) Data demonstrating that the monitoring device is accurate to within ±2.0 percent, and

(iv) Procedures to ensure that the accuracy of the monitoring measurements is maintained. These procedures shall, at a minimum, consist of periodic calibration of all monitoring devices.

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§ 63.1304 Testing requirements.

Owners and operators of affected sources shall use the test methods listed in this section, as applicable, to demonstrate compliance with this subpart.

(a) Test method and procedures to determine equipment leaks. Monitoring, as required under §63.1296, shall comply with the following requirements:

(1) Monitoring shall comply with Method 21 of 40 CFR part 60, appendix A.

(2) The detection instrument shall meet the performance criteria of Method 21 of 40 CFR part 60, appendix A, except that the instrument response factor criteria in section 3.1.2(a) of Method 21 shall be for the average composition of the source fluid, rather than for each individual VOC in the stream. For source streams that contain nitrogen, air, or other inerts which are not HAP or VOC, the average stream response factor shall be calculated on an inert-free basis. The response factor may be determined at any concentration for which monitoring for leaks will be conducted.

(3) The instrument shall be calibrated before use on each day of its use by the procedures specified in Method 21 of 40 CFR part 60, appendix A.

(4) Calibration gases shall be:

(i) Zero air (less than 10 ppm of hydrocarbon in air); and

(ii) A mixture of methane and air at a concentration of approximately, 1,000 ppm for all transfer pumps; and 500 ppm for all other equipment, except as provided in paragraph (a)(4)(iii) of this section.

(iii) The instrument may be calibrated at a higher methane concentration (up to 2,000 ppm) than the leak definition concentration for a specific piece of equipment for monitoring that piece of equipment. If the monitoring instrument's design allows for multiple calibration gas concentrations, then the lower concentration calibration gas shall be no higher than 2,000 ppm methane and the higher concentration calibration gas shall be no higher than 10,000 ppm methane.

(5) Monitoring shall be performed when the equipment is in HAP ABA service, in use with an acceptable surrogate volatile organic compound which is not a HAP ABA, or is in use with any other detectable gas or vapor.

(6) If no instrument is available on-site that will meet the performance criteria specified in section 3.1.2(a) of Method 21 of 40 CFR Part 60, appendix A, the readings from an available instrument may be adjusted by multiplying by the average response factor for the stream.

(b) Test method to determine foam properties. The IFD and density of each grade of foam produced during each run of foam shall be determined using ASTM D3574-91, Standard Test Methods for Flexible Cellular Materials—Slab, Bonded, and Molded (incorporation by reference—see §63.14), using a sample of foam cut from the center of the foam bun. The maximum sample size for which the IFD and density is determined shall not be larger than 24 inches by 24 inches by 4 inches. For grades of foam where the owner or operator has designated the HAP ABA formulation limitation as zero, the owner or operator is not required to determine the IFD and density in accordance with this paragraph.

§ 63.1305 Alternative means of emission limitation.

An owner or operator of an affected source may request approval to use an alternative means of emission limitation, following the procedures in this section.

(a) The owner or operator can request approval to use an alternative means of emission limitation in the precompliance report for existing sources, the application for construction or reconstruction for new sources, or at any time.

(b) This request shall include a complete description of the alternative means of emission limitation.

(c) Each owner or operator applying for permission to use an alternative means of emission limitation under §63.6(g) shall be responsible for collecting and verifying data to demonstrate the emission reduction achieved by the alternative means of emission limitation.

(d) Use of the alternative means of emission limitation shall not begin
unti approval is granted by the Ad-
ministrator in accordance with §63.6(g).

§ 63.1306 Reporting requirements.

Owners and operators of affected sources shall comply with each applicable reporting provision in this section.

(a) Initial notification. Each affected source shall submit an initial notification in accordance with §63.9(b).

(b) Application for approval of construction or reconstruction. Each owner or operator shall submit an application for approval of construction or reconstruction in accordance with the provisions of §63.5(d).

(c) Precompliance report. Each slabstock affected source shall submit a precompliance report no later than 12 months before the compliance date. This report shall contain the information listed in paragraphs (c)(1) through (c)(8) of this section, as applicable.

(1) Whether the source will comply with the emission point specific limitations described in §63.1293(a), or with the source-wide emission limitation described in §63.1293(b).

(2) For a source complying with the emission point specific limitations, whether the source will comply on a rolling annual basis in accordance with §63.1297(b), or will comply with the monthly alternative for compliance contained in §63.1297(c).

(3) For a source complying with the source-wide emission limitation, whether the source will comply on a rolling annual basis in accordance with §63.1299(a), or will comply with the monthly alternative for compliance contained in §63.1299(b).

(4) A description of how HAP ABA and/or polyol added at the mixhead will be monitored. If the owner or operator is developing an alternative monitoring program, the alternative monitoring program containing the information listed in paragraphs (d)(1) through (d)(4) shall be submitted.

(5) Notification of the intent to use a recovery device to comply with the provisions of §63.1297 or §63.1299.

(6) For slabstock affected sources complying with §63.1297 or §63.1299 using a recovery device, the continuous recovered HAP ABA monitoring and recordkeeping program, developed in accordance with §63.1303(c).

(7) For sources complying with the source-wide emission limitation, a description of how the amount of HAP ABA in a storage vessel shall be determined.

(8) For sources complying with the source-wide emission limitation, a description of how the amount of HAP ABA added to a storage vessel during a delivery will be monitored. If the owner or operator is developing an alternative monitoring program, the alternative monitoring program containing the information in §63.1303(e)(4)(i) through (iv) shall be submitted.

(9) If the Administrator does not notify the owner or operator of objections to an alternative monitoring program submitted in accordance with (c)(4) or (c)(6) of this section, or a recovered HAP ABA monitoring and recordkeeping program submitted in accordance with (c)(7) of this section, the program shall be deemed approved 45 days after its receipt by the Administrator.

(d) Notification of compliance status. Each affected source shall submit a notification of compliance status report no later than 180 days after the compliance date. For slabstock affected sources, this report shall contain the information listed in paragraphs (d)(1) through (3) of this section, as applicable. This report shall contain the information listed in paragraph (d)(4) of this section for molded foam processes and in paragraph (d)(5) for rebond foam processes.

(1) A list of diisocyanate storage vessels, along with a record of the type of control utilized for each storage vessel.

(2) For transfer pumps in diisocyanate service, a record of the type of control utilized for each transfer pump.

(3) If the source is complying with the emission point specific limitations of §§63.1294 through 63.1298, the information listed in paragraphs (b)(3)(i) through (iii) of this section.

(i) A list of HAP ABA storage vessels, along with a record of the type of control utilized for each storage vessel.

(ii) A list of pumps, valves, connectors, pressure-relief devices, and open-
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ended valves or lines in HAP ABA service.

(iii) A list of any modifications to equipment in HAP ABA service made to comply with the provisions of § 63.1296.

(4) A statement that the molded foam affected source is in compliance with § 63.1301, or a statement that molded foam processes at an affected source are in compliance with § 63.1300.

(5) A statement that the rebond foam affected source is in compliance with § 63.1301, or that rebond processes at an affected source are in compliance with § 63.1301.

(e) Semiannual reports. Each slabstock affected source shall submit a report containing the information specified in paragraphs (e)(1) through (5) of this section semiannually no later than 60 days after the end of each 180 day period. The first report shall be submitted no later than 240 days after the date that the Notification of Compliance Status is due and shall cover the 6-month period beginning on the date that the Notification of Compliance Status Report is due.

(1) For slabstock affected sources complying with the rolling annual compliance provisions of either § 63.1297 or § 63.1299, the allowable and actual HAP ABA emissions (or allowable and actual source-wide HAP emissions) for each of the 12-month periods ending on each of the six months in the reporting period. This information is not required to be included in the initial semi-annual compliance report.

(2) For sources complying with the monthly compliance alternative of either § 63.1297 or § 63.1299 (between rolling annual and monthly) shall notify the Administrator no later than 180 days prior to the change.

(3) For sources complying with the storage vessel provisions of § 63.1294(a) or § 63.1295 using a carbon adsorption system, unloading events that occurred after breakthrough was detected and before the carbon was replaced.

(4) Any equipment leaks that were not repaired in accordance with § 63.1294(a)(1)(ii) or § 63.1295(b)(2).

(f) Other reports. (1) Change in selected emission limitation. An owner or operator electing to change their slabstock flexible polyurethane foam emission limitation (from emission point specific limitations to a source-wide emission limitation, or vice versa), selected in accordance with § 63.1293, shall notify the Administrator no later than 180 days prior to the change.

(2) Change in selected compliance method. An owner or operator changing the period of compliance for either § 63.1297 or § 63.1299 (between rolling annual and monthly) shall notify the Administrator no later than 180 days prior to the change.

(g) Annual compliance certifications. Each affected source subject to the provisions in §§ 63.1293 through 63.1301 shall submit a compliance certification annually.

(1) The compliance certification shall be based on information consistent with that contained in § 63.1308 of this section, as applicable.

(2) A compliance certification required pursuant to a State or local operating permit program may be used to satisfy the requirements of this section, provided that the compliance certification is based on information consistent with that contained in § 63.1308 of this section, and provided that the Administrator has approved the State or local operating permit program under part 70 of this chapter.

(3) Each compliance certification submitted pursuant to this section shall be signed by a responsible official of the company that owns or operates the affected source.

§ 63.1307 Recordkeeping requirements.

The applicable records designated in paragraphs (a) through (c) of this section shall be maintained by owners and operators of all affected sources.

(a) Storage vessel records. (1) A list of diisocyanate storage vessels, along with a record of the type of control utilized for each storage vessel.

(2) For each slabstock affected source complying with the emission point specific limitations of §§ 63.1294 through
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63.1298, a list of HAP ABA storage vessels, along with a record of the type of control utilized for each storage vessel.

(3) For storage vessels complying through the use of a carbon adsorption system, paragraph (a)(3)(i) or (ii), and paragraph (a)(3)(iii) of this section.

(i) Records of dates and times when the carbon adsorption system is monitored for carbon breakthrough and the monitoring device reading, when the device is monitored in accordance with §63.1303(a); or

(ii) For affected sources monitoring at an interval no greater than 20 percent of the carbon replacement interval, in accordance with §63.1303(a)(2), the records listed in paragraphs (a)(3)(iii)(A) and (B) of this section.

(A) Records of the design analysis, including all the information listed in §63.1303(a)(2)(i) through (iii), and

(B) Records of dates and times when the carbon adsorption system is monitored for carbon breakthrough and the monitoring device reading.

(iii) Date when the existing carbon in the carbon adsorption system is replaced with fresh carbon.

(4) For storage vessels complying through the use of a vapor return line, paragraphs (a)(4)(i) through (iii) of this section.

(i) Dates and times when each unloading event occurs and each inspection of the vapor return line for leaks occurs.

(ii) Records of dates and times when a leak is detected in the vapor return line.

(iii) Records of dates and times when a leak is repaired.

(b) Equipment leak records. (1) A list of components as specified below in paragraphs (b)(1)(i) and (ii).

(i) For all affected sources, a list of components in diisocyanate service,

(ii) For affected sources complying with the emission point specific limitations of §§63.1294 through 63.1298, a list of components in HAP ABA service.

(2) For transfer pumps in diisocyanate service, a record of the type of control utilized for each transfer pump and the date of installation.

(3) When a leak is detected as specified in §63.1294(b)(1), §63.1296(a)(2), (b)(1), (c)(1), and (d)(1), the requirements listed in paragraphs (b)(3)(i) and (ii) of this section apply:

(i) Leaking equipment shall be identified in accordance with the requirements in paragraphs (b)(3)(i)(A) through (C) of this section.

(A) A readily visible identification, marked with the equipment identification number, shall be attached to the leaking equipment.

(B) The identification on a valve may be removed after it has been monitored for 2-successive quarters as specified in §63.1296(b)(1) and no leak has been detected during those 2 quarters.

(C) The identification on equipment, other than a valve, may be removed after it has been repaired.

(ii) The information in paragraphs (b)(3)(ii)(A) through (H) shall be recorded for leaking components.

(A) The instrument and operator identification numbers and the equipment identification number.

(B) The date the leak was detected and the dates of each attempt to repair the leak.

(C) Repair methods applied in each attempt to repair the leak.

(D) The words “above leak definition” if the maximum instrument reading measured by the methods specified in §63.1304(a) after each repair attempt is equal or greater than the leak definitions for the specified equipment.

(E) The words “repair delayed” and the reason for the delay if a leak is not repaired within 15 calendar days after discovery of the leak.

(F) The expected date of the successful repair of the leak if a leak is not repaired within 15 calendar days.

(G) The date of successful repair of the leak.

(H) The date the identification is removed.

(c) HAP ABA records—(1) Emission point specific limitations—rolling annual compliance and monthly compliance alternative records. Each slabstock affected source complying with the emission point specific limitations of §61A3.1294 through 63.1298, and the rolling annual compliance provisions of §63.1297(a)(1), shall maintain the records listed in paragraphs (c)(1)(i), (ii), (iii), and (iv) of this section. Each flexible polyurethane foam slabstock source complying with the emission point specific limitations of §63.1294 through 63.1298, and the rolling annual compliance provisions of §63.1297(a)(1), shall maintain the records listed in paragraphs (c)(1)(i), (ii), (iii), and (iv) of this section.
limitations of §§63.1294 through 63.1298, and the monthly compliance alternative of §63.1297(a)(2), shall maintain the records listed in paragraphs (c)(1)(i), (ii), and (iv) of this section.

(i) Daily records of the information listed below in paragraphs (c)(1)(i)(A) through (C) of this section.
   (A) A log of foam runs each day. For each run, the log shall include a list of the grades produced during the run.
   (B) Results of the density and IFD testing for each grade of foam produced during each run of foam, conducted in accordance with the procedures in §63.1304(b). The results of this testing shall be recorded within 10 working days of the production of the foam. For grades of foam where the owner or operator has designated the HAP ABA formulation limitation as zero, the owner or operator is not required to keep records of the IFD and density.
   (C) The amount of polyol added to the slabstock foam production line at the mixhead for each run of foam, determined in accordance with §63.1303(b).

(ii) Monthly records of the information listed in paragraphs (c)(1)(ii)(A) through (E) of this section.
   (A) A listing of all foam grades produced during the month.
   (B) For each foam grade produced, the HAP ABA formulation limitation, calculated in accordance with §63.1297(d).
   (C) With the exception of those grades for which the owner or operator has designated zero as the HAP ABA formulation limitation, the total amount of polyol used in the month for each foam grade produced.
   (D) The total allowable HAP ABA emissions for the month, determined in accordance with §63.1297(b)(2).
   (E) The total amount of HAP ABA added to the slabstock foam production line at the mixhead during the month, determined in accordance with §63.1303(b).

(iii) Each source complying with the rolling annual compliance provisions of §63.1297(b) shall maintain the records listed in paragraphs (c)(1)(iii)(A) and (B) of this section.
   (A) The sum of the total allowable HAP ABA emissions for the month and the previous 11 months.
   (B) The sum of the total actual HAP ABA emissions for the month and the previous 11 months.

(iv) Records of all calibrations for each device used to measure polyol and HAP ABA added at the mixhead, conducted in accordance with §63.1303(b)(3).

(2) Source-wide limitations—rolling annual compliance and monthly compliance alternative records. Each slabstock affected source complying with the source-wide limitations of §63.1299, and the rolling annual compliance provisions in §63.1299(a), shall maintain the records listed in paragraphs (c)(2)(i) through (c)(2)(vii) of this section. Each flexible polyurethane foam slabstock source complying with the source-wide limitations of §63.1299, and the monthly compliance alternative of §63.1299(b), shall maintain the records listed in paragraphs (c)(2)(i) through (c)(2)(vii) of this section.

(i) Daily records of the information listed in paragraphs (c)(2)(i)(A) through (C) of this section.
   (A) A log of foam runs each day. For each run, the log shall include a list of the grades produced during the run.
   (B) Results of the density and IFD testing for each grade of foam produced during each run of foam, conducted in accordance with the procedures in §63.1304(b). The results of this testing shall be recorded within 10 working days of the production of the foam. For grades of foam where the owner or operator has designated the HAP ABA formulation limitation as zero, the owner or operator is not required to keep records of the IFD and density.
   (C) With the exception of those grades for which the owner or operator has designated zero as the HAP ABA formulation limitation, the amount of polyol added to the slabstock foam production line at the mixhead for each grade produced during each run of foam, determined in accordance with §63.1303(b).

(ii) For sources complying with the source-wide emission limitation, weekly records of the storage tank level, determined in accordance with §63.1303(d).
(iii) Monthly records of the information listed below in paragraphs (c)(2)(iii)(A) through (E) of this section.

(A) A listing of all foam grades produced during the month.

(B) For each foam grade produced, the residual HAP formulation limitation, calculated in accordance with §63.1297(d).

(C) With the exception of those grades for which the owner or operator has designated zero as the HAP ABA formulation limitation, the total amount of polyol used in the month for each foam grade produced.

(D) The total allowable HAP ABA and equipment cleaning emissions for the month, determined in accordance with §63.1297(b)(2).

(E) The total actual source-wide HAP ABA emissions for the month, determined in accordance with §63.1299(c)(1), along with the information listed in paragraphs (c)(2)(iii)(E)(1) and (2) of this section.

1 The amounts of HAP ABA in the storage vessel at the beginning and end of the month, determined in accordance with §63.1299(c)(2); and

2 The amount of each delivery of HAP ABA to the storage vessel, determined in accordance with §63.1299(c)(3).

(iv) Each source complying with the rolling annual compliance provisions of §63.1299(a) shall maintain the records listed in paragraphs (c)(2)(iv)(A) and (B) of this section.

(A) The sum of the total allowable HAP ABA and equipment cleaning HAP emissions for the month and the previous 11 months.

(B) The sum of the total actual HAP ABA and equipment cleaning HAP emissions for each device used to measure polyol added at the mixhead, conducted in accordance with §63.1303(b)(3).

(v) Records of all calibrations for each device used to measure the amount of HAP ABA in the storage vessel, conducted in accordance with §63.1303(d)(1).

(vi) Records of all calibrations for each device used to measure the amount of HAP ABA added to the storage vessel meet the requirements of §63.1303(e)(3). For scales meeting the criteria of §63.1303(e)(3)(i), this documentation shall be in the form of written confirmation of the State or local approval. For scales complying with §63.1303(e)(3)(ii), this documentation shall be in the form of a report provided by the registered scale technician.

(d) The owner or operator of each affected source complying with §63.1297 or §63.1299 through the use of a recovery device shall maintain the following records:

1 A copy of the recovered HAP ABA monitoring and recordkeeping program, developed pursuant to §63.1303(c);

2 Certification of the accuracy of the monitoring device,

3 Records of periodic calibration of the monitoring devices,

4 Records of parameter monitoring results, and

5 The amount of HAP ABA recovered each time it is measured.

(e) The owner or operator of an affected source subject to §63.1298 of this subpart shall maintain a product data sheet for each equipment cleaner used which includes the HAP content, in kg of HAP/kg solids (lb HAP/lb solids).

(f) The owner or operator of an affected source following the compliance methods in §63.1308(b)(1) and (c)(1) shall maintain records of each use of a vapor return line during unloading, of any leaks detected during unloading, and of repairs of leaks detected during unloading.

(g) The owner or operator of an affected source subject to §63.1300 or §63.1301 of this subpart shall maintain a product data sheet for each compound other than diisocyanates used to flush the mixhead and associated piping during periods of startup or maintenance, which includes the HAP content, in kg of HAP/kg solids (lb HAP/lb solids), of each solvent other than diisocyanates used to flush the mixhead and associated piping during periods of startup or maintenance.

(h) The owner or operator of an affected source subject to §63.1300 or §63.1301 of this subpart shall maintain a product data sheet for each mold release agent used that includes the HAP content, in kg of HAP/kg solids (lb
$63.1308$ Compliance demonstrations.

(a) For each affected source, compliance with the requirements listed in paragraphs (a)(1) through (a)(2) of this section shall mean compliance with the requirements contained in §§63.1293 through 63.1301, absent any credible evidence to the contrary.

(1) The requirements described in Tables 3, 4, and 5 of this subpart; and

(2) The requirement to submit a compliance certification annually as required under $63.1306(g).

(b) All slabstock affected sources. For slabstock affected sources, failure to meet the requirements contained in §63.1294 shall be considered a violation of this subpart. Violation of each item listed in the paragraphs (b)(1) through (b)(6) of this section, as applicable, shall be considered a separate violation.

(1) For each affected source complying with §63.1294(a) in accordance with §63.1294(a)(1), each unloading event that occurs when the diisocyanate storage vessel is not equipped with a vapor return line from the storage vessel to the tank truck or rail car, each unloading event that occurs when the vapor line is not connected, each unloading event that the vapor line is not inspected for leaks as described in §63.1294(a)(1)(i), each unloading event that a leak has been detected and not repaired, and each calendar day after a leak is detected, but not repaired as soon as practicable;

(2) For each affected source complying with §63.1294(a) in accordance with §63.1294(a)(2), each unloading event that the diisocyanate storage vessel is not equipped with a carbon adsorption system, each unloading event (or each month if more than one unloading event occurs in a month) that the carbon adsorption system is not monitored for breakthrough in accordance with §§63.1303(a)(3) or (4), and each unloading event that occurs when the carbon is not replaced after an indication of breakthrough;

(3) For each affected source complying with §63.1294(a) in accordance with §63.1294(a)(2) through the alternative monitoring procedures in §63.1303(a)(2), each unloading event that the diisocyanate storage vessel is not equipped with a carbon adsorption system, each time that the carbon adsorption system is not monitored for breakthrough in accordance with §63.1303(a)(3) or (4) at the interval established in the design analysis, and each unloading event that occurs when the carbon is not replaced after an indication of breakthrough;

(4) For each affected source complying with §63.1294(b) in accordance with §63.1294(b)(1), each calendar day that a transfer pump in diisocyanate service is not a sealless pump;

(5) For each affected source complying with §63.1294(b) in accordance with §63.1294(b)(2), each calendar day that a transfer pump in diisocyanate service is not submerged as described in §63.1294(b)(2)(ii), each week that the pump is not visually monitored for leaks, each calendar day after 5 calendar days after detection of a leak that a first attempt at repair has not been made in accordance with §63.1294(b)(2)(iii)(B), and the earlier of each calendar day after 15 calendar days after detection of a leak that a leak is not repaired, or a leak is not repaired as soon as practicable, each subsequent calendar day (with the exception of situations meeting the criteria of §63.1294(d));

(6) For each affected source complying with §63.1294(c), each calendar day after 5 calendar days after detection of a leak that a first attempt at repair has not been made, and the earlier of each calendar day after 15 calendar days after detection of a leak that a leak is not repaired, or if a leak is not repaired as soon as practicable, each subsequent calendar day (with the exception of situations meeting the criteria of §63.1294(f));

(c) Slabstock affected sources complying with the emission point specific limitations. For slabstock affected sources complying with the emission point specific limitations as provided in §63.1293(a), failure to meet the requirements contained in §§63.1296 through 63.1298 shall be considered a violation of this subpart. Violation of each item listed in the paragraphs (c)(1) through (c)(17) of this section, as applicable,
shall be considered a separate violation.

(1) For each affected source complying with §63.1295(a) in accordance with §63.1295(b), each unloading event that occurs when the HAP ABA storage vessel is not equipped with a vapor return line from the storage vessel to the tank truck or rail car, each unloading event that occurs when the vapor line is not connected, each unloading event that occurs when the vapor line is not inspected for leaks as described in §63.1295(b)(1), each unloading event that occurs after a leak has been detected and not repaired, and each calendar day after a leak is detected but not repaired as soon as practicable;

(2) For each affected source complying with §63.1295(a) in accordance with §63.1295(c), each unloading event that the HAP ABA storage vessel is not equipped with a carbon adsorption system, each unloading event (or each month if more than one unloading event occurs in a month) that the carbon adsorption system is not monitored for breakthrough in accordance with §63.1303(a)(3) or (4), and each unloading event that occurs when the carbon is not replaced after an indication of breakthrough;

(3) For each affected source complying with §63.1295(a) in accordance with §63.1295(c) through the alternative monitoring procedures in §63.1303(a)(2), each unloading event that the HAP ABA storage vessel is not equipped with a carbon adsorption system, each time that the carbon adsorption system is not monitored for breakthrough in accordance with §63.1303(a)(3) or (4) at the interval established in the design analysis, and each unloading event that occurs when the carbon is not replaced after an indication of breakthrough;

(4) For each affected source complying with §63.1296(a) in accordance with §63.1296(a)(1), each calendar day that a transfer pump in HAP ABA service is not a sealless pump;

(5) For each affected source complying with §63.1296(a) in accordance with §63.1296(a)(2), each week that a visual inspection of a pump in HAP ABA service is not performed, each quarter that a pump in HAP ABA service is not monitored to detect leaks in accordance with §63.1304(a), each calendar day after 5 calendar days after detection of a leak that a first attempt at repair has not been made in accordance with §63.1296(b)(2)(iii)(B), and the earlier of each calendar day after 15 calendar days after detection of a leak that a leak is not repaired, or if a leak is not repaired as soon as practicable, each subsequent calendar day (with the exception of situations meeting the criteria of §63.1296(f));

(6) For each affected source complying with §63.1296(b) in accordance with §63.1296(b)(1) and (2), each quarter that a valve in HAP ABA service is not monitored to detect leaks in accordance with §63.1304(a), each calendar day after 5 calendar days after detection of a leak that a first attempt at repair has not been made in accordance with §63.1296(b)(2)(ii), and each calendar day after 15 calendar days after detection of a leak that a leak is not repaired, or if a leak is not repaired as soon as practicable, whichever is earlier (with the exception of situations meeting the criteria of §63.1296(f));

(7) For each affected source complying with §63.1296(b)(3) for each valve designated as unsafe to monitor as described in §63.1296(b)(3)(i), failure to develop the written plan required by §63.1296(b)(3)(ii), each period specified in the written plan that an unsafe-to-monitor valve in HAP ABA service is not monitored, and each calendar day in which a leak is not repaired in accordance with the written plan;

(8) For each affected source complying with §63.1296(b)(4) for one or more valves designated as difficult-to-monitor in accordance with §63.1296(b)(4)(i) and (ii), failure to develop the written plan required by §63.1296(b)(4)(iii), each calendar year that a difficult-to-monitor valve in HAP ABA service is not monitored, and each calendar day in which a leak is not repaired in accordance with the written plan;

(9) For each affected source complying with §63.1296(c) in accordance with §63.1296(c)(1) and (2), each year that a connector in HAP ABA service is not monitored to detect leaks in accordance with §63.1304(a); each calendar day after 3 months after a connector has been opened, has otherwise
had the seal broken, or a leak is re-
paired, that each connector in HAP
ABA service is not monitored to detect
leaks in accordance with §63.1304(a);
each calendar day after 5 calendar days
after detection of a leak that a first at-
tempt at repair has not been made, and
the earlier of each calendar day after 15
calendar days after detection of a leak
that a leak is not repaired, or if a leak
is not repaired as soon as practicable,
each subsequent calendar day (with the
exception of situations meeting the
criteria of §63.1296(f));

(10) For each affected source com-
plying with §63.1296(c)(3) for one or
more connectors designated as unsafe-
to-monitor in accordance with
§63.1296(c)(3)(i), failure to develop the
written plan required by
§63.1296(c)(3)(ii), each period specified
in the written plan that an unsafe-to-
monitor valve in HAP ABA service is
not monitored, each calendar day after
5 calendar days after detection of a
leak of an unsafe-to-monitor connector
that a first attempt at repair has not
been made, and the earlier of each cal-
endar day after 15 calendar days after
detection of a leak that a leak is not
repaired, or if a leak is not repaired as
soon as practicable, each subsequent
calendar day (with the exception of sit-
tuations meeting the criteria of §63.1296(f));

(11) For each affected source com-
plying with §63.1296(c)(4) for one or
more connectors designated as unsafe
to repair, each year that one or more
unsafe-to-repair connectors in HAP
ABA service is not monitored to detect
leaks in accordance with §63.1304(a);
each calendar day after 3 months after
one or more unsafe-to-repair connec-
tors has been opened, has otherwise
had the seal broken, or a leak is re-
paired, that each unsafe-to-repair con-
nector in HAP ABA service is not mon-
titored to detect leaks in accordance
with §63.1304(a); and the earlier of each
calendar day after six months after de-
tection of a leak that a leak is not re-
paired, or if a leak is not repaired as
soon as practicable, each subsequent
calendar day;

(12) For each affected source com-
plying with §63.1296(d) in accordance
with §63.1304(b), each calendar day after
the 5 days that the
pressure-relief device has not been
monitored in accordance with
§63.1304(a) after a potential leak was
discovered as described in §63.1296(d)(1),
each calendar day after 5 calendar days
after detection of a leak that a first at-
tempt at repair has not been made, and
the earlier of each calendar day after 15
calendar days after detection of a leak
that a leak is not repaired, or if a leak
is not repaired as soon as practicable,
each subsequent calendar day (with the
exception of situations meeting the
criteria of §63.1296(f));

(13) For each affected source com-
plying with §63.1296(e) in accordance
with §63.1296(e)(1) through (5), each cal-
endar day that an open-ended valve or
line has no cap, blind flange, plug or
second valve as described in
§63.1296(e)(2), and each calendar day
that a valve on the process fluid end of
an open-ended valve or line equipped
with a second valve is not closed before
the second valve is closed;

(14) For each affected source com-
plying with §63.1297(a) in accordance
with the rolling annual compliance op-
tion in §63.1297(a)(1) and (b), each cal-
endar day in the 12-month period for
which the actual HAP ABA emissions
exceeded the allowable HAP ABA emis-
sions level, each calendar day in which
foam is being poured where the amount
of polyol added at the mixhead is not
monitored (as required) in accordance
with §63.1303(b)(1)(i), each calendar day
in which foam is being poured where
the amount of HAP ABA added at the
mixhead is not monitored (as required)
in accordance with §63.1303(b)(1)(ii),
each calendar day in a 6-month period
in which the polyol pumps are not cali-
brated in accordance with
§63.1303(b)(3)(i), each calendar day in a
month in which the HAP ABA pumps
are not calibrated in accordance with
§63.1303(b)(3)(ii), and each calendar day
after 10 working days after production
where the IFD and density of a foam
grade are not determined (where re-
quired) in accordance with §63.1304(b);

(15) For each affected source com-
plying with §63.1297(a) in accordance
with the monthly compliance option in
§63.1297(a)(2) and (c), each calendar day
of each month for which the actual
HAP ABA emissions exceeded the al-
lowable HAP ABA emissions level for
that month, each calendar day in which foam is being poured where the amount of polyol added at the mixhead is not monitored (as required) in accordance with §63.1303(b)(1)(i), each calendar day in which foam is being poured where the amount of HAP ABA added at the mixhead is not monitored (as required) in accordance with §63.1303(b)(1)(ii), each 6-month period in which the polyol pumps are not calibrated in accordance with §63.1303(b)(3)(i), each month in which the HAP ABA pumps are not calibrated in accordance with §63.1303(b)(3)(ii), and each calendar day after 10 working days after production where the IFD and density of a foam grade are not determined (where required) in accordance with §63.1304(b):

16. For each affected source complying with §63.1297(a) by using a recovery device as allowed under §63.1297(e), the items listed in (c)(16)(i) or (ii) of this section, as applicable.

(i) If complying with rolling annual compliance option in §63.1299(a)(1) and (b), each item listed in (c)(14) of this section, failure to develop a recovered HAP ABA monitoring and record-keeping program in accordance with §63.1303(c), and each instance when an element of the program is not followed.

(ii) If complying with the monthly compliance option in §63.1299(a)(2) and (c), each item listed in (c)(15) of this section, failure to develop a recovered HAP ABA monitoring and record-keeping program in accordance with §63.1303(c), and each instance when an element of the program is not followed.

17. For each affected source complying with §63.1298, each calendar day that a HAP or any HAP-based material is used as an equipment cleaner.

(d) Slabstock affected sources complying with the source-wide emission limitation. For slabstock affected sources complying with the source-wide emission limitation as provided in §63.1299(b), failure to meet the requirements contained in §63.1299 shall be considered a violation of this subpart. Violation of each item listed in the paragraphs (d)(1) through (d)(3) of this section, as applicable, shall be considered a separate violation.

1. For each affected source complying with §63.1299 in accordance with the rolling annual compliance option in §63.1299(a), each calendar day in the 12-month period for which the actual HAP ABA emissions exceeded the allowable HAP ABA emissions level, each calendar day in which foam is being poured where the amount of polyol added at the mixhead is not monitored (as required) in accordance with §63.1303(b)(1)(i), each calendar day in a week in which the amount of HAP ABA in a storage vessel is not determined in accordance with §63.1303(d), each delivery of HAP ABA in which the amount of HAP ABA added to the storage vessel is not determined in accordance with §63.1303(e), each calendar day in a 6-month period in which the polyol pumps are not calibrated in accordance with §63.1303(b)(3)(ii), and each calendar day after 10 working days after production where the IFD and density of a foam grade are not determined (where required) in accordance with §63.1304(b):

2. For each affected source complying with §63.1299 in accordance with the monthly compliance option in §63.1299(b), each calendar day of each month for which the actual HAP ABA emissions exceeded the allowable HAP ABA emissions level for that month, each calendar day in which foam is being poured where the amount of polyol added at the mixhead is not monitored (as required) in accordance with §63.1303(b)(1)(i), each calendar day in a week in which the amount of HAP ABA in a storage vessel is not determined in accordance with §63.1303(d), each delivery of HAP ABA in which the amount of HAP ABA added to the storage vessel is not determined in accordance with §63.1303(e), each calendar day in a 6-month period in which the polyol pumps are not calibrated in accordance with §63.1303(b)(3)(ii), and each calendar day after 10 working days after production where the IFD and density of a foam grade are not determined (where required) in accordance with §63.1304(b).

3. For each affected source complying with §63.1299 by using a recovery device as allowed under §63.1299(e), the items listed in (d)(3)(i) or (ii) of this section, as applicable.

(i) If complying with rolling annual compliance option in §63.1299(a), each...
item listed in (d)(1) of this section, failure to develop a recovered HAP ABA monitoring and recordkeeping program in accordance with § 63.1303(c), and each instance when an element of the program is not followed.

(ii) If complying with the monthly compliance option in § 63.1299(b), each item listed in (d)(2) of this section, failure to develop a recovered HAP ABA monitoring and recordkeeping program in accordance with § 63.1303(c), and each instance when an element of the program is not followed.

(e) Molded and rebond foam affected sources. For molded and rebond foam affected sources, failure to meet the requirements contained in § 63.1300 and § 63.1301, respectively, shall be considered a violation of this subpart. Violation of each item listed in the following paragraphs shall be considered a separate violation.

(1) For each molded foam affected source subject to the provisions in § 63.1300(a), each calendar day that a HAP-based material is used as an equipment cleaner (except for diisocyanates used to flush the mixhead and associated piping during periods of startup or maintenance, provided that the diisocyanate compounds are contained in a closed-loop system and are re-used in production);

(2) For each molded foam affected source subject to the provisions of § 63.1300(b), each calendar day that a HAP-based material is used as a mold release agent;

(3) For each rebond foam affected source subject to the provisions of § 63.1301(a), each calendar day that a HAP-based material is used as an equipment cleaner; and

(4) For each rebond foam affected source complying with § 63.1301(b), each calendar day that a HAP-based mold release agent is used.

§ 63.1309 Delegation of authority.

(a) In delegating implementation and enforcement authority to a State under § 112(d) of the Clean Air Act, the authorities contained in paragraph (b) of this section shall be retained by the Administrator and not transferred to a State.

(b) The authority conferred in § 63.1303(b)(5) and § 63.1305(d) shall not be delegated to any State.

APPENDIX TO SUBPART III—TABLES

For the convenience of the readers of subpart III, the tables below summarize the requirements in §§ 63.1290 to 63.1307. These tables are intended to assist the reader in determining the requirements applicable to affected sources and do not alter an affected source's obligation to comply with the requirements in §§ 63.1290 to 63.1307.

TABLE 1 TO SUBPART III—HAP ABA FORMULATION LIMITATIONS MATRIX FOR NEW SOURCES (see § 63.1297(d)(2)]
TABLE 2 TO SUBPART III—APPLICABILITY OF GENERAL PROVISIONS (40 CFR PART 63, SUBPART A) TO SUBPART III.

<table>
<thead>
<tr>
<th>Subpart A reference</th>
<th>Applies to subpart III</th>
<th>Comment</th>
</tr>
</thead>
<tbody>
<tr>
<td>§ 63.1</td>
<td>YES</td>
<td>Excerpt that §63.1(c)(2) is not applicable to the extent area sources are not subject to subpart III.</td>
</tr>
<tr>
<td>§ 63.2</td>
<td>YES</td>
<td>Definitions are modified and supplemented by §63.1292.</td>
</tr>
<tr>
<td>§ 63.3</td>
<td>YES</td>
<td>Owners and operators of subpart III affected sources are not required to develop and implement a startup, shutdown, and malfunction plan.</td>
</tr>
<tr>
<td>§ 63.5</td>
<td>YES</td>
<td>Subpart III does not require opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.6 (a)–(d)</td>
<td>NO</td>
<td>Performance tests not required by subpart III.</td>
</tr>
<tr>
<td>§ 63.6(e)(3)</td>
<td>NO</td>
<td>Continuous monitoring, as defined in subpart A, is not required by subpart III.</td>
</tr>
<tr>
<td>§ 63.6 (f)–(g)</td>
<td>YES</td>
<td>Subpart III specifies Notification of Compliance Status requirements.</td>
</tr>
<tr>
<td>§ 63.6(h)</td>
<td>NO</td>
<td>Except that the records specified in §63.10(b)(2)(vi) through (xiii) are not required.</td>
</tr>
<tr>
<td>§ 63.7</td>
<td>NO</td>
<td></td>
</tr>
<tr>
<td>§ 63.8</td>
<td>NO</td>
<td></td>
</tr>
<tr>
<td>§ 63.9 (a)–(d)</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>§ 63.9(g)</td>
<td>NO</td>
<td></td>
</tr>
<tr>
<td>§ 63.9(h)</td>
<td>NO</td>
<td></td>
</tr>
<tr>
<td>§ 63.10 (a)–(b)</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>§ 63.10(c)</td>
<td>NO</td>
<td></td>
</tr>
</tbody>
</table>
### TABLE 2 TO SUBPART III—APPLICABILITY OF GENERAL PROVISIONS (40 CFR PART 63, SUBPART A) TO SUBPART III—Continued

<table>
<thead>
<tr>
<th>Subpart A reference</th>
<th>Applies to subpart III</th>
<th>Comment</th>
</tr>
</thead>
<tbody>
<tr>
<td>§ 63.10(d)(1)</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>§ 63.10 (d) (2)–(3)</td>
<td>NO</td>
<td></td>
</tr>
<tr>
<td>§ 63.10 (d) (4)–(5)</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>§ 63.10(e)</td>
<td>NO</td>
<td></td>
</tr>
<tr>
<td>§ 63.10(f)</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>§ 63.11</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>§ 63.12</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>§ 63.13</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>§ 63.14</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>§ 63.15</td>
<td>YES</td>
<td></td>
</tr>
<tr>
<td>Emission point</td>
<td>Emission point compliance option</td>
<td>Emission, work practice, and equipment standards</td>
</tr>
<tr>
<td>--------------------------------</td>
<td>----------------------------------</td>
<td>--------------------------------------------------</td>
</tr>
<tr>
<td>Diisocyanate storage vessels § 63.1294(a)</td>
<td>Vapor balance</td>
<td>§ 63.1294(a)(1) and (1)(ii)</td>
</tr>
<tr>
<td></td>
<td>Carbon adsorber</td>
<td>§ 63.1294(a)(2)</td>
</tr>
<tr>
<td></td>
<td>Carbon adsorber—alternative monitoring</td>
<td>§ 63.1294(a)(2)</td>
</tr>
<tr>
<td></td>
<td>Sealless pump</td>
<td>§ 63.1294(b)(1)</td>
</tr>
<tr>
<td></td>
<td>Submerged pump</td>
<td>§ 63.1294(b)(2)(i) and (ii)</td>
</tr>
<tr>
<td></td>
<td>Other components in diisocyanate service § 63.1294(c)</td>
<td>N/A</td>
</tr>
<tr>
<td></td>
<td>HAP ABA storage vessels § 63.1295</td>
<td>Vapor balance</td>
</tr>
<tr>
<td></td>
<td>Carbon adsorber</td>
<td>§ 63.1295(c)</td>
</tr>
<tr>
<td></td>
<td>Carbon adsorber—alternative monitoring</td>
<td>§ 63.1295(c)</td>
</tr>
<tr>
<td></td>
<td>Sealless pump</td>
<td>§ 63.1296(a)(1)</td>
</tr>
<tr>
<td></td>
<td>Quarterly monitoring</td>
<td>§ 63.1296(b)(2)(i) and (ii)</td>
</tr>
<tr>
<td></td>
<td>Unsafe-to-monitor</td>
<td>§ 63.1296(b)(3)(i), (ii), and (iv)</td>
</tr>
<tr>
<td></td>
<td>Difficult-to-monitor</td>
<td>§ 63.1296(b)(4)(i), (ii), (iii), and (iv)</td>
</tr>
<tr>
<td></td>
<td>Annual monitoring</td>
<td>§ 63.1296(c)(1) and (c)(2)</td>
</tr>
<tr>
<td></td>
<td>Unsafe-to-repair</td>
<td>§ 63.1296(d)(2), (3), and (i)</td>
</tr>
<tr>
<td></td>
<td>Pressure-relief devices § 63.1296(d)</td>
<td>N/A</td>
</tr>
<tr>
<td></td>
<td>Open-ended valves or lines § 63.1296(e)</td>
<td>N/A</td>
</tr>
<tr>
<td>Production line § 63.1297</td>
<td>Rolling annual compliance</td>
<td>§ 63.1297(a)(1) and (b)</td>
</tr>
<tr>
<td></td>
<td>Monthly compliance</td>
<td>§ 63.1297(a)(2) and (c)</td>
</tr>
</tbody>
</table>
### Compliance Using a Recovery device.

**Equipment Cleaning**

$\S$ 63.1299(a), (d), and (e) for rolling annual compliance or $\S$ 63.1299(b), (d), and (e) for monthly compliance.

<table>
<thead>
<tr>
<th>Emission point</th>
<th>Emission point compliance option</th>
<th>Emission, work practice, and equipment standards</th>
<th>Monitoring</th>
<th>Recordkeeping</th>
<th>Reporting</th>
</tr>
</thead>
<tbody>
<tr>
<td>Disocyanate storage vessels $\S$ 63.1294(a).</td>
<td>Vapor balance</td>
<td>$\S$ 63.1294(a)(1) and (1)(ii)</td>
<td>$\S$ 63.1294(a)(1)(ii)</td>
<td>$\S$ 63.1307(a)(1) and (4)</td>
<td>$\S$ 63.1307(a)(1) and (5).</td>
</tr>
<tr>
<td>Carbon adsorber</td>
<td>$\S$ 63.1294(a)(2)</td>
<td>$\S$ 63.1294(a)(1), (3), and (4)</td>
<td>$\S$ 63.1303(b) except (b)(1)(ii), (6), and (e).</td>
<td>$\S$ 63.1307(c)(2) and (d)</td>
<td>$\S$ 63.1306(e)(1) or (2).</td>
</tr>
<tr>
<td>Carbon adsorber—alternative monitoring.</td>
<td>$\S$ 63.1294(a)(2)</td>
<td>$\S$ 63.1294(a)(1), (3), and (4)</td>
<td>$\S$ 63.1303(b) except (b)(1)(ii), (6), and (e).</td>
<td>$\S$ 63.1307(c)(2) and (d)</td>
<td>$\S$ 63.1306(e)(1) or (2).</td>
</tr>
<tr>
<td>Sealless pump</td>
<td>$\S$ 63.1294(b)(1)</td>
<td>$\S$ 63.1294(b)(2)(i) and (ii)</td>
<td>$\S$ 63.1307(b)(1)(i) and (2)</td>
<td>$\S$ 63.1306(e)(4).</td>
<td></td>
</tr>
<tr>
<td>Submerged pump</td>
<td>$\S$ 63.1294(b)(2)(i) and (iii)</td>
<td>$\S$ 63.1294(b)(2)(i) and (ii)</td>
<td>$\S$ 63.1307(b)(1)(i) and (2)</td>
<td>$\S$ 63.1306(e)(4).</td>
<td></td>
</tr>
<tr>
<td>Rolling annual compliance</td>
<td>$\S$ 63.1299(a), (c)(1) through (4), and (d).</td>
<td>$\S$ 63.1303(b) except (b)(1)(ii), (6), and (e).</td>
<td>$\S$ 63.1307(c)(2)</td>
<td>$\S$ 63.1306(e)(1).</td>
<td></td>
</tr>
<tr>
<td>Monthly compliance</td>
<td>$\S$ 63.1299(b), (c)(1) through (4), and (d).</td>
<td>$\S$ 63.1303(b) except (b)(1)(ii), (6), and (e).</td>
<td>$\S$ 63.1307(c)(2)</td>
<td>$\S$ 63.1306(e)(2).</td>
<td></td>
</tr>
<tr>
<td>Compliance Using a Recovery device.</td>
<td>$\S$ 63.1299(b), (c)(1) through (4), and (d).</td>
<td>$\S$ 63.1303(b) except (b)(1)(ii), (6), and (e).</td>
<td>$\S$ 63.1307(c)(2) and (d)</td>
<td>$\S$ 63.1306(e)(1) or (2).</td>
<td></td>
</tr>
</tbody>
</table>

### Compliance Requirements for Molded and Rebond Foam Production Affected Sources

**TABLE 5 TO SUBPART III.—COMPLIANCE REQUIREMENTS FOR MOLDED AND REBOND FOAM PRODUCTION AFFECTED SOURCES**

<table>
<thead>
<tr>
<th>Emission point</th>
<th>Emission point compliance option</th>
<th>Emission, work practice, and equipment standards</th>
<th>Monitoring</th>
<th>Recordkeeping</th>
<th>Reporting</th>
</tr>
</thead>
<tbody>
<tr>
<td>Molded Foam Equipment cleaning</td>
<td>N/A</td>
<td>$\S$ 63.1300(a)</td>
<td></td>
<td>$\S$ 63.1307(g)</td>
<td>$\S$ 63.1307(h)</td>
</tr>
<tr>
<td>Mold release agent</td>
<td>N/A</td>
<td>$\S$ 63.1300(b)</td>
<td></td>
<td>$\S$ 63.1307(h)</td>
<td>$\S$ 63.1307(h)</td>
</tr>
<tr>
<td>Emission point</td>
<td>Emission point compliance option</td>
<td>Emission, work practice, and equipment standards</td>
<td>Monitoring</td>
<td>Recordkeeping</td>
<td>Reporting</td>
</tr>
<tr>
<td>------------------------</td>
<td>----------------------------------</td>
<td>-----------------------------------------------</td>
<td>------------</td>
<td>---------------</td>
<td>-----------</td>
</tr>
<tr>
<td>Rebond Foam</td>
<td>N/A</td>
<td>§ 63.1301(a)</td>
<td>§ 63.1307 (g)</td>
<td>§ 63.1307 (h)</td>
<td></td>
</tr>
<tr>
<td>Equipment cleaning</td>
<td>N/A</td>
<td>§ 63.1301(b)</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Mold release agent</td>
<td>N/A</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

TABLE 5 TO SUBPART III.—COMPLIANCE REQUIREMENTS FOR MOLDED AND REBOND FOAM PRODUCTION AFFECTED SOURCES—Continued
Subpart JJJ—National Emission Standards for Hazardous Air Pollutant Emissions: Group IV Polymers and Resins

SOURCE: 61 FR 48229, Sept. 12, 1996, unless otherwise noted.

§ 63.1310 Applicability and designation of affected sources.

(a) Definition of affected source. The provisions of this subpart apply to each affected source. An affected source is either an existing affected source or a new affected source. Existing affected source is defined in paragraph (a)(6) of this section, and new affected source is defined in paragraph (a)(7) of this section. The affected source also includes the emission points and equipment specified in paragraphs (a)(1) through (a)(5) of this section that are associated with each group of TPPU.

(1) Each wastewater stream.

(2) Each wastewater operation.

(3) Each heat exchange system.

(4) Each process contact cooling tower used in the manufacture of PET that is associated with a new affected source.

(5) Each process contact cooling tower used in the manufacture of PET using a continuous terephthalic acid high viscosity multiple end finisher process that is associated with an existing affected source.

(6) Except as specified in paragraphs (b) through (d) of this section, an existing affected source is defined as each group of one or more thermoplastic product process units (TPPUs) that is not part of a new affected source as defined in paragraph (a)(7) of this section, that is manufacturing the same primary product, where each TPPU uses as a reactant, or uses as a process solvent, or produces as a by-product or co-product any organic HAP, and that is located at a plant site that is a major source.

(7) Except as specified in paragraphs (b) through (d) of this section, a new affected source is defined as a source meeting the criteria of paragraph (a)(7)(i), (a)(7)(ii), or (a)(7)(iii) of this section:

(i) At a plant site previously without HAP emissions points, each group of one or more TPPUs manufacturing the same primary product that is part of a major source on which construction commenced after March 29, 1995;

(ii) A TPPU meeting the criteria in paragraph (i)(1)(i) of this section; or

(iii) A reconstructed affected source meeting the criteria in paragraph (i)(2)(i) of this section.

(b) TPPUs exempted from the affected source. For a TPPU to be excluded from the designation of affected source due to the fact that it does not use as a reactant, or use as a process solvent, or produce as a by-product or co-product any organic HAP, the owner or operator shall comply with the requirements of paragraph (b)(1) of this section and shall comply with the requirements of paragraph (b)(2) of this section if requested to do so by the Administrator.

(1) Retain information, data, and analysis used to document the basis for the determination that the TPPU does not use as a reactant or use as a process solvent, or manufacture as a by-product or a co-product any organic HAP. Types of information that could document this determination include, but are not limited to, records of chemicals purchased for the process, analyses of process stream composition, or engineering calculations.

(2) When requested by the Administrator, demonstrate that the TPPU does not use as a reactant, or use as a process solvent, or manufacture as a by-product or co-product any organic HAP.

(c) Emission points exempted from the affected source. The affected source does not include the emission points listed in paragraphs (c)(1) through (c)(6) of this section:

(1) Stormwater from segregated sewers;

(2) Water from fire-fighting and deluge systems in segregated sewers;

(3) Spills;

(4) Water from safety showers;

(5) Vessels and equipment storing and/or handling material that contain no organic HAP and/or organic HAP as impurities only; and

(6) Equipment that is intended to operate in organic HAP service for less than 300 hours during the calendar year.
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(d) Processes exempted from the affected source. The processes specified in paragraphs (d)(1) through (d)(5) of this section are exempted from the affected source:

1. Research and development facilities;
2. Polymerization processes occurring in a mold;
3. Processes which manufacture binder systems containing a thermoplastic product for paints, coatings, or adhesives;
4. Finishing processes including equipment such as compounding units, spinning units, drawing units, extruding units, and other finishing steps; and
5. Solid state polymerization processes.

(e) Applicability determination of non-thermoplastic equipment included in a TPPU producing a thermoplastic product. If a polymer that is not subject to this subpart is produced within the equipment (i.e., collocated) making up a TPPU and at least 50 percent of said polymer is used in the production of a thermoplastic product manufactured by said TPPU, the unit operations involved in the production of said polymer are considered part of the TPPU and are subject to this rule except as specified in this paragraph (e). If said unit operations are subject to another MACT standard regulating the same emission points, said unit operations are not subject to this subpart.

(f) Primary product determination and applicability. The primary product of a process unit shall be determined according to the procedures specified in paragraphs (f)(1) through (f)(2) of this section. Paragraphs (f)(3) through (f)(4) of this section describe whether or not a process unit is subject to this subpart. Paragraphs (f)(5) through (f)(7) of this section discuss compliance for those TPPUs operated as flexible operation units, as specified in paragraph (f)(2) of this section.

1. If a process unit only manufactures one product, then that product shall represent the primary product of the process unit.
2. If a process unit is designed and operated as a flexible operation unit, the primary product shall be determined as specified in paragraphs (f)(2)(i) or (f)(2)(ii) of this section based on the anticipated operations for the 5 years following September 12, 1996 for existing affected sources and for the first 5 years after initial start-up for new affected sources.
   i. If the flexible operation unit will manufacture one product for the greatest operating time over the five year period, then that product shall represent the primary product of the flexible operation unit.
   ii. If the flexible operation unit will manufacture multiple products equally based on operating time, then the product with the greatest production on a mass basis over the five year period shall represent the primary product of the flexible operation unit.
3. If the primary product of a process unit is a thermoplastic product, said process unit is considered a TPPU. If said TPPU meets all the criteria of paragraph (a) of this section, it is either an affected source or is part of an affected source comprised of other TPPU subject to this rule at the same plant site with the same primary product. The status of a process unit as a TPPU and as an affected source or part of an affected source shall not change regardless of what products are produced in the future by said TPPU, with the exception noted in paragraph (f)(3)(i) of this section.
   i. If a process unit terminates the production of all thermoplastic products and does not anticipate the production of any thermoplastic product in the future, the process unit is no longer a TPPU and is not subject to this rule after notification is made as specified in paragraph (f)(3)(ii) of this section.
   ii. The owner or operator of a process unit that wishes to remove the TPPU designation from the process unit, as specified in paragraph (f)(3)(i) of this section, shall notify the Administrator. This notification shall be accompanied by rationale for why it is anticipated that no thermoplastic products will be produced in the process unit in the future.
   iii. If a process unit meeting the criteria of paragraph (f)(3)(i) of this section begins the production of a thermoplastic product in the future, the owner or operator shall use the procedures in
paragraph (f)(4)(i) of this section to determine if the process unit is re-designated as a TPPU.

(4) If the primary product of a process unit is not a thermoplastic product, then said process unit is not an affected source nor is it part of any affected source subject to this rule. Said process unit is not subject to this rule at any time, regardless of what product is being produced. The status of a process unit as not being a TPPU, and therefore not an affected source nor part of an affected source subject to this subpart, shall not change regardless of what products are produced in the future by said TPPU, with the exception noted in paragraph (f)(4)(i) of this section.

(i) If, at any time beginning September 12, 2001, the owner or operator determines that a thermoplastic product is the primary product for the process unit based on actual production data for any preceding consecutive five-year period, then the process unit shall be designated as a TPPU. If said TPPU meets all the criteria of paragraph (a) of this section and is not subject to another subpart of 40 CFR part 63, it is either an affected source or part of an affected source and shall be subject to this rule.

(ii) If a process unit meets the criteria of paragraph (f)(4)(i) of this section, the owner or operator shall notify the Administrator within 6 months of making this determination. The TPPU, as the entire affected source or part of an affected source, shall be in compliance with the provisions of this rule within 3 years from the date of such notification.

(iii) If a process unit is re-designated as a TPPU but does not meet all the criteria of paragraph (a) of this section, the owner or operator shall notify the Administrator within 6 months of making this determination. Said notification shall include documentation justifying the TPPU’s status as not being an affected source or not being part of an affected source.

(5) Once the primary product of a process unit has been determined to be a thermoplastic product and it has been determined that all the criteria of paragraph (a) of this section are met for said TPPU, the owner or operator of the affected source shall comply with the standards for the primary product. Owners or operators of flexible operation units shall comply with the standards for the primary product as specified in either paragraph (f)(5)(i) or (f)(5)(ii) of this section, except as specified in paragraph (f)(5)(iii) of this section.

(i) Each owner or operator shall determine the group status of each emission point that is part of said flexible operation unit based on emission point characteristics when the primary product is being manufactured. Based on this finding, the owner or operator shall comply with the applicable standards for the primary product for each emission point, as appropriate, at all times, regardless of what product is being produced.

(ii) Alternatively, each owner or operator shall determine the group status of each emission point that is part of said flexible operation unit based on the emission point characteristics when each product produced by the flexible operation unit is manufactured, regardless of whether said product is a thermoplastic product or not. Based on these findings, the owner or operator shall comply with the applicable standards for the primary product for each emission point, as appropriate, regardless of what product is being produced.

NOTE: Under this scenario it is possible that the group status, and therefore the requirement to achieve emission reductions, for an emission point may change depending on the product being produced.

(iii) Whenever a flexible operation unit manufactures a product that meets the criteria of paragraph (b) of this section (i.e., does not use or produce any organic HAP), all activities associated with the manufacture of said product shall be exempt from the requirements of this rule, to include the operation and monitoring of control or recovery devices.

(6) The determination of the primary product for a process unit, to include the determination of applicability of this subpart to process units that are designed and operated as flexible operation units, shall be reported in the Notification of Compliance Status required by §63.1339(e)(5) when the primary product is determined to be a
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thermoplastic product. The Notification of Compliance Status shall include the information specified in either paragraph (f)(6)(i) or (f)(6)(ii) of this section. If the primary product is determined to be something other than a thermoplastic product, the owner or operator shall retain information, data, and analysis used to document the basis for the determination that the primary product is not a thermoplastic product.

(i) If the TPPU manufactures only one thermoplastic product, identification of said thermoplastic product.

(ii) If the TPPU is designed and operated as a flexible operation unit, the information specified in paragraphs (f)(6)(ii)(A) through (f)(6)(ii)(C) of this section, as appropriate.

(A) Identification of the primary product.

(B) Information concerning operating time and/or production mass for each product that was used to make the determination of the primary product under paragraph (f)(2)(i) or (f)(2)(ii) of this section.

(C) Identification of which compliance option, either paragraph (f)(5)(i) or (f)(5)(ii) of this section, has been selected by the owner or operator.

To demonstrate compliance with the rule during those periods when a flexible operation unit that is subject to this subpart is producing a product other than a thermoplastic product or is producing a thermoplastic product that is not the primary product, the owner or operator shall comply with either paragraphs (f)(7)(i) through (f)(7)(ii) or paragraph (f)(7)(iii) of this section.

(i) Establish parameter monitoring levels, as specified in §63.1334, for those emission points designated as Group 1, as appropriate.

(ii) Submit the parameter monitoring levels developed under paragraph (f)(7)(i) of this section and the basis for them in the Notification of Compliance Status report as specified in §63.1335(e)(5).

(iii) Demonstrate that the parameter monitoring levels established for the primary product are also appropriate for those periods when products other than the primary product are being produced. Material demonstrating this finding shall be submitted in the Notification of Compliance Status report as specified in §63.1335(e)(5).

(g) Storage vessel ownership determination. The owner or operator shall follow the procedures specified in paragraphs (g)(1) through (g)(8) of this section to determine to which process unit a storage vessel shall belong.

(1) If a storage vessel is already subject to another subpart of 40 CFR part 63 on September 12, 1996, said storage vessel shall belong to the process unit subject to the other subpart.

(2) If a storage vessel is dedicated to a single process unit, the storage vessel shall belong to that process unit.

(3) If a storage vessel is shared among process units, then the storage vessel shall belong to that process unit located on the same plant site as the storage vessel that has the greatest input into or output from the storage vessel (i.e., said process unit has the predominant use of the storage vessel).

(4) If predominant use cannot be determined for a storage vessel that is shared among process units and if one of those process units is a TPPU subject to this subpart, the storage vessel shall belong to said TPPU.

(5) If predominant use cannot be determined for a storage vessel that is shared among process units and if more than one of the process units are TPPUs that have different primary products and that are subject to this subpart, then the owner or operator shall assign the storage vessel to any one of the said TPPUs.

(6) If the predominant use of a storage vessel varies from year to year, then predominant use shall be determined based on the utilization that occurred during the year preceding September 12, 1996 or based on the expected utilization for the 5 years following September 12, 1996 for existing affected sources, whichever is more representative of the expected operations for said storage vessel, and based on the first 5 years after initial start-up for new affected sources. The determination of predominant use shall be reported in the Notification of Compliance Status required by §63.1335(e)(5). If the predominant use
(7) If the storage vessel begins receiving material from (or sending material to) another process unit; or ceasing to receive material from (or send material to) a process unit; or if the applicability of this subpart to a storage vessel has been determined according to the provisions of paragraphs (g)(1) through (g)(6) of this section and there is a significant change in the use of the storage vessel that could reasonably change the predominant use, the owner or operator shall reevaluate the applicability of this subpart to the storage vessel.

(8) Where a storage vessel is located at a major source that includes one or more process units which place material into, or receive materials from the storage vessel, but the storage vessel is located in a tank farm, the applicability of this subpart shall be determined according to the provisions in paragraphs (g)(8)(i) through (g)(8)(iv) of this section.

(i) The storage vessel may only be assigned to a process unit that utilizes the storage vessel and does not have an intervening storage vessel for that product (or raw materials, as appropriate). With respect to any process unit, an intervening storage vessel means a storage vessel connected by hard-piping to the process unit and to the storage vessel in the tank farm so that product or raw material entering or leaving the process unit flows into (or from) the intervening storage vessel and does not flow directly into (or from) the storage vessel in the tank farm.

(ii) If there is no process unit at the major source that meets the criteria of paragraph (g)(8)(i) of this section with respect to a storage vessel, this subpart does not apply to the storage vessel.

(iii) If there is only one process unit at the major source that meets the criteria of paragraph (g)(8)(i) of this section with respect to a storage vessel, the storage vessel shall be assigned to that process unit.

(iv) If there are two or more process units at the major source that meet the criteria of paragraph (g)(8)(i) of this section with respect to a storage vessel, the storage vessel shall be assigned to one of those process units according to the provisions of paragraph (g)(7) of this section. The predominant use shall be determined among only those thermoplastic product process units that meet the criteria of paragraph (g)(8)(i) of this section.

(h) Recovery operation equipment ownership determination. The owner or operator shall follow the procedures specified in paragraphs (h)(1) through (h)(7) of this section to determine to which process unit recovery operation equipment shall belong.

(1) If recovery operation equipment is already subject to another subpart of 40 CFR part 63 on September 12, 1996, said recovery operation equipment shall belong to the process unit subject to the other subpart.

(2) If recovery operation equipment is used exclusively by a single process unit, the recovery operation shall belong to that process unit.

(3) If recovery operation equipment is shared among process units, then the recovery operation equipment shall belong to that process unit located on the same plant site as the recovery operation equipment that has the greatest input into or output from the recovery operation equipment (i.e., said process unit has the predominant use of the recovery operation equipment).

(4) If predominant use cannot be determined for recovery operation equipment that is shared among process units and if one of those process units is a TPPU subject to this subpart, the recovery operation equipment shall belong to said TPPU.

(5) If predominant use cannot be determined for recovery operation equipment that is shared among process units and if more than one of the process units are TPPUs that have different primary products and that are subject to this subpart, then the owner or operator shall assign the recovery operation equipment to any one of said TPPUs.

(6) If the predominant use of recovery operation equipment varies from year to year, then predominant use shall be determined based on the utilization that occurred during the year preceding September 12, 1996 or based on the expected utilization for the 5 years preceding September 12, 1996.
following September 12, 1996 for existing affected sources, whichever is the more representative of the expected operations for said recovery operations equipment, and based on the first 5 years after initial start-up for new affected sources. This determination shall be reported in the Notification of Compliance Status required by §63.1335(e)(5). If the predominant use changes, the redetermination of predominant use shall be reported in the next Periodic Report.

(7) If there is an unexpected change in the utilization of recovery operation equipment that could reasonably change the predominant use, the owner or operator shall redetermine to which process unit the recovery operation belongs by reperforming the procedures specified in paragraphs (h)(2) through (h)(6) of this section.

(i) Changes or additions to plant sites. The provisions of paragraphs (i)(1) through (i)(4) of this section apply to owners or operators that change or add to their plant site or affected source. Paragraph (i)(5) of this section provides examples of what are and are not considered process changes for purposes of paragraph (i) of this section.

(1) Adding a TPPU to a plant site. The provisions of paragraphs (i)(1)(i) through (i)(1)(ii) of this section apply to owners or operators that add TPPUs to a plant site.

(i) If a TPPU is added to a plant site, said addition shall be a new affected source and shall be subject to the requirements for a new affected source in this subpart upon initial start-up or by September 12, 1996, whichever is later, if said addition meets the criteria specified in paragraphs (i)(1)(i)(A) through (i)(1)(i)(B) and either (i)(1)(i)(C) or (i)(1)(i)(D) of this section:

(A) Said addition meets the definition of construction in §63.2;

(B) Such construction commenced after March 29, 1995;

(C) Said addition has the potential to emit 10 tons per year or more of any HAP or 25 tons per year or more of any combination of HAP, and the primary product of said addition is currently produced at the plant site as the primary product of an affected source; or

(D) The primary product of said addition is not currently produced at the

plant site as the primary product of an affected source and the plant site meets, or after the addition is completed will meet, the definition of major source.

(ii) If a TPPU is added to a plant site, said addition shall be subject to the requirements for an existing affected source in this subpart upon initial start-up or by 3 years after September 12, 1996, whichever is later, if said addition does not meet the criteria specified in paragraph (i)(1)(i) of this section and the plant site meets, or after the addition is completed will meet, the definition of major source.

(2) Adding emission points or making process changes to existing affected sources. The provisions of paragraphs (i)(2)(i) through (i)(2)(iii) of this section apply to owners or operators that add emission points or make process changes to an existing affected source.

(i) If any process change is made or emission point is added to an existing affected source, or if a process change creating one or more additional Group 1 emission point(s) is made to an existing affected source, said affected source shall be a new affected source and shall be subject to the requirements for a new affected source in this subpart upon initial start-up or by September 12, 1996, whichever is later, if said process change or addition meets the criteria specified in paragraphs (i)(2)(i)(A) through (i)(2)(i)(B) of this section:

(A) Said process change or addition meets the definition of reconstruction in §63.2; and

(B) Such reconstruction commenced after March 29, 1995.

(ii) If any process change is made or emission point is added to an existing affected source, or if a process change creating one or more additional Group 1 emission point(s) is made to an existing affected source, said affected source shall be a new affected source and shall be subject to the requirements for a new affected source in this subpart upon initial start-up or by September 12, 1996, whichever is later, if said process change or addition does not meet the criteria specified in paragraphs (i)(2)(i)(A) through (i)(2)(i)(B) of this section, the resulting emission point(s) shall be subject to the requirements for an existing affected source in this subpart. Said emission point(s) shall be in compliance upon initial start-up or by
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3 years after September 12, 1996, whichever is later, unless the owner or operator demonstrates to the Administrator that achieving compliance will take longer than making said process change or addition. If this demonstration is made to the Administrator’s satisfaction, the owner or operator shall follow the procedures in paragraphs (i)(2)(iii)(A) through (i)(2)(iii)(C) of this section to establish a compliance date.

(iii) To establish a compliance date for an emission point or points specified in paragraph (i)(2)(ii) of this section, the procedures specified in paragraphs (i)(2)(iii)(A) through (i)(2)(iii)(C) of this section shall be followed.

(A) The owner or operator shall submit to the Administrator for approval a compliance schedule, along with a justification for the schedule.

(B) The compliance schedule shall be submitted within 180 days after the process change or addition is made or the information regarding said change or addition is known to the owner or operator, unless the compliance schedule has been previously submitted to the permitting authority. The compliance schedule may be submitted in the next Periodic Report if the process change or addition is made after the date the Notification of Compliance Status report is due.

(C) The Administrator shall approve the compliance schedule or request changes within 120 calendar days of receipt of the compliance schedule and justification.

(3) Existing source requirements for Group 2 emission points that become Group 1 emission points. If a process change or addition that does not meet the criteria in paragraph (i)(1) or (i)(2) of this section is made to an existing plant site or existing affected source, and the change causes a Group 2 emission point to become a Group 1 emission point, for said emission point, the owner or operator shall comply with the requirements of this subpart for existing Group 1 emission points. Compliance shall be achieved as expeditiously as practicable, but in no event later than 3 years after said emission point becomes a Group 1 emission point.

(4) Existing source requirements for some emission points that become subject to the requirements of subpart H of this part. If a compressor becomes subject to §63.164, the owner or operator shall be in compliance upon initial start-up or by 3 years after September 12, 1996, whichever is later, unless the owner or operator demonstrates to the Administrator that achieving compliance will take longer than making the change. If this demonstration is made to the Administrator’s satisfaction, the owner or operator shall follow the procedures in paragraphs (i)(2)(iii)(A) through (i)(2)(iii)(C) of this section to establish a compliance date.

(5) Determining what are and are not process changes. For purposes of paragraph (i) of this section, examples of process changes include, but are not limited to, changes in production capacity, feedstock type, or catalyst type, or whenever there is a replacement, removal, or the addition of recovery equipment. For purposes of paragraph (i) of this section, process changes do not include: process upsets, unintentional temporary process changes, and changes that are within the equipment configuration and operating conditions documented in the Notification of Compliance Status report required by §63.1339(e)(5).

(j) Applicability of this subpart except during periods of start-up, shutdown, and malfunction. Each provision set forth in this subpart or referred to in this subpart shall apply at all times except during periods of start-up, shutdown, and malfunction if the start-up, shutdown, or malfunction precludes the ability of a particular emission point of an affected source to comply with one or more specific provisions to which it is subject. Start-up, shutdown, and malfunction is defined in §63.1312 for all emission points except equipment leaks subject to subpart H of this part, which shall follow the provisions for periods of start-up, malfunction, and process unit shutdown, as defined in §63.161. Only then shall an emission point not be required to comply with all applicable provisions of this subpart.
§ 63.1311 Compliance schedule and relationship to existing applicable rules.  

(a) Affected sources are required to achieve compliance on or before the dates specified in paragraphs (b) through (d) of this section. Paragraph (e) of this section provides information on requesting compliance extensions. Paragraphs (f) through (l) of this section discuss the relationship of this subpart to subpart A of this part and to other applicable rules. Where an override of another authority of the Act is indicated in this subpart, only compliance with the provisions of this subpart is required. Paragraph (m) of this section specifies the meaning of time periods.  

(b) New affected sources that commence construction or reconstruction after March 29, 1995 shall be in compliance with this subpart upon initial start-up or February 27, 1998, whichever is later, as provided in § 63.6(b), except that new affected sources whose primary product, as determined using the procedures specified in § 63.1310(f), is poly(ethylene terephthalate) (PET) shall be in compliance with § 63.1331 upon initial start-up or February 27, 2001, whichever is later.  

[NOTE: The compliance date for new affected sources with an initial start-up date on or after March 9, 1999 is stayed indefinitely. The EPA will publish a document in the Federal Register establishing a new compliance date for existing affected sources.]  

(d) Except as provided for in paragraphs (d)(1) through (d)(6) of this section, existing affected sources shall be in compliance with § 63.1331 no later than February 27, 1998 unless a request for a compliance extension is granted pursuant to section 112(i)(3)(B) of the Act, as discussed in § 63.182(a)(6).  

(1) Compliance with the compressor provisions of § 63.164 shall occur no later than February 27, 1998 for any compressor meeting one or more of the criteria in paragraphs (d)(1)(i) through (d)(1)(iii) of this section if the work can be accomplished without a process unit shutdown, as defined in § 63.161:  

(i) The seal system will be replaced;  

(ii) A barrier fluid system will be installed;  

(iii) A new barrier fluid will be utilized which requires changes to the existing barrier fluid system; or  

(iv) The compressor will be modified to permit connecting the compressor to a fuel gas system or a closed vent system or modified so that emissions from the compressor can be routed to a process.  

(2) Compliance with the compressor provisions of § 63.164 shall occur no later than March 12, 1998, for any compressor meeting all the criteria in paragraphs (d)(2)(i) through (d)(2)(ii) of this section.  

(i) The compressor meets one or more of the criteria specified in paragraphs (d)(1)(i)(A) through (d)(1)(i)(B) of this section:  

(A) The work can be accomplished without a process unit shutdown as defined in § 63.161; or  

(B) The additional time is actually necessary due to the unavailability of parts beyond the control of the owner or operator.  

(ii) The owner or operator submits the request for a compliance extension to the U.S. Environmental Protection Agency (EPA) Regional Office at the addresses listed in § 63.13 no later than June 16, 1997. The request for a compliance extension shall contain the information specified in § 63.6(i)(6)(i)(A), (B), and (D). Unless the EPA Regional
Office objects to the request for a compliance extension within 30 calendar days after receipt of the request, the request shall be deemed approved.

(3) If compliance with the compressor provisions of §63.164 cannot reasonably be achieved without a process unit shutdown, as defined in §63.161, the owner or operator shall achieve compliance no later than September 14, 1998. The owner or operator who elects to use this provision shall submit a request for a compliance extension in accordance with the requirements of paragraph (d)(2)(ii) of this section.

(4) Compliance with the compressor provisions of §63.164 shall occur no later than September 12, 1999 for any compressor meeting one or more of the criteria in paragraphs (d)(4)(i) through (d)(4)(iii) of this section. The owner or operator who elects to use these provisions shall submit a request for an extension of compliance in accordance with the requirements of paragraph (d)(2)(iv) of this section.

(i) Compliance cannot be achieved without replacing the compressor;
(ii) Compliance cannot be achieved without recasting the distance piece; or
(iii) Design modifications are required to connect to a closed-vent or recovery system.

(5) Compliance with the provisions of §63.170 shall occur no later than September 13, 1999.

(6) Notwithstanding paragraphs (d)(1) through (d)(4) of this section, existing affected sources whose primary product, as determined using the procedures specified in §63.1310(f), is PET shall be in compliance with §63.1331 no later than February 27, 2001.

(e) Pursuant to section 112(ii)(3)(B) of the Act, an owner or operator may request an extension allowing the existing source up to 1 additional year to comply with section 112(d) standards. For purposes of this subpart, a request for an extension shall be submitted to the operating permit authority as part of the operating permit application or to the Administrator as a separate submittal or as part of the Precompliance Report. Requests for extensions shall be submitted no later than the date the Precompliance Report is required to be submitted in §63.1335(e)(3)(i). The dates specified in §63.6(i) for submittal of requests for extensions shall not apply to this subpart.

(1) A request for an extension of compliance shall include the data described in §63.6(i)(6)(i)(A), (B), and (D).

(2) The requirements in §63.6(i)(8) through §63.6(i)(14) shall govern the review and approval of requests for extensions of compliance with this subpart.

(f) Table 1 of this subpart specifies the provisions of subpart A of this part that apply and those that do not apply to owners and operators of affected sources subject to this subpart.

(g)(1) After the compliance dates specified in this section, an affected source subject to this subpart that is also subject to the provisions of subpart I of this part, is required to comply only with the provisions of this subpart. After the compliance dates specified in this section, said affected source shall no longer be subject to subpart I of this part.

(2) Said affected sources that elected to comply with subpart I of this part through a quality improvement program, as specified in §63.175 or §63.176 or both, may elect to continue these programs without interruption as a means of complying with this subpart. In other words, becoming subject to this subpart does not restart or reset the “compliance clock” as it relates to reduced burden earned through a quality improvement program.

(h) After the compliance dates specified in this section, a storage vessel that belongs to an affected source subject to this subpart that is also subject to the provisions of 40 CFR part 60, subpart Kb, is required to comply only with the provisions of this subpart. After the compliance dates specified in this section, said storage vessel shall no longer be subject to 40 CFR part 60, subpart Kb.

(i)(1) Except as provided in paragraph (i)(2) of this section, after the compliance dates specified in this section, affected sources producing PET using a continuous terephthalic acid process, producing PET using a continuous dimethyl terephthalate process, or producing polystyrene resin using a continuous process subject to this subpart that are also subject to the provisions
§63.1311 Compliance schedule and relationship to existing applicable rules.  

(2) Existing affected sources producing PET using a continuous terephthalic acid high viscosity multiple end finisher process shall continue to be subject to 40 CFR 60.562-1(c)(2)(ii)(C). Once said affected source becomes subject to and achieves compliance with §63.1329(c) of this subpart, said affected source is no longer subject to the provisions of 40 CFR part 60, subpart DDD. 

(j) Affected sources subject to this subpart that are also subject to the provisions of subpart Q of this part shall comply with both subparts. 

(k) After the compliance dates specified in this section, an affected source subject to this subpart that is also subject to the provisions of 40 CFR part 60, subpart VV, is required to comply only with the provisions of this subpart. After the compliance dates specified in this section, said source shall no longer be subject to 40 CFR part 60, subpart VV. 

(m) All terms in this subpart that define a period of time for completion of required tasks (e.g., weekly, monthly, quarterly, annual), unless specified otherwise in the section or subsection that imposes the requirement, refer to the standard calendar periods. 

(1) Notwithstanding time periods specified in this subpart for completion of required tasks, such time periods may be changed by mutual agreement between the owner or operator and the Administrator, as specified in subpart A of this part (e.g., a period could begin on the compliance date or another date, rather than on the first day of the standard calendar period). For each time period that is changed by agree-
poly(ethylene terephthalate) (PET) shall be in compliance with §63.1331 upon initial start-up or by September 12, 1999, whichever is later.

(d) * * *

(6) Notwithstanding paragraphs (d)(1) through (d)(4) of this section, existing affected sources whose primary product, as determined using the procedures specified in §63.1310(f), is PET shall be in compliance with §63.1331 no later than September 12, 1999.

2. At 64 FR 35028, June 30, 1999, §63.1311 was amended by revising paragraphs (b) and (c), effective Aug. 30, 1999. For the convenience of the user, paragraph (b) in effect from Aug. 9, 1999 until Aug. 30, 1999 and paragraph (c) is set forth as follows:

§ 63.1311 Compliance schedule and relationship to existing applicable rules.

(b) New affected sources that commence construction or reconstruction after March 29, 1995 shall be in compliance with this subpart upon initial start-up or September 12, 1996, whichever is later, as provided in §63.6(b), except that new affected sources whose primary product, as determined using the procedures specified in §63.1310(f), is PET shall be in compliance with §63.1331 upon initial start-up or February 27, 2001, whichever is later.

(c) Existing affected sources shall be in compliance with this subpart (except for §63.1331 for which compliance is covered by paragraph (d) of this section) no later than September 12, 1999, as provided in §63.6(c), unless an extension has been granted as specified in paragraph (e) of this section, except that the compliance date for the provisions contained in 40 CFR 63.1320 is temporarily extended from September 12, 1999, to February 27, 2001, for existing affected sources whose primary product, as determined using the procedures specified in §63.1310(f), is PET using a continuous terephthalic acid high viscosity multiple end finisher process.

§ 63.1312 Definitions.

(a) The following terms used in this subpart shall have the meaning given them in §63.2, §63.101, §63.111, and §63.161 as specified after each term:

Act §63.2

Administrator §63.2

Automated monitoring and recording system §63.111

Average concentration §63.111

Boiler §63.111

Bottoms receiver §63.161

By compound §63.111

By-product §63.101

Car-seal §63.111

Chemical manufacturing process unit §63.101

Closed-vent system §63.111

Co-product §63.101

Combustion device §63.111

Committed §63.2

Compliance date §63.2

Compliance schedule §63.2

Connector §63.161

Construction §63.2

Continuous monitoring system §63.2

Continuous record §63.2

Continuous recorder §63.2

Distillation unit §63.111

Emission standard §63.2

Emissions averaging §63.2

EPA §63.2

Equipment §63.161

Equipment leak §63.101

Existing source §63.2

External floating roof §63.111

Fill §63.111

Fixed roof §63.111

Flame zone §63.111

Flexible operation unit §63.101

Floating roof §63.111

Flow indicator §63.111

Group 1 wastewater streams §63.111

Group 2 wastewater streams §63.111

Halogens and hydrogen halides §63.111

Hazardous air pollutant §63.2

Impurity §63.101

Inorganic hazardous air pollutant service §63.161

Incinerator §63.111

Instrumentation system §63.161

Internal floating roof §63.111

Lesser quantity §63.2

Major source §63.2

Malfunction §63.2

Mass flow rate §63.111

Maximum true vapor pressure §63.111

New source §63.2

Open-ended valve or line §63.161

Operating permit §63.101

Organic HAP service §63.161

Organic monitoring device §63.111

Owner or operator §63.2

Performance evaluation §63.2

Performance test §63.2
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Permitting authority (§ 63.2)
Plant site (§ 63.101)
Point of generation (§ 63.111)
Potential to emit (§ 63.2)
Primary fuel (§ 63.111)
Process heater (§ 63.111)
Process unit shutdown (§ 63.161)
Process wastewater (§ 63.101)
Process wastewater stream (§ 63.111)
Product separator (§ 63.111)
Reactor (§ 63.111)
Reconstruction (§ 63.2)
Recovery device (§ 63.111)
Reference control technology for process vents (§ 63.111)
Reference control technology for storage vessels (§ 63.111)
Reference control technology for wastewater (§ 63.111)
Relief valve (§ 63.111)
Research and development facility (§ 63.101)
Residual (§ 63.111)
Run (§ 63.2)
Secondary fuel (§ 63.111)
Sensor (§ 63.161)
Shutdown (§ 63.2)
Specific gravity monitoring device (§ 63.111)
Start-up (§ 63.2)
Start-up, shutdown, and malfunction plan (§ 63.101)
State (§ 63.2)
Surge control vessel (§ 63.161)
Temperature monitoring device (§ 63.111)
Test method (§ 63.2)
Total resource effectiveness index value (§ 63.111)
Treatment process (§ 63.111)
Unit operation (§ 63.101)
Visible emission (§ 63.2)
Waste management unit (§ 63.111)
Wastewater (§ 63.101)
Wastewater stream (§ 63.111)

(b) All other terms used in this subpart shall have the meaning given them in this section. If a term is defined in §§ 63.2, 63.101, 63.111, or 63.161 and in this section, it shall have the meaning given in this section for purposes of this subpart.

Acrylonitrile butadiene styrene latex resin (ABS latex) means ABS produced through an emulsion process, however the product is not coagulated or dried as typically occurs in an emulsion process.

Acrylonitrile butadiene styrene resin (ABS) means styrenic terpolymers consisting primarily of acrylonitrile, 1,3-butadiene, and styrene monomer units. ABS is usually composed of a styrene-acrylonitrile copolymer continuous phase with dispersed butadiene derived rubber.

Acrylonitrile styrene acrylate resin (ASA) means a resin formed using acrylic ester-based elastomers to impact-modify styrene acrylonitrile resin matrices.

Aggregate batch vent stream means a gaseous emission stream containing only the exhausts from two or more batch process vents that are ducted together before being routed to a control device that is in continuous operation. Affected source is defined in § 63.1310(a).

Alpha methyl styrene acrylonitrile resin (AM SAN) means copolymers consisting primarily of alpha methyl styrene and acrylonitrile.

Average flow rate, as used in conjunction with wastewater provisions, is determined by the specifications in § 63.144(c); or, as used in conjunction with batch process vent provisions, is determined by the specifications in § 63.1323(e).

Batch cycle means the operational step or steps, from start to finish, that occur as part of a batch unit operation. Batch cycle limitation means an enforceable restriction on the number of batch cycles that can be performed in a year for an individual batch process vent.

Batch emission episode means a discrete emission venting episode associated with a single batch unit operation. Multiple batch emission episodes may occur from a single batch unit operation.

Batch process means a discontinuous process involving the bulk movement of material through sequential manufacturing steps. Mass, temperature, concentration, and other properties of the process vary with time. Addition of raw material and withdrawal of product do not typically occur simultaneously in a batch process. For the purposes of this subpart, a process producing polymers is characterized as continuous or batch based on the operation of the polymerization reactors.
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Batch process vent means a point of emission from a batch unit operation having a gaseous emission stream with annual organic HAP emissions greater than 225 kilograms per year. Batch process vents exclude relief valve discharges and leaks from equipment regulated under §63.1331.

Batch unit operation means a unit operation operated in a batch process mode.

Combustion device burner means a device designed to mix and ignite fuel and air to provide a flame to heat and oxidize waste organic vapors in a combustion device.

Compounding unit means a unit operation which blends, melts, and resolidifies solid polymers for the purpose of incorporating additives, colorants, or stabilizers into the final thermoplastic product. A unit operation whose primary purpose is to remove residual monomers from polymers is not a compounding unit.

Continuous process means a process where the inputs and outputs flow continuously through sequential manufacturing steps throughout the duration of the process. Continuous processes typically approach steady-state conditions. Continuous processes typically involve the simultaneous addition of raw material and withdrawal of product. For the purposes of this subpart, a process producing polymers is characterized as continuous or batch based on the operation of the polymerization reactors.

Continuous process vent means a point of emission from a continuous unit operation within an affected source having a gaseous emission stream containing greater than 0.005 weight percent total organic HAP. Continuous process vents exclude relief valve discharges and leaks from equipment regulated under §63.1331.

Continuous unit operation means a unit operation operated in a continuous process mode.

Control device is defined in §63.111, except that the term “process vents” shall be replaced with the term “continuous process vents subject to §63.1315” for the purpose of this subpart.

Drawing unit means a unit operation which converts polymer into a different shape by melting or mixing the polymer and then pulling it through an orifice to create a continuously extruded product.

Emission point means an individual continuous process vent, batch process vent, storage vessel, wastewater stream, equipment leak, heat exchange system, or process contact cooling tower.

Emulsion process means a process carried out with the reactants in an emulsified form (e.g., polymerization reaction).

Expandable polystyrene resin (EPS) means a polystyrene bead to which a blowing agent has been added using either an in-situ suspension process or a post-impregnation suspension process.

Extruding unit means a unit operation which converts polymer into a different shape by melting or mixing the polymer and then forcing it through an orifice to create a continuously extruded product.

Group 1 batch process vent means a batch process vent releasing annual organic HAP emissions greater than the level specified in §63.1323(d) and with a cutoff flow rate, calculated in accordance with §63.1323(f), greater than or equal to the annual average flow rate.

Group 2 batch process vent means a batch process vent that does not fall within the definition of a Group 1 batch process vent.

Group 1 continuous process vent means a continuous process vent releasing a gaseous emission stream that has a total resource effectiveness index value, calculated according to §63.115, less than or equal to 1.0 unless the continuous process vent is associated with existing thermoplastic product process units that produce methyl methacrylate butadiene styrene resin, then said vent falls within the Group 1 definition if the released emission stream has a total resource effectiveness index value less than or equal to 3.7.

Group 2 continuous process vent means a continuous process vent that does not fall within the definition of a Group 1 continuous process vent.

Group 1 storage vessel means a storage vessel at an existing affected source that meets the applicability criteria specified in Table 2 or Table 3 of this
subpart, or a storage vessel at a new affected source that meets the applicability criteria specified in Table 4 or Table 5 of this subpart.

Group 2 storage vessel means a storage vessel that does not fall within the definition of a Group 1 storage vessel.

Halogenated aggregate batch vent stream means an aggregate batch vent stream determined to have a total mass emission rate of halogen atoms contained in organic compounds of 3,750 kilograms per year or greater determined by the procedures specified in §63.1323(h).

Halogenated batch process vent means a batch process vent determined to have a mass emission rate of halogen atoms contained in organic compounds of 3,750 kilograms per year or greater determined by the procedures specified in §63.1323(h).

Halogenated continuous process vent means a continuous process vent determined to have a mass emission rate of halogen atoms contained in organic compounds of 0.45 kilograms per hour or greater determined by the procedures specified in §63.115(d)(2)(v).

Heat exchange system means any cooling tower system or once-through cooling water system (e.g., river or pond water) designed and operated to not allow contact between the cooling medium and process fluid or gases (i.e., a noncontact system). A heat exchange system can include more than one heat exchanger and can include recirculating or once-through cooling systems.

Maintenance wastewater means wastewater generated by the draining of process fluid from components in the TPPU into an individual drain system prior to or during maintenance activities. Maintenance wastewater can be generated during planned and unplanned shutdowns and during periods not associated with a shutdown. Examples of activities that can generate maintenance wastewater include descaling of heat exchanger tubing bundles, cleaning distillation column traps, draining of low legs and high point bleeds, draining of pumps into an individual drain system, reactor and equipment washdown, and draining of portions of the TPPU for repair.

Mass process means a process carried out through the use of thermal energy (e.g., polymerization reaction). Mass processes do not utilize emulsifying or suspending agents, but can utilize catalysts or other additives.

Material recovery section means the equipment that recovers unreacted or by-product materials from any process section for return to the TPPU, off-site purification or treatment, or sale. Equipment used to store recovered materials are not included. Equipment designed to separate unreacted or by-product material from the polymer product are to be included in this process section, provided that at the time of initial compliance some of the material is recovered for reuse in the process, off-site purification or treatment, or sale. Otherwise, such equipment are to be assigned to one of the other process sections, as appropriate. If equipment are used to recover unreacted or by-product material and return it directly to the same piece of process equipment from which it was emitted, then said recovery equipment are considered part of the process section that contains the process equipment. On the other hand, if equipment are used to recover unreacted or by-product material and return it to a different piece of process equipment in the same process section, said recovery equipment are considered part of a material recovery section. Equipment that treats recovered materials are to be included in this process section, but equipment that also treats raw materials are not to be included in this process section. The latter equipment are to be included in the raw materials preparation section. Equipment used for the on-site recovery of ethylene glycol from PET plants, however, are not included in the material recovery section; they are to be included in the polymerization reaction section. Equipment used for the on-site recovery of ethylene glycol and other materials (e.g., methanol) from PET plants are not included in the material recovery section; these equipment are to be included in the polymerization reaction section.

Methyl methacrylate acrylonitrile butadiene styrene resin (MABS) means styrenic polymers containing methyl...
methacrylate, acrylonitrile, butadiene, and styrene. MABS is prepared by dissolving or dispersing polybutadiene rubber in a mixture of methyl methacrylate-acrylonitrile-styrene and butadiene monomer. The graft polymerization is carried out by a bulk or a suspension process.

Methyl methacrylate butadiene styrene resin (MBS) means styrenic polymers containing methyl methacrylate, butadiene, and styrene. Production of MBS is achieved using an emulsion process in which methyl methacrylate and styrene are grafted onto a styrene-butadiene rubber.

Nitrile resin means a resin produced through the polymerization of acrylonitrile, methyl acrylate, and butadiene latex using an emulsion process.

Organic hazardous air pollutant(s) (organic HAP) means one or more of the chemicals listed in Table 6 of this subpart or any other chemical which is:

1. Knowingly introduced into the manufacturing process other than as an impurity, or has been or will be reported under any Federal or State program, such as Title V or the Emergency Planning and Community Right-To-Know Act section 311, 312, or 313; and
2. Listed in Table 2 of subpart F of this part.

PET using a dimethyl terephthalate process means the manufacturing of PET based on the esterification reaction of dimethyl terephthalate with ethylene glycol to form the intermediate monomer bis-(2-hydroxyethyl)terephthalate that is subsequently polymerized to form PET.

PET using a terephthalic acid process means the manufacturing of PET based on the esterification reaction of terephthalic acid with ethylene glycol to form the intermediate monomer bis-(2-hydroxyethyl)terephthalate that is subsequently polymerized to form PET.

Poly(ethylene terephthalate) resin (PET) means a polymer or copolymer comprised of at least 50 percent bis-(2-hydroxyethyl)terephthalate by weight.

Polymerization reaction section means the equipment designed to cause monomer(s) to react to form polymers, including equipment designed primarily to cause the formation of short polymer chains (e.g., oligomers or low polymers), but not including equipment designed to prepare raw materials for polymerization (e.g., esterification vessels). For the purposes of these standards, the polymerization reaction section begins with the equipment used to transfer the materials from the raw materials preparation section and ends with the last vessel in which polymerization occurs. Equipment used for the on-site recovery of ethylene glycol from PET plants, however, are included in this process section, rather than in the material recovery process section.

Polystyrene resin means a thermoplastic polymer or copolymer comprised of at least 80 percent styrene or para-methylstyrene by weight.

Primary product is defined in and determined by the procedures specified in §63.1310(f).

Process contact cooling tower system means a cooling tower system that is designed and operated to allow contact between the cooling medium and process fluid or gases.

Process section means the equipment designed to accomplish a general but well-defined task in polymers production. Process sections include, but are not limited to, raw materials preparation, polymerization reaction, and material recovery. A process section may be dedicated to a single TPPU or common to more than one TPPU.

Process unit means a collection of equipment assembled and connected by pipes or ducts to process raw materials and to manufacture a product.

Process vent means a point of emission from a unit operation having a gaseous emission stream. Typical process vents include condenser vents, dryer vents, vacuum frimps, steam ejectors, and atmospheric vents from reactors and other process vessels, but do not include pressure relief valves.

Product means a compound or material which is manufactured by a process unit. By-products, isolated intermediates, impurities, wastes, and trace contaminants are not considered products.

Raw materials preparation section means the equipment at a polymer manufacturing plant designed to prepare raw materials, such as monomers and solvents, for polymerization. For
the purposes of these standards, this process section begins with the equipment used to transfer raw materials from storage and/or the equipment used to transfer recovered material from the material recovery process sections, and ends with the last piece of equipment that prepares the material for polymerization. The raw materials preparation section may include equipment that is used to purify, dry, or otherwise treat raw materials or raw and recovered materials together; to activate catalysts; and to promote esterification including the formation of some short polymer chains (oligomers). The raw materials preparation section does not include equipment that is designed primarily to accomplish the formation of oligomers, the treatment of recovered materials alone, or the storage of raw materials.

Recovery operations equipment means the equipment used to separate the components of process streams. Recovery operations equipment includes distillation unit, condensers, etc. Equipment used for wastewater treatment shall not be considered recovery operations equipment.

Solid state polymerization unit means a unit operation which, through the application of heat, furthers the polymerization (i.e., increases the intrinsic viscosity) of polymer chips.

Steady-state conditions means that all variables (temperatures, pressures, volumes, flow rates, etc.) in a process do not vary significantly with time; minor fluctuations about constant mean values can occur.

Storage vessel means a tank or other vessel that is used to store liquids that contain one or more organic HAP and that has been assigned, according to the procedures in §63.1310(g), to a TPPU that is subject to this subpart. Storage vessels do not include:

1. Vessels permanently attached to motor vehicles such as trucks, railcars, barges, or ships;
2. Pressure vessels designed to operate in excess of 204.9 kilopascals and without breathing or working losses to the atmosphere;
3. Vessels with capacities smaller than 38 cubic meters;
4. Vessels and equipment storing and/or handling material that contains no organic HAP and/or organic HAP as impurities only; and
5. Wastewater storage tanks.

Supplemental combustion air means the air that is added to a vent stream after the vent stream leaves the unit operation. Air that is part of the vent stream as a result of the nature of the unit operation is not considered supplemental combustion air. Air required to operate combustion device burner(s) is not considered supplemental combustion air.

Styrene acrylonitrile resin (SAN) means copolymers consisting primarily of styrene and acrylonitrile monomer units.

Suspension process means a process carried out with the reactants in a state of suspension, typically achieved through the use of water and/or suspending agents (e.g., polymerization reaction).

Thermoplastic product means one of the following types of products:

1. ABS latex;
2. ABS using a batch emulsion process;
3. ABS using a batch suspension process;
4. ABS using a continuous emulsion process;
5. ABS using a continuous mass process;
6. ASA/AMSAN;
7. EPS;
8. MABS;
9. MBS;
10. nitrile resin;
11. PET using a batch dimethyl terephthalate process;
12. PET using a batch terephthalic acid process;
13. PET using a continuous dimethyl terephthalate process;
14. PET using a continuous terephthalic acid process;
15. PET using a continuous terephthalic acid high viscosity multiple end finisher process;
16. Polystyrene resin using a batch process;
17. Polystyrene resin using a continuous process;
18. SAN using a batch process; or
19. SAN using a continuous process.
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Thermoplastic product process unit (TPPU) means a collection of equipment assembled and connected by process pipes or ducts, excluding gas, sanitary sewage, water (i.e., not wastewater), and steam connections, used to process raw materials and to manufacture a thermoplastic product as its primary product. This collection of equipment includes process vents from process vessels; storage vessels, as determined in §63.1310(g); and the equipment (i.e., pumps, compressors, agitators, pressure relief devices, sampling connection systems, open-ended valves or lines, valves, connectors, and instrumentation systems that are associated with the thermoplastic product process unit) that are subject to the equipment leak provisions as specified in §63.1331.

Total organic compounds (TOC) means those compounds excluding methane and ethane measured according to the procedures of Method 18 or Method 25A, 40 CFR part 60, appendix A.

Year means any consecutive 12-month period or 365 rolling days. For the purposes of emissions averaging, the term year applies to any 12-month period selected by the facility and defined in its Emissions Averaging Plan. For the purposes of batch cycle limitations, the term year applies to the 12-month period defined by the facility in its Notification of Compliance Status.

§ 63.1313 Emission standards.

(a) Except as allowed under paragraphs (b) and (c) of this section, the owner or operator of an existing or new affected source shall comply with the provisions in:

(1) Section 63.1314 for storage vessels;
(2) Sections 63.1315 or 63.1316 through 63.1320, as appropriate, for continuous process vents;
(3) Section 63.1321 for batch process vents;
(4) Section 63.1328 for heat exchange systems;
(5) Section 63.1329 for process contact cooling towers;
(6) Section 63.1330 for wastewater;
(7) Section 63.1331 for equipment leaks;
(8) Section 63.1333 for additional test methods and procedures;
(9) Section 63.1334 for parameter monitoring levels and excursions; and
(10) Section 63.1335 for general recordkeeping and reporting requirements.

(b) Instead of complying with §§63.1314, 63.1315, 63.1316 through 63.1320, 63.1321, and 63.1330, the owner or operator of an existing affected source may elect to control any or all of the storage vessels, batch process vents, continuous process vents, and wastewater streams within the affected source to different levels using an emissions averaging compliance approach that uses the procedures specified in §63.1332. An owner or operator electing to use emissions averaging must still comply with the provisions of §§63.1314, 63.1315, 63.1316 through 63.1320, 63.1321, and 63.1330 for affected source emission points not included in the emissions average.

(c) A State may decide not to allow the use of the emissions averaging compliance approach specified in paragraph (b) of this section.

§ 63.1314 Storage vessel provisions.

(a) This section applies to each storage vessel that belongs to an affected source, as determined by §63.1310(g). Except as provided in paragraphs (b) through (d) of this section, the owner or operator of said storage vessels shall comply with the requirements of §§63.119 through 63.123 and 63.148, with the differences noted in paragraphs (a)(1) through (a)(16) of this section for the purposes of this subpart.

(1) When the term “storage vessel” is used in §§63.119 through 63.123 and 63.148, the definition of this term in §63.1312 shall apply for the purposes of this subpart.

(2) When the term “Group 1 storage vessel” is used in §§63.119 through 63.123 and 63.148, the definition of this term in §63.1312 shall apply for the purposes of this subpart.

(3) When the term “Group 2 storage vessel” is used in §§63.119 through 63.123 and 63.148, the definition of this term in §63.1312 shall apply for the purposes of this subpart.

(4) When the emissions averaging provisions of §63.150 are referred to in §§63.119 and 63.123, the emissions averaging provisions contained in §63.1332...
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shall apply for the purposes of this subpart.

(5) When December 31, 1992, is referred to in § 63.119, March 29, 1995 shall apply instead, for the purposes of this subpart.

(6) When April 22, 1994, is referred to in § 63.119, September 12, 1996 shall apply instead, for the purposes of this subpart.

(7) Each owner or operator shall comply with this paragraph (a)(7) instead of § 63.120(d)(1)(ii) for the purposes of this subpart. If the control device used to comply with this section is also used to comply with §§ 63.1315 through 63.1330, the performance test required for these sections is acceptable for demonstrating compliance with § 63.119(e) for the purposes of this subpart. The owner or operator is not required to prepare a design evaluation for the control device as described in § 63.120(d)(1)(i) for the purposes of this subpart if the performance test meets the criteria specified in § 63.120(d)(1)(ii)(A) and (d)(1)(ii)(B).

(8) When the term “operating range” is used in § 63.120(d)(3), the term “level” shall apply instead, for the purposes of this subpart. This level shall be established using the procedures specified in § 63.1334.

(9) When the Notification of Compliance Status requirements contained in § 63.152(b) are referred to in §§ 63.120, 63.122, and 63.123, the Notification of Compliance Status requirements contained in § 63.1335(e)(5) shall apply for the purposes of this subpart.

(10) When the Periodic Report requirements contained in § 63.152(c) are referred to in §§ 63.120, 63.122, and 63.123, the Periodic Report requirements contained in § 63.1335(e)(6) shall apply for the purposes of this subpart.

(11) When other reports as required in § 63.152(d) are referred to in § 63.122, the reporting requirements contained in § 63.1335(e)(7) shall apply for the purposes of this subpart.

(12) When the Implementation Plan requirements contained in § 63.151(c) are referred to in § 63.120 and § 63.122, the owner or operator of an affected source subject to this subpart need not comply for the purposes of this subpart.

(13) When the Initial Notification Plan requirements contained in § 63.151(b) are referred to in § 63.122, the owner or operator of an affected source subject to this subpart need not comply for the purposes of this subpart.

(14) When the determination of equivalence criteria in § 63.102(b) is referred to in § 63.121(a), the provisions in § 63.119(e) shall apply for the purposes of this subpart.

(15) When a performance test is required under the provisions of § 63.120(d)(1)(i), the use of Method 18 or Method 25A, 40 CFR part 60, appendix A is allowed for the purposes of this subpart. The use of Method 25A, 40 CFR part 60, appendix A shall comply with paragraphs (a)(15)(i) and (a)(15)(ii) of this section.

(i) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A shall be the single organic HAP representing the largest percent by volume of the emissions.

(ii) The use of Method 25A, 40 CFR part 60, appendix A is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(16) The compliance date for storage vessels at affected sources subject to the provisions of this section is specified in § 63.1311.

(b) Owners or operators of Group 1 storage vessels that belong to a new affected source producing SAN using a continuous process shall control emissions to the levels indicated in paragraphs (b)(1) and (b)(2) of this section.

(1) For storage vessels with capacities greater than or equal to 2,271 cubic meters (m³) containing a liquid mixture having a vapor pressure greater than or equal to 0.5 kilopascal (kPa) but less than 0.7 kPa, emissions shall be controlled by at least 90 percent relative to uncontrolled emissions.

(2) For storage vessels with capacities less than 151 m³ containing a liquid mixture having a vapor pressure greater than or equal to 10 kPa, emissions shall be controlled by at least 90 percent relative to uncontrolled emissions.
§ 63.1315 Continuous process vents provisions.

(a) For each continuous process vent located at an affected source, the owner or operator shall comply with the requirements of §§ 63.113 through 63.118, with the differences noted in paragraphs (a)(1) through (a)(18) of this section for the purposes of this subpart, except as provided in paragraphs (b) through (e) of this section.

(1) When the term “process vent” is used in §§ 63.113 through 63.118, apply the term “continuous process vent,” and the definition of this term in § 63.1312 shall apply for the purposes of this subpart.

(2) When the term “Group 1 process vent” is used in §§ 63.113 through 63.118, apply the term “Group 1 continuous process vent,” and the definition of this term in § 63.1312 shall apply for the purposes of this subpart.

(3) When the term “Group 2 process vent” is used in §§ 63.113 through 63.118, apply the term “Group 2 continuous process vent,” and the definition of this term in § 63.1312 shall apply for the purposes of this subpart.

(4) When December 31, 1992, (i.e., subpart G of this part proposal date) is referred to in §§ 63.113, apply the date March 29, 1995 (i.e., proposal date for this subpart) for the purposes of this subpart.

(5) When § 63.151(f), alternative monitoring parameters, and § 63.152(e), submission of an operating permit, are referred to in §§ 63.114(c) and 63.117(e), § 63.1335(f), for the purposes of this subpart, respectively, apply as provided in paragraphs (a)(1) through (a)(9) of this section, for the purposes of this subpart.

(6) When the Notification of Compliance Status requirements contained in § 63.152(b) are referred to in §§ 63.114, 63.117, and 63.118, the Notification of Compliance Status requirements contained in § 63.1335(e)(5) shall apply for the purposes of this subpart.

(7) When the Periodic Report requirements contained in § 63.152(c) are referred to in §§ 63.114, 63.117, and 63.118, the Periodic Report requirements contained in § 63.1335(e)(6) shall apply for the purposes of this subpart.

(8) When the definition of excursion in § 63.152(c)(2)(ii)(A) is referred to in § 63.118(f)(2), the definition of excursion in § 63.1334(f) of this subpart shall apply for the purposes of this subpart.

(9) Owners and operators shall comply with § 63.1334, parameter monitoring levels and excursions, instead of § 63.114(e) for the purposes of this subpart. When the term “range” is used in §§ 63.117 and 63.118, the term “level” shall be used instead for the purposes of this subpart. This level is determined in accordance with § 63.1334.

(10) If a batch process vent is combined with a continuous process vent prior to being routed to a control device, the combined vent stream shall comply with either paragraph (a)(10)(i) or (a)(10)(ii) of this section, as appropriate.

(i) If the continuous process vent is a Group 1 continuous process vent, the combined vent stream shall comply with all requirements for a Group 1 continuous process vent stream in §§ 63.113 through 63.118, with the differences noted in paragraphs (a)(1) through (a)(9) of this section, for the purposes of this subpart.

(ii) If the continuous process vent is a Group 2 continuous process vent, the total resource effectiveness (TRE) index value for the combined vent stream shall be calculated at the exit of any recovery device and prior to the control device at maximum representative operating conditions. For combined vent streams containing continuous and batch process vents, the maximum representative operating conditions shall be during periods when
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(11) If a batch process vent is combined with a continuous process vent prior to being routed to a recovery device, the TRE index value for the combined vent stream shall be calculated at the exit of the recovery device at maximum representative operating conditions for the purposes of this subpart. For combined vent streams containing continuous and batch process vents, the maximum representative operating conditions shall be during periods when batch emission episodes are venting to the recovery device, resulting in the highest concentration of organic HAP in the combined vent stream.

(12) When reports of process changes are required under §63.118 (g), (h), (i), and (j), paragraphs (a)(12)(i) through (a)(12)(iv) of this section shall apply for the purposes of this subpart:

(i) For the purposes of this subpart, whenever a process change, as defined in §63.115(e), is made that causes a Group 2 continuous process vent to become a Group 1 continuous process vent, the owner or operator shall submit a report within 180 operating days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included in the next Periodic Report, as specified in §63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(A) A description of the process change; and
(B) A schedule for compliance with the provisions of this subpart, as required under §63.1335(e)(6)(iii)(D)(2).

(ii) Whenever a process change, as defined in §63.115(e), is made that causes a Group 2 process vent with an organic HAP concentration less than 50 parts per million by volume to become a Group 2 process vent with an organic HAP concentration of 50 parts per million or greater and a TRE index value less than or equal to 4.0, the owner or operator shall submit a report within 180 operating days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included in the next Periodic Report, as specified in §63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(A) A description of the process change; and
(B) A schedule for compliance with the provisions of this subpart, as required under §63.1335(e)(6)(iii)(D)(2).

(iii) Whenever a process change, as defined in §63.115(e), is made that causes Group 1 process vent with a flow rate less than 0.005 standard cubic meter per minute to become a Group 2 process vent with a flow rate of 0.005 standard cubic meter per minute or greater and a TRE index value less than or equal to 4.0, the owner or operator shall submit a report within 180 operating days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included in the next Periodic Report, as specified in §63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(A) A description of the process change; and
(B) A schedule for compliance with the provisions of this subpart, as required under §63.1335(e)(6)(iii)(D)(2).

(iv) Whenever a process change, as defined in §63.115(e), is made that causes a Group 2 process vent with an organic HAP concentration less than 50 parts per million by volume to become a Group 2 process vent with an organic HAP concentration of 50 parts per million or greater and a TRE index value less than or equal to 4.0, the owner or operator shall submit a report within 180 operating days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included in the next Periodic Report, as specified in §63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(A) A description of the process change; and
(B) A schedule for compliance with the provisions of this subpart, as required under §63.1335(e)(6)(iii)(D)(2).

(13) When the provisions of §63.116 (c)(3) and (c)(4) specify that Method 18, 40 CFR part 60, appendix A shall be used, Method 18 or Method 25A, 40 CFR part 60, appendix A may be used for the purposes of this subpart. The use of Method 25A, 40 CFR part 60, appendix A...
shall comply with paragraphs (a)(13)(i) and (a)(13)(ii) of this section.

(i) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A shall be the single organic HAP representing the largest percent by volume of the emissions.

(ii) The use of Method 25A, 40 CFR part 60, appendix A is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(14) When the provisions of §63.116(b) identify conditions under which a performance test is not required, for purposes of this subpart, the exemption in paragraph (a)(14)(i) shall also apply. Further, if a performance test meeting the conditions specified in paragraph (a)(14)(ii) of this section has been conducted by the owner or operator, the results of said performance test may be submitted and a performance test, as required by this section, is not required.

(i) An incinerator burning hazardous waste for which the owner or operator complies with the requirements of 40 CFR part 264, subpart O.

(ii) Performance tests done for other subparts in 40 CFR part 60 or part 63 where total organic HAP or TOC was measured, provided the owner or operator can demonstrate that operating conditions for the process and control or recovery device during the performance test are representative of current operating conditions.

(15) The compliance date for continuous process vents subject to the provisions of this section is specified in §63.1311.

(16)–(17) [Reserved]

(18) When a combustion device is used to comply with the 20 parts per million by volume outlet concentration standard specified in §63.113(a)(2), the correction to 3 percent oxygen is only required when supplemental combustion air is used to combust the emissions, for the purposes of this subpart. Finally, when a combustion device is used to comply with the 20 parts per million by volume outlet concentration standard specified in §63.113(a)(2), an owner or operator shall record and report the outlet concentration required in §63.117(a)(4)(ii) and (a)(4)(iv) corrected to 3 percent oxygen when supplemental combustion air is used to combust the emissions, for the purposes of this subpart. When supplemental combustion air is not used to combust the emissions, an owner or operator may record and report the outlet concentration required in §63.117(a)(4)(ii) and (a)(4)(iv) on an uncorrected basis or corrected to 3 percent oxygen, for the purposes of this subpart.

(b) Existing affected sources producing MBS shall comply with either paragraph (b)(1) or (b)(2) of this section.

(1) Comply with paragraph (a) of this section, as specified in paragraphs (b)(1)(i) and (b)(1)(ii).

(i) As specified in §63.1312, Group 1 continuous process vents at MBS existing affected sources are those with a total resource effectiveness value less than or equal to 3.7.

(ii) When complying with this paragraph (b), the term ‘‘TRE of 4.0’’, or related terms indicating a TRE value of 4.0, referred to in §63.113 through §63.118 shall be replaced with ‘‘TRE of 6.7’’, for the purposes of this subpart. The TRE range of 3.7 to 6.7 for continuous process vents at existing affected sources producing MBS corresponds to the TRE range of 1.0 to 4.0 for other continuous process vents, as it applies to monitoring, recordkeeping, and reporting.

(2) Not allow organic HAP emissions from the collection of continuous process vents at the affected source to be greater than 0.000590 kg organic HAP/Mg of product. Compliance with this paragraph (b)(2) shall be determined using the procedures specified in §63.1333(b).

(c) New affected sources producing SAN using a batch process shall comply with the applicable requirements in §63.1321.

(d) Affected sources producing PET or polystyrene using a continuous process are subject to the emissions...
§ 63.1316 PET and polystyrene affected sources—emissions control provisions.

(a) The owner or operator of an affected source producing PET using a continuous process shall comply with paragraph (b) of this section. The owner or operator of an affected source producing polystyrene using a continuous process shall comply with paragraph (c) of this section.

(b) Each owner or operator of an affected source producing PET using a continuous process shall comply with the requirements specified in paragraphs (b)(1) or (b)(2) of this section, as appropriate, and not with any of the requirements specified in 40 CFR part 60, subpart DDD. Compliance can be based on either organic HAP or TOC.

(1) Each owner or operator of an affected source producing PET using a continuous dimethyl terephthalate process shall comply with paragraphs (b)(1)(i) through (b)(1)(iv) of this section.

(ii) For purpose of this section, the group determination procedure required by §63.1323 shall not apply.

(c) For each aggregate batch vent stream, comply with §§63.1321 through 63.1327 as specified in paragraphs (e)(3)(i) through (e)(3)(ii) of this section.

(i) For purpose of this section, each aggregate batch vent stream shall be considered to be a Group 1 aggregate batch vent stream and the owner or operator of that aggregate batch vent stream shall comply with the requirements for a Group 1 aggregate batch vent stream contained in §§63.1321 through 63.1327, except that each aggregate batch vent stream shall be controlled to reduce organic HAP emissions by 98 weight-percent.

(ii) For purposes of this section, the group determination procedure required by §63.1323 shall not apply.

[61 FR 48229, Sept. 12, 1996, as amended at 64 FR 11547, Mar. 9, 1999]
(b)(1)(i)(B), or (b)(1)(i)(C) of this section.

(A) Organic HAP emissions from all continuous process vents in each individual material recovery section shall, as a whole, be no greater than 0.018 kg organic HAP per Mg of product from the associated TPPU(s); or alternatively, organic HAP emissions from all continuous process vents in the collection of material recovery sections within the affected source shall, as a whole, be no greater than 0.018 kg organic HAP per Mg product from all associated TPPU(s).

(B) As specified in §63.1318(d), the owner or operator shall maintain the daily average outlet gas stream temperature from each final condenser in a material recovery section at a temperature of +3°C (+37°F) or less (i.e., colder); or

(C) Comply with paragraph (b)(1)(v) of this section.

(ii) Limit organic HAP emissions from continuous process vents in the collection of polymerization reaction sections within the affected source by complying with either paragraph (b)(1)(ii)(A) or (b)(1)(ii)(B) of this section.

(A) Organic HAP emissions from all continuous process vents in each individual polymerization reaction section within the affected source (including emissions from any equipment used to further recover ethylene glycol, but excluding emissions from process contact cooling towers) shall, as a whole, be no greater than 0.02 kg organic HAP per Mg of product from the associated TPPU(s); or alternatively, organic HAP emissions from all continuous process vents associated with the esterification vessels in each individual raw materials preparation section shall, as a whole, be no greater than 0.02 kg organic HAP per Mg product from all associated TPPU(s); or

(B) Comply with paragraph (b)(1)(v) of this section.

(iii) Limit organic HAP emissions from continuous process vents not included in a material recovery section, as specified in paragraph (b)(1)(i) of this section, or not included in a polymerization reaction section, as specified in paragraph (b)(1)(ii) of this section, by complying with §63.1315.

(iv) Limit organic HAP emissions from all batch process vents by complying with §63.1321.

(v) Comply with one of the following:

(A) Reduce the emissions in a combustion device to achieve 98 weight percent reduction or to achieve a concentration of 20 parts per million by volume (ppmv) on a dry basis, whichever is less stringent. If an owner or operator elects to comply with the 20 ppmv standard, the concentration shall include a correction to 3 percent oxygen only when supplemental combustion air is used to combust the emissions;

(B) Combust the emissions in a boiler or process heater with a design heat input capacity of 150 million Btu/hr or greater by introducing the emissions into the flame zone of the boiler or process heater; or

(C) Combust the emissions in a flare that complies with the requirements of §63.1333(e).

(2) Each owner or operator of an affected source producing PET using a continuous terephthalic acid process shall comply with paragraphs (b)(2)(i) through (b)(2)(iv) of this section.

(i) Limit organic HAP emissions from continuous process vents in the collection of raw material preparation sections within the affected source by complying with either paragraph (b)(2)(i)(A) or (b)(2)(i)(B) of this section.

(A) Organic HAP emissions from all continuous process vents associated with the esterification vessels in each individual raw materials preparation section shall, as a whole, be no greater than 0.04 kg organic HAP per Mg of product from the associated TPPU(s); or alternatively, organic HAP emissions from all continuous process vents in the collection of polymerization reaction sections within the affected source shall, as a whole, be no greater than 0.02 kg organic HAP per Mg product from all associated TPPU(s); or

(B) Comply with paragraph (b)(2)(v) of this section.

(ii) Limit organic HAP emissions from continuous process vents not associated with the esterification vessels in each individual raw materials preparation section by complying with §63.1315; or

(B) Comply with paragraph (b)(2)(v) of this section.
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(ii) Limit organic HAP emissions from continuous process vents in the collection of polymerization reaction sections within the affected source by complying with either paragraph (b)(2)(ii)(A) or (b)(2)(ii)(B) of this section.

(A) Organic HAP emissions from all continuous process vents in each individual polymerization reaction section (including emissions from any equipment used to further recover ethylene glycol, but excluding emissions from process contact cooling towers) shall, as a whole, be no greater than 0.02 kg organic HAP per Mg of product from the associated TPPU(s); or alternatively, organic HAP emissions from all continuous process vents in the collection of polymerization reaction sections within the affected source shall, as a whole, be no greater than 0.02 kg organic HAP per Mg of product from all associated TPPU(s); or

(B) Comply with paragraph (b)(2)(v) of this section.

(iii) Limit organic HAP emissions from continuous process vents not included in a raw materials preparation section, as specified in paragraphs (b)(2)(i) of this section, or not included in a polymerization reaction section, as specified in paragraph (b)(2)(ii) of this section, by complying with § 63.1315.

(iv) Limit organic HAP emissions from all batch process vents by complying with § 63.1321.

(v) Comply with one of the following:

(A) Reduce emissions by 98 weight percent or to a concentration of 20 parts per million by volume (ppmv) on a dry basis, whichever is less stringent. If an owner or operator elects to comply with the 20 ppmv standard, the concentration shall include a correction to 3 percent oxygen only when supplemental combustion air is used to combust the emissions;

(B) Combust the emissions in a boiler or process heater with a design heat input capacity of 150 million Btu/hr or greater by introducing the emissions into the flame zone of the boiler or process heater; or

(C) Combust the emissions in a flare that complies with the requirements of § 63.1333(e).

(c) Each owner or operator of an affected source producing polystyrene resin using a continuous process shall comply with the requirements specified in paragraphs (c)(1) through (c)(3) of this section, as appropriate, and not with any of the requirements specified in 40 CFR part 60, subpart DDD. Compliance can be based on either organic HAP or TOC.

(1) Limit organic HAP emissions from continuous process vents in the collection of material recovery sections within the affected source by complying with one of the following:

(i) Not allow emissions to be greater than 0.0036 kg organic HAP/Mg of product;

(ii) Not allow the outlet gas stream temperature from each final condenser in a material recovery section to exceed -25°C (-13°F); or

(iii) Comply with one of the following:

(A) Reduce emissions by 98 weight percent or to a concentration of 20 parts per million by volume (ppmv) on a dry basis, whichever is less stringent. If an owner or operator elects to comply with the 20 ppmv standard, the concentration shall include a correction to 3 percent oxygen only when supplemental combustion air is used to combust the emissions;

(B) Combust the emissions in a boiler or process heater with a design heat input capacity of 150 million Btu/hr or greater by introducing the emissions into the flame zone of the boiler or process heater; or

(C) Combust the emissions in a flare that complies with the requirements of § 63.1311(b).

(2) Limit organic HAP emissions from continuous process vents not included in a material recovery section, as specified in paragraph (c)(1)(i) of this section, by complying with § 63.1315.

(3) Limit organic HAP emissions from all batch process vents by complying with § 63.1321.
§ 63.1317 PET and polystyrene continuous process affected sources—monitoring provisions.

Continuous process vents using a control or recovery device to comply with § 63.1316 shall comply with the applicable monitoring provisions specified in § 63.1315(a), except as specified in paragraphs (a) and (b) of this section.

(a) For the purposes of paragraph (a) of this section, owners or operators shall ignore references to group determinations (i.e., total resource effectiveness) and are not required to comply with § 63.113.

(b) The monitoring period for condenser exit temperature when complying with § 63.1316(b)(1)(i)(B) or § 63.1316(c)(1)(ii) shall be each consecutive 3-hour continuous period (e.g., 6 am to 9 am, 9 am to 12 pm). Each owner or operator shall designate said monitoring period in the Notification of Compliance Status required by § 63.1335(e)(5).

§ 63.1318 PET and polystyrene continuous process affected sources—testing and compliance demonstration provisions.

(a) Except as specified in paragraphs (b) through (d) of this section, continuous process vents using a control or recovery device to comply with § 63.1316 shall comply with the applicable testing and compliance provisions for continuous process vents specified in § 63.1315, except that, for the purposes of this paragraph (a), owners or operators shall ignore references to group determination (i.e., total resource effectiveness) and are not required to comply with § 63.113.

(b) PET Affected Sources Using a Dimethyl Terephthalate Process—Applicability Determination Procedure. Owners or operators shall calculate organic HAP emissions from the collection of material recovery sections at an existing affected source producing PET using a continuous dimethyl terephthalate process to determine whether § 63.1316(a)(1)(i) is applicable using the procedures specified in either paragraph (b)(1) or (b)(2) of this section.

(i) Use Equation 1 of this subpart to determine mass emissions per mass product as specified in paragraphs (b)(1)(i) and (b)(1)(ii) of this section.

\[
ER = \sum_{i=1}^{n} \frac{E_i}{0.001 \cdot P_p} \tag{Eq. 1}
\]

where:

- \(ER\) = Emission rate of total organic HAP or TOC, kg/Mg product.
- \(E_i\) = Emission rate of total organic HAP or TOC in continuous process vent \(i\), kg/hr.
- \(P_p\) = The rate of polymer produced, kg/hr.
- \(n\) = Number of continuous process vents in the collection of material recovery sections at the affected source.
- 0.001 = Conversion factor, kg to Mg.

(ii) The mass emission rate for each continuous process vent, \(E_i\), shall be determined according to the procedures specified in § 63.116(c)(4). The sampling site for determining whether § 63.1316(a)(1)(i) is applicable shall be before any add-on control devices (i.e., those required by regulation) and after those recovery devices installed as part of operating the material recovery section. When the provisions of § 63.116(c)(4) specify that Method 18, 40 CFR part 60, appendix A shall be used, Method 18 or Method 25A, 40 CFR part 60, appendix A may be used for the purposes of this subpart. The use of Method 25A, 40 CFR part 60, appendix A shall comply with paragraphs (b)(1)(i)(A) and (b)(1)(i)(B) of this section.

(A) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A shall be the single organic HAP representing the largest percent by volume of the emissions.

(B) The use of Method 25A, 40 CFR part 60, appendix A is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(ii) The rate of polymer produced, \(P_p\) (kg/hr), shall be determined by dividing the weight (kg) of polymer pulled from the process line during the performance test by the number of hours taken to perform the performance test. The
weight of polymer pulled shall be determined by direct measurement or by an alternate methodology, such as materials balance. If an alternate methodology is used, a description of the methodology, including all procedures, data, and assumptions shall be submitted as part of the Notification of Compliance Status required by §63.1335(e)(5).

(2) Use engineering assessment, as described in §63.1323(b)(6)(i), to demonstrate that mass emissions per mass product are less than or equal to 0.07 kg organic HAP/Mg product. If engineering assessment shows that mass emissions per mass product are greater than 0.07 kg organic HAP/Mg product and the owner or operator wishes to demonstrate that mass emissions per mass product are less than the threshold emission rate of 0.12 kg organic HAP/Mg product, the owner or operator shall use the procedures specified in paragraph (b)(1) of this section.

(c) Compliance with Mass Emissions per Mass Product Standards. Owners or operators complying with §63.1316 (b)(1)(i)(A), (b)(1)(ii), (b)(2)(i), (b)(2)(ii), and (c)(1)(i) shall demonstrate compliance with the mass emissions per mass product requirements using the procedures specified in paragraph (b)(1) of this section, except that the sampling site specified in paragraph (b)(1)(i) of this section shall be at the outlet of the last control or recovery device.

(d) Compliance with Temperature Limits for Final Condensers. Owners or operators complying with §63.1316(b)(1)(i)(B) or §63.1316(c)(1)(ii) shall perform an initial performance test as specified in paragraph (d)(1) of this section to demonstrate initial compliance with the temperature limit requirements and shall demonstrate continuous compliance as specified in paragraph (d)(2) of this section.

(1) Using the temperature monitoring device specified by the applicable monitoring provisions specified for continuous process vents in §63.1315, an average exit temperature shall be determined based on the average exit temperature for three performance tests. The average exit temperature for each 3-hour performance test shall be based on measurements taken at least every 15 minutes for 3 hours of continuous operation under maximum representative operating conditions for the process. For emissions streams containing continuous and batch process vents, the maximum representative operating conditions shall be during periods when batch emission episodes are venting to the control device resulting in the highest concentration of organic HAP in the emissions stream.

(2) As specified in §63.1317(b), continuous compliance shall be determined based on an average exit temperature determined for each consecutive 3-hour continuous period. Each 3-hour period where the average exit temperature is more than 6 °C (10 °F) above the applicable specified temperature limit shall be considered an exceedance of the monitoring provisions.

§63.1319 PET and polystyrene continuous process affected sources—recordkeeping provisions.

(a) Except as specified in paragraphs (b) and (c) of this section, owners or operators using a control or recovery device to comply with §63.1316 shall comply with the applicable recordkeeping provisions specified in §63.1315, except that, for the purposes of this paragraph (a), owners or operators shall ignore references to group determinations (i.e., total resource effectiveness) and are not required to comply with §63.113.

(b) Records Demonstrating Compliance With the Applicability Determination Procedure for PET Affected Sources Using a Dimethyl Terephthalate Process. Each owner or operator, as appropriate, shall keep the following data, as appropriate, up-to-date and readily accessible:

(1) Results of the mass emissions per mass product calculation specified in §63.1318(b).

(2) If complying with §63.1316 by demonstrating that mass emissions per mass product are less than or equal to the level specified in §63.1316(a)(1)(i), the information specified in paragraphs (b)(2)(i) and (b)(2)(ii) of this section.

(i) Each process operation variable (e.g., pressure, temperature, type of catalyst) that may result in an increase in the mass emissions per mass product shall said variable be changed.
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§ 63.1321 Batch process vents provisions.

(a) Batch process vents. Except as specified in paragraphs (b) and (c) of this section, owners and operators of new and existing affected sources with batch process vents shall comply with the requirements in §§ 63.1322 through 63.1327. The batch process vent group status shall be determined in accordance with § 63.1323. Batch process vents classified as Group 1 shall comply with the reference control technology requirements for Group 1 batch process vents in the collection of material recovery sections (i.e., methanol recovery) within the affected source to be greater than 0.12 kg organic HAP/Mg of product, the owner or operator shall submit a report within 180 operating days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included in the next Periodic Report as specified in § 63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(i) A description of the process change; and

(ii) A schedule for compliance with the provisions of this subpart, as required under § 63.1335(e)(6)(iii)(D)(2).

(c) Reporting for Affected Sources Complying With Temperature Limits for Final Condensers. Each owner or operator complying with § 63.1316(b)(1)(i)(B) or § 63.1316(c)(1)(ii) shall comply with paragraphs (c)(1) and (c)(2) of this section.

(1) Report periods when the 3-hour average exit temperature is more than 6 °C (10 °F) above the applicable specified temperature limit in each Periodic Report, required by § 63.1335(e)(6), as appropriate.

(2) Include the information specified in § 63.1319(c)(2) in the Notification of Compliance Status, required by § 63.1335(e)(5), for the initial performance test and in the appropriate Periodic Report, required by § 63.1335(e)(6), for any subsequent performance tests that may be required.

(3) Include the information specified in § 63.1317(b) in the Notification of Compliance Status, required by § 63.1335(e)(5).

§ 63.1320 PET and polystyrene continuous process affected sources—reporting provisions.

(a) Except as specified in paragraphs (b) and (c) of this section, owners and operators using a control or recovery device to comply with § 63.1316 shall comply with the applicable reporting provisions specified in § 63.1315, except that, for the purposes of this paragraph (a), owners or operators shall ignore references to group determinations (i.e., total resource effectiveness) and are not required to comply with § 63.113.

(b) Reporting for PET Affected Sources Using a Dimethyl Terephthalate Process. Each owner or operator complying with § 63.1316 by demonstrating that mass emissions per mass product are less than or equal to the level specified in § 63.1316(a)(1)(i) shall comply with paragraphs (b)(1) through (b)(3) of this section.

(1) Include the information specified in § 63.1319(b)(2)(i) in each Periodic Report, required by § 63.1335(e)(6), as appropriate.

(2) Include the information specified in § 63.1319(b)(1) or (b)(2) in the Notification of Compliance Status, required by § 63.1335(e)(5), for the initial determination and in the appropriate Periodic Report, required by § 63.1335(e)(6), for any subsequent determinations that may be required.

(3) Whenever a process change, as defined in § 63.115(e), is made that causes emissions from continuous process vents in the collection of material recovery sections (i.e., methanol recovery) within the affected source to be greater than 0.12 kg organic HAP/Mg of product, the owner or operator shall submit a report within 180 operating days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included in the next Periodic Report as specified in § 63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(i) A description of the process change; and

(ii) A schedule for compliance with the provisions of this subpart, as required under § 63.1335(e)(6)(iii)(D)(2).

(c) Reporting for Affected Sources Complying With Temperature Limits for Final Condensers. Each owner or operator complying with § 63.1316(b)(1)(i)(B) or § 63.1316(c)(1)(ii) shall comply with paragraphs (c)(1) and (c)(2) of this section.

(1) Report periods when the 3-hour average exit temperature is more than 6 °C (10 °F) above the applicable specified temperature limit in each Periodic Report, required by § 63.1335(e)(6), as appropriate.

(2) Include the information specified in § 63.1319(c)(2) in the Notification of Compliance Status, required by § 63.1335(e)(5), for the initial performance test and in the appropriate Periodic Report, required by § 63.1335(e)(6), for any subsequent performance tests that may be required.

(3) Include the information specified in § 63.1317(b) in the Notification of Compliance Status, required by § 63.1335(e)(5).

§ 63.1321 Batch process vents provisions.

(a) Batch process vents. Except as specified in paragraphs (b) and (c) of this section, owners and operators of new and existing affected sources with batch process vents shall comply with the requirements in §§ 63.1322 through 63.1327. The batch process vent group status shall be determined in accordance with § 63.1323. Batch process vents classified as Group 1 shall comply with the reference control technology requirements for Group 1 batch process vents in the collection of material recovery sections (i.e., methanol recovery) within the affected source to be greater than 0.12 kg organic HAP/Mg of product, the owner or operator shall submit a report within 180 operating days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included in the next Periodic Report as specified in § 63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(i) A description of the process change; and

(ii) A schedule for compliance with the provisions of this subpart, as required under § 63.1335(e)(6)(iii)(D)(2).
§ 63.1322 Batch process vents—reference control technology.

(a) Batch process vents. The owner or operator of a Group 1 batch process vent, as determined using the procedures in §63.1323, shall comply with the requirements of either paragraph (a)(1) or (a)(2) of this section, except as provided for in paragraph (a)(3) of this section. Compliance can be based on either organic HAP or TOC.

(1) For each batch process vent, reduce organic HAP emissions using a flare.

   (i) The flare shall comply with the requirements of §63.11(b).

   (ii) Halogenated batch process vents, as defined in §63.1312, shall not be vented to a flare.

(2) For each batch process vent, reduce organic HAP emissions for the batch cycle by 90 weight percent using a control device. Owners or operators may achieve compliance with this paragraph (a)(2) through the control of selected batch emission episodes or the control of portions of selected batch emission episodes. Documentation demonstrating how the 90 weight percent emission reduction is achieved is required by §63.1325(c).

(3) The owner or operator of a new affected source producing SAN using a batch process shall reduce organic HAP emissions from the collection of batch process vents, aggregate batch vent streams, and continuous process vents by 84 weight percent. Compliance with this paragraph (a)(3) shall be demonstrated using the procedures specified in §63.1333(c).

(b) Aggregate batch vent streams. The owner or operator of an aggregate batch vent stream that contains one or more Group 1 batch process vents shall comply with the requirements of either paragraph (b)(1) or (b)(2) of this section, except as provided for in paragraph (b)(3) of this section. Compliance
For each aggregate batch vent stream, reduce organic HAP emissions using a flare.

(i) The flare shall comply with the requirements of §63.11(b).

(ii) Halogenated aggregate batch vent streams, as defined in §63.1312, shall not be vented to a flare.

(2) For each aggregate batch vent stream, reduce organic HAP emissions by 90 weight percent or to a concentration of 20 parts per million by volume, whichever is less stringent, on a continuous basis using a control device.

For purposes of complying with the 20 parts per million by volume concentration standard, the outlet concentration shall be calculated on a dry basis. When a combustion device is used for purposes of complying with the 20 parts per million by volume outlet concentration standard, the concentration shall be corrected to 3 percent oxygen if supplemental combustion air is used to combust the emissions. If supplemental combustion air is not used, a correction to 3 percent oxygen is not required.

(3) The owner or operator of a new affected source producing SAN using a batch process shall comply with paragraph (a)(3) of this section.

(c) Halogenated emissions. Halogenated Group 1 batch process vents, halogenated aggregate batch vent streams, and halogenated continuous process vents that are combusted as part of complying with paragraph (a)(2), (a)(3), (b)(2), or (b)(3) of this section, as appropriate, shall be controlled according to either paragraph (c)(1) or (c)(2) of this section.

(1) If a combustion device is used to comply with paragraph (a)(2), (a)(3), (b)(2), or (b)(3) of this section for a halogenated batch process vent, halogenated aggregate batch vent stream, or halogenated continuous process vent, said emissions shall be ducted from the combustion device to an additional control device that reduces overall emissions of hydrogen halides and halogens by 99 percent before said emissions are discharged to the atmosphere.

(2) A control device may be used to reduce the halogen atom mass emission rate of said emissions to less than 3,750 kg/yr for batch process vents or aggregate batch vent streams and to less than 0.45 kilograms per hour for continuous process vents prior to venting to any combustion control device, and thus make the batch process vent, aggregate batch vent stream, or continuous process vent nonhalogenated. The nonhalogenated batch process vent, aggregate batch vent stream, or continuous process vent must then comply with the requirements of either paragraph (a) or (b) of this section, as appropriate.

(d) If a boiler or process heater is used to comply with the percent reduction requirement specified in paragraph (a)(2), (a)(3), (b)(2), or (b)(3) of this section, the batch process vent, aggregate batch vent stream, or continuous process vent shall be introduced into the flame zone of such a device.

(e) Combination of batch process vents or aggregate batch vent streams with continuous process vents.

(1) The batch process vent or aggregate batch vent stream is combined with a continuous process vent prior to routing the continuous process vent to a control or recovery device. In this paragraph (e)(1), the definitions of control device and recovery device as they relate to continuous process vents shall be used.

(2) The only emissions to the atmosphere from the batch process vent or aggregate batch vent stream prior to being combined with the continuous process vent are from equipment subject to and in compliance with §63.1331.

(3) If the batch process vent or aggregate batch vent stream is combined with a continuous process vent prior to being routed to a control device, the combined vent stream shall comply with the requirements in §63.1315(a)(10). In this paragraph (e)(3), the definition of control device as it relates to continuous process vents shall be used.
§ 63.1323 Batch process vents—methods and procedures for group determination.

(a) General requirements. Except as provided in paragraph (a)(3) of this section and in §63.1321(b)(1), the owner or operator of batch process vents at affected sources shall determine the group status of each batch process vent in accordance with the provisions of this section. This determination may be based on either organic HAP or TOC emissions.

(4) If the batch process vent or aggregate batch vent stream is combined with a continuous process vent prior to being routed to a recovery device, the combined vent stream shall comply with the requirements in §63.1315(a)(11). In this paragraph (e)(4), the definition of recovery device as it relates to continuous process vents shall be used.

(f) Group 2 batch process vents with annual emissions greater than or equal to the level specified in §63.1323(d). The owner or operator of a Group 2 batch process vent with annual emissions greater than or equal to the level specified in §63.1323(d) shall comply with the provisions of (f)(1) and (f)(2) of this section.

(1) Establish a batch cycle limitation that ensures the Group 2 batch process vent does not become a Group 1 batch process vent.

(2) Comply with the recordkeeping requirements in §63.1326(d)(2), and the reporting requirements in §63.1327(a)(3) and (b).

(g) Group 2 batch process vents with annual emissions less than the level specified in §63.1323(d). The owner or operator of a Group 2 batch process vent with annual emissions less than the level specified in §63.1323(d) shall comply with either paragraphs (g)(1) and (g)(2) of this section or with paragraphs (f)(1) and (f)(2) of this section.

(1) Establish a batch cycle limitation that ensures emissions do not exceed the level specified in §63.1323(d).

(2) Comply with the recordkeeping requirements in §63.1326(d)(1), and the reporting requirements in §63.1327(a)(2), (b), and (c).

[61 FR 48229, Sept. 12, 1996, as amended at 64 FR 11549, Mar. 9, 1999]

§ 63.1323 Batch process vents—methods and procedures for group determination.

(1) The procedures specified in paragraphs (b) through (h) of this section shall be followed for the expected mix of products for a given batch process vent, as specified in paragraph (a)(1)(i) of this section, or for the worst-case HAP emitting product, as specified in paragraphs (a)(1)(ii) through (a)(1)(iv) of this section. “Worst-case HAP emitting product” is defined in paragraph (a)(1)(iii) of this section.

(i) If an owner or operator chooses to follow the procedures specified in paragraphs (b) through (h) of this section for the expected mix of products, an identification of the different products and the number of batch cycles accomplished for each is required as part of the group determination documentation, as specified in §63.1328(a)(1).

(ii) If an owner or operator chooses to follow the procedures specified in paragraphs (b) through (h) of this section for the worst-case HAP emitting product, documentation identifying the worst-case HAP emitting product is required as part of the group determination documentation, as specified in §63.1328(a)(1).

(iii) Except as specified in paragraph (a)(1)(iii)(B) of this section, the worst-case HAP emitting product is as defined in paragraph (a)(1)(iii)(A) of this section.

(A) The worst-case HAP emitting product is the one with the highest mass emission rate (kg organic HAP per hour) averaged over the entire time period of the batch cycle.

(B) Alternatively, when one product is produced more than 75 percent of the time, accounts for more than 75 percent of the annual mass of product, and the owner or operator can show that the mass emission rate (kg organic HAP per hour) averaged over the entire time period of the batch cycle can reasonably be expected to be similar to the mass emission rate for other products having emissions from the same batch process vent, said product may be considered the worst-case HAP emitting product.

(C) An owner or operator shall determine the worst-case HAP emitting product for a batch process vent as specified in paragraphs (a)(1)(ii)(C)(1) through (a)(1)(iii)(C)(3) of this section.
The emissions per batch emission episode shall be determined using any of the procedures specified in paragraph (b) of this section. The mass emission rate (kg organic HAP per hour) averaged over the entire time period of the batch cycle shall be determined by summing the emissions for each batch emission episode making up a complete batch cycle and dividing by the total duration in hours of the batch cycle.

(2) To determine the worst-case HAP emitting product as specified under paragraph (a)(1)(iii)(A) of this section, the mass emission rate for each product shall be determined and compared.

(3) To determine the worst-case HAP emitting product as specified under paragraph (a)(1)(iii)(B) of this section, the mass emission rate for the product meeting the time and mass criteria of paragraph (a)(1)(iii)(B) of this section shall be determined, and the owner or operator shall provide adequate information to demonstrate that the mass emission rate for said product is similar to the mass emission rates for the other products having emissions from the same batch process vent. In addition, the owner or operator shall provide information demonstrating that the selected product meets the time and mass criteria of paragraph (a)(1)(iii)(B) of this section.

(iv) The annual production of the worst-case HAP emitting product shall be determined by ratioing the production time of said product up to a 12 month period of actual production. It is not necessary to ratio up to a maximum production rate (i.e., 8,760 hours per year at maximum design production).

(2) The annual uncontrolled organic HAP or TOC emissions and annual average batch vent flow rate shall be determined at the exit from the batch unit operation. For the purposes of these determinations, the primary condenser operating as a reflux condenser on a reactor or distillation column, the primary condenser recovering monomer, reaction products, by-products, or solvent from a stripper operated in batch mode, and the primary condenser recovering monomer, reaction products, by-products, or solvent from a distillation operation operated in batch mode shall be considered part of the batch unit operation. All other devices that recover or oxidize organic HAP or TOC vapors shall be considered control devices as defined in §63.1312.

(3) The owner or operator of a batch process vent complying with the flare provisions in §63.1322(a)(1) or §63.1322(b)(1) or routing the batch process vent to a control device to comply with the requirements in §63.1322(a)(2) or §63.1322(b)(2) is not required to perform the batch process vent group determination described in this section, but shall comply with all requirements applicable to Group 1 batch process vents for said batch process vent.

(b) Determination of annual emissions. The owner or operator shall calculate annual uncontrolled TOC or organic HAP emissions for each batch process vent using the methods described in paragraphs (b)(1) through (b)(8) of this section. Paragraphs (b)(1) through (b)(4) of this section present procedures that can be used to calculate the emissions from individual batch emission episodes. Emissions from batch processes involving multicomponent systems are to be calculated using the procedures in paragraphs (b)(1) through (b)(4) of this section. Individual HAP partial pressures in multicomponent systems shall be determined by the following methods: If the components are miscible in one another, use Raoult's law to calculate the partial pressures; if the solution is a dilute aqueous mixture use Henry's law constants to calculate partial pressures; if Raoult's law or Henry's law are not appropriate (or available) use experimentally obtained activity coefficients, Henry's law constants, or solubility data; if Raoult's law or Henry's law are not appropriate use models, such as the group-contribution models, to predict activity coefficients; and if Raoult's law or Henry's law are not appropriate assume the components of the system behave independently and use the summation of all vapor pressures from the HAP's as the total HAP partial pressure. Chemical property data can be obtained from standard reference texts. Paragraph
(b)(5) of this section describes how direct measurement can be used to estimate emissions. If the owner or operator can demonstrate that the procedures in paragraphs (b)(1) through (b)(4) of this section are not appropriate to estimate emissions from a batch emission episode, emissions may be estimated using engineering assessment, as described in paragraph (b)(6) of this section. Owners or operators are not required to demonstrate that direct measurement is not appropriate before utilizing engineering assessment. Paragraph (b)(6)(ii) of this section describes how an owner or operator shall demonstrate that the procedures in paragraphs (b)(1) through (b)(4) of this section are not appropriate. Emissions from a batch cycle shall be calculated in accordance with paragraph (b)(7) of this section, and annual emissions from the batch process vent shall be calculated in accordance with paragraph (b)(8) of this section.

(1) TOC or organic HAP emissions from the purging of an empty vessel shall be calculated using Equation 2 of this subpart. Equation 2 of this subpart does not take into account evaporation of any residual liquid in the vessel.

\[
E_{\text{episode}} = \frac{(V_{\text{ves}})(P)(M_{\text{wavg}})}{RT} (1 - 0.37^m) \quad \text{[Eq. 2]}
\]

where:

- \(E_{\text{episode}}\) = Emissions, kg/episode.
- \(V_{\text{ves}}\) = Volume of vessel, m\(^3\).
- \(P\) = TOC or total organic HAP partial pressure, kPa.
- \(M_{\text{wavg}}\) = Weighted average molecular weight of TOC or organic HAP in vapor, determined in accordance with paragraph (b)(4)(iii) of this section, kg/kmol.
- \(R\) = Ideal gas constant, 8.314 m\(^3\)kPa/kmol·K.
- \(T\) = Temperature of vessel vapor space, K.
- \(m\) = Number of volumes of purge gas used.

(2) TOC or organic HAP emissions from the purging of a filled vessel shall be calculated using Equation 3 of this subpart.

\[
E_{\text{episode}} = \frac{(y)(V_{\text{ves}})(P^2)(M_{\text{wavg}})}{RT} \left( P - \sum_{i=1}^{n} P_i X_i \right) \quad \text{[Eq. 3]}
\]

where:

- \(E_{\text{episode}}\) = Emissions, kg/episode.
- \(y\) = Saturated mole fraction of all TOC or organic HAP in vapor phase.
- \(V_{\text{ves}}\) = Volumetric gas displacement rate, m\(^3\)/min.
- \(P\) = Pressure in vessel vapor space, kPa.
- \(M_{\text{wavg}}\) = Weighted average molecular weight of TOC or organic HAP in vapor, determined in accordance with paragraph (b)(4)(iii) of this section, kg/kmol.
- \(R\) = Ideal gas constant, 8.314 m\(^3\)kPa/kmol·K.
- \(T\) = Temperature of vessel vapor space, K.
- \(P_i\) = Vapor pressure of TOC or individual organic HAP i in the liquid.
- \(X_i\) = Mole fraction of TOC or organic HAP i in stream.
- \(n\) = Number of organic HAP in stream.

\text{NOTE:} \ Summation not required if TOC emissions are being estimated.
or out of a vessel shall be calculated using Equation 4 of this subpart.

\[ E_{\text{episode}} = \frac{yV(P)(\text{MW}_{\text{wavg}})}{RT} \]  

where:

- \( E_{\text{episode}} \) = Emissions, kg/episode.
- \( y \) = Saturated mole fraction of all TOC or organic HAP in vapor phase.
- \( V \) = Volume of gas displaced from the vessel, m\(^3\).
- \( P \) = Pressure in vessel vapor space, kPa.
- \( \text{MW}_{\text{wavg}} \) = Weighted average molecular weight of TOC or organic HAP in vapor, determined in accordance with paragraph (b)(4)(i)(D) of this section, kg/kmol.
- \( R \) = Ideal gas constant, 8.314 m\(^3\)kPa/(kmol \( \cdot \)K).
- \( T \) = Temperature of vessel vapor space, K.

(4) Emissions caused by the heating of a vessel shall be calculated using the procedures in either paragraphs (b)(4)(i), (b)(4)(ii), or (b)(4)(iii) of this section, as appropriate.

(i) If the final temperature to which the vessel contents is heated is lower than 50 K below the boiling point of the HAP in the vessel, then emissions shall be calculated using the equations in paragraphs (b)(4)(i)(A) through (b)(4)(i)(D) of this section.

(A) Emissions caused by heating of a vessel shall be calculated using Equation 5 of this subpart. The assumptions made for this calculation are atmospheric pressure of 760 millimeters of mercury (mm Hg) and the displaced gas is always saturated with volatile organic compounds (VOC) vapor in equilibrium with the liquid mixture.

\[ E_{\text{episode}} = \left( \sum_{i=1}^{n} \frac{(P_i)_{T_1}}{101.325} \right) - \left( \sum_{i=1}^{n} \frac{(P_i)_{T_2}}{101.325} \right) \begin{bmatrix} \Delta_n \left( \text{MW}_{\text{wavg}} \right) \end{bmatrix} \]  

where:

- \( E_{\text{episode}} \) = Emissions, kg/episode.
- \( (P_i)_{T_1} \) and \( (P_i)_{T_2} \) = Partial pressure (kPa) of TOC or each organic HAP i in the vessel headspace at initial (T1) and final (T2) temperature.
- \( n \) = Number of organic HAP in stream.
- \( \Delta_n \) = Number of kilogram-moles (kg-moles) of gas displaced, determined in accordance with paragraph (b)(4)(i)(D) of this section, kg/kmol.

(B) The moles of gas displaced, \( \Delta_n \), is calculated using Equation 6 of this subpart.

\[ \Delta_n = \frac{V_n}{R} \left( \frac{P_{a_1}}{T_1} - \frac{P_{a_2}}{T_2} \right) \]  

where:

- \( \Delta_n \) = Number of kg-moles of gas displaced.
- \( V_n \) = Volume of free space in the vessel, m\(^3\).
- \( R \) = Ideal gas constant, 8.314 m\(^3\)kPa/(kmol \( \cdot \)K).
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Pa₁=Initial noncondensible gas pressure in the vessel, kPa.
Pa₂=Final noncondensible gas pressure, kPa.
T₁=Initial temperature of vessel, K.
T₂=Final temperature of vessel, K.

(C) The initial and final pressure of the noncondensible gas in the vessel shall be calculated using Equation 7 of this subpart.

\[ Pa = 101.325 - \sum_{i=1}^{n} (P_i)_{T} \]  
[Eq. 7]

where:

\[ C=\text{TOC or organic HAP component} \]
\[ n=\text{Number of TOC or organic HAP components in stream} \]

(MW)_{wavg} = \sum_{i=1}^{n} \frac{(\text{mass of } C)_i (\text{molecular weight of } C)_i}{\sum_{i=1}^{n} (\text{mass of } C)_i}  
[Eq. 8]

where:

\[ C=\text{TOC or organic HAP component} \]
\[ n=\text{Number of TOC or organic HAP components in stream} \]

(D) The weighted average molecular weight of TOC or organic HAP in the displaced gas, \( MW_{wavg} \), shall be calculated using Equation 8 of this subpart.

(ii) If the vessel contents are heated to a temperature greater than 50 K below the boiling point, then emissions from the heating of a vessel shall be calculated as the sum of the emissions calculated in accordance with paragraphs (b)(4)(ii)(A) and (b)(4)(ii)(B) of this section.

(A) For the interval from the initial temperature to the temperature 50 K below the boiling point, emissions shall be calculated using Equation 5 of this subpart, where \( T_{2} \) is the temperature 50 K below the boiling point.

(B) For the interval from the temperature 50 K below the boiling point to the final temperature, emissions shall be calculated as the summation of emissions for each 5 K increment, where the emissions for each increment shall be calculated using Equation 5 of this subpart.

(i) If the final temperature of the heatup is lower than 5 K below the boiling point, the final temperature for the last increment shall be the final temperature of the heatup, even if the last increment is less than 5 K.

(ii) If the final temperature of the heatup is higher than 5 K below the boiling point, the final temperature for the last increment shall be the temperature 5 K below the boiling point, even if the last increment is less than 5 K.

(iii) If the vessel contents are heated to the boiling point and the vessel is not operating with a condenser, the primary condenser, as specified in paragraph (a)(2) of this section, is considered part of the process. Emissions shall be calculated as the sum of emissions calculated using Equation 5 of this subpart, which calculates emissions due to heating the vessel contents to the temperature of the gas existing the condenser, and emissions calculated using Equation 4 of this subpart, which calculates emissions due to the displacement of the remaining saturated noncondensible gas in the...
vessel. The final temperature in Equation 5 of this subpart shall be set equal to the exit gas temperature of the condenser. Equation 4 of this subpart shall be used as written below in Equation 4a of this subpart, using free space volume, and T is set equal to the condenser exit gas temperature.

\[
E_{\text{episode}} = \frac{(y)(V_f)(P)(MW_{wavg})}{RT} \quad \text{[Eq. 4a]}
\]

where:
- \( E_{\text{episode}} \) = Emissions, kg/episode.
- \( y \) = Saturated mole fraction of all TOC or organic HAP in vapor phase.
- \( V_f \) = Volume of the free space in the vessel, m³.
- \( P \) = Pressure in vessel vapor space, kPa.
- \( MW_{wavg} \) = Weighted average molecular weight of TOC or organic HAP in vapor, determined in accordance with paragraph (b)(4)(i)(D) of this section, kg/kmol.
- \( R \) = Ideal gas constant, 8.314 m³/kg/kmol/°K.
- \( T \) = Temperature of condenser exit stream, K.

The owner or operator may estimate annual emissions for a batch emission episode by direct measurement. If direct measurement is used, the owner or operator shall either perform a test for the duration of a representative batch emission episode or perform a test during only those periods of the batch emission episode for which the emission rate for the entire episode can be determined or for which the emissions are greater than the average emission rate of the batch emission episode. The owner or operator choosing either of these options must develop an emission profile for the entire batch emission episode, based on either process knowledge or test data collected, to demonstrate that test periods are representative. Examples of information that could constitute process knowledge include calculations based on material balances and process stoichiometry. Previous test results may be used provided the results are still relevant to the current batch process vent conditions. Performance tests shall follow the procedures specified in paragraphs (b)(5)(i) through (b)(5)(iii) of this section. The procedures in either paragraph (b)(5)(iv) or (b)(5)(v) of this section shall be used to calculate the emissions per batch emission episode.

(i) Method 1 or 1A, 40 CFR part 60, appendix A as appropriate, shall be used for selection of the sampling sites if the flow measuring device is a pitot tube. No traverse is necessary when Method 2A or 2D, 40 CFR part 60, appendix A is used to determine gas stream volumetric flow rate.

(ii) Gas stream volumetric flow rate and/or average flow rate shall be determined as specified in paragraph (e) of this section.

(iii) Method 18 or Method 25A, 40 CFR part 60, appendix A, shall be used to determine the concentration of TOC or organic HAP, as appropriate. Alternatively, any other method or data that has been validated according to the applicable procedures in Method 301 of appendix A of this part may be used. The use of Method 25A, 40 CFR part 60, appendix A shall comply with paragraphs (b)(5)(iii)(A) and (b)(5)(iii)(B) of this section.

(A) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A shall be the single organic HAP representing the largest percent by volume of the emissions.

(B) The use of Method 25A, 40 CFR part 60, appendix A is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(iv) If an integrated sample is taken over the entire batch emission episode to determine TOC or average total organic HAP concentration, emissions shall be calculated using Equation 9 of this subpart.
where:
\( E_{\text{episode}} \) = Emissions, kg/episode.
\( K \) = Constant, \( 2.494 \times 10^{-6} \) (ppmv)\(^{-1}\) (gm-mole/scm) (kg/gm) (min/hr), where standard temperature is 20°C.
\( C_j \) = Average concentration of TOC or sample organic HAP component \( j \) of the gas stream, dry basis, ppmv.
\( M_j \) = Molecular weight of TOC or sample organic HAP component \( j \) of the gas stream, gm/gm-mole.
\( AFR \) = Average flow rate of gas stream, dry basis, scmm.
\( T_h \) = Hours/episode.
\( n \) = Number of organic HAP in stream.

**NOTE:** Summation not required if TOC emissions are being estimated using a TOC concentration measured using Method 25A, 40 CFR part 60, appendix A.

(v) If grab samples are taken to determine TOC or average total organic HAP concentration, emissions shall be calculated according to paragraphs (b)(5)(v)(A) and (b)(5)(v)(B) of this section.

(A) For each measurement point, the emission rate shall be calculated using Equation 10 of this subpart.

\[
E_{\text{point}} = K \left[ \sum_{j=1}^{n} \left( C_j \right) \left( M_j \right) \right] \times \left( \text{FR} \right) \quad [\text{Eq. 10}]
\]

where:
\( E_{\text{point}} \) = Emission rate for individual measurement point, kg/hr.
\( K \) = Constant, \( 2.494 \times 10^{-6} \) (ppmv)\(^{-1}\) (gm-mole/scm) (kg/gm) (min/hr), where standard temperature is 20°C.
\( C_j \) = Concentration of TOC or sample organic HAP component \( j \) of the gas stream, dry basis, ppmv.
\( M_j \) = Molecular weight of TOC or sample organic HAP component \( j \) of the gas stream, gm/gm-mole.
\( \text{FR} \) = Flow rate of gas stream for the measurement point, dry basis, scmm.
\( n \) = Number of organic HAP in stream.

**NOTE:** Summation not required if TOC emissions are being estimated using a TOC concentration measured using Method 25A, 40 CFR part 60, appendix A.

(B) The emissions per batch emission episode shall be calculated using Equation 11 of this subpart.

\[
E_{\text{episode}} = \left( \text{DUR} \right) \sum_{i=1}^{n} \left( E_i \right) \quad [\text{Eq. 11}]
\]

where:
\( E_{\text{episode}} \) = Emissions, kg/episode.
\( \text{DUR} \) = Duration of the batch emission episode, hr/episode.
\( E_i \) = Emissions for measurement point \( i \), kg/hr.
\( n \) = Number of measurements.

If the owner or operator can demonstrate that the methods in paragraphs (b)(1) through (b)(4) of this section are not appropriate to estimate emissions for a batch emissions episode, the owner or operator may use engineering assessment to estimate emissions as specified in paragraphs (b)(6)(i) and (b)(6)(ii) of this section. All data, assumptions, and procedures used in an engineering assessment shall be documented.

(i) Engineering assessment includes, but is not limited to, the following:

(A) Previous test results, provided the tests are representative of current operating practices;

(B) Bench-scale or pilot-scale test data representative of the process under representative operating conditions;

(C) Flow rate, TOC emission rate, or organic HAP emission rate specified or implied within a permit limit applicable to the batch process vent; and

(D) Design analysis based on accepted chemical engineering principles, measurable process parameters, or physical or chemical laws or properties. Examples of analytical methods include, but are not limited to:

1. Use of material balances;

2. Estimation of flow rate based on physical equipment design such as pump or blower capacities; and
(3) Estimation of TOC or organic HAP concentrations based on saturation conditions.

(ii) The emissions estimation equations in paragraphs (b)(1) through (b)(4) of this section shall be considered inappropriate for estimating emissions for a given batch emissions episode if one or more of the criteria in paragraphs (b)(6)(ii)(A) through (b)(6)(ii)(B) of this section are met.

(A) Previous test data are available that show a greater than 20 percent discrepancy between the test value and the estimated value.

(B) The owner or operator can demonstrate to the Administrator that the emissions estimation equations are not appropriate for a given batch emissions episode.

(C) Data or other information supporting a finding that the emissions estimation equations are inappropriate as specified under paragraph (b)(6)(ii)(A) of this section shall be reported in the Notification of Compliance Status, as required in §63.1335(e)(5).

(D) Data or other information supporting a finding that the emissions estimation equations are inappropriate as specified under paragraph (b)(6)(ii)(B) of this section shall be reported in the Precompliance Report, as required in §63.1335(e)(3).

(7) For each batch process vent, the TOC or organic HAP emissions associated with a single batch cycle shall be calculated using Equation 12 of this subpart.

\[
E_{\text{cycle}} = \sum_{i=1}^{n} E_{\text{episode},i} \quad \text{[Eq. 12]}
\]

where:
- \(E_{\text{cycle}}\) = Emissions for an individual batch cycle, kg/batch cycle
- \(E_{\text{episode},i}\) = Emissions from batch emission episode \(i\), kg/episode
- \(n\) = Number of batch emission episodes for the batch cycle

(8) Annual TOC or organic HAP emissions from a batch process vent shall be calculated using Equation 13 of this subpart.

\[
AE = \sum_{i=1}^{n} (N_i)\left(E_{\text{cycle},i}\right) \quad \text{[Eq. 13]}
\]

where:
- \(AE\) = Annual emissions from a batch process vent, kg/yr.
- \(N_i\) = Number of type \(i\) batch cycles performed annually, cycles/yr
- \(E_{\text{cycle},i}\) = Emissions from the batch process vent associated with a single type \(i\) batch cycle, as determined in paragraph (b)(7) of this section, kg/batch cycle
- \(n\) = Number of different types of batch cycles that cause the emission of TOC or organic HAP from the batch process vent

(c) [Reserved]

(d) Minimum emission level exemption.
A batch process vent with annual emissions less than 11,800 kg/yr is considered a Group 2 batch process vent and the owner or operator of said batch process vent shall comply with the requirements in §63.1322 (f) or (g). The owner or operator of said batch process vent is not required to comply with the provisions in paragraphs (e) through (g) of this section.

(e) Determination of average flow rate.
The owner or operator shall determine the average flow rate for each batch emission episode in accordance with one of the procedures provided in paragraphs (e)(1) through (e)(2) of this section. The annual average flow rate for a batch process vent shall be calculated as specified in paragraph (e)(3) of this section.

(1) Determination of the average flow rate for a batch emission episode by direct measurement shall be made using the procedures specified in paragraphs (e)(1)(i) through (e)(1)(iii) of this section.

(i) The volumetric flow rate for a batch emission episode, in standard cubic meters per minute (scmm) at 20°C, shall be determined using Method 2A, 2C, or 2D, 40 CFR part 60, appendix A, as appropriate.

(ii) The volumetric flow rate of a representative batch emission episode shall be measured every 15 minutes.

(iii) The average flow rate for a batch emission episode shall be calculated using Equation 14 of this subpart.
where:

\[
AFR_{\text{episode}} = \frac{\sum_{i=1}^{n} FR_i}{n} \quad [\text{Eq. 14}]
\]

\[
AFR_{\text{DUR}} = AFR_{\text{episode},i} \quad [\text{Eq. 15}]
\]

\[
CFR = (0.00437) (AE) - 5.6 \quad [\text{Eq. 16}]
\]

where:

\(AFR_{\text{episode}}\) = Average flow rate for the batch emission episode, scmm.

\(FR_i\) = Flow rate for individual measurement \(i\), scmm.

\(n\) = Number of flow rate measurements taken during the batch emission episode.

(2) The average flow rate for a batch emission episode may be determined by engineering assessment, as defined in paragraph (b)(6)(i) of this section. All data, assumptions, and procedures used shall be documented.

(3) The annual average flow rate for a batch process vent shall be calculated using Equation 15 of this subpart.

\[
AFR = \frac{\sum_{i=1}^{n} (DUR_i)(AFR_{\text{episode},i})}{\sum_{i=1}^{n} (DUR_i)} \quad [\text{Eq. 15}]
\]

where:

\(AFR\) = Annual average flow rate for the batch process vent, scmm.

\(DUR_i\) = Duration of type \(i\) batch emission episodes annually, hrs/yr.

\(AFR_{\text{episode},i}\) = Average flow rate for type \(i\) batch emission episode, scmm.

\(n\) = Number of types of batch emission episodes venting from the batch process vent.

(f) Determination of cutoff flow rate.

For each batch process vent, the owner or operator shall calculate the cutoff flow rate using Equation 16 of this subpart.

\[
CFR = (0.00437) (AE) - 5.6 \quad [\text{Eq. 16}]
\]

where:

\(CFR\) = Cutoff flow rate, scmm.

\(AE\) = Annual TOC or organic HAP emissions, as determined in paragraph (b)(8) of this section, kg/yr.

(g) Group 1/Group 2 status determination. The owner or operator shall compare the cutoff flow rate, calculated in accordance with paragraph (f) of this section, with the annual average flow rate, determined in accordance with paragraph (e)(4) of this section. The group determination status for each batch process vent shall be made using the criteria specified in paragraphs (g)(1) and (g)(2) of this section.

(1) If the cutoff flow rate is greater than or equal to the annual average flow rate of the stream, the batch process vent is classified as a Group 1 batch process vent.

(2) If the cutoff flow rate is less than the annual average flow rate of the stream, the batch process vent is classified as a Group 2 batch process vent.

(h) Determination of halogenation status. To determine whether a batch process vent or an aggregate batch vent stream is halogenated, the annual mass emission rate of halogen atoms contained in organic compounds shall be calculated using the procedures specified in paragraphs (h)(1) through (h)(3) of this section.

(1) The concentration of each organic compound containing halogen atoms (ppmv, by compound) for each batch emission episode shall be determined based on any one of the following procedures:

(i) Process knowledge that no halogens or hydrogen halides are present in the process may be used to demonstrate that a batch emission episode is nonhalogenated. Halogens or hydrogen halides that are unintentionally introduced into the process shall not be considered in making a finding that a batch emission episode is nonhalogenated.

(ii) Engineering assessment as discussed in paragraph (b)(6)(i) of this section.

(iii) Concentration of organic compounds containing halogens and hydrogen halides as measured by Method 26 or 26A, 40 CFR part 60, appendix A.

(iv) Any other method or data that has been validated according to the applicable procedures in Method 301 of appendix A of this part.

(2) The annual mass emissions of halogen atoms for a batch process vent shall be calculated using Equation 17 of this subpart.
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\[ E_{\text{halogen}} = K \left[ \sum_{j=1}^{n} \sum_{i=1}^{m} \left( C_{\text{avg}j} \right) \left( L_{j,i} \right) \left( M_{j,i} \right) \right] \text{AFR} \]  

[Eq. 17]

where:

\( E_{\text{halogen}} \) = Mass of halogen atoms, dry basis, kg/yr.

\( K \) = Constant, 0.022 (ppmv)^{-1} (kg-mole per scm) (minute/yr), where standard temperature is 20°C.

\( \text{AFR} \) = Annual average flow rate of the batch process vent, determined according to paragraph (e) of this section, scmm.

\( M_{j,i} \) = Molecular weight of halogen atom \( i \) in compound \( j \), kg/mol.

\( L_{j,i} \) = Number of atoms of halogen \( i \) in compound \( j \).

\( n \) = Number of halogenated compounds \( j \) in the batch process vent.

\( m \) = Number of different halogens \( i \) in each compound \( j \) of the batch process vent.

\( C_{\text{avg}j} \) = Average annual concentration of halogenated compound \( j \) in the batch process vent as determined by using Equation 18 of this subpart, dry basis, ppmv.

\[ C_{\text{avg}j} = \frac{\sum_{i=1}^{n} \left( \text{DUR}_{i} \right) \left( C_{i} \right)}{\sum_{i=1}^{n} \left( \text{DUR}_{i} \right)} \]  

[Eq. 18]

where:

\( \text{DUR}_{i} \) = Duration of type \( i \) batch emission episodes annually, hrs/yr.

\( C_{i} \) = Average concentration of halogenated compound \( j \) in type \( i \) batch emission episode, ppmv.

\( n \) = Number of types of batch emission episodes venting from the batch process vent.

(3) The annual mass emissions of halogen atoms for an aggregate batch vent stream shall be the sum of the annual mass emissions of halogen atoms for all batch process vents included in the aggregate batch vent stream.

(i) Process changes affecting Group 2 batch process vents. Whenever process changes, as described in paragraph (i)(1) of this section, are made that affect one or more Group 2 batch process vents, the owner or operator shall comply with paragraphs (i) (2) and (3) of this section.

(1) Examples of process changes include, but are not limited to, changes in production capacity, production rate, feedstock type, or catalyst type; or whenever there is replacement, removal, or modification of recovery equipment considered part of the batch unit operation as specified in paragraph (a)(2) of this section. An increase in the annual number of batch cycles beyond the batch cycle limitation constitutes a process change. For purposes of this paragraph (i), process changes do not include: process upsets; unintentional, temporary process changes; and changes that are within the margin of variation on which the original group determination was based.

(2) For each batch process vent affected by a process change, the owner or operator shall redetermine the group status by repeating the procedures specified in paragraphs (b) through (g) of this section, as applicable; alternatively, engineering assessment, as described in paragraph (b)(6)(i) of this section, can be used to determine the effects of the process change.

(3) Based on the results from paragraph (i)(2) of this section, owners or operators shall comply with either paragraph (i)(3)(i), (ii), or (iii) of this section.

(i) If the redetermination described in paragraph (i)(2) of this section indicates that a Group 2 batch process vent has become a Group 1 batch process vent as a result of the process change, the owner or operator shall submit a report as specified in § 63.1327(b) and shall comply with the Group 1 provisions in § 63.1322 through § 63.1327 in accordance with the compliance schedule described in § 63.1335(e)(6)(iii)(D)(2).

(ii) If the redetermination described in paragraph (i)(2) of this section indicates that a Group 2 batch process vent with annual emissions less than the
§ 63.1324 Batch process vents—monitoring provisions.

(a) General requirements. Each owner or operator of a batch process vent or aggregate batch vent stream that uses a control device to comply with the requirements in §63.1322(a) or §63.1322(b), shall install the monitoring equipment specified in paragraph (c) of this section.

(i) If the redetermination described in paragraph (i)(2) of this section indicates no change in group status or no change in the relation of annual emissions to the levels specified in paragraph (d) of this section, the owner or operator shall submit a report as specified in §63.1327(c) and shall comply with §63.1322(f) in accordance with the compliance schedule required by §63.1335(e)(6)(iii)(D)(2).

(ii) If the redetermination described in paragraph (i)(2) of this section indicates a change in group status or a change in the relation of annual emissions to the levels specified in paragraph (d) of this section, the owner or operator shall submit a report as specified in §63.1327(c) and shall comply with §63.1322(f) in accordance with the compliance schedule required by §63.1335(e)(6)(iii)(D)(2).

§ 63.1324 Batch process vents—monitoring provisions.

(a) General requirements. Each owner or operator of a batch process vent or aggregate batch vent stream that uses a control device to comply with the requirements in §63.1322(a) or §63.1322(b), shall install the monitoring equipment specified in paragraph (c) of this section.

(i) If the redetermination described in paragraph (i)(2) of this section indicates no change in group status or no change in the relation of annual emissions to the levels specified in paragraph (d) of this section, the owner or operator shall submit a report as specified in §63.1327(c) and shall comply with §63.1322(f) in accordance with the compliance schedule described in §63.1335(e)(6)(iii)(D)(2).

[61 FR 48229, Sept. 12, 1996, as amended at 64 FR 11549, Mar. 9, 1999]

§ 63.1324 Batch process vents—monitoring provisions.

(a) General requirements. Each owner or operator of a batch process vent or aggregate batch vent stream that uses a control device to comply with the requirements in §63.1322(a) or §63.1322(b), shall install the monitoring equipment specified in paragraph (c) of this section.

(i) If the redetermination described in paragraph (i)(2) of this section indicates no change in group status or no change in the relation of annual emissions to the levels specified in paragraph (d) of this section, the owner or operator shall submit a report as specified in §63.1327(c) and shall comply with §63.1322(f) in accordance with the compliance schedule described in §63.1335(e)(6)(iii)(D)(2).

[61 FR 48229, Sept. 12, 1996, as amended at 64 FR 11549, Mar. 9, 1999]
(ii) Where a catalytic incinerator is used, temperature monitoring devices shall be installed in the gas stream immediately before and after the catalyst bed.

(2) Where a flare is used, a device (including but not limited to a thermocouple, ultra-violet beam sensor, or infrared sensor) capable of continuously detecting the presence of a pilot flame is required.

(3) Where a boiler or process heater of less than 44 megawatts design heat input capacity is used, a temperature monitoring device in the firebox equipped with a continuous recorder is required. Any boiler or process heater in which all batch process vents or agglomerated batch vent streams are introduced with the primary fuel or are used as the primary fuel is exempt from this requirement.

(4) Where a scrubber is used with an incinerator, boiler, or process heater in concert with the combustion of halogenated batch process vents or halogenated aggregate batch vent streams, the following monitoring equipment is required for the scrubber.

(i) A pH monitoring device equipped with a continuous recorder to monitor the pH of the scrubber effluent.

(ii) A flow meter equipped with a continuous recorder shall be located at the scrubber influent to monitor the scrubber liquid flow rate.

(5) Where an absorber is used, a scrubbing liquid temperature monitoring device and a specific gravity monitoring device are required, each equipped with a continuous recorder.

(6) Where a condenser is used, a condenser exit temperature (product side) monitoring device equipped with a continuous recorder is required.

(7) Where a carbon adsorber is used, an integrating regeneration stream flow monitoring device having an accuracy of ±10 percent, capable of recording the total regeneration stream mass flow for each regeneration cycle; and a carbon bed temperature monitoring device, capable of recording the carbon bed temperature after each regeneration and within 15 minutes of completing any cooling cycle are required.

(8) As an alternate to paragraphs (c)(5) through (c)(7) of this section, the owner or operator may install an organic monitoring device equipped with a continuous recorder.

(d) Alternative monitoring parameters. An owner or operator of a batch process vent or aggregate batch vent stream may request approval to monitor parameters other than those required by paragraph (c) of this section. The request shall be submitted according to the procedures specified in §63.1335(f). Approval shall be requested if the owner or operator:

(1) Uses a control device other than those included in paragraph (c) of this section; or

(2) Uses one of the control devices included in paragraph (c) of this section, but seeks to monitor a parameter other than those specified in Table 7 of this subpart and paragraph (c) of this section.

(e) Monitoring of bypass lines. Owners or operators of a batch process vent or aggregate batch vent stream using a vent system that contains bypass lines that could divert emissions away from a control device used to comply with §63.1322(a) or §63.1322(b) shall comply with either paragraph (d)(1), (d)(2), or (d)(3) of this section. Equipment such as low leg drains, high point bleeds, analyzer vents, open-ended valves or lines, and pressure relief valves needed for safety purposes are not subject to this paragraph (e).

(1) Properly install, maintain, and operate a flow indicator that takes a reading at least once every 15 minutes. Records shall be generated as specified in §63.1326(e)(3). The flow indicator shall be installed at the entrance to any bypass line that could divert emissions away from the control device and to the atmosphere; or

(2) Secure the bypass line valve in the non-diverting position with a carseal or a lock-and-key type configuration. A visual inspection of the seal or closure mechanism shall be performed at least once every month to ensure that the valve is maintained in the non-diverting position and emissions are not diverted through the bypass line. Records shall be generated as specified in §63.1326(e)(4).

(3) Continuously monitor the bypass line valve position using computer monitoring and record any periods when the position of the bypass line
§ 63.1325 Batch process vents—performance test methods and procedures to determine compliance.

(a) Use of a flare. When a flare is used to comply with §§ 63.1322(a)(1), (a)(3), (b)(1), or (b)(3), the owner or operator shall comply with the flare provisions in § 63.11(b).

(b) Exceptions to performance tests. An owner or operator is not required to conduct a performance test when a control device specified in paragraphs (b)(1) through (b)(5) of this section is used to comply with §§ 63.1322(a)(2) or (a)(3). Further, if a performance test meeting the conditions specified in paragraph (b)(6) of this section has been conducted by the owner or operator, the results of said performance test may be submitted and a performance test, as required by this section, is not required.

(1) A boiler or process heater with a design heat input capacity of 44 megawatts or greater.

(2) A boiler or process heater where the vent stream is introduced with the primary fuel or is used as the primary fuel.

(3) A control device for which a performance test was conducted for determining compliance with a New Source Performance Standard (NSPS) and the test was conducted using the same procedures specified in this section and no process changes have been made since the test. Recovery devices used for controlling emissions from continuous process vents complying with § 63.1322(a)(3) are also eligible for the exemption described in this paragraph (b)(3).

(4) A boiler or process heater burning hazardous waste for which the owner or operator:

(i) Has been issued a final permit under 40 CFR part 270 and complies with the requirements of 40 CFR part 266, subpart H; or

(f) Establishment of parameter monitoring levels. Parameter monitoring levels for batch process vents and aggregate batch vent streams shall be established as specified in paragraphs (f)(1) through (f)(3) of this section. For continuous process vents complying with § 63.1322(a)(3), parameter monitoring levels shall be established as specified in § 63.1315(a), except as specified in paragraph (f)(4) of this section.

(1) For each parameter monitored under paragraph (c) of this section, the owner or operator shall establish a level, defined as either a maximum or minimum operating parameter as denoted in Table 8 of this subpart, that indicates proper operation of the control device. The level shall be established in accordance with the procedures specified in § 63.1334.

(i) For batch process vents using a control device to comply with §§ 63.1322(a)(2), the established level shall reflect the control efficiency established as part of the initial compliance demonstration specified in § 63.1325(c)(2).

(ii) For aggregate batch vent streams using a control device to comply with §§ 63.1322(b)(2), the established level shall reflect the control efficiency requirement specified in § 63.1322(b)(2).

(iii) For batch process vents and aggregate batch vent streams using a control device to comply with §§ 63.1322(a)(3), the established level shall reflect the control efficiency established as part of the initial compliance demonstration specified in § 63.1325(f)(4).

(2) The established level, along with supporting documentation, shall be submitted in the Notification of Compliance Status or the operating permit application as required in § 63.1335(e)(5) or § 63.1335(e)(8), respectively.

(3) The operating day shall be defined as part of establishing the parameter monitoring level and shall be submitted with the information in paragraph (f)(2) of this section. The definition of operating day shall specify the times at which an operating day begins and ends. The operating day shall not exceed 24 hours.

(4) For continuous process vents using a control or recovery device to comply with § 63.1322(a)(3), the established level shall reflect the control efficiency established as part of the initial compliance demonstration specified in § 63.1325(f)(4).
(ii) Has certified compliance with the interim status requirements of 40 CFR part 266, subpart H.

(5) An incinerator burning hazardous waste for which the owner or operator complies with the requirements of 40 CFR part 264, subpart O.

(6) Performance tests done for other subparts in 40 CFR part 60 or part 63 where total organic HAP or TOC was measured, provided the owner or operator can demonstrate that operating conditions for the process and control device during the performance test are representative of current operating conditions.

(c) Batch process vent testing and procedures for compliance with § 63.1322(a)(2). Except as provided in paragraph (b) of this section, an owner or operator using a control device to comply with § 63.1322(a)(2) shall conduct a performance test using the procedures specified in paragraph (c)(1) of this section in order to determine the control efficiency of the control device. An owner or operator shall determine the percent reduction for the batch cycle using the control efficiency of the control device as specified in paragraphs (c)(2)(i) through (c)(2)(iii) of this section and the procedures specified in paragraph (c)(2) of this section. Compliance may be based on either total organic HAP or TOC. For purposes of this paragraph (c) and all paragraphs that are part of this paragraph (c), the term “batch emission episode” shall have the meaning “period of the batch emission episode selected for control,” which may be the entire batch emission episode or may only be a portion of the batch emission episode.

(1) Performance tests shall be conducted as specified in paragraphs (c)(1)(i) through (c)(1)(v) of this section.

(i) Except as specified in paragraph (c)(1)(i)(A) of this section, a test shall be performed for the entire period of each batch emission episode in the batch cycle that the owner or operator selects to control as part of achieving the required 90 percent emission reduction for the batch cycle specified in § 63.1322(a)(2). Only one test is required for each batch emission episode selected by the owner or operator for control. The owner or operator shall follow the procedures listed in paragraphs (c)(1)(i)(B) through (c)(1)(i)(D) of this section.

(A) Alternatively, an owner or operator may choose to test only those periods of the batch emission episode during which the emission rate for the entire episode can be determined or during which the emissions are greater than the average emission rate of the batch emission episode. The owner or operator choosing either of these options must develop an emission profile for the entire batch emission episode, based on either process knowledge or test data collected, to demonstrate that test periods are representative. Examples of information that could constitute process knowledge include calculations based on material balances and process stoichiometry. Previous test results may be used provided the results are still relevant to the current batch process vent conditions.

(B) Method 1 or 1A, 40 CFR part 60, appendix A, as appropriate, shall be used for selection of the sampling sites if the flow measuring device is a pitot tube. No traverse is necessary when Method 2A or 2D, 40 CFR part 60, appendix A is used to determine gas stream volumetric flow rate. Inlet sampling sites shall be located as specified in paragraphs (c)(1)(i)(B)(1) and (c)(1)(i)(B)(2) of this section. Outlet sampling sites shall be located at the outlet of the control device prior to release to the atmosphere.

(1) The control device inlet sampling site shall be located at the exit from the batch unit operation before any control device. § 63.1323(a)(2) describes those recovery devices considered part of the unit operation. Inlet sampling sites would be after those specified recovery devices.

(2) If a batch process vent is introduced with the combustion air or as a secondary fuel into a boiler or process heater with a design capacity less than 44 megawatts, selection of the location of the inlet sampling sites shall ensure the measurement of total organic HAP or TOC (minus methane and ethane) concentrations in all batch process vents and primary and secondary fuels introduced into the boiler or process heater.
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(C) Gas stream volumetric flow rate and/or average flow rate shall be determined as specified in § 63.1323(e).

(D) Method 18 or Method 25A, 40 CFR part 60, appendix A shall be used to determine the concentration of organic HAP or TOC, as appropriate. Alternatively, any other method or data that has been validated according to the applicable procedures in Method 301 of appendix A of this part may be used. The use of Method 25A, 40 CFR part 60, appendix A shall comply with paragraphs (c)(1)(i)(D)(1) and (c)(1)(i)(D)(2) of this section.

(1) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A shall be the single organic HAP representing the largest percent by volume of the emissions.

(2) The use of Method 25A, 40 CFR part 60, appendix A is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(ii) If an integrated sample is taken over the entire test period to determine TOC or average total organic HAP concentration, emissions per batch emission episode shall be calculated using Equations 19 and 20 of this subpart.

\[
E_{\text{episode.inlet}} = K \sum_{j=1}^{n} \left(C_{j,\text{inlet}} \left(M_{j} \right) \right) (AFR_{\text{inlet}}) (T_{h}) \quad \text{[Eq. 19]}
\]

\[
E_{\text{episode.outlet}} = K \sum_{j=1}^{n} \left(C_{j,\text{outlet}} \left(M_{j} \right) \right) (AFR_{\text{outlet}}) (T_{h}) \quad \text{[Eq. 20]}
\]

where:

\( E_{\text{episode}} = \) Inlet or outlet emissions, kg/episode.

\( K = \) Constant, \( 2.494 \times 10^{-6} \) (ppmv)\(^{-1}\) \((\text{gm-mole} / \text{scm}) \) \((\text{kg/gm}) \) \((\text{min/hr})\), where standard temperature is 20°C.

\( C_{j} = \) Average inlet or outlet concentration of TOC or sample component \( j \) of the gas stream for the batch emission episode, dry basis, ppmv.

\( M_{j} = \) Molecular weight of TOC or sample component \( j \) of the gas stream, gm/gm-mole.

\( AFR = \) Average inlet or outlet flow rate of gas stream for the batch emission episode, dry basis, scmm.

\( T_{h} = \) Hours/episode

\( n = \) Number of organic HAP in stream.

NOTE: Summation not required if TOC emissions are being estimated using a TOC concentration measured using Method 25A, 40 CFR part 60, appendix A.

(iii) If grab samples are taken to determine TOC or total organic HAP concentration, emissions shall be calculated according to paragraphs (c)(1)(iii) (A) and (B) of this section.

(A) For each measurement point, the emission rates shall be calculated using Equations 21 and 22 of this subpart.
\[ E_{\text{point,inlet}} = K \sum_{j=1}^{n} C_j M_j \text{FR}_{\text{inlet}} \quad [\text{Eq. 21}] \]

\[ E_{\text{point,outlet}} = K \sum_{j=1}^{n} C_j M_j \text{FR}_{\text{outlet}} \quad [\text{Eq. 22}] \]

where:
\[ E_{\text{point}} = \text{Inlet or outlet emission rate for the measurement point, kg/hr.} \]
\[ K = \text{Constant, } 2.494 \times 10^{-6} \text{ (ppmv)}^{-1} (\text{gm-mole/scm}) (\text{kg/gm}) (\text{min/hr}), \text{ where standard temperature is 20°C.} \]
\[ C_j = \text{Inlet or outlet concentration of TOC or sample organic HAP component j of the gas stream, dry basis, ppmv.} \]
\[ M_j = \text{Molecular weight of TOC or sample organic HAP component j of the gas stream, gm/gm-mole.} \]
\[ \text{FR} = \text{Inlet or outlet flow rate of gas stream for the measurement point, dry basis, scmm.} \]
\[ n = \text{Number of organic HAP in stream.} \]

**Note:** Summation not required if TOC emissions are being estimated using a TOC concentration measured using Method 25A, 40 CFR part 60, appendix A.

(B) The emissions per batch emission episode shall be calculated using Equations 23 and 24 of this subpart.

\[ E_{\text{episode,inlet}} = (\text{DUR}) \left[ \frac{\sum_{i=1}^{n} E_{\text{point,inlet},i}}{n} \right] \quad [\text{Eq. 23}] \]

\[ E_{\text{episode,outlet}} = (\text{DUR}) \left[ \frac{\sum_{i=1}^{n} E_{\text{point,outlet},i}}{n} \right] \quad [\text{Eq. 24}] \]

where:
\[ E_{\text{episode}} = \text{Inlet or outlet emissions, kg/episode.} \]
\[ \text{DUR} = \text{Duration of the batch emission episode, hr/episode.} \]
\[ E_{\text{point},i} = \text{Inlet or outlet emissions for measurement point i, kg/hr.} \]
\[ n = \text{Number of measurements.} \]

(iv) The control efficiency for the control device shall be calculated using Equation 25 of this subpart.
where:

- **R** = Control efficiency of control device, percent.
- **E_{inlet,i}** = Mass rate of TOC or total organic HAP for batch emission episode \(i\) at the inlet to the control device as calculated under paragraph (c)(1)(ii) or (c)(1)(iii) of this section, kg/hr.
- **E_{outlet,i}** = Mass rate of TOC or total organic HAP for batch emission episode \(i\) at the outlet of the control device, as calculated under paragraph (c)(1)(ii) or (c)(1)(iii) of this section, kg/hr.
- **n** = Number of batch emission episodes in the batch cycle selected to be controlled.

(v) If the batch process vent entering a boiler or process heater with a design capacity less than 44 megawatts is introduced with the combustion air or as a secondary fuel, the weight-percent reduction of total organic HAP or TOC across the device shall be determined by comparing the TOC or total organic HAP in all combusted batch process vents and primary and secondary fuels with the TOC or total organic HAP exiting the combustion device, respectively.

(2) The percent reduction for the batch cycle shall be determined using Equation 26 of this subpart and the control device efficiencies specified in paragraphs (c)(2)(i) through (c)(2)(iii) of this section. All information used to calculate the batch cycle percent reduction, including a definition of the batch cycle identifying all batch emission episodes, must be recorded as specified in §63.1326(b)(2). This information shall include identification of those batch emission episodes, or portions thereof, selected for control.

\[
PR = \frac{\sum_{i=1}^{n} E_{inlet,con} - (1-R) \sum_{i=1}^{n} E_{inlet,con}}{\sum_{i=1}^{n} E_{inlet} + \sum_{i=1}^{n} E_{inlet,con}} \times 100 \tag{Eq. 26}
\]

where:

- **PR** = Percent reduction
- **E_{unc,i}** = Mass rate of TOC or total organic HAP for uncontrolled batch emission episode \(i\), kg/hr.
- **E_{inlet,con,i}** = Mass rate of TOC or total organic HAP for controlled batch emission episode \(i\) at the inlet to the control device, kg/hr.
- **R** = Control efficiency of control device as specified in paragraphs (c)(2)(i) through (c)(2)(iii) of this section.
- **n** = Number of uncontrolled batch emission episodes, controlled batch emission episodes, and control devices. The value of \(n\) is not necessarily the same for these three items.

(i) If a performance test is required by paragraph (c) of this section, the control efficiency of the control device shall be as determined in paragraph (c)(3)(iv) of this section.

(ii) If a performance test is not required by paragraph (c) of this section for a combustion control device, as specified in paragraph (b) of this section, the control efficiency shall be 98
percent. The control efficiency for a flare shall be 98 percent.

(iii) If a performance test is not required by paragraph (c) of this section for a noncombustion control device, the control efficiency shall be determined by the owner or operator based on engineering assessment.

(d) Batch process vent and aggregate batch vent stream testing for compliance with §63.1322(c) [halogenated emission streams]. An owner or operator controlling halogenated emissions in compliance with §63.1322(c) shall conduct a performance test to determine compliance with the control efficiency specified in §63.1322(c)(1) or the emission limit specified in §63.1322(c)(2) for hydrogen halides and halogens.

(1) Sampling sites shall be located at the inlet and outlet of the scrubber or other control device used to reduce halogen emissions in complying with §63.1322(c)(1) or at the outlet of the control device used to reduce halogen emissions in complying with §63.1322(c)(2).

(2) The mass emissions of each hydrogen halide and halogen compound for the batch cycle or aggregate batch vent stream shall be calculated from the measured concentrations and the gas stream flow rate(s) determined by the procedures specified in paragraphs (d)(2)(i) and (d)(2)(ii) of this section except as specified in paragraph (d)(5) of this section.

(i) Method 26 or Method 26A, 40 CFR part 60, appendix A, shall be used to determine the concentration, in Mg per dry scm, of total hydrogen halides and halogens present in the emissions stream.

(ii) Gas stream volumetric flow rate and/or average flow rate shall be determined as specified in §63.1323(e).

(3) To determine compliance with the percent reduction specified in §63.1322(c)(1), the mass emissions for any hydrogen halides and halogens present at the inlet of the scrubber or other control device shall be summed together. The mass emissions of any hydrogen halides or halogens present at the outlet of the scrubber or other control device shall be summed together. Percent reduction shall be determined by subtracting the outlet mass emissions from the inlet mass emissions and then dividing the result by the inlet mass emissions.

(4) To determine compliance with the emission limit specified in §63.1322(c)(2), the annual mass emissions for any hydrogen halides and halogens present at the outlet of the control device and prior to any combustion device shall be summed together and compared to the emission limit specified in §63.1322(c)(2).

(5) The owner or operator may use any other method to demonstrate compliance if the method or data has been validated according to the applicable procedures of Method 301 of appendix A of this part.

(e) Aggregate batch vent stream testing for compliance with §63.1322(b)(2) or (b)(3). Except as specified in paragraphs (e)(1) through (e)(3) of this section, owners or operators of aggregate batch vent streams complying with §63.1322(b)(2) or (b)(3) shall conduct a performance test using the performance testing procedures for continuous process vents in §63.116(c).

(1) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A, shall be the single organic HAP representing the largest percent by volume of the emissions.

(2) The use of Method 25A, 40 CFR part 60, appendix A, is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(3) When a combustion device is used to comply with the 20 parts per million by volume outlet concentration standard specified in §63.1322(b)(2), the correction to 3 percent oxygen specified in the performance testing procedures of §63.116(c)(3) and §63.116(c)(3)(iii) is only required when supplemental combustion air is used to combust the emissions, for the purposes of this subpart.

(f) Compliance with §63.1322(a)(3) [new SAN batch affected sources]. Except as provided in paragraph (b) of this section, an owner or operator using a control or recovery device to comply with the percent reduction requirement in
§ 63.1322(a)(3) shall conduct performance tests as specified in either paragraph (f)(1), (f)(2), or (f)(3) of this section, as applicable. Compliance with § 63.1322(a)(3) shall be determined as specified in paragraph (f)(4) of this section.

(1) For batch process vents, performance tests shall be conducted using the procedures specified in paragraph (c) of this section, except that the owner or operator is not required to determine the percent reduction for the batch cycle as specified in paragraph (c)(2) of this section.

(2) For continuous process vents, performance tests shall be conducted as required by the applicable requirements of § 63.1315(a) as specified in § 63.1321(b).

(3) For aggregate batch vent streams, performance tests shall be conducted as specified in paragraph (e) of this section.

(4) Compliance with the percent reduction requirement of § 63.1322(a)(3) shall be demonstrated using the procedures specified in § 63.1333(c) and the control device efficiencies specified in either paragraph (f)(4)(i) or (f)(4)(ii) of this section. Emissions for uncontrolled continuous process vents and aggregate batch vent streams shall be determined based on the direct measurement procedures specified in paragraph (f)(2) and (f)(3) of this section, respectively, or based on engineering assessment, as specified in § 63.1323(b)(6)(i). At the discretion of the owner or operator, emissions for uncontrolled batch process vents shall be determined based on any of the procedures in § 63.1323(b).

(i) For noncombustion devices, the control efficiency shall be as determined by the performance test required by paragraph (f)(1), (f)(2), or (f)(3) of this section. Alternatively, if a performance test is not required by paragraph (c) of this section, the control efficiency shall be determined by the owner or operator based on engineering assessment.

(ii) For combustion devices, the control efficiency shall be as determined by the performance test required by paragraph (f)(1), (f)(2), or (f)(3) of this section. Alternatively, if a performance test is not required, the control efficiency shall be 98 percent. The control efficiency for a flare shall be 98 percent.

(g) Batch cycle limitation. The batch cycle limitation required by § 63.1322(f) and (g) shall be established as specified in paragraph (g)(1) of this section and shall include the elements specified in paragraph (g)(2) of this section.

(1) The batch cycle limitation shall be determined by the owner or operator such that annual emissions for the batch process vent remain less than the level specified in § 63.1323(d) when complying with § 63.1322(g). Alternatively, when complying with § 63.1322(f), the batch cycle limitation shall ensure that annual emissions remain at a level such that said batch process vent remains a Group 2 batch process vent, given the actual annual flow rate for said batch process vent determined according to the procedures specified in § 63.1323(e). The batch cycle limitation shall be determined using the same basis, as described in § 63.1323[a](1), used to make the group determination (i.e., expected mix of products or worst-case HAP emitting product). The establishment of the batch cycle limitation is not dependent upon any past production or activity level.

(i) If the expected mix of products serves as the basis for the batch cycle limitation, the batch cycle limitation shall be determined such that any foreseeable combination of products which the owner or operator desires the flexibility to manufacture shall be allowed. Combinations of products not accounted for in the documentation required by paragraph (g)(2)(iv) of this section shall not be allowed within the restrictions of the batch cycle limitation.

(ii) If, for a batch process vent with more than one product, a single worst-case HAP emitting product serves as the basis for the batch cycle limitation, the batch cycle limitation shall be determined such that the maximum number of batch cycles the owner or operator desires the flexibility to accomplish, using the worst-case HAP emitting product and ensuring that the batch process vent remains a Group 2 batch process vent or that emissions remain less than the level specified in
§ 63.1326 Batch process vents—record-keeping provisions.

(a) Group determination records for batch process vents. Except as provided in paragraphs (a)(7) through (a)(9) of this section, each owner or operator of an affected source shall maintain the records specified in paragraphs (a)(1) through (a)(6) of this section for each batch process vent subject to the group determination procedures of § 63.1323.

Except for paragraph (a)(1) of this section, the records required by this paragraph (a) are restricted to the information developed and used to make the group determination under § 63.1323(b) through § 63.1323(g), as appropriate. The information required by paragraph (a)(1) of this section is required for all batch process vents subject to the group determination procedures of § 63.1323. If an owner or operator did not need to develop certain information (e.g., annual average flow rate) to determine the group status, this paragraph (a) does not require that additional information be developed.

(1) An identification of each unique product that has emissions from one or more batch emission episodes venting from the batch process vent.

(2) A description of, and an emission estimate for, each batch emission episode, and the total emissions associated with one batch cycle for each unique product identified in paragraph (a)(1) of this section that was considered in making the group determination under § 63.1323.

(3) Total annual uncontrolled TOC or organic HAP emissions, determined at the exit from the batch unit operation before any control device, determined in accordance with § 63.1323.

(i) For Group 2 batch process vents, said emissions shall be determined at the batch cycle limitation.

(ii) For Group 1 batch process vents, said emissions shall be those used to determine the group status of the batch process vent.

(4) The annual average flow rate for the batch process vent, determined in accordance with § 63.1323.

(i) For Group 2 batch process vents, said emissions shall be determined at the batch cycle limitation.

(ii) For Group 1 batch process vents, said emissions shall be those used to determine the group status of the batch process vent.

(5) The cutoff flow rate, determined in accordance with § 63.1323.

(6) The results of the batch process vent group determination, conducted in accordance with § 63.1323.

[61 FR 48229, Sept. 12, 1996, as amended at 64 FR 11549, Mar. 9, 1999]
(7) If a batch process vent is in compliance with §63.1322(a) or (b) and the control device is operating at all times when batch emission episodes are venting from the batch process vent, none of the records in paragraphs (a)(1) through (a)(6) of this section are required.

(8) If a batch process vent is in compliance with §63.1322(a) or (b), but the control device is operated only during selected batch emission episodes, only the records in paragraphs (a)(1) through (a)(3) of this section are required.

(9) If the total annual emissions from the batch process vent are less than the appropriate level specified in §63.1323(d), only the records in paragraphs (a)(1) through (a)(3) of this section are required.

(b) Compliance demonstration records. Each owner or operator of a batch process vent or aggregate batch vent stream complying with §63.1322(a) or (b), shall keep the following records, as applicable, up-to-date and readily accessible:

(1) The annual mass emissions of halogen atoms in the batch process vent or aggregate batch vent stream determined according to the procedures specified in §63.1323(h);

(2) If a batch process vent is in compliance with §63.1322(a)(2), records documenting the batch cycle percent reduction as specified in §63.1325(c)(2); and

(3) When using a flare to comply with §63.1322(a)(1), (a)(3), (b)(1), or (b)(3):

(i) The flare design (i.e., steam-assisted, air-assisted or non-assisted);

(ii) All visible emission readings, heat content determinations, flow rate measurements, and exit velocity determinations made during the compliance determination required by §63.1325(a); and

(iii) All periods during the compliance determination required by §63.1325(a) when the pilot flame is absent.

(4) The following information when using a control device to meet the percent reduction requirement specified in §63.1322(a)(2), (a)(3), (b)(2), or (b)(3):

(i) For an incinerator or non-combustion control device, the percent reduction of organic HAP or TOC achieved, as determined using the procedures specified in §63.1325(c) for batch process vents and §63.1325(e) for aggregate batch vent streams;

(ii) For a boiler or process heater, a description of the location at which the vent stream is introduced into the boiler or process heater;

(iii) For a boiler or process heater with a design heat input capacity of less than 44 megawatts and where the vent stream is introduced with combustion air or used as a secondary fuel and is not mixed with the primary fuel, the percent reduction of organic HAP or TOC achieved, as determined using the procedures specified in §63.1325(c) for batch process vents and §63.1325(e) for aggregate batch vent streams; and

(iv) For a scrubber or other control device following a combustion device to control halogenated batch process vents or halogenated aggregate batch vent streams, the percent reduction of total hydrogen halides and halogens as determined under §63.1325(d)(3) or the emission limit determined under §63.1325(d)(4).

(5) When complying with the 20 parts per million by volume outlet concentration standard specified in §63.1322(b)(2), records of the outlet concentration of organic HAP or TOC on a dry basis. If supplemental combustion air is used to combust the emissions, the outlet concentration shall be corrected to 3 percent oxygen. If supplemental combustion air is not used, a correction to 3 percent oxygen is not required.

(c) Establishment of parameter monitoring level records. For each parameter monitored according to §63.1324(c) and Table 7 of this subpart, or for alternate parameters and/or parameters for alternate control devices monitored according to §63.1327(f) as allowed under §63.1324(d), maintain documentation showing the establishment of the level that indicates proper operation of the control device as required by §63.1324(f) for parameters specified in §63.1324(c) and as required by §63.1335(e) for alternate parameters. Said documentation shall include the parameter monitoring data used to establish the level.

(d) Group 2 batch process vent continuous compliance records. The owner or operator of a Group 2 batch process
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Controlled batch process vent continuous compliance records.

Each owner or operator of a batch process vent that uses a control device to comply with § 63.1322(a) shall keep the following records, as applicable, up-to-date and readily accessible:

1. Continuous records of the equipment operating parameters specified to be monitored under § 63.1324(c) as applicable, and listed in Table 7 of this subpart, or specified by the Administrator in accordance with § 63.1322(f) as allowed under § 63.1324(d). Said records shall be kept as specified under § 63.1335(d), except as specified in paragraphs (e)(1)(i) and (e)(1)(ii) of this section.

(i) For flares, the records specified in Table 7 of this subpart shall be kept rather than averages.

(ii) For carbon adsorbers, the records specified in Table 7 of this subpart shall be kept rather than averages.

2. Records of the batch cycle daily average value of each continuously monitored parameter, except as provided in paragraph (e)(2)(iii) of this section, as calculated using the procedures specified in paragraphs (e)(2)(i) through (e)(2)(iii) of this section.

(i) The batch cycle daily average shall be calculated as the average of all parameter values measured for an operating day during those batch emission episodes, or portions thereof, in the batch cycle that the owner or operator has selected to control.

(ii) Monitoring data recorded during periods of monitoring system breakdowns, repairs, calibration checks, and zero (low-level) and high-level adjustments shall not be included in computing the batch cycle daily averages.

(iii) If all recorded values for a monitored parameter during an operating day are above the minimum or below the maximum level established in accordance with § 63.1324(f), the owner or operator may record that all values were above the minimum or below the maximum level established rather than calculating and recording a batch cycle daily average for that operating day.

3. Hourly records of whether the flow indicator for bypass lines specified in § 63.1324(e)(1) was operating and whether a diversion was detected at any time during the hour. Also, records of the times of all periods when the vent is diverted from the control device or the flow indicator specified in § 63.1324(e)(1) is not operating.

4. Where a seal or closure mechanism is used to comply with § 63.1324(e)(2), the owner or operator shall record whether the monthly visual inspection of the seals or closure mechanisms has been done, and shall record the occurrence of all periods when the seal mechanism is broken, the bypass line valve position has changed, or the key for a lock-and-key type configuration has been checked out, and records of any car-seal that has broken.

(i) For compliance with § 63.1324(e)(2), the owner or operator shall record the times of all periods when the bypass line valve position has changed.

(ii) For compliance with § 63.1324(e)(3), the owner or operator shall record the times of all periods when the bypass line valve position has changed.

5. Records specifying the times and duration of periods of monitoring system breakdowns, repairs, calibration checks, and zero (low-level) and high-
§ 63.1327 Batch process vents—reporting requirements.

(a) The owner or operator of a batch process vent or aggregate batch vent stream at an affected source shall submit the information specified in paragraphs (a)(1) through (a)(4) of this section, as appropriate, as part of the Notification of Compliance Status specified in § 63.1335(e)(5).

(1) For each batch process vent complying with § 63.1322(a) and each aggregate batch vent stream complying with § 63.1322(b), the information specified in § 63.1326(b) and (c), as applicable.

(2) For each Group 2 batch process vent with annual emissions less than the level specified in § 63.1323(d), the information specified in § 63.1326(d)(1)(i).

(3) For each Group 2 batch process vent with annual emissions greater than or equal to the level specified in § 63.1323(d), the information specified in § 63.1326(d)(1)(i).

(4) For each batch process vent subject to the group determination procedures, the information specified in § 63.1326(a), as appropriate.

(b) Whenever a process change, as defined in § 63.1323(j)(1), is made that causes a Group 2 batch process vent to become a Group 1 batch process vent, the owner or operator shall submit a report within 180 operating days after the process change is known to the owner or operator. This report may be included in the next Periodic Report, as specified in § 63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(1) A description of the process change; and

(2) A schedule for compliance with the provisions of § 63.1322(a) or (b), as appropriate, as required under § 63.1335(e)(6)(iii)(D)(2).

(c) Whenever a process change, as defined in § 63.1323(j)(1), is made that causes a Group 2 batch process vent with annual emissions less than the level specified in § 63.1323(d) that is in compliance with § 63.1322(g) to have annual emissions greater than or equal to the level specified in § 63.1323(d) but remains a Group 2 batch process vent, the owner or operator shall submit a report within 180 operating days after the process change is known to the owner or operator. This report may be included in the next Periodic Report, as specified in § 63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(1) A description of the process change;

(2) The results of the redetermination of the annual emissions, average flow rate, and cutoff flow rate required under § 63.1323(i) and recorded under § 63.1326(a)(3) through (a)(5); and

(3) The batch cycle limitation determined in accordance with § 63.1322(f)(1).

(d) Whenever a process change, as defined in § 63.1323(j)(1), is made that causes the percent reduction for all process vents at a new SAN affected source using a batch process to be less than 84 percent, the owner or operator shall submit a report within 180 operating days after the process change is known to the owner or operator. This report may be included in the next Periodic Report, as specified in § 63.1335(e)(6)(iii)(D)(2). The following information shall be submitted:

(1) A description of the process change; and

(2) A schedule for compliance with the provisions of § 63.1322(a)(3), as required under § 63.1335(e)(6)(iii)(D)(2).

(e) The owner or operator is not required to submit a report of a process change.
§ 63.1329  Process contact cooling towers provisions.

(a) This section applies to each new affected source that manufactures PET and each existing affected source that manufactures PET using a continuous terephthalic acid high viscosity multiple end finisher process. The owner or operator a new affected source shall comply with paragraph (b) of this section. The owner or operator of an existing affected source that manufactures PET using a continuous terephthalic acid high viscosity multiple end finisher process shall comply with paragraph (c) of this section. The compliance data for process contact cooling towers subject to the provisions of this section is specified in §63.1311.

(b) New affected source requirements. The owner or operator of a new affected source subject to this section shall comply with paragraphs (b)(1) through (b)(2) of this section.

(1) The owner or operator of a new affected source subject to this section shall not send contact condenser effluent associated with a vacuum system to a process contact cooling tower.

(2) The owner or operator of a new affected source subject to this section shall indicate in the Notification of Compliance Status, as required in
§ 63.1335(e)(5), that contact condenser effluent associated with vacuum systems is not sent to process contact cooling towers.

(c) Existing affected source requirements. The owner or operator of an existing affected source subject to this section who manufactures PET using a continuous terephthalic acid high viscosity multiple end finisher process, and who is subject or becomes subject to 40 CFR part 60, subpart DDD, shall maintain an ethylene glycol concentration in the cooling tower at or below 4.0 percent by weight averaged on a daily basis over a rolling 14-day period of operating days. Compliance with this paragraph (c) shall be determined as specified in paragraphs (c)(1) through (c)(4) of this section.

(1) To determine the ethylene glycol concentration, owners or operators shall follow the procedures specified in 40 CFR 60.564(j)(1), except as provided in paragraph (c)(2) of this section. An average ethylene glycol concentration by weight shall be calculated on a daily basis over a rolling 14-day period of operating days. Each daily average ethylene glycol concentration so calculated constitutes a performance test. Exceedance of the standard during the reduced testing program specified in paragraph (b)(1)(ii) of this section is a violation of these standards.

(ii) The owner or operator may elect to reduce the sampling program to any 14 consecutive day period once every two calendar months, if at least seventeen consecutive 14-day rolling average concentrations immediately preceding the reduced sampling program are each less than 1.2 weight percent ethylene glycol. If the average concentration obtained over the 14 day sampling during the reduced test period exceeds the upper 95 percent confidence interval calculated from the most recent test results in which no one 14-day average exceeded 1.2 weight percent ethylene glycol, then the owner or operator shall reinstitute a daily sampling program. The 95 percent confidence interval shall be calculated as specified in paragraph (b)(1)(iii) of this section. A reduced program may be reinstituted if the requirements specified in this paragraph (c)(1)(ii) are met.

(iii) The upper 95 percent confidence interval shall be calculated using the Equation 27 of this subpart:

\[
CI_{95} = \frac{\sum_{i=1}^{n} X_i}{n} + 2 \sqrt{\frac{n \sum X_i^2 - \left( \sum X_i \right)^2}{n(n-1)}} \quad [\text{Eq. 27}]
\]

where:

\( X_i \) = daily ethylene glycol concentration for each day used to calculate each 14-day rolling average used in test results to justify implementing the reduced testing program.

\( n \) = number of ethylene glycol concentrations.

(2) Measuring an alternative parameter, such as carbon oxygen demand or biological oxygen demand, that is demonstrated to be directly proportional to the ethylene glycol concentration shall be allowed. Such parameter shall be measured during the initial 14-day performance test during which the facility is shown to be in compliance with the ethylene glycol concentration standard whereby the ethylene glycol concentration is determined using the procedures described in paragraph (b)(1) of this section. The alternative parameter shall be measured on a daily basis and the average value of the alternative parameter shall be calculated on a daily basis over a rolling 14-day period of operating days. Each daily average value of the alternative parameter constitutes a performance test.

(3) During each performance test, daily measurement and daily average 14-day rolling averages of the ethylene
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§ 63.1330 Wastewater provisions.

(a) The owner or operator of each affected source shall comply with the requirements of §§ 63.131 through 63.140, with the differences noted in paragraphs (a)(1) through (a)(12) of this section for the purposes of this subpart.

(1) When the determination of equivalence criteria in § 63.102(b) is referred to in §§ 63.132, 63.133, and 63.137, the provisions in § 63.6(g) shall apply.

(2) When the storage tank requirements contained in §§ 63.119 through 63.123 are referred to in §§ 63.132 through 63.148, §§ 63.119 through 63.123 are applicable, with the exception of the differences referred to in § 63.1314, for the purposes of this subpart.

(3) When the owner or operator requests to use alternatives to the continuous operating parameter monitoring and recordkeeping provisions referred to in § 63.151(g), or the owner or operator submits an operating permit application instead of an Implementation Plan as specified in § 63.151(e)(2) which specify that owners or operators shall demonstrate that 95 percent of the mass of HAP, as listed in Table 9 of subpart G of this part, is removed from the wastewater stream or combination of wastewater streams by the procedure specified in § 63.145(i) for a biological treatment unit.

(4) When the Notification of Compliance Status requirements contained in § 63.152(b) are referred to in §§ 63.146 and 63.147, the Notification of Compliance Status requirements contained in § 63.1335(e)(5) shall apply for the purposes of this subpart.

(5) When the Periodic Report requirements contained in § 63.152(c) are referred to in §§ 63.146 and 63.147, the Periodic Report requirements contained in § 63.1335(e)(6) shall apply for the purposes of this subpart.

(6) When the Initial Notification Plan requirements in § 63.151(b) are referred to in § 63.146, the owner or operator of an affected source subject to this subpart need not comply for the purposes of this subpart.

(7) When the Implementation Plan requirements contained in § 63.151 are referred to in § 63.146, the owner or operator of an affected source subject to this subpart need not comply for the purposes of this subpart.

(8) When the term “range” is used in § 63.143(f), the term “level” shall be used instead for the purposes of this subpart. This level shall be determined using the procedures specified in § 63.1334.

(9) For the purposes of this subpart, owners or operators are not required to comply with the provisions of § 63.138(j)(3) which specify that owners or operators shall use the procedures specified in appendix C of this part to demonstrate compliance when using a biological treatment unit.

(10) When the provisions of § 63.139(c)(1)(ii) or the provisions of § 63.145(e)(2)(ii)(B) specify that Method 18, 40 CFR part 60, appendix A, shall be used, Method 18 or Method 25A, 40 CFR part 60, appendix A, may be used for the purposes of this subpart. The use of Method 25A, 40 CFR part 60, appendix A, is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(11) When the provisions of § 63.139(c)(1)(ii) or the provisions of § 63.145(e)(2)(ii)(B) specify that Method 18, 40 CFR part 60, appendix A, shall be used, Method 25A, 40 CFR part 60, appendix A, may be used for the purposes of this subpart. The use of Method 25A, 40 CFR part 60, appendix A, shall comply with paragraphs (a)(11)(i) and (a)(11)(ii) of this section.

(i) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A, shall be the single organic HAP representing the largest percent by volume of the emissions.

(ii) The use of Method 25A, 40 CFR part 60, appendix A, is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(b) For each affected source, the owner or operator shall comply with the requirements for maintenance wastewater in § 63.105, except that when...
§ 63.1331 Equipment leak provisions.

(a) Except as provided in paragraphs (b) and (c) of this section, the owner or operator of each affected source shall comply with the requirements of subpart H of this part, with the differences noted in paragraphs (a)(1) through (a)(10) of this section.

(1) For an affected source producing polystyrene, the indications of liquids dripping, as defined in subpart H of this part, from bleed ports in pumps and agitator seals in light liquid service shall not be considered to be a leak. For purposes of this subpart, a “bleed port” is a technologically-required feature of the pump or seal whereby polymer fluid used to provide lubrication and/or cooling of the pump or agitator shaft exits the pump, thereby resulting in a visible dripping of fluid.

(2) The compliance date for the equipment leak provisions contained in this section is provided in § 63.1311.

(3) Owners and operators of an affected source subject to this subpart are not required to submit the Initial Notification required by § 63.182(a)(1) and § 63.182(b).

(4) The Notification of Compliance Status required by paragraphs § 63.182(a)(2) and § 63.182(c) shall be submitted within 150 days (rather than 90 days) of the applicable compliance date specified in § 63.1311 for the equipment leak provisions. Said notification can be submitted as part of the Notification of Compliance Status required by § 63.1335(e)(5).

(5) The Periodic Reports required by § 63.182(a)(3) and § 63.182(d) may be submitted as part of the Periodic Reports required by § 63.1335(e)(6).

(6) For an affected source producing PET, an owner or operator shall comply with the requirements of paragraphs (a)(6)(i) and (a)(6)(ii) of this section instead of with the requirements of § 63.169 for pumps, valves, connectors, and agitators in heavy liquid service; pressure relief devices in light liquid or heavy liquid service; and instrumentation systems.

(i) A leak is determined to be detected if there is evidence of a potential leak found by visual, audible, olfactory, or any other detection method except that Method 21, 40 CFR part 60, appendix A shall not be used to determine if a leak is detected.

(ii)(A) When a leak is detected, it shall be repaired as soon as practicable, but not later than 15 calendar days after it is detected, except as provided in § 63.171.

(B) The first attempt at repair shall be made no later than 5 calendar days after each leak is detected.

(C) Repaired shall mean that the visual, audible, olfactory, or other indications of a leak have been eliminated; that no bubbles are observed at potential leak sites during a leak check using soap solution; or that the system will hold a test pressure.

(7) For each affected source producing PET, an owner or operator is not required to develop an initial list of identification numbers for the equipment identified in paragraph (a)(6) of this section (i.e., pumps, valves, connectors, and agitators in heavy liquid service; pressure relief devices in light liquid or heavy liquid service; and instrumentation systems) as would otherwise be required under § 63.181(b)(1)(i).

(8) When the provisions of subpart H of this part specify that Method 18, 40 CFR part 60, appendix A, shall be used, Method 18 or Method 25A, 40 CFR part 60, appendix A, may be used for the purposes of this section. The use of Method 25A, 40 CFR part 60, appendix A, shall comply with paragraphs (a)(8)(i) and (a)(8)(ii) of this section.

(i) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A, shall be the single organic HAP representing the largest percent by volume of the emissions.
(ii) The use of Method 25A, 40 CFR part 60, appendix A, is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(9) For purposes of this subpart, bottoms receivers and surge control vessels are not considered equipment for purposes of this section and are not subject to the requirements of subpart H of this part.

(10) The owner or operator of each affected source shall substitute the phrase “the provisions of subparts F, I, or JJJ of this part” for both the phrases “the provisions of subparts F or I of this part” and the phrase “the provisions of subpart F or I of this part” throughout §§63.163 and 63.168, for the purposes of this subpart. In addition, the owner or operator of each affected source shall substitute the phrase “subparts F and I” in §63.174(c)(2)(iii), for the purposes of this subpart.

(b) The provisions of this section do not apply to each TPPU producing PET using a process other than a continuous terephthalic acid (TPA) high viscosity multiple end finisher process that is part of an affected source if all of the components in the TPPU are either in vacuum service or in heavy liquid service.

(1) Owners and operators of a TPPU exempted under paragraph (b) of this section shall retain at the facility information, data, and analyses used to demonstrate that all of the components in the exempted TPPU are either in vacuum service or in heavy liquid service.

(2) If changes occur at a TPPU exempted under paragraph (b) of this section such that all of the components in the TPPU are no longer either in vacuum service or in heavy liquid service (e.g., by either process changes or the addition of new components), the owner or operator shall comply with the provisions of this section for all of the components at the TPPU. The owner or operator shall submit a report within 180 days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included in the next Periodic Report, as specified in paragraph (a)(5) of this section. The following information shall be submitted:

(i) A description of the process change; and

(ii) A schedule for compliance with the provisions of §63.1331(a), as specified in paragraphs (b)(2)(ii)(A) and (b)(2)(ii)(B) of this section.

(A) The owner or operator shall submit to the Administrator for approval a compliance schedule and a justification for the schedule.

(B) The Administrator shall approve the compliance schedule or request changes within 120 operating days of receipt of the compliance schedule and justification.

(c) The provisions of this section do not apply to each affected source producing PET using a continuous TPA high viscosity multiple end finisher process.

compliance, the number of emission points allowed in the emissions average for said affected source is limited to twenty. This number may be increased by up to five additional emission points if pollution prevention measures are used to control five or more of the emission points included in the emissions average.

(B) If a plant site has two or more affected sources for which emissions averaging is being used to demonstrate compliance, the number of emission points allowed in the emissions averages for said affected sources is limited to twenty. This number may be increased by up to five additional emission points if pollution prevention measures are used to control five or more of the emission points included in the emissions averages.

(2) Compliance with the provisions of this section may be based on either organic HAP or TOC.

(3) For the purposes of these provisions, whenever Method 18, 40 CFR part 60, appendix A, is specified within the paragraphs of this section or is specified by reference through provisions outside this section, Method 18 or Method 25A, 40 CFR part 60, appendix A, may be used. The use of Method 25A, 40 CFR part 60, appendix A, shall conform with the requirements in paragraphs (a)(3)(i) and (a)(3)(ii) of this section.

(i) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A, is specified within the paragraphs of this section or is specified by reference through provisions outside this section, Method 18 or Method 25A, 40 CFR part 60, appendix A, may be used. The use of Method 25A, 40 CFR part 60, appendix A, is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(b) Unless an operating permit application has been submitted, the owner or operator shall develop and submit for approval an Emissions Averaging Plan containing all of the information required in §63.1339(e)(4) for all emission points to be included in an emissions average.

(c) Paragraphs (c)(1) through (c)(5) of this section describe the emission points that may be used to generate emissions averaging credits if control was applied after November 15, 1990, and if sufficient information is available to determine the appropriate value of credits for the emission point. Paragraph (c)(6) of this section discusses the use of pollution prevention in generating emissions averaging credits.

(1) Storage vessels, batch process vents, aggregate batch vent streams, continuous process vents subject to §63.1315, and process wastewater streams that are determined to be Group 2 emission points. The term “continuous process vents subject to §63.1315” includes continuous process vents subject to §63.1316 (b)(1)(iii), (b)(2)(iii), and (c)(2), which reference §63.1315.

(2) Continuous process vents located in the collection of material recovery sections within the affected source at an existing affected source producing PET using a continuous dimethyl terephthalate process subject to §63.1316(b)(1)(i) where the uncontrolled organic HAP emissions from said continuous process vents are equal to or less than 0.12 kg organic HAP per Mg of product. These continuous process vents shall be considered Group 2 emission points for the purposes of this section.

(3) Storage vessels, continuous process vents subject to §63.1315, and process wastewater streams that are determined to be Group 1 emission points and that are controlled by a technology that the Administrator or permitting authority agrees has a higher nominal efficiency than the reference control technology. Information on the nominal efficiencies for such technologies shall be submitted and approved as provided in paragraph (i) of this section.

(4) Batch process vents and aggregate batch vent streams that are determined to be Group 1 emission points and that are controlled to a level more stringent than the applicable standard.

(5) Continuous process vents subject to §63.1316 (b)(1)(i), (b)(2)(i), (b)(2)(ii), (c)(1) located in the collection of process sections within the affected source, as specified in paragraphs (c)(5)(i) through (c)(5)(ii) of this section.
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section. The continuous process vents identified in paragraphs (c)(5)(i) through (c)(5)(ii) of this section shall be considered to be Group 1 emission points for the purposes of this section.

(i) Continuous process vents subject to §63.1316(b)(1)(i) located in the collection of material recovery sections within the affected source where the uncontrolled organic HAP emissions for said continuous process vents are greater than 0.12 kg organic HAP per Mg of product and said continuous process vents are controlled to a level more stringent than the applicable standard.

(ii) Continuous process vents subject to §63.1316(b)(1)(ii), (b)(2)(i), (b)(2)(ii), or (c)(1) located in the collection of process sections within the affected source where the uncontrolled organic HAP emissions from said continuous process vents are controlled to a level more stringent than the applicable standard.

(6) The percent reduction for any storage vessel, batch process vent, aggregate batch vent stream, continuous process vent, and process wastewater stream from which emissions are reduced by pollution prevention measures shall be determined using the procedures specified in paragraph (j) of this section.

(i) For a Group 1 storage vessel, batch process vent, aggregate batch vent stream, continuous process vent, or process wastewater stream, the pollution prevention measure must reduce emissions more than if the applicable reference control technology or standard had been applied instead of the pollution prevention measure.

(d) The following emission points cannot be used to generate emissions averaging credits:

(1) Emission points already controlled on or before November 15, 1990, cannot be used to generate credits unless the level of control is increased after November 15, 1990. In this case, credit will be allowed only for the increase in control after November 15, 1990.

(2) Group 1 emission points, identified in paragraph (c)(3) of this section, that are controlled by a reference control technology cannot be used to generate credits unless the reference control technology has been approved for use in a different manner and a higher nominal efficiency has been assigned according to the procedures in paragraph (i) of this section.

(3) Emission points for nonoperating TPPU cannot be used to generate credits. TPPU that are shutdown cannot be used to generate credits or debits.

(4) Maintenance wastewater cannot be used to generate credits. Wastewater streams treated in biological treatment units cannot be used to generate credits. These two types of wastewater cannot be used to generate credits or debits. For the purposes of this section, the terms wastewater and wastewater stream are used to mean process wastewater.

(5) Emission points controlled to comply with a State or Federal rule other than this subpart cannot be used to generate credits, unless the level of control has been increased after November 15, 1990, to a level above what is required by the other State or Federal rule. Only the control above what is required by the other State or Federal rule will be credited. However, if an emission point has been used to generate emissions averaging credit in an approved emissions average, and the emission point is subsequently made subject to a State or Federal rule other than this subpart, the emission point may continue to generate emissions averaging credit for the purpose of complying with the previously approved emissions average.

(e) For all emission points included in an emissions average, the owner or

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Operator shall perform the following tasks:

(1) Calculate and record monthly debits for all Group 1 emission points that are controlled to a level less stringent than the reference control technology or standard for those emission points. Said Group 1 emission points are identified in paragraphs (c)(3) through (c)(5) of this section. Equations in paragraph (g) of this section shall be used to calculate debits.

(2) Calculate and record monthly credits for all Group 1 and Group 2 emission points that are over-controlled to compensate for the debits. Equations in paragraph (h) of this section shall be used to calculate credits. Emission points and controls that meet the criteria of paragraph (c) of this section may be included in the credit calculation, whereas those described in paragraph (d) of this section shall not be included.

(3) Demonstrate that annual credits calculated according to paragraph (h) of this section are greater than or equal to debits calculated for the same annual compliance period according to paragraph (g) of this section.

(i) The owner or operator may choose to include more than the required number of credit-generating emission points in an emissions average in order to increase the likelihood of being in compliance.

(ii) The initial demonstration in the Emissions Averaging Plan or operating permit application that credit-generating emission points will be capable of generating sufficient credits to offset the debits from the debit-generating emission points shall be made under representative operating conditions. After the compliance date, actual operating data will be used for all debit and credit calculations.

(4) Demonstrate that debits calculated for a quarterly (3-month) period according to paragraph (g) of this section are not more than 1.30 times the credits for the same period calculated according to paragraph (h) of this section. Compliance for the quarter shall be determined based on the ratio of credits and debits from that quarter, with 30 percent more debits than credits allowed on a quarterly basis.

(5) Record and report quarterly and annual credits and debits in the Periodic Reports as specified in §63.1335(e)(6). Every fourth Periodic Report shall include a certification of compliance with the emissions averaging provisions as required by §63.1335(e)(6)(x)(C)(2).

(f) Debits and credits shall be calculated in accordance with the methods and procedures specified in paragraphs (g) and (h) of this section, respectively, and shall not include emissions during the following periods:

(1) Emissions during periods of start-up, shutdown, and malfunction, as described in the Start-up, Shutdown, and Malfunction Plan.

(2) Emissions during periods of monitoring excursions, as defined in §63.1334(d). For these periods, the calculation of monthly credits and debits shall be adjusted as specified in paragraphs (f)(2)(i) through (f)(2)(iii) of this section.

(i) No credits would be assigned to the credit-generating emission point.

(ii) Maximum debits would be assigned to the debit-generating emission point.

(iii) The owner or operator may demonstrate to the Administrator that full or partial credits or debits should be assigned using the procedures in paragraph (l) of this section.

(g) Debits are generated by the difference between the actual emissions from a Group 1 emission point that is uncontrolled or is controlled to a level less stringent than the applicable reference control technology or standard and the emissions allowed for the Group 1 emission point. Said Group 1 emission points are identified in paragraphs (c)(3) through (c)(5) of this section. Debits shall be calculated as follows:

(1) Source-wide debits shall be calculated using Equation 28 of this subpart. Debits and all terms of Equation 28 of this subpart are in units of megagrams per month:
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Debits \(= \sum_{i=1}^{n} \left( \text{ECPV}_{\text{ACTUAL}} - (0.02) \text{ECPV}_{\text{in}} \right) + \sum_{j=1}^{n} \left( \text{ECPVS}_{\text{ACTUAL}} - \text{ECPVS}_{\text{STD}} \right) + \sum_{i=1}^{n} \left( \text{ES}_{\text{ACTUAL}} - (b) \text{ES}_{\text{in}} \right) + \sum_{i=1}^{n} \left( \text{EWW}_{\text{ACTUAL}} - \text{EWW}_{\text{in}} \right) + \sum_{i=1}^{n} \left( \text{EBPV}_{\text{ACTUAL}} - (0.10) \text{EBPV}_{\text{in}} \right) + \sum_{i=1}^{n} \left( \text{EABV}_{\text{ACTUAL}} - (0.10) \text{EABV}_{\text{in}} \right) \)  

[Eq. 28]

Where:

\(\text{ECPV}_{\text{ACTUAL}}\) = Emissions from each Group 1 continuous process vent \(i\) subject to §63.1315 that is uncontrolled or is controlled to a level less stringent than the applicable reference control technology. \(\text{ECPV}_{\text{ACTUAL}}\) is calculated according to paragraph (g)(2) of this section.

\(\text{ECPVS}_{\text{ACTUAL}}\) = Emissions from Group 1 continuous process vents subject to §63.1316(b)(1)(i), (b)(1)(ii), (b)(2)(i), (b)(2)(ii), or (c)(1) located in the collection of process sections \(j\) within the affected source that are uncontrolled or controlled to a level less stringent than the applicable standard. \(\text{ECPVS}_{\text{ACTUAL}}\) is calculated according to paragraph (g)(3) of this section.

\(\text{ES}_{\text{ACTUAL}}\) = Emissions from each Group 1 storage vessel \(i\) that is uncontrolled or is controlled to a level less stringent than the applicable reference control technology or standard. \(\text{ES}_{\text{ACTUAL}}\) is calculated according to paragraph (g)(4) of this section.

\(\text{EWW}_{\text{ACTUAL}}\) = Emissions from each Group 1 wastewater stream \(i\) that is uncontrolled or is controlled to a level less stringent than the applicable reference control technology. \(\text{EWW}_{\text{ACTUAL}}\) is calculated according to paragraph (g)(5) of this section.

\(\text{EBPV}_{\text{ACTUAL}}\) = Emissions from each Group 1 batch process vent \(i\) that is uncontrolled or is controlled to a level less stringent than the applicable standard. \(\text{EBPV}_{\text{ACTUAL}}\) is calculated according to paragraph (g)(6) of this section.

\(\text{EABV}_{\text{ACTUAL}}\) = Emissions from each Group 1 aggregate batch vent stream \(i\) that is uncontrolled or is controlled to a level less stringent than the applicable standard. \(\text{EABV}_{\text{ACTUAL}}\) is calculated according to paragraph (g)(7) of this section.

\(n\) = The number of emission points being included in the emissions average.

(2) Emissions from continuous process vents subject to §63.1315 shall be calculated as follows:

(i) For purposes of determining continuous process vent stream flow rate, organic HAP concentrations, and temperature, the sampling site shall be after the final product recovery device, if any recovery devices are present; before any control device (for continuous process vents, recovery devices shall not be considered control devices); and before discharge to the atmosphere. Method 1 or 1A, 40 CFR part 60, appendix A, shall be used for selection of the sampling site.

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(ii) \( \text{ECPV}_{iu} \) for each continuous process vent \( i \) shall be calculated using Equation 29 of this subpart.

\[
\text{ECPV}_{iu} = \left(2.494 \times 10^{-9}\right)Q_h \sum_{j=1}^{n} C_j M_j \quad \text{[Eq. 29]}
\]

where:
- \( \text{ECPV}_{iu} \) = Uncontrolled continuous process vent emission rate from continuous process vent \( i \), megagrams per month.
- \( Q \) = Vent stream flow rate, dry standard cubic meters per minute, measured using Method 2, 2A, 2C, or 2D, 40 CFR part 60, appendix A, as appropriate.
- \( h \) = Monthly hours of operation during which positive flow is present in the continuous process vent, hours per month.
- \( C_j \) = Concentration, parts per million by volume, dry basis, of organic HAP \( j \) as measured by Method 18, 40 CFR part 60, appendix A.
- \( M_j \) = Molecular weight of organic HAP \( j \), gram per gram-mole.
- \( n \) = Number of organic HAP in stream.

(A) The values of \( Q \) and \( C_j \) shall be determined during a performance test conducted under representative operating conditions. The values of \( Q \) and \( C_j \) shall be established in the Notification of Compliance Status and shall be updated as provided in paragraph (g)(2)(ii)(B) of this section.

(B) If there is a change in capacity utilization other than a change in monthly operating hours, or if any other change is made to the process or product recovery equipment or operation such that the previously measured values of \( Q \) and \( C_j \) are no longer representative, a new performance test shall be conducted to determine new representative values of \( Q \) and \( C_j \). These new values shall be used to calculate debits and credits from the time of the change forward, and the new values shall be reported in the next Periodic Report.

(iii) The following procedures and equations shall be used to calculate \( \text{ECPV}_{\text{ACTUAL}} \): 

(A) If the continuous process vent is not controlled by a control device or pollution prevention measure, \( \text{ECPV}_{\text{ACTUAL}} = \text{ECPV}_{iu} \), where \( \text{ECPV}_{iu} \) is calculated according to the procedures in paragraphs (g)(2)(i) and (g)(2)(ii) of this section.

(B) If the continuous process vent is controlled using a control device or a pollution prevention measure achieving less than 98 percent reduction, calculate \( \text{ECPV}_{\text{ACTUAL}} \) using Equation 30 of this subpart.

\[
\text{ECPV}_{\text{ACTUAL}} = \text{ECPV}_{iu} \left(1 - \frac{\text{Percent reduction}}{100}\right) \quad \text{[Eq. 30]}
\]

(1) The percent reduction shall be measured according to the procedures in §63.116 if a combustion control device is used. For a flare meeting the criteria in §63.116(a), or a boiler or process heater meeting the criteria in §63.116(b), the percent reduction shall be 98 percent. If a noncombustion control device is used, percent reduction shall be demonstrated by a performance test at the inlet and outlet of the device, or, if testing is not feasible, by a control design evaluation and documented engineering calculations.

(2) For determining debits from Group 1 continuous process vents,
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Product recovery devices shall not be considered control devices and cannot be assigned a percent reduction in calculating ECPV<sub>ACTUAL</sub>. The sampling site for measurement of uncontrolled emissions is after the final product recovery device. However, as provided in §63.113(a)(3), a Group 1 continuous process vent may add sufficient product recovery to raise the TRE index value above 1.0 or, for Group 1 continuous process vents at an existing affected source producing MBS, above 3.7, thereby becoming a Group 2 continuous process vent. Such a continuous process vent would not be a Group 1 continuous process vent and would, therefore, not be included in determining debits under this paragraph (g)(2)(iii)(B)(2).

(3) Procedures for calculating the percent reduction of pollution prevention measures are specified in paragraph (j) of this section.

(3) Emissions from continuous process vents located in the collection of process sections within the affected source subject to §63.1316 (b)(1)(i), (b)(1)(ii), (b)(2)(i), (b)(2)(ii), or (c)(1) shall be calculated as follows:

(i) The total organic HAP emissions from continuous process vents located in the collection of process sections j within the affected source, ECPV<sub>S,ACTUAL</sub>, shall be calculated as follows. The procedures in paragraph (g)(2)(iii) of this section shall be used to determine the organic HAP emissions for each individual continuous process vent, except that paragraph (g)(2)(iii)(B)(2) of this section shall not apply and the sampling site shall be after those recovery devices installed as part of normal operation; before any add-on control devices (i.e., those required by regulation); and prior to discharge to the atmosphere. Then, individual continuous process vent emissions shall be summed to determine ECPV<sub>S,ACTUAL</sub>.

(ii)(A) ECPV<sub>S,STD</sub> shall be calculated using Equation 31 of this subpart.

\[
ECPV_{S,STD} = (EF_{STD})(PP_j) \quad \text{[Eq. 31]}
\]

where:

- ECPV<sub>S,STD</sub> = Emissions if the applicable standard had been applied to the uncontrolled emissions, megagrams per month.
- EF<sub>STD</sub> = 0.000018 Mg organic HAP/Mg of product, if the collection of process sections within the affected source is subject to §63.1316(b)(1)(i).
- EF<sub>STD</sub> = 0.00002 Mg organic HAP/Mg of product, if the collection of process sections within the affected source is subject to §63.1316(b)(1)(ii) or (b)(2)(ii).
- EF<sub>STD</sub> = 0.00004 Mg organic HAP/Mg of product, if the collection of process sections within the affected source is subject to §63.1316(b)(2)(i).
- EF<sub>STD</sub> = 0.0000036 Mg organic HAP/Mg of product, if the collection of process sections within the affected source is subject to §63.1316(c)(1).
- PP<sub>j</sub> = Polymer produced, Mg/month, for the collection of process sections j within the affected source, as calculated according to paragraph (g)(3)(ii)(B) of this section.

(B) The amount of polymer produced, Mg per month, for the collection of process sections j within the affected source shall be determined by determining the weight of polymer pulled from the process line(s) during a 30-day period. The polymer produced shall be determined by direct measurement or by an alternate methodology, such as materials balance. If an alternate methodology is used, a description of the methodology, including all procedures, data, and assumptions shall be submitted as part of the Emissions Averaging Plan required by §63.1335(e)(4).

(C) Alternatively, ECPV<sub>S,STD</sub> for continuous process vents located in the collection of process sections within the affected source subject to §63.1316(c)(1) may be calculated using the procedures in paragraph (g)(2)(i) and (g)(2)(iii) of this section to determine the organic HAP emissions for each individual continuous process vent, except that the sampling site shall be after recovery devices installed as part of normal operation; before any add-on control devices (i.e., those required by regulation); and prior to discharge to the atmosphere. Then, individual continuous process vent emissions shall be summed and multiplied by 0.02 to determine ECPV<sub>S,STD</sub>.
(4) Emissions from storage vessels shall be calculated using the procedures specified in §63.150(g)(3).

(5) Emissions from wastewater streams shall be calculated using the procedures in §63.150(g)(5).

(6) Emissions from batch process vents shall be calculated as follows:

(i) \( \text{EBPV}_{iu} \) for each batch process vent \( i \) shall be calculated using the procedures specified in §63.1323(b).

(ii) The following procedures and equations shall be used to determine \( \text{EBPV}_{i\text{ACTUAL}} \):

\[
\text{EBPV}_{i\text{ACTUAL}} = \text{EBPV}_{iu} \left( 1 - \frac{\text{Percent reduction}}{100} \right) \quad [\text{Eq. 32}]
\]

(1) The percent reduction for the batch cycle shall be calculated according to the procedures in §63.1325(c)(2).

(2) The percent reduction for control devices shall be calculated according to the procedures in §63.1325(c)(2)(i) through (c)(2)(iii).

(3) The percent reduction of pollution prevention measures shall be calculated using the procedures specified in paragraph (j) of this section.

(7) Emissions from aggregate batch vent streams shall be calculated as follows:

\[
\text{EABV}_{iu} = \left( 2.494 \times 10^{-9} \right) Q_h C M \sum_{j=1}^{n} C_j M_j \quad [\text{Eq. 33}]
\]

where:

\( \text{EABV}_{iu} \) = Uncontrolled aggregate batch vent stream emission rate from aggregate batch vent stream \( i \), megagrams per month.

\( Q \) = Vent stream flow rate, dry standard cubic meters per minute, measured using Method 2, 2A, 2C, or 2D, 40 CFR part 60, appendix A, as appropriate.

\( h \) = Monthly hours of operation during which positive flow is present from the aggregate batch vent stream, hours per month.

\( C_j \) = Concentration, parts per million by volume, dry basis, of organic HAP \( j \) as measured by Method 18, 40 CFR part 60, appendix A.

\( M_j \) = Molecular weight of organic HAP \( j \), gram per gram-mole.

\( n \) = Number of organic HAP in the stream.

(A) If the batch process vent is not controlled by a control device or pollution prevention measure, \( \text{EBPV}_{i\text{ACTUAL}} = \text{EBPV}_{iu} \), where \( \text{EBPV}_{iu} \) is calculated using the procedures in §63.1323(b).

(B) If the batch process vent is controlled using a control device or a pollution prevention measure achieving less than 90 percent reduction for the batch cycle, calculate \( \text{EBPV}_{i\text{ACTUAL}} \) using Equation 32 of this subpart, where percent reduction is for the batch cycle.

(i) For purposes of determining aggregate batch vent stream flow rate, organic HAP concentrations, and temperature, the sampling site shall be before any control device and before discharge to the atmosphere. Method 1 or 1A, 40 CFR part 60, appendix A, shall be used for selection of the sampling site.

(ii) \( \text{EABV}_{iu} \) for each aggregate batch vent stream \( i \) shall be calculated using Equation 33 of this subpart.
(B) If there is a change in capacity utilization other than a change in monthly operating hours, or if any other change is made to the process or product recovery equipment or operation such that the previously measured values of $Q$ and $C_j$ are no longer representative, a new performance test shall be conducted to determine new representative values of $Q$ and $C_j$. These new values shall be used to calculate debits and credits from the time of the change forward, and the new values shall be reported in the next Periodic Report.

(iii) The following procedures and equations shall be used to calculate $EABV_{\text{actual}}$:

(A) If the aggregate batch vent stream is not controlled by a control device or pollution prevention measure, $EABV_{\text{actual}} = EABV_{\text{in}}$ where $EABV_{\text{in}}$ is calculated according to the procedures in paragraphs (g)(7)(i) and (g)(7)(ii) of this section.

(B) If the aggregate batch vent stream is controlled using a control device or a pollution prevention measure achieving less than 90 percent reduction, calculate $EABV_{\text{actual}}$ using Equation 34 of this subpart.

$$EABV_{\text{actual}} = EABV_{\text{in}} \left(1 - \frac{\text{Percent reduction}}{100}\right) \quad \text{[Eq. 34]}$$

(1) The percent reduction for control devices shall be determined according to the procedures in §63.1325(e).

(2) The percent reduction for pollution prevention measures shall be calculated according to the procedures specified in paragraph (j) of this section.

(h) Credits are generated by the difference between emissions that are allowed for each Group 1 and Group 2 emission point and the actual emissions from that Group 1 or Group 2 emission point that has been controlled after November 15, 1990 to a level more stringent than what is required by this subpart or any other State or Federal rule or statute. Said Group 1 and Group 2 emission points are identified in paragraphs (c)(1) through (c)(5) of this section. Credits shall be calculated using Equation 35 of this subpart.

(1) Sourcewide credits shall be calculated using Equation 35 of this subpart. Credits and all terms of Equation 35 of this subpart are in units of megagrams per month, and the baseline date is November 15, 1990:

$$\text{Credits} = D \sum_{i} [(0.10) \text{EBPV}_{i} - \text{EBPV}_{i,\text{actual}}] + D \sum_{i} [(\text{ECPV1}_{i} - \text{ECPV1}_{i,\text{actual}})] + D \sum_{i} [(\text{ECPV2}_{i} - \text{ECPV2}_{i,\text{actual}})] + D \sum_{i} [(\text{EBPV1}_{i} - \text{EBPV1}_{i,\text{actual}})] + D \sum_{i} [(\text{EBPV2}_{i} - \text{EBPV2}_{i,\text{actual}})] + D \sum_{i} [(\text{EWW1}_{i} - \text{EWW1}_{i,\text{actual}})] + D \sum_{i} [(\text{EWW2}_{i} - \text{EWW2}_{i,\text{actual}})] + D \sum_{i} [(0.10) \text{EABV1}_{i} - \text{EABV1}_{i,\text{actual}}] + D \sum_{i} [(0.10) \text{EABV2}_{i} - \text{EABV2}_{i,\text{actual}}] \quad \text{[Eq 35]}$$

Where:

$D = \text{Discount factor} = 0.9$ for all credit generating emission points except those controlled by a pollution prevention measure.
\( \text{ES}_1 \text{ACTUAL} = \text{Emissions from each Group 1 storage vessel} \text{ that is controlled} \text{ to a level more stringent} \text{ than the applicable reference control technology or standard.} \)

\( \text{ES}_1 \text{BASE} = \text{Emissions from each Group 1 storage vessel} \text{ at the baseline date.} \)

\( \text{ES}_2 \text{ACTUAL} = \text{Emissions from each Group 2 storage vessel} \text{ that is controlled.} \)

\( \text{ES}_2 \text{BASE} = \text{Emissions from each Group 2 storage vessel} \text{ at the baseline date.} \)
EABV_{2,\text{BASE}} = \text{Emissions from each Group 2 aggregate batch vent stream } i \text{ at the baseline date. } EABV_{2,\text{BASE}} \text{ is calculated according to paragraph (h)(7) of this section.}

EABV_{2,\text{ACTUAL}} = \text{Emissions from each Group 2 aggregate batch vent stream } i \text{ that is controlled. } EABV_{2,\text{ACTUAL}} \text{ is calculated according to paragraph (h)(7) of this section.}

n = \text{Number of Group 1 emission points included in the emissions average. The value of } n \text{ is not necessarily the same for continuous process vents, batch process vents, aggregate batch vent streams, storage vessels, wastewater streams, or the collection of process sections within the affected source. }

m = \text{Number of Group 2 emission points included in the emissions average. The value of } m \text{ is not necessarily the same for continuous process vents, batch process vents, aggregate batch vent streams, storage vessels, wastewater streams, or the collection of process sections within the affected source. }

(i) \text{Except as specified in paragraph (h)(1)(iv) of this section, for an emission point controlled using a reference control technology, the percent reduction for calculating credits shall be no greater than the nominal efficiency associated with the reference control technology, unless a higher nominal efficiency is assigned as specified in paragraph (h)(1)(ii) of this section.}

(ii) \text{For an emission point controlled to a level more stringent than the reference control technology, the nominal efficiency for calculating credits shall be assigned as described in paragraph (i) of this section. A reference control technology may be approved for use in a different manner and assigned a higher nominal efficiency according to the procedures in paragraph (i) of this section.}

(iii) \text{For an emission point controlled using a pollution prevention measure, the nominal efficiency for calculating credits shall be as determined as described in paragraph (i) of this section.}

(iv) \text{For Group 1 and Group 2 batch process vents and Group 1 and Group 2 aggregate batch vent streams, the percent reduction for calculating credits shall be the percent reduction determined according to the procedures in paragraphs (h)(6)(ii) and (h)(6)(iii) of this section for batch process vents and paragraphs (h)(7)(ii) and (h)(7)(iii) of this section for aggregate batch vent streams.}

(2) \text{Emissions from continuous process vents subject to §63.1315 shall be determined as follows:}

(i) \text{Uncontrolled emissions from Group 1 continuous process vents } (ECPV_{1,u}) \text{ shall be calculated according to the procedures and equation for } ECPV_{u} \text{ in paragraphs (g)(2)(i) and (g)(2)(ii) of this section.}

(ii) \text{Actual emissions from Group 1 continuous process vents controlled using a technology with an approved nominal efficiency greater than 98 percent or a pollution prevention measure achieving greater than 98 percent emission reduction } (ECPV_{1,\text{ACTUAL}}) \text{ shall be calculated using Equation 36 of this subpart.}

\[
ECPV_{1,\text{ACTUAL}} = ECPV_{1,u} \left(1 - \frac{\text{Nominal efficiency } \%}{100}\right) \quad \text{[Eq. 36]}
\]

(iii) \text{The following procedures shall be used to calculate actual emissions from Group 2 continuous process vents } (ECPV_{2,\text{ACTUAL}}): 

(A) \text{For a Group 2 continuous process vent controlled by a control device, a recovery device applied as a pollution prevention project, or a pollution prevention measure, where the control achieves a percent reduction less than or equal to 98 percent reduction, use Equation 37 of this subpart.}

\[
ECPV_{2,\text{ACTUAL}} = ECPV_{2,u} \left(1 - \frac{\text{Percent reduction}}{100}\right) \quad \text{[Eq. 37]}
\]
(1) ECPV2\textsubscript{iu} shall be calculated according to the equations and procedures for ECPV\textsubscript{iu} in paragraphs (g)(2)(i) and (g)(2)(ii) of this section, except as provided in paragraph (h)(2)(iii)(A)(3) of this section.

(2) The percent reduction shall be calculated according to the procedures in paragraphs (g)(2)(iii)(B)(1) through (g)(2)(iii)(B)(3) of this section, except as provided in paragraph (h)(2)(iii)(A)(4) of this section.

(3) If a recovery device was added as part of a pollution prevention project, ECPV\textsubscript{2i} shall be calculated prior to that recovery device. The equation for ECPV\textsubscript{iu} in paragraph (g)(2)(ii) of this section shall be used to calculate ECPV\textsubscript{2i} however, the sampling site for measurement of vent stream flow rate and organic HAP concentration shall be at the inlet of the recovery device.

(4) If a recovery device was added as part of a pollution prevention project, the percent reduction shall be demonstrated by conducting a performance test at the inlet and outlet of that recovery device.

(B) For a Group 2 continuous process vent controlled using a technology with an approved nominal efficiency greater than 98 percent or a pollution prevention measure achieving greater than 98 percent reduction, use Equation 38 of this subpart.

\[
\text{ECPV}_{\text{2i,\text{ACTUAL}}} = \text{ECPV}_{\text{2i,\text{iu}}} \left( 1 - \frac{\text{Nominal efficiency \%}}{100} \right) \text{ [Eq. 38]}
\]

(iv) Emissions from Group 2 continuous process vents at baseline shall be calculated as follows:

(A) If the continuous process vent was uncontrolled on November 15, 1990, ECPV\textsubscript{2BASE}=ECPV\textsubscript{2i} and shall be calculated according to the procedures and equation for ECPV\textsubscript{iu} in paragraphs (g)(2)(i) and (g)(2)(ii) of this section.

(B) If the continuous process vent was controlled on November 15, 1990, use Equation 39 of this subpart.

\[
\text{ECPV}_{\text{2i,\text{BASE}}} = \text{ECPV}_{\text{2i,\text{iu}}} \left( 1 - \frac{\text{Percent reduction \%}}{100} \right) \text{ [Eq. 39]}
\]

(1) ECPV\textsubscript{2i} is calculated according to the procedures and equation for ECPV\textsubscript{iu} in paragraphs (g)(2)(i) and (g)(2)(ii) of this section.

(2) The percent reduction shall be calculated according to the procedures specified in paragraphs (g)(2)(iii)(B)(1) through (g)(2)(iii)(B)(3) of this section.

(C) If a recovery device was added as part of a pollution prevention project initiated after November 15, 1990, ECPV\textsubscript{2BASE}=ECPV\textsubscript{2i}, where ECPV\textsubscript{2i} is calculated according to paragraph (h)(2)(iii)(A)(3) of this section.

(3) Emissions from continuous process vents subject to §63.1316(b)(1)(i), (b)(1)(ii), (b)(2)(i), (b)(2)(ii), or (c)(1) shall be determined as follows:

(i) Emissions from Group 1 continuous process vents located in the collection of process sections \(j\) within the affected source if the applicable standard had been applied to the uncontrolled emissions (ECPV\textsubscript{S1,\text{BASE}}) shall be calculated according to paragraph (g)(3)(iii) of this section.

(ii) Actual emissions from Group 1 continuous process vents located in the collection of process sections \(j\) within the affected source controlled to a level more stringent than the applicable standard (ECPV\textsubscript{S1,\text{ACTUAL}}) shall be calculated using the procedures in paragraphs (g)(3)(iii)(A) and (g)(3)(iii)(B) of this section, except that the actual emission level, Mg organic HAP/Mg of
product, shall be used as $\text{EF}_{\text{std}}$ in Equation 31 of this subpart. Further, the procedures in paragraphs (g)(3)(ii)(A) and (g)(3)(ii)(B) of this section, except that the actual emission level, $\text{Mg organic HAP/Mg of product},$ at baseline shall be used as $\text{EF}_{\text{std}}$ in Equation 31 of this subpart.

(ii) Emissions from storage vessels shall be calculated using the procedures specified in §63.150(h)(3).

(iii) Actual emissions from Group 1 storage vessels at an existing affected source producing ASA/AMSAN subject to §63.1314(c) using a technology with an approved nominal efficiency greater than 98 percent or a pollution prevention measure achieving greater than 98 percent emission reduction shall be calculated using the procedures specified in §63.150(h)(5).

(5) Emissions from wastewater streams shall be calculated using the procedures specified in §63.150(h)(5).

(6) Emissions from batch process vents shall be determined as follows:

(i) Uncontrolled emissions from Group 1 batch process vents ($\text{EBPV}_{1u}$) shall be calculated using the procedures specified in §63.1323(b).

(ii) Actual emissions from Group 1 batch process vents controlled to a level more stringent than the standard ($\text{EBPV}_{1\text{ACTUAL}}$) shall be calculated using Equation 40 of this subpart, where percent reduction is for the batch cycle:

$$\text{EBPV}_{1\text{ACTUAL}} = \text{EBPV}_{1u} \left(1 - \frac{\text{Percent reduction}}{100}\right)$$

[Eq. 40]

(A) The percent reduction for the batch cycle shall be calculated according to the procedures in §63.1325(c)(2).

(B) The percent reduction for control devices shall be determined according to the procedures in §63.1325(c)(2)(i) through (c)(2)(iii).

(C) The percent reduction of pollution prevention measures shall be calculated using the procedures specified in paragraph (j) of this section.

(iii) Actual emissions from Group 2 batch process vents ($\text{EBPV}_{2\text{ACTUAL}}$) shall be calculated using Equation 41 of this subpart.

$$\text{EBPV}_{2\text{ACTUAL}} = \text{EBPV}_{2u} \left(1 - \frac{\text{Percent reduction}}{100}\right)$$

[Eq. 41]
(iv) Emissions from Group 2 batch process vents at baseline (EBPV2\textsubscript{BASE}) shall be calculated as follows:

(A) If the batch process vent was uncontrolled on November 15, 1990, EBPV2\textsubscript{BASE} = EBPV2\textsubscript{iu} and shall be calculated using the procedures specified in §63.1323(b).

(B) If the batch process vent was controlled on November 15, 1990, use Equation 42 of this subpart and the procedures in paragraphs (h)(6)(ii)(A) through (h)(6)(ii)(C) of this section. EBPV2\textsubscript{iu} shall be calculated using the procedures specified in §63.1323(b).

\[\text{EBPV2}_{\text{BASE}} = \text{EBPV2}_{\text{iu}} \left(1 - \frac{\text{Percent reduction}}{100}\right) \quad \text{[Eq. 42]}\]

(7) Emissions from aggregate batch vent streams shall be determined as follows:

(i) Uncontrolled emissions from Group 1 aggregate batch vent streams (EABV1\textsubscript{iu}) shall be calculated according to the procedures and equation for EABV\textsubscript{iu} in paragraphs (g)(7)(i) and (g)(7)(ii) of this section.

(ii) Actual emissions from Group 1 aggregate batch vent streams controlled to a level more stringent than the standard (EABV1\textsubscript{ACTUAL}) shall be calculated using Equation 43 of this subpart:

\[\text{EABV1}_{\text{ACTUAL}} = \text{EABV1}_{\text{IU}} \left(1 - \frac{\text{Percent reduction}}{100}\right) \quad \text{[Eq. 43]}\]

(A) The percent reduction for control devices shall be determined according to the procedures in §63.1325(e).

(B) The percent reduction of pollution prevention measures shall be calculated using the procedures specified in paragraph (j) of this section.

(iii) Actual emissions from Group 2 aggregate batch vent streams (EABV2\textsubscript{ACTUAL}) shall be calculated using Equation 44 of this subpart and the procedures in paragraphs (h)(7)(ii)(A) through (h)(7)(ii)(B) of this section. EABV2\textsubscript{iu} shall be calculated according to the equations and procedures for EABV\textsubscript{iu} in paragraphs (g)(7)(i) and (g)(7)(ii) of this section.

\[\text{EABV2}_{\text{ACTUAL}} = \text{EABV2}_{\text{iu}} \left(1 - \frac{\text{Percent reduction}}{100}\right) \quad \text{[Eq. 44]}\]

(iv) Emissions from Group 2 aggregate batch vent streams at baseline shall be calculated as follows:

(A) If the aggregate batch vent stream was uncontrolled on November 15, 1990, EABV2\textsubscript{BASE} = EABV2\textsubscript{iu} and shall be calculated according to the procedures and equation for EABV\textsubscript{iu} in paragraphs (g)(7)(i) and (g)(7)(ii) of this section.

(B) If the aggregate batch vent stream was controlled on November 15, 1990, use Equation 45 of this subpart and the procedures in paragraphs (h)(7)(ii)(A) through (h)(7)(ii)(B) of this section. EABV2\textsubscript{iu} shall be calculated according to the equations and procedures for EABV\textsubscript{iu} in paragraphs (g)(7)(i) and (g)(7)(ii) of this section.
(i) The following procedures shall be followed to establish nominal efficiencies for emission controls for storage vessels, continuous process vents, and process wastewater streams. The procedures in paragraphs (i)(1) through (i)(6) of this section shall be followed for control technologies that are different in use or design from the reference control technologies and achieve greater percent reductions than the percent efficiencies assigned to the reference control technologies in §63.111.

(1) In those cases where the owner or operator is seeking permission to take credit for use of a control technology that is different in use or design from the reference control technology, and the different control technology will be used in more than three applications at a single plant-site, the owner or operator shall submit the information specified in paragraphs (i)(1)(i) through (i)(1)(iv) of this section, as specified in §63.1335(e)(7)(ii), to the Director of the EPA Office of Air Quality Planning and Standards in writing:

(i) Emission stream characteristics of each emission point to which the control technology is or will be applied including the kind of emission point, flow, organic HAP concentration, and all other stream characteristics necessary to design the control technology or determine its performance.

(ii) Description of the control technology including design specifications.

(iii) Documentation demonstrating to the Administrator’s satisfaction the control efficiency of the control technology. This may include performance test data collected using an appropriate EPA Method or any other method validated according to Method 301, 40 CFR part 63, appendix A, of this part. If it is infeasible to obtain test data, documentation may include a design evaluation and calculations. The engineering basis of the calculation procedures and all inputs and assumptions made in the calculations shall be documented.

(iv) A description of the parameter or parameters to be monitored to ensure that the control technology will be operated in conformance with its design and an explanation of the criteria used for selection of that parameter (or parameters).

(2) The Administrator shall determine within 120 days whether an application presents sufficient information to determine nominal efficiency. The Administrator reserves the right to request specific data in addition to the items listed in paragraph (i)(1) of this section.

(3) The Administrator shall determine within 120 days of the submittal of sufficient data whether a control technology shall have a nominal efficiency and the level of that nominal efficiency. If, in the Administrator’s judgment, the control technology achieves a level of emission reduction greater than the reference control technology for a particular kind of emission point, the Administrator will publish a FEDERAL REGISTER notice establishing a nominal efficiency for the control technology.

(4) The Administrator may grant permission to take emission credits for use of the control technology. The Administrator may also impose requirements that may be necessary to ensure operation and maintenance to achieve the specified nominal efficiency.

(5) In those cases where the owner or operator is seeking permission to take credit for use of a control technology that is different in use or design from the reference control technology and the different control technology will be used in no more than three applications at a single plant site, the owner or operator shall submit the information listed in paragraphs (i)(1)(i) through (i)(1)(iv) of this section, as specified in §63.1335(e)(7)(ii), to the Administrator.

(i) In these instances, use and conditions for use of the control technology may be approved by the permitting authority as part of an operating permit.
application or modification. The permitting authority shall follow the procedures specified in paragraphs (i)(2) through (i)(4) of this section except that, in these instances, a Federal Register notice is not required to establish the nominal efficiency for the different technology.

(ii) If, in reviewing the application, the permitting authority believes the control technology has broad applicability for use by other affected sources, the permitting authority shall submit the information provided in the application to the Director of the EPA Office of Air Quality Planning and Standards. The Administrator shall review the technology for broad applicability and may publish a Federal Register notice; however, this review shall not affect the permitting authority's approval of the nominal efficiency of the control technology for the specific application.

(6) If, in reviewing an application for a control technology for an emission point, the Administrator or permitting authority determines that the control technology is not different in use or design from the reference control technology, the Administrator or permitting authority shall deny the application.

(j) The following procedures shall be used for calculating the efficiency (percent reduction) of pollution prevention measures for storage vessels, continuous process vents, batch process vents, aggregate batch vent streams, and wastewater streams:

(1) A pollution prevention measure is any practice that meets the criteria of paragraphs (j)(1)(i) and (j)(1)(ii) of this section.

(i) A pollution prevention measure is any practice that results in a lesser quantity of organic HAP emissions per unit of product released to the atmosphere prior to out-of-process recycling, treatment, or control of emissions, while the same product is produced.

(ii) Pollution prevention measures may include: substitution of feedstocks that reduce organic HAP emissions; alterations to the production process to reduce the volume of materials released to the environment; equipment modifications; housekeeping measures; and in-process recycling that returns waste materials directly to production as raw materials. Production cutbacks do not qualify as pollution prevention.

(2) The emission reduction efficiency of pollution prevention measures implemented after November 15, 1990, may be used in calculating the actual emissions from an emission point in the debit and credit equations in paragraphs (g) and (h) of this section.

(i) For pollution prevention measures, the percent reduction used in the equations in paragraphs (g)(2) through (g)(7) of this section and paragraphs (h)(2) through (h)(7) of this section is the percent difference between the monthly organic HAP emissions for each emission point after the pollution prevention measure for the most recent month versus monthly emissions from the same emission point before the pollution prevention measure, adjusted by the volume of product produced during the two monthly periods.

(ii) Equation 46 of this subpart shall be used to calculate the percent reduction of a pollution prevention measure for each emission point.

\[
\text{Percent reduction} = \left( \frac{E_B}{E_{PP}} \right) \left( \frac{P_B}{P_{PP}} \right) \times 100\% \quad [\text{Eq. 46}]
\]

where:

\begin{align*}
E_B & = \text{Monthly emissions before the pollution prevention measure, megagrams per month, determined as specified in paragraphs} \\
E_{PP} & = \text{Efficiency of pollution prevention measure (percent organic HAP reduction).}
\end{align*}

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(j)(2)(ii)(A), (j)(2)(ii)(B), and (j)(2)(ii)(C) of this section.

E_p = Monthly emissions after the pollution prevention measure, megagrams per month, as determined for the most recent month.

P_B = Monthly production before the pollution prevention measure, megagrams per month, during the same period over which E_B is calculated.

P_pp = Monthly production after the pollution prevention measure, megagrams per month, as determined for the most recent month.

(A) The monthly emissions before the pollution prevention measure, E_B, shall be determined in a manner consistent with the equations and procedures in paragraph (g)(2) and (g)(3) of this section for continuous process vents, paragraph (g)(4) of this section for storage vessels, paragraph (g)(6) of this section for batch process vents, and paragraph (g)(7) of this section for aggregate batch vent streams.

(B) For wastewater, E_B shall be calculated using Equation 47 of this subpart:

\[
E_B = \sum_{i=1}^{n} \left[ (6.0 \times 10^{-8}) Q_{Bi} H_{Bi} \sum_{m=1}^{s} F_{em} HAP_{Bim} \right] \quad \text{[Eq. 47]}
\]

Where:
- \( n \) = Number of wastewater streams.
- \( Q_{Bi} \) = Annual average flow rate for wastewater stream \( i \) before the pollution prevention measure, defined and determined according to §63.144(c)(3), liters per minute, before implementation of the pollution prevention measure.
- \( H_{Bi} \) = Number of hours per month that wastewater stream \( i \) was discharged before the pollution prevention measure, hours per month.
- \( s \) = Total number of organic HAP in wastewater stream \( i \).
- \( F_{em} \) = Fraction emitted of organic HAP \( m \) in wastewater from Table 34 of subpart G of this part, dimensionless.
- \( HAP_{Bim} \) = Annual average concentration of organic HAP \( m \) in wastewater stream \( i \), defined and determined according to paragraph §63.150(g)(5)(i) of this section, before the pollution prevention measure, parts per million by weight, as measured before the implementation of the pollution prevention measure.

(C) If the pollution prevention measure was implemented prior to September 12, 1996 records may be used to determine E_B.

(D) The monthly emissions after the pollution prevention measure, E_pp, may be determined during a performance test or by a design evaluation and documented engineering calculations. Once an emissions-to-production ratio has been established, the ratio can be used to estimate monthly emissions from monthly production records.

(E) For wastewater, E_pp shall be calculated using Equation 48 of this subpart and \( n \), \( Q_{ppi} \), \( H_{ppi} \), \( s \), \( F_{em} \), and \( HAP_{ppim} \) are defined and determined as described in paragraph (j)(2)(ii)(B) of this section, except that \( Q_{ppi} \), \( H_{ppi} \), and \( HAP_{ppim} \) shall be determined after the pollution prevention measure has been implemented.

\[
E_{pp} = \sum_{i=1}^{n} \left[ (6.0 \times 10^{-8}) Q_{ppi} H_{ppi} \sum_{m=1}^{s} F_{em} HAP_{ppim} \right] \quad \text{[Eq. 48]}
\]

(iii) All equations, calculations, test procedures, test results, and other information used to determine the percent reduction achieved by a pollution prevention measure for each emission point shall be fully documented.
(iv) The same pollution prevention measure may reduce emissions from multiple emission points. In such cases, the percent reduction in emissions for each emission point shall be calculated.

(v) For the purposes of the equations in paragraphs (h)(2) through (h)(7) of this section used to calculate credits for emission points controlled more stringently than the reference control technology or standard, the nominal efficiency of a pollution prevention measure is equivalent to the percent reduction of the pollution prevention measure. When a pollution prevention measure is used, the owner or operator of an affected source is not required to apply to the Administrator for a nominal efficiency and is not subject to paragraph (i) of this section.

(k) The owner or operator shall demonstrate that the emissions from the emission points proposed to be included in the emissions average will not result in greater hazard or, at the option of the Administrator, greater risk to human health or the environment than if the emission points were controlled according to §§63.1314, 63.1315, 63.1316 through 63.1320, 63.1321, and 63.1330.

(1) This demonstration of hazard or risk equivalency shall be made to the satisfaction of the Administrator.

(i) The Administrator may require owners and operators to use specific methodologies and procedures for making a hazard or risk determination.

(ii) The demonstration and approval of hazard or risk equivalency shall be made according to any guidance that the Administrator makes available for use.

(2) Owners and operators shall provide documentation demonstrating the hazard or risk equivalency of their proposed emissions average in their operating permit application or in their Emissions Averaging Plan if an operating permit application has not yet been submitted.

(3) An Emissions Averaging Plan that does not demonstrate hazard or risk equivalency to the satisfaction of the Administrator shall not be approved. The Administrator may require such adjustments to the Emissions Averaging Plan as are necessary in order to ensure that the emissions average will not result in greater hazard or risk to human health or the environment than would result if the emission points were controlled according to §§63.1314, 63.1315, 63.1316 through 63.1320, 63.1321, and 63.1330.

(4) A hazard or risk equivalency demonstration shall:

(i) Be a quantitative, bona fide chemical hazard or risk assessment;

(ii) Account for differences in chemical hazard or risk to human health or the environment; and

(iii) Meet any requirements set by the Administrator for such demonstrations.

(l) For periods of parameter monitoring excursions, an owner or operator may request that the provisions of paragraphs (l)(1) through (l)(4) of this section be followed instead of the procedures in paragraphs (f)(2)(i) and (f)(2)(ii) of this section.

(1) The owner or operator shall notify the Administrator of monitoring excursions in the Periodic Reports as required in §63.1335(e)(6).

(2) The owner or operator shall demonstrate that other types of monitoring data or engineering calculations are appropriate to establish that the control device for the emission point was operating in such a fashion to warrant assigning full or partial credits and debits. This demonstration shall be made to the Administrator's satisfaction, and the Administrator may establish procedures of demonstrating compliance that are acceptable.

(3) The owner or operator shall provide documentation of the excursion and the other type of monitoring data or engineering calculations to be used to demonstrate that the control device for the emission point was operating in such a fashion to warrant assigning full or partial credits and debits.

(4) The Administrator may assign full or partial credit and debits upon review of the information provided.

(m) For each emission point included in an emissions average, the owner or operator shall perform testing, monitoring, recordkeeping, and reporting equivalent to that required for Group 1 emission points complying with §§63.1314, 63.1315, 63.1316 through 63.1320, 63.1321, and 63.1330, as applicable. The
specific requirements for continuous process vents, batch process vents, aggregate batch vent streams, storage vessels, and wastewater operations that are included in an emissions average for an affected source are identified in paragraphs (m)(1) through (m)(7) of this section.

(1) For each continuous process vent subject to §63.1315 equipped with a flare, incinerator, boiler, or process heater, as appropriate to the control technique:
   (i) Determine whether the continuous process vent is Group 1 or Group 2 according to the procedures specified in §63.1315;
   (ii) Conduct initial performance tests to determine percent reduction according to the procedures specified in §63.1315; and
   (iii) Monitor the operating parameters, keep records, and submit reports according to the procedures specified in §63.1315.

(2) For each continuous process vent subject to §63.1315 equipped with a carbon adsorber, absorber, or condenser but not equipped with a control device, as appropriate to the control technique:
   (i) Determine the flow rate, organic HAP concentration, and TRE index value according to the procedures specified in §63.1315; and
   (ii) Monitor the operating parameters, keep records, and submit reports according to the procedures specified in §63.1315.

(3) For continuous process vents subject to §63.1316(b)(1)(i), (b)(1)(ii), (b)(2)(i), (b)(2)(ii), or (c)(1):
   (i) Determine whether the emissions from the continuous process vents subject to §63.1316(b)(1)(i) located in the collection of material recovery sections within the affected source are greater than, equal to, or less than 0.12 kg organic HAP per Mg of product according to the procedures specified in §63.1318(b); and
   (ii) Determine the emission rate, \( \text{ER}_{\text{HAP}} \), for each collection of process sections within the affected source according to the procedures specified in §63.1318(b); and
   (iii) [Reserved]
   (iv) Monitor the operating parameters, keep records, and submit reports according to the procedures specified in §63.1317, §63.1319, §63.1320.

(4) For each storage vessel controlled with an internal floating roof, external roof, or a closed vent system with a control device, as appropriate to the control technique:
   (i) Perform the monitoring or inspection procedures according to the procedures specified in §63.1314;
   (ii) Perform the reporting and recordkeeping procedures according to the procedures specified in §63.1314; and
   (iii) For closed vent systems with control devices, conduct an initial design evaluation and submit an operating plan according to the procedures specified in §63.1314.

(5) For wastewater emission points, as appropriate to the control technique:
   (i) For wastewater treatment processes, conduct tests according to the procedures specified in §63.1319, §63.1320, §63.1321, and §63.1330;
   (ii) Conduct inspections and monitoring according to the procedures specified in §63.1319, §63.1320, §63.1321, and §63.1330;
   (iii) Implement a recordkeeping program according to the procedures specified in §63.1319, §63.1320, §63.1321, and §63.1330;
   (iv) Implement a reporting program according to the procedures specified in §63.1319, §63.1320, §63.1321, and §63.1330.

(6) For each batch process vent and aggregate batch vent stream equipped with a control device, as appropriate to the control technique:
   (i) Determine whether the batch process vent or aggregate batch vent stream is Group 1 or Group 2 according to the procedures specified in §63.1320;
   (ii) Conduct performance tests according to the procedures specified in §63.1325; and
   (iii) Conduct monitoring according to the procedures specified in §63.1325; and
   (iv) Perform the recordkeeping and reporting procedures according to the procedures specified in §63.1326 and §63.1327.

(7) If an emission point in an emissions average is controlled using a pollution prevention measure or a device or technique for which no monitoring parameters or inspection procedures are required by §§63.1314, §63.1315, §63.1316 through §63.1320, §63.1321, or §63.1330, the
§ 63.1333 Additional test methods and procedures.

(a) Performance testing shall be conducted in accordance with §63.7(a)(3), (d), (e), (g), and (h), with the exceptions specified in paragraphs (a)(1) through (a)(4) of this section and the additions specified in paragraphs (b) through (d) of this section. Sections 63.1314 through 63.1330 also contain specific testing requirements.

(1) Performance tests shall be conducted according to the provisions of §63.7(e), except that performance tests shall be conducted at maximum representative operating conditions for the process.

(2) References in §63.7(g) to the Notification of Compliance Status requirements in §63.7(h) shall refer to the requirements specified in §63.1325(e)(5).

(3) Because the site-specific test plans in §63.7(c)(3) are not required, §63.7(h)(4)(ii) is not applicable.

(4) The owner or operator shall notify the Administrator of the intention to conduct a performance test at least 30 calendar days before the performance test is scheduled to allow the Administrator the opportunity to have an observer present during the test.

(b) Each owner or operator of an existing affected source producing MBS complying with §63.1315(b)(2) shall determine compliance with the mass emission per mass product standard by using Equation 49 of this subpart.

\[
ER_{MBS} = \frac{\sum E_i}{PP_M} \quad \text{[Eq. 49]}
\]

where:

- \( ER_{MBS} \): Emission rate of organic HAP or TOC from continuous process vents, kg/Mg product.
- \( E_i \): Emission rate of organic HAP or TOC from continuous process vent \( i \) as calculated using the procedures specified in §63.116(c)(4), kg/month.
- \( PP_M \): Amount of polymer produced in one month as determined by the procedures specified in §63.1318(b)(1)(ii), Mg/month.

\( n \): Number of continuous process vents.

When determining \( E_i \), when the provisions of §63.116(c)(4) specify that Method 18, 40 CFR part 60, appendix A, shall be used, Method 18 or Method 25A, 40 CFR part 60, appendix A, may be used for the purposes of this subpart. The use of Method 25A, 40 CFR part 60, appendix A, shall comply with paragraphs (b)(1) and (b)(2) of this section.

(1) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A, shall be the single organic HAP representing the largest percent by volume.

(2) The use of Method 25A, 40 CFR part 60, appendix A, is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(c) The owner or operator of an affected source, complying with §63.1322(a)(3) shall determine compliance with the percent reduction requirement using Equation 50 of this subpart.
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\[
PR = \frac{\left( \sum_{j=1}^{n} (E_j - E_o) \right)}{\left( \sum_{j=1}^{n} E_j \right)} + \sum_{k=1}^{n} H_k E_{ku} + \sum_{l=1}^{n} AE_{unc} - () \left[ \sum_{j=1}^{n} E_j \right] + \sum_{k=1}^{n} H_k E_{ku} + \sum_{l=1}^{n} AE_{unc}
\]

[Eq. 50]

where:

PR = Percent reduction

H_j = Number of operating hours in a year for control device j.

E_j = Mass rate of TOC or total organic HAP at the inlet of control device j, calculated as specified in §63.1325(f), kg/hr. This value includes all continuous process vents, batch process vents, and aggregate batch vent streams routed to control device j.

E_o = Mass rate of TOC or total organic HAP at the outlet of control device j, calculated as specified in §63.1325(f), kg/hr.

H_k = Number of hours of operation during which positive flow is present in uncontrolled continuous process vent or aggregate batch vent stream k, hr/yr.

E_{ku} = Mass rate of TOC or total organic HAP of uncontrolled continuous process vent or aggregate batch vent stream k, calculated as specified in §63.1325(f)(4), kg/hr.

AE_{unc} = Mass rate of TOC or total organic HAP of uncontrolled batch process vent l, calculated as specified in §63.1325(f)(4), kg/yr.

n = Number of control devices, uncontrolled continuous process vents and aggregate batch vent streams, and uncontrolled batch process vents. The value of n is not necessarily the same for these three items.

(d) Data shall be reduced in accordance with the EPA approved methods specified in the applicable subpart or, if other test methods are used, the data and methods shall be validated according to the protocol in Method 301 of appendix A of this part.

§ 63.1334 Parameter monitoring levels and excursions.

(a) Establishment of parameter monitoring levels. The owner or operator of a control or recovery device that has one or more parameter monitoring level requirements specified under this subpart shall establish a maximum or minimum level for each measured parameter using the procedures specified in paragraph (b), (c), or (d) of this section. The procedures specified in paragraph (b) of this section have been approved by the Administrator. The procedures in paragraphs (c) and (d) of this section have not been approved by the Administrator and determination of the parameter monitoring level using the procedures in paragraph (c) or (d) of this section is subject to review and approval by the Administrator. Said determination and supporting documentation shall be included in the Precompliance Report, specified in §63.1335(e)(3).

(1) The owner or operator shall operate control and recovery devices such that monitored parameters remain above the minimum established level or below the maximum established level.

(2) As specified in §63.1335(e)(5) and §63.1335(e)(8), all established levels, along with their supporting documentation and the definition of an operating day, shall be approved as part of and incorporated into the Notification of Compliance Status or operating permit, respectively.

(3) Nothing in this section shall be construed to allow a monitoring parameter excursion caused by an activity that violates other applicable provisions of subpart A, F, or G of this part.
(b) Establishment of parameter monitoring levels based on performance tests. The procedures specified in paragraphs (b)(1) through (b)(3) of this section shall be used, as applicable, in establishing parameter monitoring levels. Level(s) established under this paragraph (b) shall be based on the parameter values measured during the performance test.

(1) Storage tanks and wastewater. The maximum and/or minimum monitoring levels shall be based on the parameter values measured during the performance test, supplemented, if desired, by engineering assessments and/or manufacturer’s recommendations.

(2) Continuous process vents. During initial compliance testing, the appropriate parameter shall be continuously monitored during the required 1-hour runs. The monitoring level(s) shall then be established as the average of the maximum (or minimum) point values from the three test runs. The average of the maximum values shall be used when establishing a maximum level, and the average of the minimum values shall be used when establishing a minimum level.

(3) Batch process vents. The monitoring level(s) shall be established using the procedures specified in paragraphs (b)(3)(i) through (b)(3)(ii) of this section, as appropriate. The procedures specified in this paragraph (b)(3) may only be used if the batch emission episodes, or portions thereof, selected to be controlled were tested, and monitoring data were collected, during the entire period in which emissions were vented to the control device, as specified in §63.1325(c)(1)(i). If the owner or operator chose to test only a portion of the batch emission episode, or portion thereof, selected to be controlled, as specified in §63.1325(c)(1)(i)(A), the procedures in paragraphs (c) of this section must be used.

(i) If more than one batch emission episode or more than one portion of a batch emission episode has been selected to be controlled, a single level for the batch cycle shall be calculated as follows:

(A) During initial compliance testing, the appropriate parameter shall be monitored continuously at all times when batch emission episodes, or portions thereof, selected to be controlled are vented to the control device. (B) The average monitored parameter value shall be calculated for each batch emission episode, or portion thereof, in the batch cycle selected to be controlled. The average shall be based on all values measured during the required performance test.

(C) If the level to be established is a maximum operating parameter, the level shall be defined as the maximum of the average parameter values of the batch emission episodes, or portions thereof, in the batch cycle selected to be controlled.

(D) If the level to be established is a minimum operating parameter, the level shall be defined as the maximum of the average parameter values of the batch emission episodes, or portions thereof, in the batch cycle selected to be controlled.

(E) Alternatively, an average monitored parameter value shall be calculated for the entire batch cycle based on all values measured during each batch emission episode, or portion thereof, selected to be controlled.

(ii) Instead of establishing a single level for the batch cycle, as described in paragraph (b)(3)(i) of this section, an owner or operator may establish separate levels for each batch emission episode, or portion thereof, selected to be controlled. Each level shall be determined as specified in paragraphs (b)(3)(i)(A) and (b)(3)(i)(B) of this section.

(iii) The batch cycle shall be defined in the Notification of Compliance Status, as specified in §63.1325(e)(5). Said definition shall include an identification of each batch emission episode and the information required to determine parameter monitoring compliance for partial batch cycles (i.e., when part of a batch cycle is accomplished during two different operating days).

(4) Aggregate batch vent streams. For aggregate batch vent streams, the monitoring level shall be established in accordance with paragraph (b)(2) of this section.

(c) Establishment of parameter monitoring levels based on performance tests, engineering assessments, and/or manufacturer’s recommendations. As required in
paragraph (a) of this section, the information specified in paragraphs (c)(2) and (c)(3) of this section shall be provided in the Precompliance Report.

Parameter monitoring levels established under this paragraph (c) shall be based on the parameter values measured during the performance test supplemented by engineering assessments and manufacturer's recommendations. Performance testing is not required to be conducted over the entire range of expected parameter values.

The parameter monitoring levels established under this paragraph (c) shall be based on the parameter values measured during the performance test supplemented by engineering assessments and manufacturer's recommendations. Performance testing is not required to be conducted over the entire range of expected parameter values.

The specific level of the monitored parameter(s) for each emission point.

The rationale for the specific level for each parameter for each emission point, including any data and calculations used to develop the level and a description of why the level indicates proper operation of the control or recovery device.

Establishment of parameter monitoring based on engineering assessments and/or manufacturer's recommendations. If a performance test is not required by this subpart for a control or recovery device, the maximum or minimum level may be based solely on engineering assessments and/or manufacturer's recommendations. As required in paragraph (a) of this section, the determined level and all supporting documentation shall be provided in the Precompliance Report.

Compliance determinations. The provisions of this paragraph (e) apply only to emission points and control or recovery devices for which continuous monitoring is required under this subpart.

The parameter monitoring data for storage vessels, process vents, process wastewater streams, and emission points included in emissions averages that are required to perform continuous monitoring shall be used to determine compliance for the monitored control or recovery devices.

Except as provided in paragraphs (e)(3) and (g) of this section, for each excursion, as defined in paragraph (f) of this section, the owner or operator shall be deemed out of compliance with the provisions of this subpart.

If the daily average value of a monitored parameter is above the maximum level or below the minimum level established, or if monitoring data cannot be collected during monitoring device calibration check or monitoring device malfunction, but the affected source is operated during the periods of start-up, shutdown, or malfunction in accordance with the affected source's Start-up, Shutdown, and Malfunction Plan, then the event shall not be considered a monitoring parameter excursion.

Parameter monitoring excursion definitions. (1) For storage vessels, continuous process vents, aggregate batch vent streams, and wastewater streams, an excursion means any of the three cases listed in paragraphs (f)(1)(i) through (f)(1)(iii) of this section. For a control or recovery device where multiple parameters are monitored, if one or more of the parameters meets the excursion criteria in paragraphs (f)(1)(i) through (f)(1)(iii) of this section, this is considered a single excursion for the control or recovery device.

(i) When the daily average value of one or more monitored parameters is above the maximum level or below the minimum level established for the given parameters.

(ii) When the period of control or recovery device operation is 4 hours or greater in an operating day and monitoring data are insufficient, as defined in paragraph (f)(1)(iv) of this section, to constitute a valid hour of data for at least 75 percent of the operating hours.

(iii) When the period of control or recovery device operation is less than 4 hours in an operating day and more than two of the hours during the period of operation do not constitute a valid hour of data due to insufficient monitoring data, as defined in paragraph (f)(1)(iv) of this section.

Monitoring data are insufficient to constitute a valid hour of data, as used in paragraphs (f)(1)(ii) and (f)(1)(iii) of this section, if measured values are unavailable for any of the 15-minute periods within the hour. For data compression systems approved under §63.1335(g)(3), monitoring data are insufficient to calculate a valid hour of data if there are less than four data measurements made during the hour.

(2) For batch process vents, an excursion means one of the two cases listed
§63.1335 General recordkeeping and reporting provisions.

(a) Data retention. Each owner or operator of an affected source shall keep copies of all applicable records and reports required by this subpart for at least 5 years, unless otherwise specified in this subpart.

(b) Requirements of subpart A of this part. The owner or operator of an affected source shall comply with the applicable recordkeeping and reporting requirements in subpart A of this part as specified in Table 1 of this subpart. These requirements include, but are not limited to, the requirements specified in paragraphs (b)(1) and (b)(2) of this section.

(1) Start-up, shutdown, and malfunction plan. The owner or operator of an affected source shall develop and implement a written start-up, shutdown, and malfunction plan as specified in §63.6(e)(3). This plan shall describe, in detail, procedures for operating and maintaining the affected source during periods of start-up, shutdown, and malfunction and a program for corrective action for malfunctioning process and air pollution control equipment used to comply with this subpart. The affected source shall keep this plan onsite and shall incorporate it by reference into their operating permit. Records associated with the plan shall be kept as specified in paragraphs (b)(1)(i)(A) through (b)(1)(i)(D) of this section. Reports related to the plan shall be submitted as specified in paragraph (b)(1)(ii) of this section.

(i) Records of start-up, shutdown, and malfunction. The owner or operator shall keep the records specified in paragraphs (b)(1)(i)(A) through (b)(1)(i)(D) of this section.

(A) Records of the occurrence and duration of each malfunction of air pollution control equipment or continuous monitoring systems used to comply with this subpart.

(B) For each start-up, shutdown, or malfunction, a statement that the procedures specified in the affected source’s start-up, shutdown, and malfunction plan were followed; alternatively, documentation of any actions taken that are not consistent with the plan.

(C) For continuous monitoring systems used to comply with this subpart, records documenting the completion of calibration checks and maintenance of continuous monitoring systems that are specified in the manufacturer’s instructions.

(D) Records specified in paragraphs (b)(1)(i)(B) and (b)(1)(i)(C) of this section are not required if they pertain solely to Group 2 emission points that
are not included in an emissions average or to Group 2 continuous process vents subject to §63.1315(a) with a total resource effectiveness value greater than 4.0 or, for Group 2 continuous process vents subject to §63.1315(b), with a total resource effectiveness value greater than 6.7.

(ii) Reports of start-up, shutdown, and malfunction. For the purposes of this subpart, the semiannual start-up, shutdown, and malfunction reports shall be submitted on the same schedule as the Periodic Reports required under paragraph (e)(6) of this section instead of the schedule specified in §63.10(d)(5)(i). Said reports shall include the information specified in paragraphs (b)(1)(i)(A) through (b)(1)(i)(C) of this section and shall contain the name, title, and signature of the owner or operator or other responsible official who is certifying its accuracy.

(2) Application for approval of construction or reconstruction. For new affected sources, each owner or operator shall comply with the provisions in §63.5 regarding construction and reconstruction, excluding the provisions specified in §63.5 (d)(1)(ii)(H), (d)(2), and (d)(3)(ii).

(c) Requirements of subpart H of this part. Owners or operators of affected sources shall comply with the reporting and recordkeeping requirements in subpart H of this part, except as specified in §63.1331.

(d) Recordkeeping and documentation. Owners or operators required to keep continuous records shall keep records as specified in paragraphs (d)(1) through (d)(8) of this section, unless an alternative recordkeeping system has been requested and approved as specified in paragraph (g) or (h) of this section. Documentation requirements are specified in paragraphs (d)(9) and (d)(10) of this section.

(c) The monitoring system shall measure data values at least once every 15 minutes.

(2) The owner or operator shall record either each measured data value or block average values for 1 hour or shorter periods calculated from all measured data values during each period. If values are measured more frequently than once per minute, a single value for each minute may be used to calculate the hourly (or shorter period) block average instead of all measured values. Owners or operators of batch process vents must record each measured data value.

(3) Daily average (or batch cycle daily average) values of each continuously monitored parameter shall be calculated for each operating day as specified in paragraphs (d)(3)(i) through (d)(3)(ii) of this section, except as specified in paragraph (d)(6) of this section.

(i) The daily average value or batch cycle daily average shall be calculated as the average of all parameter values recorded during the operating day. As specified in §63.1326(e)(2)(ii), only parameter values measured during those batch emission episodes, or portions thereof, in the batch cycle that the owner or operator has chosen to control shall be used to calculate the average. The calculated average shall cover a 24-hour period if operation is continuous, or the number of hours of operation per operating day if operation is not continuous.

(ii) The operating day shall be the period the owner or operator specifies in the operating permit or the Notification of Compliance Status. It may be from midnight to midnight or another 24-hour period.

(4) Records required when out of compliance. If the daily average (or batch cycle daily average) value of a monitored parameter for a given operating day is below the minimum level or above the maximum level established in the Notification of Compliance Status or operating permit, the owner or operator shall retain the data recorded that operating day under paragraph (d)(2) of this section.

(5) Records required when in compliance for daily average value or batch cycle daily average value. If the daily average (or batch cycle daily average) value of a monitored parameter for a given operating day is above the minimum level or below the maximum level established in the Notification of Compliance Status or operating permit, the owner or operator shall either:

(i) Retain block average values for 1 hour or shorter periods for that operating day; or

(ii) Retain the data recorded in paragraph (d)(2) of this section.
(6) Records required when all recorded values are in compliance. If all recorded values for a monitored parameter during an operating day are above the minimum level or below the maximum level established in the Notification of Compliance Status or operating permit, the owner or operator may record that all values were above the minimum level or below the maximum level rather than calculating and recording a daily average (or batch cycle daily average) for that operating day. For these operating days, the records required in paragraph (d)(5) of this section shall also be retained for 5 years.

(7) Monitoring data recorded during periods of monitoring system breakdowns, repairs, calibration checks, and zero (low-level) and high-level adjustments shall not be included in any average computed under this subpart. Records shall be kept of the times and durations of all such periods.

(8) In addition to the periods specified in paragraph (d)(7) of this section, records shall be kept of the times and durations of any other periods during process operation or control device operation when monitors are not operating. For batch process vents, this paragraph (d)(8) only applies during batch emission episodes, or portions thereof, that the owner or operator has selected to control.

(9) For each TPPU that is not part of the affected source because it does not use as a reactant or process solvent, or produce as a by-product or co-product any organic HAP, the owner or operator shall maintain the documentation specified in §63.1310(b)(1).

(10) For each flexible operation unit in which the primary product is determined to be something other than a thermoplastic product, the owner or operator shall maintain the documentation specified in §63.1310(f)(6).

(e) Reporting and notification. (1) In addition to the reports and notifications required by subparts A and H of this part, as specified in this subpart, the owner or operator of an affected source shall prepare and submit the reports listed in paragraphs (e)(3) through (e)(8) of this section, as applicable.

(2) All reports required under this subpart shall be sent to the Administrator at the addresses listed in §63.13. If acceptable to both the Administrator and the owner or operator of an affected source, reports may be submitted on electronic media.

(3) Precompliance Report. Affected sources requesting an extension for compliance, or requesting approval to use alternative monitoring parameters, alternative continuous monitoring and recordkeeping, or alternative controls, shall submit a Precompliance Report according to the schedule described in paragraph (e)(3)(i) of this section. The Precompliance Report shall contain the information specified in paragraphs (e)(3)(ii) through (e)(3)(vi) of this section, as appropriate.

(i) Submittal dates. The Precompliance Report shall be submitted to the Administrator no later than 12 months prior to the compliance date. For new affected sources, the Precompliance Report shall be submitted to the Administrator with the application for approval of construction or reconstruction required in paragraph (b)(2) of this section.

(ii) A request for an extension for compliance must be submitted in the Precompliance Report, if it has not been submitted to the operating permit authority as part of the operating permit application. The request for a compliance extension will include the data outlined in §63.6(i)(6)(i), (A), (B), and (D), as required in §63.1311(e)(1).

(iii) The alternative monitoring parameter information required in paragraph (f) of this section shall be submitted if, for any emission point, the owner or operator of an affected source seeks to comply through the use of a control technique other than those for which monitoring parameters are specified in this subpart or in subpart G of this part.

(iv) If the affected source seeks to comply using alternative continuous monitoring and recordkeeping as specified in paragraph (g) of this section, the information requested in paragraph (e)(3)(iv)(A) or (e)(3)(iv)(B) of this section must be submitted in the Precompliance Report.
(A) The owner or operator must submit notification of the intent to use the provisions specified in paragraph (g) of this section; or

(B) The owner or operator must submit a request for approval to use alternative continuous monitoring and recordkeeping provisions as specified in paragraph (g) of this section.

(v) The owner or operator shall report the intent to use alternative controls to comply with the provisions of this subpart. Alternative controls must be deemed by the Administrator to be equivalent to the controls required by the standard, under the procedures outlined in §63.6(g).

(vi) If an owner or operator demonstrates that the emissions estimation equations contained in §63.1323(b) are inappropriate as specified in §63.1323(b)(6)(ii)(B), the information required by §63.1323(b)(6)(ii)(D) shall be submitted.

(vii) If an owner or operator establishes parameter monitoring levels according to the procedures contained in §63.1334 (c) or (d), the information specified by §63.1334 (c) or (d), as appropriate.

(4) Emissions Averaging Plan. For all existing affected sources using emissions averaging, an Emissions Averaging Plan shall be submitted for approval according to the schedule and procedures described in paragraph (e)(4)(i) of this section. The Emissions Averaging Plan shall contain the information specified in paragraph (e)(4)(ii) of this section, unless the information required in paragraph (e)(4)(ii) of this section is submitted with an operating permit application. An owner or operator of an affected source who submits an operating permit application instead of an Emissions Averaging Plan shall submit the information specified in paragraph (e)(8) of this section. In addition, a supplement to the Emissions Averaging Plan, as required under paragraph (e)(4)(iii) of this section, is to be submitted whenever alternative controls or operating scenarios may be used to comply with this subpart. Updates to the Emissions Averaging Plan shall be submitted in accordance with paragraph (e)(4)(iv) of this section.

(i) Submittal and approval. The Emissions Averaging Plan shall be submitted no later than 18 months prior to the compliance date, and it is subject to Administrator approval. The Administrator shall determine within 120 operating days whether the Emissions Averaging Plan submitted presents sufficient information. The Administrator shall either approve the Emissions Averaging Plan, request changes, or request that the owner or operator submit additional information. Once the Administrator receives sufficient information, the Administrator shall approve, disapprove, or request changes to the plan within 120 operating days.

(ii) Information required. The Emissions Averaging Plan shall contain the information listed in paragraphs (e)(4)(ii)(A) through (e)(4)(ii)(K) of this section for all emission points included in an emissions average. (A) The required information shall include the identification of all emission points in the planned emissions average and, where applicable, notation of whether each storage vessel, continuous process vent, batch process vent, aggregate batch vent stream, and process wastewater stream is a Group 1 or Group 2 emission point, as defined in §63.1312 or as designated under §63.1332 (c)(3) through (c)(5).

(B) The required information shall include the projected emission debits and credits for each emission point and the sum for the emission points involved in the average calculated according to §63.1332. The projected credits must be greater than or equal to the projected debits, as required under §63.1332(e)(3).

(C) The required information shall include the specific control technology or pollution prevention measure that will be used for each emission point included in the average and date of application or expected date of application.

(D) The required information shall include the specific identification of each emission point affected by a pollution prevention measure. To be considered a pollution prevention measure, the criteria in §63.1332(j)(1) must be met. If the same pollution prevention measure reduces or eliminates emissions from multiple emission points in the average, the owner or operator
must identify each of these emission points.

(E) The required information shall include a statement that the compliance demonstration, monitoring, inspection, recordkeeping, and reporting provisions in §63.1332 (m), (n), and (o) that are applicable to each emission point in the emissions average will be implemented beginning on or before the date of compliance.

(F) The required information shall include documentation of the data listed in paragraphs (e)(4)(ii)(F)(1) through (e)(4)(ii)(F)(5) of this section for each storage vessel and continuous process vent subject to §63.1315 included in the average.

(1) The required documentation shall include the values of the parameters used to determine whether the emission point is Group 1 or Group 2. Where TRE index value is used for continuous process vent group determination, the estimated or measured values of the parameters used in the TRE equation in §63.115(d) and the resulting TRE index value shall be submitted.

(2) The required documentation shall include the estimated values of all parameters needed for input to the emission debit and credit calculations in §63.1332 (g) and (h). These parameter values shall be specified in the affected source’s Emissions Averaging Plan (or operating permit) as enforceable operating conditions. Changes to these parameters must be reported as required by paragraph (e)(4)(iv) of this section.

(3) The required documentation shall include the estimated percent reduction if a control technology achieving a lower percent reduction than the efficiency of the applicable reference control technology or standard is or will be applied to the emission point.

(4) The required documentation shall include the anticipated nominal efficiency if a control technology achieving a greater percent emission reduction than the efficiency of the reference control technology is or will be applied to the emission point. The procedures in §63.1332(i) shall be followed to apply for a nominal efficiency.

(5) The required documentation shall include the operating plan required by §63.1314, as specified in §63.122 (a)(2) and (b) for each storage vessel controlled with a closed-vent system with a control device other than a flare.

(G) The information specified in paragraph (f) of this section shall be included in the Emissions Averaging Plan for:

(1) Each continuous process vent subject to §63.1315 controlled by a pollution prevention measure or control technique for which monitoring parameters or inspection procedures are not specified in §63.114, and

(2) Each storage vessel controlled by pollution prevention or a control technique other than an internal or external floating roof or a closed vent system with a control device.

(H) The required information shall include documentation of the data listed in paragraphs (e)(4)(ii)(H)(1) through (e)(4)(ii)(H)(5) of this section for each collection of continuous process vents located in a process section within the affected source subject to §63.1316 (b)(1)(i), (b)(1)(ii), (b)(2)(i), (b)(2)(ii), or (c)(1) included in the average.

(1) For continuous process vents subject to §63.1316(b)(1)(i), the required documentation shall include the values of the parameters used to determine whether the emission point is Group 1 or Group 2. Continuous process vents subject to §63.1316 (b)(1)(ii), (b)(2)(i), (b)(2)(ii), or (c)(1) are considered Group 1 emission points for purposes of emissions averaging, as specified in §63.1332(c)(5).

(2) The required documentation shall include the estimated values of all parameters needed for input to the emission debit and credit calculations in §63.1332 (g) and (h). These parameter values shall be specified in the affected source’s Emissions Averaging Plan (or operating permit) as enforceable operating conditions. Changes to these parameters must be reported as required by paragraph (e)(4)(iv) of this section.

(3) For process sections generating debits or credits by comparing actual emissions expressed as kg HAP per Mg of product to the applicable standard, the required documentation shall include the actual emission level expressed as kg HAP emissions per Mg of product.

(4) For process sections using combustion control devices, the required
documentation shall include the estimated percent reduction if a control technology achieving a lower percent reduction than the efficiency of the applicable reference control technology or standard is or will be applied to the emission point.

(5) For process sections using combustion control devices, the required documentation shall include the anticipated nominal efficiency if a control technology achieving a greater percent emission reduction than the efficiency of the reference control technology is or will be applied to the emission point. The procedures in §63.1332(i) shall be followed to apply for a nominal efficiency.

(I) For each pollution prevention measure or control device used to reduce air emissions of organic HAP from each collection of continuous process vents located in a process section within the affected source subject to §63.1316 (b)(1)(i), (b)(1)(ii), (b)(2)(i), (b)(2)(ii), or (c)(1) and for which no monitoring parameters or inspection procedures are specified in §63.114, the information specified in paragraph (f) of this section, Alternative Monitoring Parameters, shall be included in the Emissions Averaging Plan.

(J) The required information shall include documentation of the data listed in paragraphs (e)(4)(ii)(L)(1) through (e)(4)(ii)(L)(4) of this section for each batch process vent and aggregate batch vent stream included in the average.

(K) For each pollution prevention measure or control device used to reduce air emissions of organic HAP from batch process vents or aggregate batch vent streams and for which no monitoring parameters or inspection procedures are specified in §63.1324, the information specified in paragraph (f) of this section, Alternative Monitoring Parameters, shall be included in the Emissions Averaging Plan.

(L) The required information shall include documentation of the data listed in paragraphs (e)(4)(ii)(L)(1) through (e)(4)(ii)(L)(4) of this section for each process wastewater stream included in the average.

(1) The required documentation shall include the data used to determine whether the wastewater stream is a Group 1 or Group 2 wastewater stream.

(2) The required documentation shall include the estimated values of all parameters needed for input to the wastewater emission credit and debit calculations in §63.1332 (g) and (h). These parameter values shall be specified in the affected source's Emissions Averaging Plan (or operating permit) as enforceable operating conditions. Changes to these parameters must be reported as required by paragraph (e)(4)(iv) of this section.

(3) The required documentation shall include the estimated percent reduction if:

(i) A control technology that achieves an emission reduction less than or equal to the emission reduction that would otherwise have been achieved by a steam stripper designed to the specifications found in §63.138(g) is or will be applied to the wastewater stream;

(ii) A control technology achieving less than or equal to 95 percent emission reduction is or will be applied to the vapor stream(s) vented and collected from the treatment processes; or

(iii) A pollution prevention measure is or will be applied.

(4) The required documentation shall include the anticipated nominal efficiency if the owner or operator plans to apply for a nominal efficiency under §63.1332(i). A nominal efficiency shall be applied for if:
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(i) A control technology that achieves an emission reduction greater than the emission reduction that would have been achieved by a steam stripper designed to the specifications found in §63.138(g), is or will be applied to the wastewater stream; or

(ii) A control technology achieving greater than 95 percent emission reduction is or will be applied to the vapor stream(s) vented and collected from the treatment processes.

(M) For each pollution prevention measure, treatment process, or control device used to reduce air emissions of organic HAP from wastewater and for which no monitoring parameters or inspection procedures are specified in §63.143, the information specified in paragraph (f) of this section, Alternative Monitoring Parameters, shall be included in the Emissions Averaging Plan.

(N) The required information shall include documentation of the data required by §63.1332(k). The documentation must demonstrate that the emissions from the emission points proposed to be included in the average will not result in greater hazard or, at the option of the Administrator, greater risk to human health or the environment than if the emission points were not included in an emissions average.

(iii) Supplement to Emissions Averaging Plan. The owner or operator required to prepare an Emissions Averaging Plan under paragraph (e)(4) of this section shall also prepare a supplement to the Emissions Averaging Plan for any alternative controls or operating scenarios that may be used to achieve compliance.

(iv) Updates to Emissions Averaging Plan. The owner or operator of an affected source required to submit an Emissions Averaging Plan under paragraph (e)(4) of this section shall also submit written updates of the Emissions Averaging Plan to the Administrator for approval under the circumstances described in paragraphs (e)(4)(iv)(A) and (e)(4)(iv)(B) of this section unless the relevant information has been included and submitted in an operating permit application or amendment.

(A) The owner or operator who plans to make a change listed in either paragraph (e)(4)(iv)(A)(1) or (e)(4)(iv)(A)(2) of this section shall submit an Emissions Averaging Plan update at least 120 operating days prior to making the change.

(1) An Emissions Averaging Plan update shall be submitted whenever an owner or operator elects to achieve compliance with the emissions averaging provisions in §63.1332 by using a control technique other than that specified in the Emissions Averaging Plan or plans to monitor a different parameter or operate a control device in a manner other than that specified in the Emissions Averaging Plan.

(2) An Emissions Averaging Plan update shall be submitted whenever an emission point or a TPPU is added to an existing affected source and is planned to be included in an emissions average, or whenever an emission point not included in the emissions average described in the Emissions Averaging Plan is to be added to an emissions average. The information in paragraph (e)(4) of this section shall be updated to include the additional emission point.

(B) The owner or operator who has made a change as defined in paragraph (e)(4)(iv)(B)(1) or (e)(4)(iv)(B)(2) of this section shall submit an Emissions Averaging Plan update within 90 operating days after the information regarding the change is known to the affected source. The update may be submitted in the next quarterly periodic report if the change is made after the date the Notification of Compliance Status is due.

(1) An Emissions Averaging Plan update shall be submitted whenever a process change is made such that the group status of any emission point in an emissions average changes.

(2) An Emissions Averaging Plan update shall be submitted whenever a value of a parameter in the emission credit or debit equations in §63.1332(g) or (h) changes such that it is below the minimum or above the maximum established level specified in the Emissions Averaging Plan and causes a decrease in the projected credits or an increase in the projected debits.

(C) The Administrator shall approve or request changes to the Emissions Averaging Plan.
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Averaging Plan update within 120 operating days of receipt of sufficient information regarding the change for emission points included in emissions averages.

(5) Notification of Compliance Status. For existing and new affected sources, a Notification of Compliance Status shall be submitted within 150 operating days after the compliance dates specified in § 63.1311. The notification shall contain the information listed in paragraphs (e)(5)(i) through (e)(5)(viii) of this section.

(i) The results of any emission point group determinations, process section applicability determinations, performance tests, inspections, continuous monitoring system performance evaluations, any other information used to demonstrate compliance, and any other information required to be included in the Notification of Compliance Status under § 63.122 for storage vessels, § 63.117 for continuous process vents, § 63.146 for process wastewater, § 63.1324 for batch process vents and aggregate batch vent streams, § 63.143(f) for process wastewater, § 63.1332(m) for emission points in emissions averages, paragraph (e)(8) or (f) of this section, the Notification of Compliance Status shall contain the information specified in paragraphs (e)(5)(ii)(A) through (e)(5)(ii)(D) of this section, unless this information has been established and provided in the operating permit.

(A) The required information shall include the specific maximum or minimum level of the monitored parameter(s) for each emission point.

(B) The required information shall include the rationale for the specific maximum or minimum level for each parameter for each emission point, including any data and calculations used to develop the level and a description of why the level indicates proper operation of the control device.

(C) The required information shall include a definition of the affected source's operating day, as specified in paragraph (d)(3)(ii) of this section, for purposes of determining daily average values or batch cycle daily average values of monitored parameters.

(D) For batch process vents, the required information shall include a definition of each batch cycle that requires the control of one or more batch emission episodes during the cycle, as specified in § 63.1325(c)(1) and § 63.1334(b)(3)(ii).

(iii) For emission points included in an emissions average, the Notification of Compliance Status shall contain the values of all parameters needed for input to the emission credit and debit equations in § 63.1332 (g) and (h), calculated or measured according to the procedures in § 63.1332 (g) and (h), and the resulting calculation of credits and debits for the first quarter of the year. The first quarter begins on the compliance date specified.
(iv) The determination of applicability for flexible operation units as specified in §63.1310(f)(6).

(v) The parameter monitoring levels for flexible operation units, and the basis on which these levels were selected, or a demonstration that these levels are selected at all times, as specified in §63.1310(f)(7).

(vi) The results for each predominant use determination for storage vessels belonging to an affected source subject to this subpart that is made under §63.1310(g)(6).

(vii) The results for each predominant use determination for recovery operation equipment belonging to an affected source subject to this subpart that is made under §63.1310(h)(6).

(viii) For owners or operators of Group 2 batch process vents establishing a batch cycle limitation as specified in §63.1325(g), the affected source's operating year for purposes of determining compliance with the batch cycle limitation.

(6) Periodic Reports. For existing and new affected sources, each owner or operator shall submit Periodic Reports as specified in paragraphs (e)(6)(i) through (e)(6)(xi) of this section.

(i) Except as specified in paragraphs (e)(6)(x) and (e)(6)(xi) of this section, a report containing the information in paragraph (e)(6)(ii) of this section or containing the information in paragraphs (e)(6)(iii) through (e)(6)(ix) of this section, as appropriate, shall be submitted semiannually no later than 60 operating days after the end of each 180 day period. The first report shall be submitted no later than 240 days after the date the Notification of Compliance Status is due and shall cover the 6-month period beginning on the date the Notification of Compliance Status is due. Subsequent reports shall cover each preceding 6-month period.

(ii) If none of the compliance exceptions specified in paragraphs (e)(6)(iii) through (e)(6)(ix) of this section occurred during the 6-month period, the Periodic Report required by paragraph (e)(6)(i) of this section shall be a statement that the affected source was in compliance for the preceding 6-month period and no activities specified in paragraphs (e)(6)(iii) through (e)(6)(ix) of this section occurred during the preceding 6-month period.

(iii) For an owner or operator of an affected source complying with the provisions of §§63.1314 through 63.1330 for any emission point or process section, Periodic Reports shall include:

(A) All information specified in §63.122 for storage vessels; §§63.117 and 63.118 and §63.1320 for continuous process vents, as applicable; §63.1327 for batch process vents and aggregate batch vent streams; §63.104 for heat exchange systems; and §63.146 for process wastewater.

(B) The daily average values or batch cycle daily average values of monitored parameters for both excused excursions, as defined in §63.1334(g), and unexcused excursions, as defined in §63.1334(f). For excursions caused by lack of monitoring data, the duration of periods when monitoring data were not collected shall be specified;

(C) The periods when monitoring data were not collected shall be specified;

(D) The information in paragraphs (e)(6)(iii)(D)(1) through (e)(6)(iii)(D)(3) of this section, as applicable:

(1) Any supplements to the Emissions Averaging Plan, as required in paragraph (e)(4)(iii) of this section;

(2) Notification if a process change is made such that the group status of any emission point changes. The information submitted shall include a compliance schedule, as specified in paragraphs (e)(6)(iii)(D)(2)(i) and (e)(6)(iii)(D)(2)(ii) of this section, for emission points that are added or that change from Group 2 to Group 1 as specified in §63.1310(i)(2)(ii); for continuous process vents under the conditions listed in §63.1315(a)(12) or §63.1320(b)(3), as applicable; or for batch process vents under the conditions listed in §63.1327(b) or §63.1327(d), as applicable; and

(i) The owner or operator shall submit to the Administrator for approval a compliance schedule and a justification for the schedule.

(ii) The Administrator shall approve the compliance schedule or request changes within 120 operating days of
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receipt of the compliance schedule and justification.

(3) Notification if one or more emission point(s) or one or more TPPU is added to an affected source. The owner or operator shall submit the information contained in paragraphs (e)(6)(iii)(D)(3)(i) through (e)(6)(iii)(D)(3)(iii) of this section:

(i) A description of the addition to the affected source;

(ii) Notification of the group status of the additional emission point or all emission points in the TPPU;

(iii) A compliance schedule, as required under paragraph (e)(6)(iii)(D)(2) of this section.

(E) The information in paragraph (b)(1)(ii) of this section for reports of start-up, shutdown, and malfunction.

(iv) For each batch process vent with a batch cycle limitation, every second Periodic Report shall include the type and number of batch cycles accomplished during the preceding 12-month period and a statement that the batch process vent is either in or out of compliance with the batch cycle limitation.

(v) If any performance tests are reported in a Periodic Report, the following information shall be included:

(A) One complete test report shall be submitted for each test method used for a particular kind of emission point tested. A complete test report shall contain the information specified in paragraph (e)(5)(i)(B) of this section.

(B) For additional tests performed for the same kind of emission point using the same method, results and any other information required shall be submitted, but a complete test report is not required.

(vi) The Periodic Report shall include the results for each change made to a primary product determination for a thermoplastic product made under § 63.1310(f)(6).

(vii) The Periodic Report shall include the results for each change made to a predominant use determination for a storage vessel belonging to an affected source subject to this subpart that is made under § 63.1310(g)(6).

(viii) The Periodic Report shall include the results for each change made to a predominant use determination for recovery operation equipment belonging to an affected source subject to this subpart that is made under § 63.1310(h)(6).

(ix) The Periodic Report required by § 63.1331(a)(5) may be submitted as part of the Periodic Report required by paragraph (e)(6) of this section.

(x) The owner or operator of an affected source shall submit quarterly reports for all emission points included in an emissions average.

(A) The quarterly reports shall be submitted no later than 60 operating days after the end of each quarter. The first report shall be submitted with the Notification of Compliance Status no later than 150 days after the compliance date.

(B) The quarterly reports shall include the information specified in paragraphs (e)(6)(x)(B)(1) through (e)(6)(x)(B)(7) of this section for all emission points included in an emissions average.

(1) The credits and debits calculated each month during the quarter;

(2) A demonstration that debits calculated for the quarter are not more than 1.30 times the credits calculated for the quarter, as required under § 63.1332(e)(4);

(3) The values of any inputs to the debit and credit equations in § 63.1332(g) and (h) that change from month to month during the quarter or that have changed since the previous quarter;

(4) Results of any performance tests conducted during the reporting period including one complete report for each test method used for a particular kind of emission point as described in paragraph (e)(6)(v) of this section;

(5) Reports of daily average (or batch cycle daily average) values of monitored parameters for excursions as defined in § 63.1334(f);

(6) For excursions caused by lack of monitoring data, the duration of periods when monitoring data were not collected shall be specified; and

(7) Any other information the affected source is required to report under the operating permit or Emissions Averaging Plan for the affected source.

(C) § 63.1334 shall govern the use of monitoring data to determine compliance for Group 1 and Group 2 emission points included in emissions averages.
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(D) Every fourth quarterly report shall include the following:

(1) A demonstration that annual credits are greater than or equal to annual debits as required by §63.1332(e)(3); and

(2) A certification of compliance with all the emissions averaging provisions in §63.1332.

(xi) The owner or operator of an affected source shall submit quarterly reports for particular emission points and process sections not included in an emissions average as specified in paragraphs (e)(6)(xi)(A) through (e)(6)(xi)(E) of this section.

(A) If requested by the Administrator, the owner or operator of an affected source shall submit quarterly reports for a period of 1 year for an emission point or process section that is not included in an emissions average if either condition in paragraph (e)(6)(xi)(A)(1) or (e)(6)(xi)(A)(2) of this section is met.

(1) An emission point has any excursions, as defined in §63.1334(f), for a semiannual reporting period.

(2) A process section subject to §63.1316 is out of compliance with its applicable standard.

(B) The quarterly reports shall include all information specified in paragraphs (e)(6)(iii) through (e)(6)(ix) of this section applicable to the emission point or process section for which quarterly reporting is required under paragraph (e)(6)(xi)(A) of this section. Information applicable to other emission points within the affected source shall be submitted in the semiannual reports required under paragraph (e)(6)(i) of this section.

(C) Quarterly reports shall be submitted no later than 60 operating days after the end of each quarter.

(D) After quarterly reports have been submitted for an emission point for 1 year, the owner or operator may return to semiannual reporting for the emission point or process section unless the Administrator requests the owner or operator to continue to submit quarterly reports.

(E) §63.1334 shall govern the use of monitoring data to determine compliance for Group 1 emission points.

(7) Other reports. Other reports shall be submitted as specified in paragraphs (e)(7)(i) through (e)(7)(iii) of this section.

(i) For storage vessels, the notifications of inspections required by §63.1314 shall be submitted as specified in §63.122(h)(1) and (h)(2). (ii) For owners or operators of affected sources required to request approval for a nominal control efficiency for use in calculating credits for an emissions average, the information specified in §63.1332(i) shall be submitted.

(8) Operating permit. An owner or operator who submits an operating permit application instead of an Emissions Averaging Plan or a Precompliance Report shall submit the following information with the operating permit application:

(i) The information specified in paragraph (e)(4) of this section for points included in an emissions average;

(ii) The information specified in paragraph (e)(5) of this section, Notification of Compliance Status, as applicable; and

(iii) The information specified in paragraph (e)(3) of this section, Precompliance Report, as applicable.

(f) Alternative monitoring parameters. The owner or operator who has been directed by any section of this subpart to set unique monitoring parameters, or who requests approval to monitor a different parameter than those specified in §63.1314 for storage vessels, §63.1315 or 63.1317, as appropriate, for continuous process vents, §63.1321 for batch process vents and aggregate batch vent streams, or §63.1330 for wastewater shall submit the information specified in paragraphs (f)(1) through (f)(3) of this section in the Precompliance Report, as required by paragraph (e)(3) of this section. The owner or operator shall retain for a period of 5 years each record required by paragraphs (f)(1) through (f)(3) of this section.

(1) The required information shall include a description of the parameter(s) to be monitored to ensure the recovery device, control device, or pollution prevention measure is operated in conformance with its design and achieves the specified emission limit, percent reduction, or nominal efficiency, and an explanation of the criteria used to select the parameter(s).
(2) The required information shall include a description of the methods and procedures that will be used to demonstrate that the parameter indicates proper operation, the schedule for this demonstration, and a statement that the owner or operator will establish a level for the monitored parameter as part of the Notification of Compliance Status report required in paragraph (e)(5) of this section, unless this information has already been included in the operating permit application.

(3) The required information shall include a description of the proposed monitoring, recordkeeping, and reporting system, to include the frequency and content of monitoring, recordkeeping, and reporting. Further, the rationale for the proposed monitoring, recordkeeping, and reporting system shall be included if either condition in paragraph (f)(3)(i) or (f)(3)(ii) of this section is met:

(i) If monitoring and recordkeeping is not continuous; or

(ii) If reports of daily average values will not be included in Periodic Reports when the monitored parameter value is above the maximum level or below the minimum level as established in the operating permit or the Notification of Compliance Status.

(g) Alternative continuous monitoring and recordkeeping. An owner or operator choosing not to implement the provisions listed in §63.1315 or 63.1317, as appropriate, for continuous process vents, §63.1321 for batch process vents and aggregate batch vent streams, §63.1314 for storage vessels, or §63.1330 for wastewater, may instead request approval to use alternative continuous monitoring and recordkeeping provisions according to the procedures specified in paragraphs (g)(1) through (g)(4) of this section. Requests shall be submitted in the Precompliance Report as specified in paragraph (e)(3) of this section, if not already included in the operating permit application, and shall contain the information specified in paragraphs (g)(2)(i) and (g)(3)(ii) of this section, as applicable.

(1) The provisions in §63.8(f)(5)(ii) shall govern the review and approval of requests.

(2) An owner or operator of an affected source that does not have an automated monitoring and recording system capable of measuring parameter values at least once every 15 minutes and that does not generate continuous records may request approval to use a nonautomated system with less frequent monitoring, in accordance with paragraphs (g)(2)(i) and (g)(2)(ii) of this section.

(i) The requested system shall include manual reading and recording of the value of the relevant operating parameter no less frequently than once per hour. Daily average (or batch cycle daily average) values shall be calculated from these hourly values and recorded.

(ii) The request shall contain:

(A) A description of the planned monitoring and recordkeeping system;

(B) Documentation that the affected source does not have an automated monitoring and recording system;

(C) Justification for requesting an alternative monitoring and recordkeeping system; and

(D) Demonstration to the Administrator's satisfaction that the proposed monitoring frequency is sufficient to represent control or recovery device operating conditions, considering typical variability of the specific process and control or recovery device operating parameter being monitored.

(3) An owner or operator may request approval to use an automated data compression recording system that does not record monitored operating parameter values at a set frequency (for example, once every 15 minutes) but records all values that meet set criteria for variation from previously recorded values, in accordance with paragraphs (g)(3)(i) and (g)(3)(ii) of this section.

(i) The requested system shall be designed to:

(A) Measure the operating parameter value at least once every 15 minutes;

(B) Except for the monitoring of batch process vents, calculate hourly average values each hour during periods of operation;

(C) Record the date and time when monitors are turned off or on;

(D) Recognize unchanging data that may indicate the monitor is not functioning properly, alert the operator, and record the incident;
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(E) Calculate daily average (or batch cycle daily average) values of the monitored operating parameter based on all measured data; and

(F) If the daily average is not an excursion, as defined in §63.1334(f), the data for that operating day may be converted to hourly average values and the four or more individual records for each hour in the operating day may be discarded.

(ii) The request shall contain:
(A) A description of the monitoring system and data compression recording system, including the criteria used to determine which monitored values are recorded and retained;
(B) The method for calculating daily averages and batch cycle daily averages; and
(C) A demonstration that the system meets all criteria in paragraph (g)(3)(i) of this section.

(4) An owner or operator may request approval to use other alternative monitoring systems according to the procedures specified in §63.8(f).

(h) Reduced recordkeeping program. For any parameter with respect to any item of equipment, the owner or operator may implement the recordkeeping requirements specified in paragraph (h)(1) or (h)(2) of this section as alternatives to the provisions specified in §63.1314 for storage vessels, §63.1315 or 63.1317, as appropriate, for continuous process vents, §63.1321 for batch process vents and aggregate batch vent streams, or §63.1330 for wastewater.

The owner or operator shall retain for a period of 5 years each record required by paragraph (h)(1) or (h)(2) of this section.

(i) The owner or operator may retain only the daily average (or batch cycle daily average) value, and is not required to retain more frequent monitored operating parameter values, for a monitored parameter with respect to an item of equipment, if the requirements of paragraphs (h)(1)(i) through (h)(1)(vi) of this section are met. An owner or operator electing to comply with the requirements of paragraph (h)(1) of this section shall notify the Administrator in the Notification of Compliance Status or, if the Notification of Compliance Status has already been submitted, in the Periodic Report immediately preceding implementation of the requirements of paragraph (h)(1) of this section.

(i) The monitoring system is capable of detecting unrealistic or impossible data during periods of operation other than start-ups, shutdowns, or malfunctions (e.g., a temperature reading of −200 °C on a boiler), and will alert the operator by alarm or other means. The owner or operator shall record the occurrence. All instances of the alarm or other alert in an operating day constitute a single occurrence.

(ii) The monitoring system generates, updated at least hourly throughout each operating day, a running average of the monitoring values that have been obtained during that operating day, and the capability to observe this running average is readily available to the Administrator on-site during the operating day. The owner or operator shall record the occurrence of any period meeting the criteria in paragraphs (h)(1)(ii)(A) through (h)(1)(ii)(C) of this section. All instances in an operating day constitute a single occurrence.

(A) The running average is above the maximum or below the minimum established limits;
(B) The running average is based on at least six 1-hour periods; and
(C) The running average reflects a period of operation other than a start-up, shutdown, or malfunction.

(iii) The monitoring system is capable of detecting unchanging data during periods of operation other than start-ups, shutdowns, or malfunctions, except in circumstances where the presence of unchanging data is the expected operating condition based on past experience (e.g., pH in some scrubbers), and will alert the operator by alarm or other means. The owner or operator shall record the occurrence. All instances of the alarm or other alert in an operating day constitute a single occurrence.

(iv) The monitoring system will alert the owner or operator by an alarm, if the running average parameter value calculated under paragraph (h)(1)(ii) of this section reaches a set point that is appropriately related to the established limit for the parameter that is being monitored.
(v) The owner or operator shall verify the proper functioning of the monitoring system, including its ability to comply with the requirements of paragraph (h)(1) of this section, at the times specified in paragraphs (h)(1)(v)(A) through (h)(1)(v)(C). The owner or operator shall document that the required verifications occurred.

(A) Upon initial installation.

(B) Annually after initial installation.

(C) After any change to the programming or equipment constituting the monitoring system, which might reasonably be expected to alter the monitoring system’s ability to comply with the requirements of this section.

(vi) The owner or operator shall retain the records identified in paragraphs (h)(1)(vi)(A) through (h)(1)(vi)(C) of this section.

(A) Identification of each parameter, for each item of equipment, for which the owner or operator has elected to comply with the requirements of paragraph (h) of this section.

(B) A description of the applicable monitoring system(s), and of how compliance will be achieved with each requirement of paragraphs (h)(2)(i) through (h)(2)(v) of this section. The description shall identify the location and format (e.g., on-line storage, log entries) for each required record. If the description changes, the owner or operator shall retain both the current and the most recent superseded description.

(C) A description, and the date, of any change to the monitoring system that would reasonably be expected to affect its ability to comply with the requirements of paragraph (h)(1) of this section.

(2) If an owner or operator has elected to implement the requirements of paragraph (h)(1) of this section for a monitored parameter with respect to an item of equipment and a period of 6 consecutive months has passed without an excursion as defined in paragraph (h)(2) of this section, the owner or operator shall immediately resume retaining the daily average (or batch cycle daily average) value for each operating day and shall notify the Administrator in the next Periodic Report. The owner or operator shall continue to retain each daily average (or batch cycle daily average) value until another period of 6 consecutive months has passed without an excursion as defined in paragraph (h)(2)(iv) of this section.

(i) If the owner or operator elects not to retain the daily average (or batch cycle daily average) values, the owner or operator shall notify the Administrator in the next Periodic Report. The notification shall identify the parameter and unit of equipment.

(ii) If, on any operating day after the owner or operator has ceased recording daily average (or batch cycle daily average) values as provided in paragraph (h)(2) of this section, there is an excursion as defined in paragraph (h)(2)(iv) of this section, the owner or operator shall immediately resume retaining the daily average (or batch cycle daily average) value for each operating day and shall notify the Administrator in the next Periodic Report. The owner or operator shall continue to retain each daily average (or batch cycle daily average) value until another period of 6 consecutive months has passed without an excursion as defined in paragraph (h)(2)(iv) of this section.

(iii) The owner or operator shall retain the records specified in paragraphs (h)(2)(i), (h)(2)(ii), and (h)(2)(vi) of this section, for the duration specified in paragraph (h) of this section. For any calendar week, if compliance with paragraphs (h)(1)(i) through (h)(1)(iv) of this section does not result in retention of a record of at least one occurrence of or measured parameter value, the owner or operator shall retain at least one parameter value during a period of operation other than a start-up, shutdown, or malfunction.

(iv) For purposes of paragraph (h) of this section, an excursion means that the daily average (or batch cycle daily average) value of monitoring data for a parameter is greater than the maximum, or less than the minimum established limit. With approval by the Administrator, monitoring data generated prior to the compliance date of this subpart shall be credited toward the period of 6 consecutive months, if the parameter limit and the monitoring accomplished during the period prior to the compliance date was required and/or approved by the Administrator.

(A) The daily average (or batch cycle daily average) value during any start-
up, shutdown, or malfunction shall not be considered an excursion for purposes of paragraph (h)(2) of this section, if the owner or operator follows the applicable provisions of the start-up, shutdown, and malfunction plan required by §63.6(e)(3).

(B) An excused excursion, as described in §63.1334(g), shall not be considered an excursion for purposes of paragraph (h)(2) of this section.

[60 FR 48209, Sept. 12, 1996, as amended at 64 FR 11553, Mar. 9, 1999]

### TABLE 1—APPLICABILITY OF GENERAL PROVISIONS TO SUBPART JJJ AFFECTED SOURCES

<table>
<thead>
<tr>
<th>Reference</th>
<th>Applies to subpart JJJ</th>
<th>Comment</th>
</tr>
</thead>
<tbody>
<tr>
<td>63.1(a)(1)</td>
<td>Yes</td>
<td>§63.1312 specifies definitions in addition to or that supersede definitions in §63.2.</td>
</tr>
<tr>
<td>63.1(a)(2)–63.1(a)(3)</td>
<td>Yes.</td>
<td>Subpart JJJ (this table) specifies the applicability of each paragraph in subpart A to subpart JJJ.</td>
</tr>
<tr>
<td>63.1(a)(5)</td>
<td>Yes.</td>
<td>Subpart JJJ (this table) specifies the applicability of each paragraph in subpart A to subpart JJJ.</td>
</tr>
<tr>
<td>63.1(a)(6)–63.1(a)(8)</td>
<td>Yes.</td>
<td>Subpart JJJ (this table) specifies the applicability of each paragraph in subpart A to subpart JJJ.</td>
</tr>
<tr>
<td>63.1(a)(9)</td>
<td>Yes.</td>
<td>Subpart JJJ (this table) specifies the applicability of each paragraph in subpart A to subpart JJJ.</td>
</tr>
<tr>
<td>63.1(b)(10)</td>
<td>No.</td>
<td>§63.1310(b) provides documentation requirements for TPPUs not considered affected sources.</td>
</tr>
<tr>
<td>63.1(c)(1)</td>
<td>Yes.</td>
<td>Subpart JJJ (this table) specifies the applicability of each paragraph in subpart A to subpart JJJ.</td>
</tr>
<tr>
<td>63.1(c)(2)</td>
<td>No.</td>
<td>Area sources are not subject to subpart JJJ.</td>
</tr>
<tr>
<td>63.1(c)(3)</td>
<td>No.</td>
<td>Reserved.</td>
</tr>
<tr>
<td>63.1(c)(4)</td>
<td>Yes.</td>
<td>Except that affected sources are not required to submit notifications overridden by this table.</td>
</tr>
<tr>
<td>63.1(d)</td>
<td>No.</td>
<td>Reserved.</td>
</tr>
<tr>
<td>63.1(e)</td>
<td>Yes.</td>
<td>§63.1312 specifies those subpart A definitions that apply to subpart JJJ.</td>
</tr>
<tr>
<td>63.2</td>
<td>Yes.</td>
<td>Subpart JJJ specifies those units of measure that apply to subpart JJJ.</td>
</tr>
<tr>
<td>63.3</td>
<td>Yes.</td>
<td>Reserved.</td>
</tr>
<tr>
<td>63.4(a)(1)–63.4(a)(3)</td>
<td>Yes.</td>
<td>Reserved.</td>
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<tr>
<td>63.4(a)(4)</td>
<td>No.</td>
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<td>63.4(a)(5)</td>
<td>Yes.</td>
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<tr>
<td>63.4(b)</td>
<td>Yes.</td>
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<tr>
<td>63.4(c)</td>
<td>Yes.</td>
<td>Reserved.</td>
</tr>
<tr>
<td>63.5a</td>
<td>Yes.</td>
<td>Reserved.</td>
</tr>
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<td>63.5(b)(1)</td>
<td>Yes.</td>
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</tr>
<tr>
<td>63.5(b)(2)</td>
<td>No.</td>
<td>Reserved.</td>
</tr>
<tr>
<td>63.5(b)(3)</td>
<td>Yes.</td>
<td>Area sources are not subject to subpart JJJ.</td>
</tr>
<tr>
<td>63.5(b)(4)</td>
<td>Yes.</td>
<td>§63.1310(i) specifies requirements.</td>
</tr>
<tr>
<td>63.5(b)(5)</td>
<td>No.</td>
<td>Reserved.</td>
</tr>
<tr>
<td>63.5(c)</td>
<td>Yes.</td>
<td>Reserved.</td>
</tr>
<tr>
<td>63.5(d)(1)(i)</td>
<td>Yes.</td>
<td>Except that for affected sources subject to subpart JJJ, emission estimates specified in §63.5(d)(1)(i)(H) are not required.</td>
</tr>
<tr>
<td>63.5(d)(1)(ii)</td>
<td>Yes.</td>
<td>Except §63.5(d)(1)(ii) does not apply.</td>
</tr>
<tr>
<td>63.5(d)(1)(iii)</td>
<td>Yes.</td>
<td>Except §63.5(d)(1)(iii) does not apply.</td>
</tr>
<tr>
<td>63.5(d)(1)(iv)</td>
<td>Yes.</td>
<td>Except §63.5(d)(1)(iv) does not apply.</td>
</tr>
<tr>
<td>63.5(d)(2)</td>
<td>Yes.</td>
<td>Except §63.5(d)(2) does not apply.</td>
</tr>
<tr>
<td>63.5(d)(3)</td>
<td>No.</td>
<td>Except §63.5(d)(3) does not apply.</td>
</tr>
<tr>
<td>63.5(d)(4)</td>
<td>Yes.</td>
<td>Except §63.5(d)(4) does not apply.</td>
</tr>
<tr>
<td>63.5(e)</td>
<td>Yes.</td>
<td>Except §63.5(e) does not apply.</td>
</tr>
<tr>
<td>63.5(f)(1)</td>
<td>Yes.</td>
<td>Except §63.5(f)(1) does not apply.</td>
</tr>
</tbody>
</table>
### Table 1. Applicability of General Provisions to Subpart JJJ Affected Sources—Continued

<table>
<thead>
<tr>
<th>Reference</th>
<th>Applies to Subpart JJJ</th>
<th>Comment</th>
</tr>
</thead>
<tbody>
<tr>
<td>§ 63.6(g)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.5(f)(2)</td>
<td>Yes</td>
<td>Except that where §63.5(d)(1) is referred to, §63.5(d)(1)(i) does not apply.</td>
</tr>
<tr>
<td>§ 63.6(d)</td>
<td>Yes</td>
<td>Subpart JJJ does not require opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.7(b)</td>
<td>Yes</td>
<td>Except §63.6(i)(15), which is reserved.</td>
</tr>
<tr>
<td>§ 63.6(j)</td>
<td>Yes</td>
<td>Except §63.6(i)(15), which is reserved.</td>
</tr>
<tr>
<td>§ 63.6(f)(1)</td>
<td>Yes</td>
<td>Except that where §63.6(d)(1) is referred to, §63.6(d)(1)(i) does not apply.</td>
</tr>
<tr>
<td>§ 63.7(e)</td>
<td>Yes</td>
<td>Except that performance tests must be conducted at maximum representative operating conditions. In addition, some of the testing requirements specified in subpart JJJ are not consistent with §63.7(e)(3).</td>
</tr>
<tr>
<td>§ 63.6(h)</td>
<td>Yes</td>
<td>Subpart JJJ does not require opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.7(f)</td>
<td>Yes</td>
<td>Subpart JJJ specifies locations to conduct monitoring.</td>
</tr>
<tr>
<td>§ 63.7(g)</td>
<td>Yes</td>
<td>Timeframe for submitting request is specified in §63.1335(e).</td>
</tr>
<tr>
<td>§ 63.7(h)</td>
<td>Yes</td>
<td>Subpart JJJ does not require continuous emission monitors.</td>
</tr>
<tr>
<td>§ 63.6(a)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(b)(1)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(b)(2)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(b)(3)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(b)(4)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(b)(5)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(b)(6)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(b)(7)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(c)(1)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(c)(2)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(c)(3)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(c)(4)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(c)(5)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.6(c)(6)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(c)(7)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(c)(8)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.6(c)(9)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.6(c)(10)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.6(c)(11)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(c)(12)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(e)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(f)(1)</td>
<td>Yes</td>
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<tr>
<td>§ 63.6(f)(2)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.6(f)(3)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(f)(4)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(f)(5)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(f)(6)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(f)(7)</td>
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<td>§ 63.6(f)(8)</td>
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<td>§ 63.6(f)(9)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§ 63.6(f)(10)</td>
<td>Yes</td>
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<td>§ 63.6(f)(11)</td>
<td>Yes</td>
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<tr>
<td>§ 63.6(f)(12)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.6(h)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(i)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.6(j)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.7(a)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.7(b)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§ 63.7(c)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§ 63.7(d)</td>
<td>Yes</td>
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<td>§ 63.7(e)</td>
<td>Yes</td>
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<td>§ 63.7(f)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§ 63.7(g)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.7(h)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.7(i)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§ 63.7(j)</td>
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<td>§ 63.7(k)</td>
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<tr>
<td>§ 63.7(l)</td>
<td>Yes</td>
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<td>§ 63.7(m)</td>
<td>Yes</td>
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<td>§ 63.7(n)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§ 63.7(o)</td>
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<td>§ 63.7(p)</td>
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<td>§ 63.7(q)</td>
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<td>§ 63.7(r)</td>
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<td>§ 63.7(s)</td>
<td>Yes</td>
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<td>§ 63.7(t)</td>
<td>Yes</td>
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<td>§ 63.7(u)</td>
<td>Yes</td>
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<td>§ 63.7(v)</td>
<td>Yes</td>
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<td>§ 63.7(w)</td>
<td>Yes</td>
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<tr>
<td>§ 63.7(x)</td>
<td>Yes</td>
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<tr>
<td>§ 63.7(y)</td>
<td>Yes</td>
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<tr>
<td>§ 63.7(z)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§ 63.8(a)(1)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§ 63.8(a)(2)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.8(a)(3)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(a)(4)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(b)(1)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.8(b)(2)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.8(b)(3)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§ 63.8(c)(1)(i)</td>
<td>Yes</td>
<td>Reserved.</td>
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<tr>
<td>§ 63.8(c)(1)(ii)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(c)(1)(iii)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(c)(2)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(c)(3)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(c)(4)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(c)(5)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(c)(6)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(c)(7)</td>
<td>Yes</td>
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</tr>
<tr>
<td>§ 63.8(c)(8)</td>
<td>Yes</td>
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<tr>
<td>§ 63.8(d)</td>
<td>Yes</td>
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</tr>
<tr>
<td>§ 63.8(e)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(f)(1)–§63.8(f)(3)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(f)(4)(i)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(f)(4)(ii)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(f)(5)(i)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(f)(5)(ii)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(f)(6)</td>
<td>Yes</td>
<td>Reserved.</td>
</tr>
</tbody>
</table>
### TABLE 1.—Applicability of General Provisions to Subpart JJJ Affected Sources—Continued

<table>
<thead>
<tr>
<th>Reference</th>
<th>Applies to Subpart JJJ</th>
<th>Comment</th>
</tr>
</thead>
<tbody>
<tr>
<td>63.8(g)</td>
<td></td>
<td>Data reduction procedures specified in §63.1335(d).</td>
</tr>
<tr>
<td>63.9(a)</td>
<td>Yes</td>
<td>Subpart JJJ does not require an initial notification.</td>
</tr>
<tr>
<td>63.9(c)</td>
<td>Yes</td>
<td>Subpart JJJ does not require opacity and visible emission standards.</td>
</tr>
<tr>
<td>63.10(d)(4)</td>
<td>Yes</td>
<td>§63.1335(e)(5) specifies Notification of Compliance Status requirements.</td>
</tr>
<tr>
<td>63.10(d)(5)</td>
<td>No</td>
<td>§63.1310(b) requires documentation of sources that are not affected sources.</td>
</tr>
<tr>
<td>63.10(d)(6)</td>
<td>No</td>
<td>§63.1335 specifies recordkeeping requirements.</td>
</tr>
<tr>
<td>63.10(d)(7)</td>
<td>Yes</td>
<td>Subpart JJJ does not require opacity and visible emission standards.</td>
</tr>
<tr>
<td>63.10(d)(8)</td>
<td>Yes</td>
<td>Except that reports required by §63.10(d)(5)(i) may be submitted at the same time as Periodic Reports specified in §63.1335(e)(6). The start-up, shutdown, and malfunction plan, and any records or reports of start-up, shutdown, and malfunction do not apply to Group 2 emission points unless they are included in an emissions average.</td>
</tr>
<tr>
<td>63.10(d)(9)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.10(e)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.10(f)</td>
<td>Yes</td>
<td></td>
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<tr>
<td>63.11</td>
<td>Yes</td>
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<td>63.12</td>
<td>Yes</td>
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<td>63.13</td>
<td>Yes</td>
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<td>63.14</td>
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<tr>
<td>63.15</td>
<td>Yes</td>
<td></td>
</tr>
</tbody>
</table>

### TABLE 2.—Group 1 Storage Vessels at Existing Affected Sources

<table>
<thead>
<tr>
<th>Vessel capacity (cubic meters)</th>
<th>Vapor pressure (kilopascals)</th>
</tr>
</thead>
<tbody>
<tr>
<td>75 ≤ capacity &lt; 151</td>
<td>≥ 5.2</td>
</tr>
<tr>
<td>151 ≥ capacity</td>
<td>≥ 13.1</td>
</tr>
</tbody>
</table>

*Maximum true vapor pressure of total organic HAP at storage temperature.

### TABLE 3 TO Subpart JJJ.—Group 1 Storage Vessels at Existing Affected Sources Producing the Listed Thermoplastics

<table>
<thead>
<tr>
<th>Thermoplastic</th>
<th>Chemical&lt;sup&gt;a&lt;/sup&gt;</th>
<th>Vessel capacity (cubic meters)</th>
<th>Vapor pressure (kilopascals)</th>
</tr>
</thead>
<tbody>
<tr>
<td>ASA/AMSAN&lt;sup&gt;b&lt;/sup&gt;</td>
<td>styrene/acrylonitrile mixture</td>
<td>≥ 3.78</td>
<td>≥ 0.47</td>
</tr>
<tr>
<td></td>
<td>acrylonitrile</td>
<td>≥ 75.7</td>
<td>≥ 1.62</td>
</tr>
<tr>
<td>Polystyrene, continuous processes</td>
<td>all chemicals &lt;75.7</td>
<td>≥ 1.9</td>
<td>≥ 1.8</td>
</tr>
<tr>
<td>Nitride&lt;sup&gt;c&lt;/sup&gt;</td>
<td>acrylonitrile</td>
<td>≥ 13.25</td>
<td></td>
</tr>
</tbody>
</table>

<sup>a</sup>Vessel capacity and vapor pressure criteria are specific to the listed chemical or to "all chemicals," as indicated.

<sup>b</sup>Maximum true vapor pressure of total organic HAP at storage temperature.

<sup>c</sup>The applicability criteria in Table 2 of this subpart shall be used for chemicals not specifically listed in this table (i.e., Table 3).
### Table 4—Group 1 Storage Vessels at New Affected Sources

<table>
<thead>
<tr>
<th>Thermoplastic</th>
<th>Organic HAP/chemical name (CAS No.)</th>
<th>Vessel capacity (cubic meters)</th>
<th>Vapor pressure a (kilopascals)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Styrene/ acrylonitrile mixture</td>
<td>Acetaldehyde (75-07-0)</td>
<td>≥ 3.78</td>
<td>≥ 0.47</td>
</tr>
<tr>
<td>Acrylonitrile</td>
<td>Acrylic acid (107-13-1)</td>
<td>≥ 75.7</td>
<td>≥ 1.62</td>
</tr>
<tr>
<td>All chemicals</td>
<td>Acrylic acid (107-13-1)</td>
<td>≥ 2.271</td>
<td>≥ 0.5 and &lt; 0.7</td>
</tr>
<tr>
<td>&lt; 151</td>
<td>Acrylic acid (107-13-1)</td>
<td>≥ 10</td>
<td>0.7</td>
</tr>
<tr>
<td>SAN, continuous b</td>
<td>Acrylic acid (107-13-1)</td>
<td>≥ 13.25</td>
<td>≥ 1.8</td>
</tr>
<tr>
<td>Polystyrene, continuous processes</td>
<td>Acrylic acid (107-13-1)</td>
<td>≥ 19.6 and &lt;45.4</td>
<td>≥ 7.48</td>
</tr>
<tr>
<td>Ethylene glycol</td>
<td>Ethylene glycol (107-21-1)</td>
<td>≥ 45.4 and &lt;109.8</td>
<td>≥ 0.6</td>
</tr>
<tr>
<td>Styrene</td>
<td>Styrene</td>
<td>≥ 45.43</td>
<td>≥ 0.078</td>
</tr>
<tr>
<td>All other chemicals</td>
<td>Styrene</td>
<td>≥ 45.43</td>
<td>≥ 0.53</td>
</tr>
</tbody>
</table>

- Maximum true vapor pressure of total organic HAP at storage temperature.

### Table 5 to Subpart JJJ—Group 1 Storage Vessels at New Affected Sources Producing the Listed Thermoplastics

<table>
<thead>
<tr>
<th>Thermoplastic</th>
<th>Vessel capacity (cubic meters)</th>
<th>Vapor pressure b (kilopascals)</th>
</tr>
</thead>
<tbody>
<tr>
<td>ASA/MABS</td>
<td>Styrene/ acrylonitrile mixture</td>
<td>≥ 3.78</td>
</tr>
<tr>
<td>Acrylonitrile</td>
<td>Acrylic acid (107-13-1)</td>
<td>≥ 75.7</td>
</tr>
<tr>
<td>All chemicals</td>
<td>Acrylic acid (107-13-1)</td>
<td>≥ 2.271</td>
</tr>
<tr>
<td>&lt; 151</td>
<td>Acrylic acid (107-13-1)</td>
<td>≥ 10</td>
</tr>
<tr>
<td>Polystyrene, continuous processes</td>
<td>Acrylic acid (107-13-1)</td>
<td>≥ 13.25</td>
</tr>
<tr>
<td>Ethylene glycol</td>
<td>Ethylene glycol (107-21-1)</td>
<td>≥ 19.6 and &lt;45.4</td>
</tr>
<tr>
<td>Styrene</td>
<td>Styrene</td>
<td>≥ 45.43</td>
</tr>
<tr>
<td>All other chemicals</td>
<td>Styrene</td>
<td>≥ 45.43</td>
</tr>
</tbody>
</table>

- Vessel capacity and vapor pressure criteria are specific to the listed chemical, to “all chemicals,” or to “all other chemicals,” as indicated.
- Maximum true vapor pressure of total organic HAP at storage temperature.
- The applicability criteria in Table 4 of this subpart shall be used for chemicals not specifically listed in this table (i.e., Table 5).

[64 FR 11553, Mar. 9, 1999]
### Table 6: Known Organic Hazardous Air Pollutants from Thermoplastic Products—Continued

<table>
<thead>
<tr>
<th>Thermoplastic product/subcategory</th>
<th>Organic HAP/chemical name (CAS No.)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Acetaldehyde (75-0)</td>
<td>Acrylonitrile (107-13-1)</td>
</tr>
<tr>
<td>1,3-Butadiene (106-99-0)</td>
<td>1,4-Dioxane (123-91-1)</td>
</tr>
<tr>
<td>Ethylene Glycol (107-21-1)</td>
<td>Methanol (67-56-1)</td>
</tr>
<tr>
<td>Styrene (100-42-5)</td>
<td></td>
</tr>
</tbody>
</table>

PET using a continuous terephthalic acid high viscosity multiple end finisher process

Polystyrene resin using a batch process

Polystyrene resin using a continuous process

SAN using a batch process

SAN using a continuous process

**AAACAS No.** = Chemical Abstract Service Number.
**AAABS** = Acrylonitrile butadiene styrene resin.
**AAASA/AMSAN** = Acrylonitrile styrene resin/alpha methyl styrene acrylonitrile resin.
**AAAEPS** = expandable polystyrene resin.
**AAAMABS** = methyl methacrylate acrylonitrile butadiene styrene resin.
**AAAPET** = poly(ethylene terephthalate) resin.
**AAAN** = styrene acrylonitrile resin.
**AAAMBS** = methyl methacrylate butadiene styrene resin.

### Table 7: Group 1 Batch Process Vents—Monitoring, Recordkeeping, and Reporting Requirements

<table>
<thead>
<tr>
<th>Control device</th>
<th>Parameters to be monitored</th>
<th>Recordkeeping and reporting requirements for monitored parameters</th>
</tr>
</thead>
<tbody>
<tr>
<td>Thermal Incinerator</td>
<td>Firebox temperature*</td>
<td>1. Continuous records as specified in § 63.1326(e)(1).h</td>
</tr>
<tr>
<td></td>
<td></td>
<td>2. Record and report the average firebox temperature measured during the performance test—NCS.x</td>
</tr>
<tr>
<td></td>
<td></td>
<td>3. Record the batch cycle daily average firebox temperature as specified in § 63.1326(e)(2).j</td>
</tr>
<tr>
<td></td>
<td></td>
<td>4. Report all batch cycle daily average temperatures that are below the minimum operating temperature established in the NCS or operating permit—PR.p</td>
</tr>
<tr>
<td>Catalytic Incinerator</td>
<td>Temperature upstream and downstream of the catalyst bed.</td>
<td>1. Continuous records as specified in § 63.1326(e)(1).h</td>
</tr>
<tr>
<td></td>
<td></td>
<td>2. Record and report the average upstream and downstream temperatures and the average temperature difference across the catalyst bed measured during the performance test—NCS.x</td>
</tr>
<tr>
<td></td>
<td></td>
<td>3. Record the batch cycle daily average upstream temperature and temperature difference across catalyst bed as specified in § 63.1326(e)(2).j</td>
</tr>
<tr>
<td></td>
<td></td>
<td>4. Report all batch cycle daily upstream temperatures that are below the minimum upstream temperature established in the NCS or operating permit—PR.p</td>
</tr>
<tr>
<td></td>
<td></td>
<td>5. Report all batch cycle daily average temperature differences across the catalyst bed that are below the minimum difference established in the NCS or operating permit—PR.p</td>
</tr>
<tr>
<td></td>
<td></td>
<td>6. Report all instances when monitoring data are not collected—PR.p</td>
</tr>
<tr>
<td>Boiler or Process Heater with a design heat input capability less than 44 megawatts and where the batch process vents or aggregate batch vent streams are not introduced with or used as the primary fuel</td>
<td>Firebox temperature*</td>
<td>1. Continuous records as specified in § 63.1326(e)(1).h</td>
</tr>
<tr>
<td></td>
<td></td>
<td>2. Record and report the average firebox temperature measured during the performance test—NCS.x</td>
</tr>
<tr>
<td></td>
<td></td>
<td>3. Record the batch cycle daily average firebox temperature as specified in § 63.1326(e)(2).j</td>
</tr>
<tr>
<td></td>
<td></td>
<td>4. Report all batch cycle daily average temperatures that are below the minimum operating temperature established in the NCS or operating permit and all instances when monitoring data are not collected—PR.p</td>
</tr>
<tr>
<td>Control device</td>
<td>Parameters to be monitored</td>
<td>Recordkeeping and reporting requirements for monitored parameters</td>
</tr>
<tr>
<td>----------------</td>
<td>----------------------------</td>
<td>---------------------------------------------------------------</td>
</tr>
</tbody>
</table>
| Flare          | Presence of a flame at the pilot light. | 1. Hourly records of whether the monitor was continuously operating during batch emission episodes, or portions thereof, selected for control and whether the pilot flame was continuously present during said periods.  
2. Record and report the presence of a flame at the pilot light over the full period of the compliance determination—NCS.
3. Record the times and durations of all periods during batch emission episodes, or portions thereof, selected for control when a pilot flame is absent or the monitor is not operating.  
4. Report the times and durations of all periods during batch emission episodes, or portions thereof, selected for control when all pilot flames of a flare are absent—PR. |
| Scrubber for halogenated batch process vents or aggregate batch vent streams (Note: Controlled by a combustion device other than a flare). | pH of scrubber effluent, and. | 1. Continuous records as specified in § 63.1326(e)(1).  
2. Record and report the average pH of the scrubber effluent measured during the performance test—NCS.  
3. Record the batch cycle daily average pH of the scrubber effluent as specified in § 63.1326(e)(2).  
4. Report all batch cycle daily average pH values of the scrubber effluent that are below the minimum operating pH established in the NCS or operating permit and all instances when monitoring data are not collected—PR. |
| Do             | Scrubber liquid flow rate. | 1. Continuous records as specified in § 63.1326(e)(1).  
2. Record and report the scrubber liquid flow rate measured during the performance test—NCS.  
3. Record the batch cycle daily average scrubber liquid flow rate as specified in § 63.1326(e)(2).  
4. Report all batch cycle daily average scrubber liquid flow rates that are below the minimum flow rate established in the NCS or operating permit and all instances when monitoring data are not collected—PR. |
| Absorber        | Exit temperature of the absorbing liquid, and. | 1. Continuous records as specified in § 63.1326(e)(1).  
2. Record and report the average exit temperature of the absorbing liquid measured during the performance test—NCS.  
3. Record the batch cycle daily average exit temperature of the absorbing liquid as specified in § 63.1326(e)(2) for each batch cycle.  
4. Report all batch cycle daily average exit temperatures of the absorbing liquid that are below the minimum operating temperature established in the NCS or operating permit and all instances when monitoring data are not collected—PR. |
| Do             | Exit specific gravity for the absorbing liquid. | 1. Continuous records as specified in § 63.1326(e)(1).  
2. Record and report the average exit specific gravity measured during the performance test—NCS.  
3. Record the batch cycle daily average exit specific gravity as specified in § 63.1326(e)(2).  
4. Report all batch cycle daily average exit specific gravity values that are below the minimum operating temperature established in the NCS or operating permit and all instances when monitoring data are not collected—PR. |
| Condenser       | Exit (product side) temperature. | 1. Continuous records as specified in § 63.1326(e)(1).  
2. Record and report the average exit temperature measured during the performance test—NCS.  
3. Record the batch cycle daily average exit temperature as specified in § 63.1326(e)(2).  
4. Report all batch cycle daily average exit temperatures that are above the maximum operating temperature established in the NCS or operating permit and all instances when monitoring data are not collected—PR. |
| Carbon Adsorber | Total regeneration stream mass flow during carbon bed regeneration cycle(s), and. | 1. Record the total regeneration stream mass flow for each carbon bed regeneration cycle.  
2. Record and report the total regeneration stream mass flow during each carbon bed regeneration cycle measured during the performance test—NCS.  
3. Report all carbon bed regeneration cycles when the total regeneration stream mass flow is above the maximum mass flow rate established in the NCS or operating permit—PR. |
### TABLE 7.—GROUP 1 BATCH PROCESS VENTS—MONITORING, RECORDKEEPING, AND REPORTING REQUIREMENTS—Continued

<table>
<thead>
<tr>
<th>Control device</th>
<th>Parameters to be monitored</th>
<th>Recordkeeping and reporting requirements for monitored parameters</th>
</tr>
</thead>
<tbody>
<tr>
<td>Do</td>
<td>Temperature of the carbon bed after regeneration and within 15 minutes of completing any cooling cycle(s).</td>
<td>1. Record the temperature of the carbon bed after each regeneration and within 15 minutes of completing any cooling cycle(s).</td>
</tr>
<tr>
<td></td>
<td>Presence of flow diverted to the atmosphere from the control device or.</td>
<td>1. Hourly records of whether the flow indicator was operating during batch emission episodes, or portions thereof, selected for control and whether flow was detected at any time during said periods as specified in §63.1326(e)(3).</td>
</tr>
<tr>
<td></td>
<td>Monthly inspections of sealed valves.</td>
<td>1. Records that monthly inspections were performed as specified in §63.1326(e)(4)(i).</td>
</tr>
<tr>
<td></td>
<td>Concentration level or reading indicated by an organic monitoring device at the outlet of the control device.</td>
<td>1. Continuous records as specified in §63.1326(e)(1).</td>
</tr>
</tbody>
</table>

**All Control Devices**

1. Hourly records of whether the flow indicator was operating during batch emission episodes, or portions thereof, selected for control and whether flow was detected at any time during said periods as specified in §63.1326(e)(3).
2. Record and report the times and durations of all periods during batch emission episodes, or portions thereof, selected for control when emissions are diverted through a bypass line or the flow indicator is not operating—PR.d
3. Record the temperature of the carbon bed after each regeneration and within 15 minutes of completing any cooling cycle(s).is above the maximum temperature established in the NCS or operating permit—PR.d

**Alternately, these devices may comply with the organic monitoring device provisions listed at the end of this table.**

---

### TABLE 8.—OPERATING PARAMETERS FOR WHICH LEVELS ARE REQUIRED TO BE ESTABLISHED FOR CONTINUOUS AND BATCH PROCESS VENTS AND AGGREGATE BATCH VENT STREAMS

<table>
<thead>
<tr>
<th>Device</th>
<th>Parameters to be monitored</th>
<th>Established operating parameter(s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Thermal incinerator</td>
<td>Firebox temperature ........</td>
<td>Minimum temperature.</td>
</tr>
<tr>
<td>Catalytic incinerator</td>
<td>Temperature upstream and downstream of the catalyst bed.</td>
<td>Minimum upstream temperature; and minimum temperature difference across the catalyst bed.</td>
</tr>
<tr>
<td>Boiler or process heater</td>
<td>Firebox temperature ..........</td>
<td>Minimum temperature.</td>
</tr>
<tr>
<td>Scrubber for halogenated vents</td>
<td>pH of scrubber effluent; and scrubber liquid flow rate.</td>
<td>Minimum pH; and minimum flow rate.</td>
</tr>
<tr>
<td>Absorber</td>
<td>Exit temperature of the absorbing liquid.</td>
<td>Minimum temperature; and minimum specific gravity.</td>
</tr>
<tr>
<td>Condenser</td>
<td>Exit temperature ............</td>
<td>Maximum temperature.</td>
</tr>
<tr>
<td>Carbon absorber</td>
<td>Total regeneration stream mass flow during carbon bed regeneration cycle; and temperature of the carbon bed after regeneration (and within 15 minutes of completing any cooling cycle(s)).</td>
<td>Maximum mass flow; and maximum temperature.</td>
</tr>
<tr>
<td>Other devices (or as an alternate to the requirements previously presented in this table)</td>
<td>HAP concentration level or reading at outlet of device.</td>
<td>Maximum HAP concentration or reading.</td>
</tr>
</tbody>
</table>

*Concentration is measured instead of an operating parameter.*
Environmental Protection Agency

Subpart KKK [Reserved]

Subpart LLL—National Emission Standards for Hazardous Air Pollutants From the Portland Cement Manufacturing Industry

SOURCE: 64 FR 31925, June 14, 1999, unless otherwise noted.

§ 63.1340 Applicability and designation of affected sources.

(a) Except as specified in paragraphs (b) and (c) of this section, the provisions of this subpart apply to each new and existing portland cement plant which is a major source or an area source as defined in §63.2.

(b) The affected sources subject to this subpart are:

(1) Each kiln and each in-line kiln/raw mill at any major or area source, including alkali bypasses, except for kilns and in-line kiln/raw mills that burn hazardous waste and are subject to and regulated under subpart EEE of this part;

(2) Each clinker cooler at any portland cement plant which is a major source;

(3) Each raw mill at any portland cement plant which is a major source;

(4) Each finish mill at any portland cement plant which is a major source;

(5) Each raw material dryer at any portland cement plant which is a major source and each greenfield raw material dryer at any portland cement plant which is a major or area source;

(6) Each raw material, clinker, or finished product storage bin at any portland cement plant which is a major source;

(7) Each conveying system transfer point at any portland cement plant which is a major source;

(8) Each bagging system at any portland cement plant which is a major source;

(9) Each bulk loading or unloading system at any portland cement plant which is a major source.

(c) For portland cement plants with on-site nonmetallic mineral processing facilities, the first affected source in the sequence of materials handling operations subject to this subpart is the raw material storage, which is just prior to the raw mill. The primary and secondary crushers and any other equipment of the on-site nonmetallic mineral processing plant which precedes the raw material storage are not subject to this subpart. Furthermore, the first conveyor transfer point subject to this subpart is the transfer point associated with the conveyor transferring material from the raw material storage to the raw mill.

(d) The owner or operator of any affected source subject to the provisions of this subpart is subject to title V permitting requirements.

§ 63.1341 Definitions.

All terms used in this subpart that are not defined in this section have the meaning given to them in the CAA and in subpart A of this part.

Alkali bypass means a duct between the feed end of the kiln and the preheater tower through which a portion of the kiln exit gas stream is withdrawn and quickly cooled by air or water to avoid excessive buildup of alkali, chloride and/or sulfur on the raw feed. This may also be referred to as the “kiln exhaust gas bypass”.

Bagging system means the equipment which fills bags with portland cement.

Clinker cooler means equipment into which clinker product leaving the kiln is placed to be cooled by air supplied by a forced draft or natural draft supply system.

Continuous monitor means a device which continuously samples the regulated parameter specified in § 63.1350 of this subpart without interruption, evaluates the detector response at least once every 15 seconds, and computes and records the average value at least every 60 seconds, except during allowable periods of calibration and except as defined otherwise by the continuous emission monitoring system performance specifications in appendix B to part 60 of this chapter.

Conveying system means a device for transporting materials from one piece of equipment or location to another location within a facility. Conveying systems include but are not limited to the following: feeders, belt conveyors,
bucket elevators and pneumatic systems.

Conveying system transfer point means a point where any material including but not limited to feed material, fuel, clinker or product, is transferred to or from a conveying system, or between separate parts of a conveying system.

Dioxins and furans (D/F) means tetra-, penta-, hexa-, hepta-, and octachlorinated dibenzo dioxins and furans.

Facility means all contiguous or adjoining property that is under common ownership or control, including properties that are separated only by a road or other public right-of-way.

Feed means the prepared and mixed materials, which include but are not limited to materials such as limestone, clay, shale, sand, iron ore, mill scale, cement kiln dust and flyash, that are fed to the kiln. Feed does not include the fuels used in the kiln to produce heat to form the clinker product.

Finish mill means a roll crusher, ball and tube mill or other size reduction equipment used to grind clinker to a fine powder. Gypsum and other materials may be added to and blended with clinker in a finish mill. The finish mill also includes the air separator associated with the finish mill.

Greenfield kiln, in-line kiln/raw mill, or raw material dryer means a kiln, in-line kiln/raw mill or raw material dryer for which construction is commenced at a plant site (where no kilns and/or in-line kiln/raw mills were in operation prior to March 24, 1998) after March 24, 1998.

Hazardous waste is defined in §261.3 of this chapter.

In-line kiln/raw mill means a system in a Portland cement production process where a dry kiln system is integrated with the raw mill so that all or a portion of the kiln exhaust gases are used to perform the drying operation of the raw mill, with no auxiliary heat source used. In this system the kiln is capable of operating without the raw mill operating, but the raw mill cannot operate without the kiln gases, and consequently, the raw mill does not generate a separate exhaust gas stream.

Kiln means a device, including any associated preheater or precalciner devices, that produces clinker by heating limestone and other materials for subsequent production of Portland cement.

Kiln exhaust gas bypass means alkali bypass.

Monovent means an exhaust configuration of a building or emission control device (e.g., positive pressure fabric filter) that extends the length of the structure and has a width very small in relation to its length (i.e., length to width ratio is typically greater than 5:1). The exhaust may be an open vent with or without a roof, louvered vents, or a combination of such features.

New brownfield kiln, in-line kiln/raw mill, or raw material dryer means a kiln, in-line kiln/raw mill or raw material dryer for which construction is commenced at a plant site (where kilns and/or in-line kiln/raw mills were in operation prior to March 24, 1998) after March 24, 1998.

One-minute average means the average of thermocouple or other sensor responses calculated at least every 60 seconds from responses obtained at least once during each consecutive 15 second period.

Portland cement plant means any facility manufacturing Portland cement.

Raw material dryer means an impact dryer, drum dryer, paddle-equipped rapid dryer, air separator, or other equipment used to reduce the moisture content of feed materials.

Raw mill means a ball and tube mill, vertical roller mill or other size reduction equipment, that is not part of an in-line kiln/raw mill, used to grind feed to the appropriate size. Moisture may be added or removed from the feed during the grinding operation. If the raw mill is used to remove moisture from feed materials, it is also, by definition, a raw material dryer. The raw mill also includes the air separator associated with the raw mill.

Rolling average means the average of all one-minute averages over the averaging period.

Run average means the average of the one-minute parameter values for a run.

Environmental Protection Agency

(CDDs and CDFs) and 1989 Update, March 1989.

EMISSION STANDARDS AND OPERATING LIMITS

§ 63.1342 Standards: General.

(a) Table 1 to this subpart provides cross references to the 40 CFR part 63, subpart A, general provisions, indicating the applicability of the general provisions requirements to subpart LLL.

(b) Table 1 of this section provides a summary of emission limits and operating limits of this subpart.

<table>
<thead>
<tr>
<th>Affected source</th>
<th>Pollutant or opacity</th>
<th>Emission and operating limit</th>
</tr>
</thead>
<tbody>
<tr>
<td>All kilns and in-line kiln/raw mills at major sources (including alkali bypass).</td>
<td>PM</td>
<td>0.15 kg/Mg of feed (dry basis).</td>
</tr>
<tr>
<td>All kilns and in-line kiln/raw mills at major and area sources (including alkali bypass).</td>
<td>Opacity</td>
<td>20 percent.</td>
</tr>
<tr>
<td></td>
<td>D/F</td>
<td>0.20 ng TEQ/dscm or 0.40 ng TEQ/dscm when the average of the performance test run average particulate matter control device (PMCD) inlet temperatures is 204 °C or less. [Corrected to 7 percent oxygen]</td>
</tr>
<tr>
<td></td>
<td>Operate such that the three-hour rolling average PMCD inlet temperature is no greater than the temperature established at performance test.</td>
<td></td>
</tr>
<tr>
<td></td>
<td>If activated carbon injection is used: Operate such that the three-hour rolling average activated carbon injection rate is no less than rate established at performance test.</td>
<td></td>
</tr>
<tr>
<td></td>
<td>Operate such that either the carrier gas flow rate or carrier gas pressure drop exceeds the value established at performance test. Inject carbon of equivalent specifications to that used at performance test.</td>
<td></td>
</tr>
<tr>
<td>New greenfield kilns and in-line kiln/raw mills at major and area sources.</td>
<td>THC</td>
<td>50 ppmvd, as propane, corrected to 7 percent oxygen.</td>
</tr>
<tr>
<td>All clinker coolers at major sources</td>
<td>PM</td>
<td>0.050 kg/Mg of feed (dry basis)</td>
</tr>
<tr>
<td>All raw mills and finish mills at major sources</td>
<td>Opacity</td>
<td>10 percent.</td>
</tr>
<tr>
<td>New greenfield raw material dryers at major sources</td>
<td>Opacity</td>
<td>10 percent.</td>
</tr>
<tr>
<td>All raw material dryers and material handling points at major sources</td>
<td>THG</td>
<td>50 ppmvd, as propane, corrected to 7 percent oxygen.</td>
</tr>
</tbody>
</table>

§ 63.1343 Standards for kilns and in-line kiln/raw mills.

(a) General. The provisions in this section apply to each kiln, each in-line kiln/raw mill, and any alkali bypass associated with that kiln or in-line kiln/raw mill.

(b) Existing, reconstructed, or new brownfield/major sources. No owner or operator of an existing, reconstructed or new brownfield kiln or an existing, reconstructed or new brownfield in-line kiln/raw mill shall cause to be discharged into the atmosphere from these affected sources, any gases which:

1. Contain particulate matter (PM) in excess of 0.15 kg per Mg (0.30 lb per ton) of feed (dry basis) to the kiln. When there is an alkali bypass associated with a kiln or in-line kiln/raw mill, the combined particulate matter emissions from the kiln or in-line kiln/raw mill and the alkali bypass are subject to this emission limit.

2. Exhibit opacity greater than 20 percent.

3. Contain D/F in excess of:
   (i) 0.20 ng per dscm (8.7×10⁻¹¹ gr per dscf) (TEQ) corrected to seven percent oxygen; or
   (ii) 0.40 ng per dscm (1.7×10⁻¹⁰ gr per dscf) (TEQ) corrected to seven percent oxygen, when the average of the performance test run average temperatures at the inlet to the particulate
matter control device is 204 °C (400 °F) or less.

(c) Greenfield/major sources. No owner or operator that commences construction of a greenfield kiln or greenfield inline kiln/raw mill at a facility which is a major source subject to the provisions of this subpart shall cause to be discharged into the atmosphere from these affected sources any gases which:

1. Contain particulate matter in excess of 0.15 kg per Mg (0.30 lb per ton) of feed (dry basis) to the kiln. When there is an alkali bypass associated with a kiln or in-line kiln/raw mill, the combined particulate matter emissions from the kiln or in-line kiln/raw mill and the bypass stack are subject to this emission limit.

2. Exhibit opacity greater than 20 percent.

3. Contain D/F in excess of:
   (i) 0.20 ng per dscm (8.7×10^{-11} gr per dscf) (TEQ) corrected to seven percent oxygen; or
   (ii) 0.40 ng per dscm (1.7×10^{-10} gr per dscf) (TEQ) corrected to seven percent oxygen, when the average of the performance test run average temperatures at the inlet to the particulate matter control device is 204 °C (400 °F) or less.

4. Contain total hydrocarbon (THC), from the main exhaust of the kiln or in-line kiln/raw mill, in excess of 50 ppmvd as propane, corrected to seven percent oxygen.

(e) Greenfield/area sources. No owner or operator of a greenfield kiln or a greenfield in-line kiln/raw mill at a facility that is an area source subject to the provisions of this subpart shall cause to be discharged into the atmosphere from these affected sources any gases which:

1. Contain D/F in excess of:
   (i) 0.20 ng per dscm (8.7×10^{-11} gr per dscf) (TEQ) corrected to seven percent oxygen; or
   (ii) 0.40 ng per dscm (1.7×10^{-10} gr per dscf) (TEQ) corrected to seven percent oxygen, when the average of the performance test run average temperatures at the inlet to the particulate matter control device is 204 °C (400 °F) or less.

2. Contain THC, from the main exhaust of the kiln or in-line kiln/raw mill, in excess of 50 ppmvd as propane, corrected to seven percent oxygen.

§ 63.1344 Operating limits for kilns and in-line kiln/raw mills.

(a) The owner or operator of a kiln subject to a D/F emission limitation under § 63.1343 must operate the kiln such that the temperature of the gas at the inlet to the kiln particulate matter control device (PMCD) and alkali bypass PMCD, if applicable, does not exceed the applicable temperature limit specified in paragraph (b) of this section. The owner or operator of an in-line kiln/raw mill subject to a D/F emission limitation under § 63.1343 must operate the in-line kiln/raw mill, such that:

1. When the raw mill of the in-line kiln/raw mill is operating, the applicable temperature limit for the main in-line kiln/raw mill exhaust, specified in paragraph (b) of this section and established during the performance test when the raw mill was operating is not exceeded.

2. When the raw mill of the in-line kiln/raw mill is not operating, the applicable temperature limit for the main in-line kiln/raw mill exhaust, specified in paragraph (b) of this section and established during the performance test when the raw mill was not operating, is not exceeded.
Environmental Protection Agency

§ 63.1346 Standards for in-line kiln/raw mill systems.

(a) If the in-line kiln/raw mill is equipped with an alkali bypass, the applicable temperature limit for the alkali bypass, specified in paragraph (b) of this section and established during the performance test when the raw mill was operating, is not exceeded.

(b) The temperature limit for affected sources meeting the limits of paragraph (a) of this section or paragraphs (a)(1) through (a)(3) of this section is determined in accordance with §63.1349(b)(3)(iv).

(c) The owner or operator of an affected source subject to a D/F emission limitation under §63.1343 that employs carbon injection as an emission control technique must operate the carbon injection system in accordance with paragraphs (c)(1) and (c)(2) of this section.

(1) The three-hour rolling average activated carbon injection rate shall be equal to or greater than the activated carbon injection rate determined in accordance with §63.1349(b)(3)(vi).

(2) The owner or operator shall either:
   (i) Maintain the minimum activated carbon injection carrier gas flow rate, as a three-hour rolling average, based on the manufacturer’s specifications. These specifications must be documented in the test plan developed in accordance with §63.7(c), or
   (ii) Maintain the minimum activated carbon injection carrier gas pressure drop, as a three-hour rolling average, based on the manufacturer’s specifications. These specifications must be documented in the test plan developed in accordance with §63.7(c).

(d) Except as provided in paragraph (e) of this section, the owner or operator of an affected source subject to a D/F emission limitation under §63.1343 that employs carbon injection as an emission control technique must specify and use the brand and type of activated carbon used during the performance test until a subsequent performance test is conducted, unless the site-specific performance test plan contains documentation of key parameters that affect adsorption and the owner or operator establishes limits based on those parameters, and the limits on these parameters are maintained.

(e) The owner or operator of an affected source subject to a D/F emission limitation under §63.1343 that employs carbon injection as an emission control technique may substitute, at any time, a different brand or type of activated carbon provided that the replacement has equivalent or improved properties compared to the activated carbon specified in the site-specific performance test plan and used in the performance test. The owner or operator must maintain documentation that the substitute activated carbon will provide the same or better level of control as the original activated carbon.

§ 63.1345 Standards for clinker coolers.

(a) No owner or operator of a new or existing clinker cooler at a facility which is a major source subject to the provisions of this subpart shall cause to be discharged into the atmosphere from the clinker cooler any gases which:

(1) Contain particulate matter in excess of 0.050 kg per Mg (0.10 lb per ton) of feed (dry basis) to the kiln.

(2) Exhibit opacity greater than ten percent.

(b) [Reserved]

§ 63.1346 Standards for new and reconstructed raw material dryers.

(a) Brownfield/major sources. No owner or operator of a new or reconstructed brownfield raw material dryer at a facility which is a major source subject to this subpart shall cause to be discharged into the atmosphere from the new or reconstructed raw material dryer any gases which exhibit opacity greater than ten percent.

(b) Greenfield/area sources. No owner or operator of a greenfield raw material dryer at a facility which is an area source subject to this subpart shall cause to be discharged into the atmosphere from the greenfield raw material dryer any gases which contain THC in excess of 50 ppmvd, reported as propane, corrected to seven percent oxygen.

(c) Greenfield/major sources. No owner or operator of a greenfield raw material dryer at a facility which is a major source subject to this subpart shall...
§ 63.1347 Standards for raw and finish mills.

The owner or operator of each new or existing raw mill or finish mill at a facility which is a major source subject to the provisions of this subpart shall not cause to be discharged from the mill sweep or air separator air pollution control devices of these affected sources any gases which exhibit opacity in excess of ten percent.

§ 63.1348 Standards for affected sources other than kilns; in-line kiln/raw mills; clinker coolers; new and reconstructed raw material dryers; and raw and finish mills.

The owner or operator of each new or existing raw material, clinker, or finished product storage bin; conveying system transfer point; bagging system; and bulk loading or unloading system; and each existing raw material dryer, at a facility which is a major source subject to the provisions of this subpart shall not cause to be discharged any gases from these affected sources which exhibit opacity in excess of ten percent.

Monitoring and compliance provisions

§ 63.1349 Performance testing requirements.

(a) The owner or operator of an affected source subject to this subpart shall demonstrate initial compliance with the emission limits of § 63.1343 and §§ 63.1345 through 63.1348 using the test methods and procedures in paragraph (b) of this section and § 63.7. Performance test results shall be documented in complete test reports that contain the information required by paragraphs (a)(1) through (a)(10) of this section, as well as all other relevant information. The plan to be followed during testing shall be made available to the Administrator prior to testing, if requested.

(1) A brief description of the process and the air pollution control system;
(2) Sampling location description(s);
(3) A description of sampling and analytical procedures and any modifications to standard procedures;
(4) Test results;
(5) Quality assurance procedures and results;
(6) Records of operating conditions during the test, preparation of standards, and calibration procedures;
(7) Raw data sheets for field sampling and field and laboratory analyses;
(8) Documentation of calculations;
(9) All data recorded and used to establish parameters for compliance monitoring; and
(10) Any other information required by the test method.

(b) Performance tests to demonstrate initial compliance with this subpart shall be conducted as specified in paragraphs (b)(1) through (b)(4) of this section.

(1) The owner or operator of a kiln subject to limitations on particulate matter emissions shall demonstrate initial compliance by conducting a performance test as specified in paragraphs (b)(1)(i) through (b)(1)(iv) of this section. The owner or operator of an in-line kiln/raw mill subject to limitations on particulate matter emissions shall demonstrate initial compliance by conducting separate performance tests as specified in paragraphs (b)(1)(i) through (b)(1)(iv) of this section while the raw mill of the in-line kiln/raw mill is under normal operating conditions and while the raw mill of the in-line kiln/raw mill is not operating. The owner or operator of a clinker cooler subject to limitations on particulate matter emissions shall demonstrate initial compliance by conducting a performance test as specified in paragraphs (b)(1)(i) through (b)(1)(iii) of this section. The opacity exhibited during the period of the Method 5 of Appendix A to part 60 of this chapter performance tests required by paragraph (b)(1)(i) of this section shall be determined as required in paragraphs (b)(1)(iv) through (vi) of this section.

(i) EPA Method 5 of appendix A to part 60 of this chapter shall be used to determine PM emissions. Each performance test shall consist of three
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separate runs under the conditions that exist when the affected source is operating at the highest load or capacity level reasonably expected to occur. Each run shall be conducted for at least one hour, and the minimum sample volume shall be 0.85 dscm (30 dscf). The average of the three runs shall be used to determine compliance. A determination of the particulate matter collected in the impingers ("back half") of the Method 5 particulate sampling train is not required to demonstrate initial compliance with the PM standards of this subpart. However this shall not preclude the permitting authority from requiring a determination of the "back half" for other purposes.

(ii) Suitable methods shall be used to determine the kiln or inline kiln/raw mill feed rate, except for fuels, for each run.

(iii) The emission rate, \( E \), of PM shall be computed for each run using equation 1:

\[
E = \left( C_s Q_s \right)/P \quad (\text{Eq. 1})
\]

Where:

- \( E \) = emission rate of particulate matter, kg/Mg of kiln feed.
- \( C_s \) = concentration of PM, kg/dscm.
- \( Q_s \) = volumetric flow rate of effluent gas, dscm/hr.
- \( P \) = total kiln feed (dry basis), Mg/hr.

(iv) When there is an alkali bypass associated with a kiln or in-line kiln/raw mill, the main exhaust and alkali bypass of the kiln or in-line kiln/raw mill shall be tested simultaneously and the combined emission rate of particulate matter from the kiln or in-line kiln/raw mill and alkali bypass shall be computed for each run using equation 2:

\[
E_c = \left( C_{sk} Q_{sk} + C_{sb} Q_{sb} \right)/P \quad (\text{Eq. 2})
\]

Where:

- \( E_c \) = the combined emission rate of particulate matter from the kiln or in-line kiln/raw mill and alkali bypass stack, kg/Mg of kiln feed.
- \( C_{sk} \) = concentration of particulate matter in the kiln or in-line kiln/raw mill effluent, kg/dscm.
- \( Q_{sk} \) = volumetric flow rate of kiln or in-line kiln/raw mill effluent, dscm/hr.
- \( C_{sb} \) = concentration of particulate matter in the alkali bypass gas, kg/dscm.
- \( Q_{sb} \) = volumetric flow rate of alkali bypass gas, dscm/hr.
- \( P \) = total kiln feed (dry basis), Mg/hr.

(v) Except as provided in paragraph (b)(1)(vi) of this section the opacity exhibited during the period of the Method 5 performance tests required by paragraph (b)(1)(i) of this section shall be determined through the use of a continuous opacity monitor (COM). The maximum six-minute average opacity during the three Method 5 test runs shall be determined during each Method 5 test run, and used to demonstrate initial compliance with the applicable opacity limits of §63.1343(b)(2), §63.1343(c)(2), or §63.1345(a)(2).

(vi) Each owner or operator of a kiln, in-line kiln/raw mill, or clinker cooler subject to the provisions of this subpart using a fabric filter with multiple stacks or an electrostatic precipitator with multiple stacks may, in lieu of installing the continuous opacity monitoring system required by paragraph (b)(1)(v) of this section, conduct an opacity test in accordance with Method 9 of appendix A to part 60 of this chapter during each Method 5 performance test required by paragraph (b)(1)(i) of this section. If the control device exhausts through a monovent, or if the use of a COM in accordance with the installation specifications of Performance Specification 1 (PS-1) of appendix B to part 60 of this chapter is not feasible, a test shall be conducted in accordance with Method 9 of appendix A to part 60 of this chapter. The maximum six-minute average opacity shall be determined during the three Method 5 test runs, and used to demonstrate initial compliance with the applicable opacity limits of §63.1343(b)(2), §63.1343(c)(2), or §63.1345(a)(2).

(2) The owner or operator of any affected source subject to limitations on opacity under this subpart that is not subject to paragraph (b)(1) of this section shall demonstrate initial compliance with the affected source opacity limit by conducting a test in accordance with Method 9 of appendix A to part 60 of this chapter. The performance test shall be conducted under the conditions that exist when the affected
source is operating at the highest load or capacity level reasonably expected to occur. The maximum six-minute average opacity exhibited during the test period shall be used to determine whether the affected source is in initial compliance with the standard. The duration of the Method 9 performance test shall be 3-hours (30 six-minute averages), except that the duration of the Method 9 performance test may be reduced to 1-hour if the conditions of paragraphs (b)(2)(i) through (ii) of the section apply:

(i) There are no individual readings greater than 10 percent opacity;
(ii) There are no more than three readings of 10 percent for the first 1-hour period.

(3) The owner or operator of an affected source subject to limitations on D/F emissions shall demonstrate initial compliance with the D/F emission limit by conducting a performance test using Method 23 of appendix A to part 60 of this chapter. The owner or operator of an in-line kiln/raw mill shall demonstrate initial compliance by conducting separate performance tests while the raw mill of the in-line kiln/raw mill is under normal operating conditions and while the raw mill of the in-line kiln/raw mill is not operating. The owner or operator of a kiln or in-line kiln/raw mill equipped with an alkali bypass shall conduct simultaneous performance tests of the kiln or in-line kiln/raw mill exhaust and the alkali bypass, however the owner or operator of an in-line kiln/raw mill is not required to conduct a performance test of the alkali bypass exhaust when the raw mill of the in-line kiln/raw mill is not operating.

(i) Each performance test shall consist of three separate runs; each run shall be conducted under the conditions that exist when the affected source is operating at the highest load or capacity level reasonably expected to occur. The duration of each run shall be at least three hours and the sample volume for each run shall be at least 2.5 dscm (90 dscf). The concentration shall be determined for each run and the arithmetic average of the concentrations measured for the three runs shall be calculated and used to determine compliance.

(ii) The temperature at the inlet to the kiln or in-line kiln/raw mill PMCD, and where applicable, the temperature at the inlet to the alkali bypass mill PMCD, must be continuously recorded during the period of the Method 23 test, and the continuous temperature record(s) must be included in the performance test report.

(iii) One-minute average temperatures must be calculated for each minute of each run of the test.

(iv) The run average temperature must be calculated for each run, and the average of the run average temperatures must be determined and included in the performance test report and will determine the applicable temperature limit in accordance with § 63.1344(b).

(v) If activated carbon injection is used for D/F control, the rate of activated carbon injection to the kiln or in-line kiln/raw mill exhaust, and where applicable, the rate of activated carbon injection to the alkali bypass exhaust, must be continuously recorded during the period of the Method 23 test, and the continuous injection rate record(s) must be included in the performance test report. In addition, the performance test report must include the brand and type of activated carbon used during the performance test and a continuous record of either the carrier gas flow rate or the carrier gas pressure drop for the duration of the test. Activated carbon injection rate parameters must be determined in accordance with paragraphs (b)(3)(vi) of this section.

(vi) The run average injection rate must be calculated for each run, and the average of the run average injection rates must be determined and included in the performance test report and will determine the applicable injection rate limit in accordance with § 63.1344(c)(1).

(4) The owner or operator of an affected source subject to limitations on emissions of THC shall demonstrate initial compliance with the THC limit by operating a continuous emission monitor in accordance with Performance Specification 8A of appendix B to part 60 of this chapter. The duration of the performance test shall be three
hours, and the average THC concentration (as calculated from the one-minute averages) during the three hour performance test shall be calculated. The owner or operator of an in-line kiln/raw mill shall demonstrate initial compliance by conducting separate performance tests while the raw mill of the in-line kiln/raw mill is under normal operating conditions and while the raw mill of the in-line kiln/raw mill is not operating.

(c) Except as provided in paragraph (e) of this section, performance tests required under paragraphs (b)(1) and (b)(2) of this section shall be repeated every five years, except that the owner or operator of a kiln, in-line kiln/raw mill or clinker cooler is not required to repeat the initial performance test of opacity for the kiln, in-line kiln/raw mill or clinker cooler.

(d) Performance tests required under paragraph (b)(3) of this section shall be repeated every 30 months.

(e) The owner or operator is required to repeat the performance tests for kilns or in-line kiln/raw mills as specified in paragraphs (b)(1) and (b)(3) of this section within 90 days of initiating any significant change in the feed or fuel from that used in the previous performance test.

(f) Table 1 of this section provides a summary of the performance test requirements of this subpart.

TABLE 1 TO § 63.1349.—SUMMARY OF PERFORMANCE TEST REQUIREMENTS

<table>
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<tr>
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<th>Performance test</th>
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</thead>
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<td>EPA Method 5.</td>
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<tr>
<td>New and existing kiln and in-line kiln/raw mill opacity</td>
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<tr>
<td>New greenfield kiln and in-line kiln/raw mill</td>
<td>THC CEM (EPA PS-8A).</td>
</tr>
<tr>
<td>New and existing kiln and in-line kiln/raw mill</td>
<td>EPA Method 5.</td>
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<tr>
<td>New and existing clinker cooler opacity</td>
<td>COM or EPA Method 9 visual opacity readings.</td>
</tr>
<tr>
<td>New and existing kiln and in-line kiln/raw mill THC</td>
<td>EPA Method 9.</td>
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<tr>
<td>New and existing raw and finish mill opacity</td>
<td>EPA Method 9.</td>
</tr>
<tr>
<td>New and existing raw and finish mill opacity</td>
<td>THC CEM (EPA PS-8A).</td>
</tr>
</tbody>
</table>

§ 63.1350 Monitoring requirements.

(a) The owner or operator of each portland cement plant shall prepare for each affected source subject to the provisions of this subpart, a written operations and maintenance plan. The plan shall be submitted to the Administrator for review and approval as part of the application for a part 70 permit and shall include the following information:

(1) Procedures for proper operation and maintenance of the affected source and air pollution control devices in order to meet the emission limits and operating limits of §§ 63.1343 through 63.1348;

(2) Corrective actions to be taken when required by paragraph (e) of this section;

(3) Procedures to be used during an inspection of the components of the combustion system of each kiln and each in-line kiln/raw mill located at the facility at least once per year; and

(4) Procedures to be used to periodically monitor affected sources subject to opacity standards under §§ 63.1346 and 63.1348. Such procedures must include the provisions of paragraphs...
(a)(4)(i) through (a)(4)(iv) of this section.

(i) The owner or operator must conduct a monthly 1-minute visible emissions test of each affected source in accordance with Method 22 of Appendix A to part 60 of this chapter. The test must be conducted while the affected source is in operation.

(ii) If no visible emissions are observed in six consecutive monthly tests for any affected source, the owner or operator may decrease the frequency of testing from monthly to semi-annually for that affected source. If visible emissions are observed during any semi-annual test, the owner or operator must resume testing of that affected source on a monthly basis and maintain that schedule until no visible emissions are observed in six consecutive monthly tests.

(iii) If no visible emissions are observed during the semi-annual test for any affected source, the owner or operator may decrease the frequency of testing from semi-annually to annually for that affected source. If visible emissions are observed during any annual test, the owner or operator must resume testing of that affected source on a monthly basis and maintain that schedule until no visible emissions are observed in six consecutive monthly tests.

(iv) If visible emissions are observed during any Method 22 test, the owner or operator must conduct a 6-minute test of opacity in accordance with Method 9 of Appendix A to part 60 of this chapter. The Method 9 test must begin within one hour of any observation of visible emissions.

(b) Failure to comply with any provisions of the operations and maintenance plan developed in accordance with paragraph (a) of this section shall be a violation of the standard.

(c) The owner or operator of a kiln or in-line kiln/raw mill shall monitor opacity at each point where emissions are vented from these affected sources including alkali bypasses in accordance with paragraphs (c)(1) through (c)(3) of this section.

(1) Except as provided in paragraph (c)(2) of this section, the owner or operator shall install, calibrate, maintain, and continuously operate a continuous opacity monitor (COM) located at the outlet of the PM control device to continuously monitor the opacity. The COM shall be installed, maintained, calibrated, and operated as required by subpart A, general provisions of this part, and according to PS-1 of Appendix B to part 60 of this chapter.

(2) The owner or operator of a kiln or in-line kiln/raw mill subject to the provisions of this subpart using a fabric filter with multiple stacks or an electrostatic precipitator with multiple stacks may, in lieu of installing the continuous opacity monitoring system required by paragraph (c)(1) of this section, monitor opacity in accordance with paragraphs (c)(2)(i) through (ii) of this section. If the control device exhausts through a monovent, or if the use of a COM in accordance with the installation specifications of PS-1 of Appendix B to part 60 of this chapter is not feasible, the owner or operator must monitor opacity in accordance with paragraphs (c)(2)(i) through (ii) of this section.

(i) Perform daily visual opacity observations of each stack in accordance with the procedures of Method 9 of Appendix A of part 60 of this chapter. The Method 9 test shall begin within one hour of any observation of visible emissions.

(ii) Use the Method 9 procedures to monitor and record the average opacity for each six-minute period during the test.

(3) To remain in compliance, the opacity must be maintained such that the 6-minute average opacity for any 6-minute block period does not exceed 20 percent. If the average opacity for any 6-minute block period exceeds 20 percent, this shall constitute a violation of the standard.

(d) The owner or operator of a clinker cooler shall monitor opacity at each point where emissions are vented from the clinker cooler in accordance with paragraphs (d)(1) through (d)(3) of this section.

(1) Except as provided in paragraph (d)(2) of this section, the owner or operator shall install, calibrate, maintain,
and continuously operate a COM located at the outlet of the clinker cooler PM control device to continuously monitor the opacity. The COM shall be installed, maintained, calibrated, and operated as required by subpart A, general provisions of this part, and according to PS-1 of appendix B to part 60 of this chapter.

(2) The owner or operator of a clinker cooler subject to the provisions of this subpart using a fabric filter with multiple stacks or an electrostatic precipitator with multiple stacks may, in lieu of installing the continuous opacity monitoring system required by paragraph (d)(1) of this section, monitor opacity in accordance with paragraphs (d)(2)(i) through (ii) of this section. If the control device exhausts through a monovent, or if the use of a COM in accordance with the installation specifications of PS-1 of appendix B to part 60 of this chapter is not feasible, the owner or operator must monitor opacity in accordance with paragraphs (d)(2)(i) through (ii) of this section.

(i) Perform daily visual opacity observations of each stack in accordance with the procedures of Method 9 of appendix A of part 60 of this chapter. The Method 9 test shall be conducted while the affected source is operating at the highest load or capacity level reasonably expected to occur within the day. The duration of the Method 9 test shall be at least 30 minutes each day.

(ii) Use the Method 9 procedures to monitor and record the average opacity for each six-minute period during the test.

(3) To remain in compliance, the opacity must be maintained such that the 6-minute average opacity for any 6-minute block period does not exceed 10 percent. If the average opacity for any 6-minute block period exceeds 10 percent, this shall constitute a violation of the standard.

(e) The owner or operator of a raw mill or finish mill shall monitor opacity by conducting daily visual emissions observations of the mill sweep and air separator PMCDs of these affected sources, in accordance with the procedures of Method 22 of appendix A of part 60 of this chapter. The Method 22 test shall be conducted while the affected source is operating at the highest load or capacity level reasonably expected to occur within the day. The duration of the Method 22 test shall be six minutes. If visible emissions are observed during any Method 22 visible emissions test, the owner or operator must:

(1) Initiate, within one-hour, the corrective actions specified in the site specific operating and maintenance plan developed in accordance with paragraphs (a)(1) and (a)(2) of this section; and

(2) Within 24 hours of the end of the Method 22 test in which visible emissions were observed, conduct a visual opacity test of each stack from which visible emissions were observed in accordance with Method 9 of appendix A of part 60 of this chapter. The duration of the Method 9 test shall be thirty minutes.

(f) The owner or operator of an affected source subject to a limitation on D/F emissions shall monitor D/F emissions in accordance with paragraphs (f)(1) through (f)(6) of this section.

(1) The owner or operator shall install, calibrate, maintain, and continuously operate a continuous monitor to record the temperature of the exhaust gases from the kiln, in-line kiln/raw mill and alkali bypass, if applicable, at the inlet to, or upstream of, the kiln, in-line kiln/raw mill and/or alkali bypass PM control devices.

(i) The recorder response range must include zero and 1.5 times either of the average temperatures established according to the requirements in §63.1349(b)(3)(iv).

(ii) The reference method must be a National Institute of Standards and Technology calibrated reference thermocouple-potentiometer system or alternate reference, subject to approval by the Administrator.

(2) The owner or operator shall monitor and continuously record the temperature of the exhaust gases from the kiln, in-line kiln/raw mill and alkali bypass, if applicable, at the inlet to the kiln, in-line kiln/raw mill and/or alkali bypass PMCD.

(3) The three-hour rolling average temperature shall be calculated as the average of 180 successive one-minute average temperatures.
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(4) Periods of time when one-minute averages are not available shall be ignored when calculating three-hour rolling averages. When one-minute averages become available, the first one-minute average is added to the previous 179 values to calculate the three-hour rolling average.

(5) When the operating status of the raw mill of the in-line kiln/raw mill is changed from off to on, or from on to off the calculation of the three-hour rolling average temperature must begin anew, without considering previous recordings.

(6) The calibration of all thermocouples and other temperature sensors shall be verified at least once every three months.

(g) The owner or operator of an affected source subject to a limitation on D/F emissions that employs carbon injection as an emission control technique shall comply with the monitoring requirements of paragraphs (f)(1) through (f)(6) and (g)(1) through (g)(6) of this section to demonstrate continuous compliance with the D/F emission standard.

(1) Install, operate, calibrate and maintain a continuous monitor to record the rate of activated carbon injection. The accuracy of the rate measurement device must be ±1 percent of the rate being measured.

(2) Verify the calibration of the device at least once every three months.

(3) The three-hour rolling average activated carbon injection rate shall be calculated as the average of 180 successive one-minute average activated carbon injection rates.

(4) Periods of time when one-minute averages are not available shall be ignored when calculating three-hour rolling averages. When one-minute averages become available, the first one-minute average is added to the previous 179 values to calculate the three-hour rolling average.

(5) When the operating status of the raw mill of the in-line kiln/raw mill is changed from off to on, or from on to off the calculation of the three-hour rolling average activated carbon injection rate must begin anew, without considering previous recordings.

(6) The owner or operator must install, operate, calibrate and maintain a continuous monitor to record the activated carbon injection system carrier gas parameter (either the carrier gas flow rate or the carrier gas pressure drop) established during the D/F performance test in accordance with paragraphs (g)(6)(i) through (g)(6)(iii) of this section.

(i) The owner or operator shall install, calibrate, operate and maintain a device to continuously monitor and record the parameter value.

(ii) The owner or operator must calculate and record three-hour rolling averages of the parameter value.

(iii) Periods of time when one-minute averages are not available shall be ignored when calculating three-hour rolling averages. When one-minute averages become available, the first one-minute average shall be added to the previous 179 values to calculate the three-hour rolling average.

(h) The owner or operator of an affected source subject to a limitation on THC emissions under this subpart shall comply with the monitoring requirements of paragraphs (h)(1) through (h)(3) of this section to demonstrate continuous compliance with the THC emission standard:

(1) The owner or operator shall install, operate and maintain a THC continuous emission monitoring system in accordance with Performance Specification 8A, of appendix B to part 60 of this chapter and comply with all of the requirements for continuous monitoring systems found in the general provisions, subpart A of this part.

(2) The owner or operator is not required to calculate hourly rolling averages in accordance with section 4.9 of Performance Specification 8A.

(3) Any thirty-day block average THC concentration in any gas discharged from a greenfield raw material dryer, the main exhaust of a greenfield kiln, or the main exhaust of a greenfield in-line kiln/raw mill, exceeding 50 ppmvd, reported as propane, corrected to seven percent oxygen, is a violation of the standard.

(i) The owner or operator of any kiln or in-line kiln/raw mill subject to a D/F emission limit under this subpart shall conduct an inspection of the components of the combustion system of
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each kiln or in-line kiln raw mill at least once per year.

(j) The owner or operator of an affected source subject to a limitation on opacity under §63.1346 or §63.1348 shall monitor opacity in accordance with the operation and maintenance plan developed in accordance with paragraph (a) of this section.

(k) The owner or operator of an affected source subject to a particulate matter standard under §63.1343 shall install, calibrate, maintain and operate a particulate matter continuous emission monitoring system (PM CEMS) to measure the particulate matter discharged to the atmosphere. The compliance deadline for installing the PM CEMS and all requirements relating to performance of the PM CEMS and implementation of the PM CEMS requirement is deferred pending further rulemaking.

(l) An owner or operator may submit an application to the Administrator for approval of alternate monitoring requirements to demonstrate compliance with the emission standards of this subpart, except for emission standards for THC, subject to the provisions of paragraphs (l)(1) through (l)(6) of this section.

(1) The Administrator will not approve averaging periods other than those specified in this section, unless the owner or operator documents, using data or information, that the longer averaging period will ensure that emissions do not exceed levels achieved during the performance test over any increment of time equivalent to the time required to conduct three runs of the performance test.

(2) If the application to use an alternate monitoring requirement is approved, the owner or operator must continue to use the original monitoring requirement until approval is received to use another monitoring requirement.

(3) The owner or operator shall submit the application for approval of alternate monitoring requirements no later than the notification of performance test. The application must contain the information specified in paragraphs (l)(3)(i) through (l)(3)(iii) of this section:

(i) Data or information justifying the request, such as the technical or economic infeasibility, or the impracticality of using the required approach;

(ii) A description of the proposed alternative monitoring requirement, including the operating parameter to be monitored, the monitoring approach and technique, the averaging period for the limit, and how the limit is to be calculated; and

(iii) Data or information documenting that the alternative monitoring requirement would provide equivalent or better assurance of compliance with the relevant emission standard.

(4) The Administrator will notify the owner or operator of the approval or denial of the application within 90 calendar days after receipt of the original request, or within 60 calendar days of the receipt of any supplementary information, whichever is later. The Administrator will not approve an alternate monitoring application unless it would provide equivalent or better assurance of compliance with the relevant emission standard. Before disapproving any alternate monitoring application, the Administrator will provide:

(i) Notice of the information and findings upon which the intended disapproval is based; and

(ii) Notice of opportunity for the owner or operator to present additional supporting information before final action is taken on the application. This notice will specify how much additional time is allowed for the owner or operator to provide additional supporting information.

(5) The owner or operator is responsible for submitting any supporting information in a timely manner to enable the Administrator to consider the application prior to the performance test. Neither submittal of an application, nor the Administrator's failure to approve or disapprove the application relieves the owner or operator of the responsibility to comply with any provision of this subpart.

(6) The Administrator may decide at any time, on a case-by-case basis that additional or alternative operating
§ 63.1351 Compliance dates.

(a) The compliance date for an owner or operator of an existing affected source subject to the provisions of this subpart is June 10, 2002.

(b) The compliance date for an owner or operator of an affected source subject to the provisions of this subpart that commences new construction or reconstruction after March 24, 1998 is

TABLE 1 TO § 63.1350—MONITORING REQUIREMENTS

<table>
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<tr>
<th>Affected source/pollutant or opacity</th>
<th>Monitor type/operation/process</th>
<th>Monitoring requirements</th>
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<tbody>
<tr>
<td>All affected sources ..................</td>
<td>Operations and maintenance plan</td>
<td>Prepare written plan for all affected sources and control devices.</td>
</tr>
<tr>
<td>All kilns and in-line kiln raw mills at major sources (including alkali bypass)/opacity.</td>
<td>Continuous opacity monitor, if applicable</td>
<td>Install, calibrate, maintain and operate in accordance with general provisions and with PS-1.</td>
</tr>
<tr>
<td>Kilns and in-line kiln raw mills at major and area sources (including alkali bypass)/opacity.</td>
<td>Method 9 opacity test, if applicable</td>
<td>Daily test of at least 30-minutes, while kiln is at highest load or capacity level.</td>
</tr>
<tr>
<td>Kilns and in-line kiln raw mills at major and area sources (including alkali bypass)/D/F.</td>
<td>Particulate matter continuous emission monitoring system.</td>
<td>Deferred.</td>
</tr>
<tr>
<td>Kilns and in-line kiln raw mills at major and area sources (including alkali bypass)/D/F (continued).</td>
<td>Activated carbon injection rate monitor, if applicable</td>
<td>Install, operate, calibrate and maintain continuous activated carbon injection rate monitor; calculate three-hour rolling averages; verify calibration at least quarterly; install, operate, calibrate and maintain carrier gas flow rate monitor or carrier gas pressure drop monitor; calculate three-hour rolling averages; document carbon specifications.</td>
</tr>
<tr>
<td>New greenfield kilns and in-line kiln raw mills at major and area sources/THC.</td>
<td>Total hydrocarbon continuous emission monitor.</td>
<td>Install, operate, and maintain THC CEM in accordance with PS-8A; calculate 30-day block average THC concentration.</td>
</tr>
<tr>
<td>Clinker coolers at major sources/opacity ..</td>
<td>Continuous opacity monitor, if applicable</td>
<td>Install, calibrate, maintain and operate in accordance with general provisions and with PS-1.</td>
</tr>
<tr>
<td>Raw mills and finish mills at major sources/opacity.</td>
<td>Method 9 opacity test, if applicable</td>
<td>Daily test of at least 30-minutes, while kiln is at highest load or capacity level.</td>
</tr>
<tr>
<td>Raw mills and finish mills at major sources/opacity.</td>
<td>Method 22 visible emissions test</td>
<td>Conduct daily 6-minute Method 22 visible emissions test while mill is operating at highest load or capacity level; if visible emissions are observed, initiate corrective action within one hour and conduct 30-minute Method 9 test within 24 hours.</td>
</tr>
<tr>
<td>New greenfield raw material dryers at major and area sources/THC.</td>
<td>Total hydrocarbon continuous emission monitor.</td>
<td>Install, operate, and maintain THC CEM in accordance with PS-8A; calculate 30-day block average THC concentration.</td>
</tr>
<tr>
<td>Raw material dryers; raw material, clinker, finished product storage bins; conveying system transfer points; bagging systems; and bulk loading and unloading systems at major sources/opacity.</td>
<td>Method 22 visible emissions test</td>
<td>As specified in operation and maintenance plan.</td>
</tr>
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</table>
§ 63.1354 Reporting requirements.

(a) The reporting provisions of 40 CFR part 63, subpart A of this part that apply and those that do not apply to owners and operators of affected sources subject to this subpart are listed in Table 1 of this subpart. If any State requires a report that contains all of the information required in a report listed in this section, the owner or operator may send the Administrator a copy of the report sent to the State to satisfy the requirements of this section for that report.

(b) The owner or operator of an affected source shall comply with the notification requirements in § 63.1353 as follows:

(1) Initial notifications as required by § 63.9(b) through (d). For the purposes of this subpart, a Title V or 40 CFR part 70 permit application may be used in lieu of the initial notification required under § 63.9(b), provided the same information is contained in the permit application as required by § 63.9(b), and the State to which the permit application has been submitted has an approved operating permit program under part 70 of this chapter and has received delegation of authority from the EPA. Permit applications shall be submitted by the same due dates as those specified for the initial notification.

(2) Notification of performance tests, as required by §§ 63.7 and 63.9(e).

(3) Notification of opacity and visible emission observations required by § 63.1349 in accordance with §§ 63.6(h)(5) and 63.9(f).

(4) Notification, as required by § 63.9(g), of the date that the continuous emission monitor performance evaluation required by § 63.9(e) is scheduled to begin.

(5) Notification of compliance status, as required by § 63.9(h).

§ 63.1353 Notification requirements.

(a) The notification provisions of 40 CFR part 63, subpart A that apply and those that do not apply to owners and operators of affected sources subject to this subpart are listed in Table 1 of this subpart. If any State requires a report that contains all of the information required in a notification listed in this section, the owner or operator may send the Administrator a copy of the notification sent to the State to satisfy the requirements of this section for that notification.

(b) The owner or operator of an affected source shall comply with the notification requirements in § 63.9 as follows:

(1) Initial notifications as required by § 63.9(b) through (d). For the purposes of this subpart, a Title V or 40 CFR part 70 permit application may be used in lieu of the initial notification required under § 63.9(b), provided the same information is contained in the permit application as required by § 63.9(b), and the State to which the permit application has been submitted has an approved operating permit program under part 70 of this chapter and has received delegation of authority from the EPA. Permit applications shall be submitted by the same due dates as those specified for the initial notification.

(2) Notification of performance tests, as required by §§ 63.7 and 63.9(e).

(3) Notification of opacity and visible emission observations required by § 63.1349 in accordance with §§ 63.6(h)(5) and 63.9(f).

(4) Notification, as required by § 63.9(g), of the date that the continuous emission monitor performance evaluation required by § 63.9(e) is scheduled to begin.

(5) Notification of compliance status, as required by § 63.9(h).

§ 63.1352 Additional test methods.

(a) Owners or operators conducting tests to determine the rates of emission of hydrogen chloride (HCl) from kilns, in-line kiln/raw mills and associated bypass stacks at portland cement manufacturing facilities, for use in applicability determinations under § 63.1340 are permitted to use Method 320 or Method 321 of appendix A of this part.

(b) Owners or operators conducting tests to determine the rates of emission of hydrogen chloride (HCl) from kilns, in-line kiln/raw mills and associated bypass stacks at portland cement manufacturing facilities, for use in applicability determinations under § 63.1340 are permitted to use Methods 26 or 26A of appendix A to part 60 of this chapter, except that the results of these tests shall not be used to establish status as an area source.

(c) Owners or operators conducting tests to determine the rates of emission of specific organic HAP from raw material dryers, kilns and in-line kiln/raw mills at portland cement manufacturing facilities, for use in applicability determinations under § 63.1340 are permitted to use Method 320 of appendix A to this part, or Method 18 of appendix A to part 60 of this chapter.

NOTIFICATION, REPORTING AND RECORDKEEPING

§ 63.1353 Notification requirements.

(a) The notification provisions of 40 CFR part 63, subpart A that apply and those that do not apply to owners and operators of affected sources subject to this subpart are listed in Table 1 of this subpart. If any State requires a report that contains all of the information required in a notification listed in this section, the owner or operator may send the Administrator a copy of the notification sent to the State to satisfy the requirements of this section for that notification.

(b) The owner or operator of an affected source shall comply with the notification requirements in § 63.9 as follows:

(1) Initial notifications as required by § 63.9(b) through (d). For the purposes of this subpart, a Title V or 40 CFR part 70 permit application may be used in lieu of the initial notification required under § 63.9(b), provided the same information is contained in the permit application as required by § 63.9(b), and the State to which the permit application has been submitted has an approved operating permit program under part 70 of this chapter and has received delegation of authority from the EPA. Permit applications shall be submitted by the same due dates as those specified for the initial notification.

(2) Notification of performance tests, as required by §§ 63.7 and 63.9(e).

(3) Notification of opacity and visible emission observations required by § 63.1349 in accordance with §§ 63.6(h)(5) and 63.9(f).

(4) Notification, as required by § 63.9(g), of the date that the continuous emission monitor performance evaluation required by § 63.9(e) is scheduled to begin.

(5) Notification of compliance status, as required by § 63.9(h).
who is required to submit progress reports as a condition of receiving an extension of compliance under §63.6(i) shall submit such reports by the dates specified in the written extension of compliance.

(4) As required by §63.10(d)(5), if actions taken by an owner or operator during a startup, shutdown, or malfunction of an affected source (including actions taken to correct a malfunction) are consistent with the procedures specified in the source’s startup, shutdown, and malfunction plan specified in §63.6(e)(3), the owner or operator shall state such information in a semiannual report. Reports shall only be required if a startup, shutdown, or malfunction occurred during the reporting period. The startup, shutdown, and malfunction plan report may be submitted simultaneously with the excess emissions and continuous monitoring system performance reports; and

(5) Any time an action taken by an owner or operator during a startup, shutdown, or malfunction (including actions taken to correct a malfunction) is not consistent with the procedures in the startup, shutdown, and malfunction plan, the owner or operator shall make an immediate report of the actions taken for that event within 2 working days, by telephone call or facsimile (FAX) transmission. The immediate report shall be followed by a letter, certified by the owner or operator or other responsible official, explaining the circumstances of the event, the reasons for not following the startup, shutdown, and malfunction plan, and whether any excess emissions and/or parameter monitoring exceedances are believed to have occurred.

(6) As required by §63.10(e)(2), the owner or operator shall submit a written report of the results of the performance evaluation for the continuous opacity monitoring system required by §63.8(e). The owner or operator shall submit the report simultaneously with the results of the performance test.

(7) As required by §63.10(e)(2), the owner or operator of an affected source using a continuous opacity monitoring system to determine opacity compliance during any performance test required under §63.7 and described in §63.6(d)(6) shall report the results of the continuous opacity monitoring system performance evaluation conducted under §63.8(e).

(8) As required by §63.10(e)(3), the owner or operator of an affected source equipped with a continuous emission monitor shall submit an excess emissions and continuous monitoring system performance report for any event when the continuous monitoring system data indicate the source is not in compliance with the applicable emission limitation or operating parameter limit.

(9) The owner or operator shall submit a summary report semiannually which contains the information specified in §63.10(e)(3)(vi). In addition, the summary report shall include:

(i) All exceedences of maximum control device inlet gas temperature limits specified in §63.1344(a) and (b);

(ii) All failures to calibrate thermocouples and other temperature sensors as required under §63.1350(f)(7) of this subpart; and

(iii) All failures to maintain the activated carbon injection rate, and the activated carbon injection carrier gas flow rate or pressure drop, as applicable, as required under §63.1344(c).

(iv) The results of any combustion system component inspections conducted within the reporting period as required under §63.1350(i).

(v) All failures to comply with any provision of the operation and maintenance plan developed in accordance with §63.1390(a).

(10) If the total continuous monitoring system downtime for any CEM or any continuous monitoring system (CMS) for the reporting period is ten percent or greater of the total operating time for the reporting period, the owner or operator shall submit an excess emissions and continuous monitoring system performance report along with the summary report.

§63.1355 Recordkeeping requirements.

(a) The owner or operator shall maintain files of all information (including all reports and notifications) required by this section recorded in a form suitable and readily available for inspection and review as required by §63.10(b)(1). The files shall be retained for at least five years following the
Environmental Protection Agency

§ 63.1357 Temporary, conditioned exemption from particulate matter and opacity standards.

(a) Subject to the limitations of paragraphs (b) through (f) of this section, an owner or operator conducting PM CEMS correlation tests (that is, correlation with manual stack methods) is exempt from:

1. Any particulate matter and opacity standards of part 60 or part 63 of this chapter that are applicable to cement kilns and in-line kiln/raw mills.

2. Any permit or other emissions or operating parameter or other limitation on workplace practices that are applicable to cement kilns and in-line kiln raw mills to ensure compliance with any particulate matter and opacity standards of this part or part 60 of this chapter.

(b) The owner or operator must develop a PM CEMS correlation test plan. The plan must be submitted to the Administrator for approval at least 90 days before the correlation test is scheduled to be conducted. The plan must include:

1. The number of test conditions and the number of runs for each test condition;

2. The target particulate matter emission level for each test condition;

3. How the operation of the affected source will be modified to attain the desired particulate matter emission rate; and

4. The anticipated normal particulate matter emission level.

(c) The Administrator will review and approve or disapprove the correlation test plan in accordance with §63.7(c)(3)(i) and (iii). If the Administrator fails to approve or disapprove the correlation test plan within the time period specified in §63.7(c)(3)(iii), the plan shall be considered approved, unless the Administrator has requested additional information.

(d) The stack sampling team must be on-site and prepared to perform correlation testing no later than 24 hours after operations are modified to attain the desired particulate matter emission concentrations, unless the correlation test plan documents that a longer period is appropriate.

§ 63.1356 Exemption from new source performance standards.

(a) Except as provided in paragraphs (a)(1) and (a)(2) of this section, any affected source subject to the provisions of this subpart is exempted from any otherwise applicable new source performance standard contained in 40 CFR part 60, subpart F.

1. Kilns and in-line kiln/raw mills, as applicable under 40 CFR 60.60(b), located at area sources are subject to PM and opacity limits and associated reporting and recordkeeping, under 40 CFR part 60, subpart F.

2. Greenfield raw material dryers, as applicable under 40 CFR 60.60(b), located at area sources are subject to opacity limits and associated reporting and recordkeeping under 40 CFR part 60, subpart F.
§ 63.1358 Delegation of authority.

(a) In delegating implementation and enforcement authority to a State under subpart E of this part, the authorities contained in paragraph (b) of this section shall be retained by the Administrator and not transferred to a State.

(b) Authority which will not be delegated to States:

(1) Approval of alternative non-opacity emission standards under §63.6(g).

(2) Approval of alternative opacity standards under §63.6(h)(9).

(3) Approval of major changes to test methods under §§63.7(e)(2)(ii) and 63.7(f). A major change to a test method is a modification to a federally enforceable test method that uses unproven technology or procedures or is an entirely new method (sometimes necessary when the required test method is unsuitable).

(4) Approval of major changes to monitoring under §63.8(f). A major change to monitoring is a modification to federally enforceable monitoring that uses unproven technology or procedures, is an entirely new method (sometimes necessary when the required monitoring is unsuitable), or is a change in the averaging period.

(5) Waiver of recordkeeping under §63.10(f).

§ 63.1359 [Reserved]

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### Subpart MMM—National Emission Standards for Hazardous Air Pollutants for Pesticide Active Ingredient Production

**Source:** 64 FR 33589, June 23, 1999, unless otherwise noted.

**§ 63.1360 Applicability.**

(a) **Definition of affected source.** The affected source subject to this subpart is the facility-wide collection of pesticide active ingredient manufacturing process units (PAI process units) that process, use, or produce HAP, and are located at a plant site that is a major source, as defined in section 112(a) of the CAA. An affected source also includes waste management units, heat exchange systems, and cooling towers that are associated with the PAI process units. Exemptions from an affected source are specified in paragraph (d) of this section.

(b) **New source applicability.** A new affected source subject to this subpart and to which the requirements for new sources apply is defined according to the criteria in either paragraph (b)(1) or (2) of this section:

(1) An affected source for which construction or reconstruction commenced after November 10, 1997;

(2) Any single PAI process unit that:

(i) is not part of a process unit group; and

(ii) For which construction, as defined in §63.1361, commenced after November 10, 1997; and

(iii) Has the potential to emit 10 tons/yr of any one HAP or 25 tons/yr of combined HAP.

(c) **General provisions.** Table 1 of this subpart specifies the provisions of subpart A of this part that apply to an owner or operator of an affected source subject to this subpart, and clarifies specific provisions in subpart A of this part as necessary for this subpart.

(d) **Exemptions from the requirements of this subpart.** The provisions of this subpart do not apply to:

(1) Research and development facilities;

(2) PAI process units that are subject to subpart F of this part;

(3) Production of ethylene; and

(4) The following emission points listed:

(i) Storm water from segregated sewers;

(ii) Water from fire-fighting and deluge systems, including testing of such systems;

(iii) Spills;

(iv) Water from safety showers;

(v) Noncontact steam boiler blowdown and condensate;

(vi) Laundry water;

(vii) Vessels storing material that contains no organic HAP or contains organic HAP as impurities only; and

(viii) Equipment, as defined in §63.1363, that is intended to operate in
organic HAP service for less than 300 hours during the calendar year.

(e) Applicability of this subpart except during periods of startup, shutdown, and malfunction. (1) Each provision set forth in this subpart shall apply at all times except that emission limitations shall not apply during periods of startup, shutdown, and malfunction, as defined in §63.1361, if:

(i) The startup, shutdown, or malfunction precludes the ability of the owner or operator of an affected source to comply with one or more specific emission limitations to which a particular emission point is subject; and

(ii) The owner or operator follows the provisions for periods of startup, shutdown, and malfunction, as specified in §§63.1367(a)(3) and 63.1368(i).

(2) The provisions set forth in §63.1363 shall apply at all times except during periods of nonoperation of the PAI process unit (or specific portion thereof) in which the lines are drained and depressurized resulting in the cessation of the emissions to which §63.1363 applies.

(3) The owner or operator shall not shut down items of equipment that are required or utilized for compliance with the emissions limitations of this subpart during times when emissions (or, where applicable, wastewater streams or residuals) are being routed to such items of equipment, if the shutdown would contravene emissions limitations of this subpart applicable to such items of equipment. This paragraph does not apply if the item of equipment is malfunctioning, or if the owner or operator must shut down the equipment to avoid damage due to a malfunction of the PAI process unit or portion thereof.

(4) During startups, shutdowns, and malfunctions when the emissions limitations of this subpart do not apply pursuant to paragraphs (e)(1) through (3) of this section, the owner or operator shall implement, to the extent reasonably available, measures to prevent or minimize excess emissions. For purposes of this paragraph, “excess emissions” means emissions in excess of those that would have occurred if there were no startup, shutdown, or malfunction and the owner or operator complied with the relevant provisions of this subpart. The measures to be taken shall be identified in the applicable startup, shutdown, and malfunction plan, and may include, but are not limited to, air pollution control technologies, work practices, pollution prevention, monitoring, and/or changes in the manner of operation of the source. Back-up control devices are not required, but may be used if available.

(f) Storage vessel applicability determination. An owner or operator shall follow the procedures specified in paragraphs (f)(1) through (4) of this section to determine whether a storage vessel is part of the affected source to which this subpart applies.

(1) If a storage vessel is already subject to another subpart of 40 CFR part 63 on June 23, 1999, the storage vessel shall belong to the process unit subject to the other subpart.

(2) Unless otherwise excluded under paragraph (f)(1) of this section, the storage vessel is part of a PAI process unit if either the input to the vessel from the PAI process unit is greater than or equal to the input from any other PAI or non-PAI process unit, or the output from the vessel to the PAI process unit is greater than or equal to the output to any other PAI or non-PAI process unit. If the greatest input to and/or output from a shared storage vessel is the same for two or more process units, including at least one PAI process unit, the owner or operator may assign the storage vessel to any one of the PAI process units that meet this condition. If the use varies from year to year, then the use for purposes of this subpart for existing sources shall be based on the utilization that occurred during the year preceding June 23, 1999 or, if the storage vessel was not in operation during that year, the use shall be based on the expected use in the 5 years after startup. This determination shall be reported as part of an operating permit application or as otherwise specified by the permitting authority.

(3) Unless otherwise excluded under paragraph (f)(1) of this section, where a storage vessel is located in a tank farm (including a marine tank farm), the applicability of this subpart shall be determined according to the provisions in

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paragraphs (f)(3)(i) through (iv) of this section.

(i) The storage vessel may only be assigned to a process unit that utilizes the storage vessel and does not have an intervening storage vessel for that product (or raw material, as appropriate). With respect to a process unit, an intervening storage vessel means a storage vessel connected by hard-piping to the process unit and to the storage vessel in the tank farm so that product or raw material entering or leaving the process unit flows into (or from) the intervening storage vessel and does not flow directly into (or from) the storage vessel in the tank farm.

(ii) If no PAI process unit meets the criteria of paragraph (f)(3)(i) of this section with respect to a storage vessel, this subpart does not apply to the storage vessel.

(iii) If only one PAI process unit, and no non-PAI process unit, meets the criteria of paragraph (f)(3)(i) of this section with respect to a storage vessel, the storage vessel shall be assigned to that PAI process unit.

(iv) If two or more process units, including at least one PAI process unit, meet the criteria of paragraph (f)(3)(i) of this section with respect to a storage vessel, the storage vessel shall be assigned to one of those process units according to the provisions of paragraph (f)(2) of this section. The input and output shall be determined among only those process units that meet the criteria of paragraph (f)(3)(i) of this section. If the storage vessel is not assigned to a PAI process unit according to the provisions of paragraph (f)(2) of this section, this subpart does not apply to the storage vessel.

(4) If the storage vessel begins receiving material from (or sending material to) another process unit, or ceasing to receive material from (or send material to) a PAI process unit, or if the applicability of this subpart has been determined according to the provisions of paragraph (f)(2) of this section, and there is a significant change in the use of the storage vessel, the owner or operator shall reevaluate the ownership determination for the storage vessel.

(g) Designating production of an intermediate as a PAI process unit. Except as specified in paragraph (d) of this section, an owner or operator may elect to designate production of any intermediate that does not meet the definition of integral intermediate as a PAI process unit subject to this subpart. Any storage vessel containing the intermediate is assigned to a PAI process unit according to the procedures in paragraph (f) of this section. Any process tank containing the intermediate is part of the process unit used to produce the intermediate.

(h) Applicability of process units included in a process unit group. (1) If any of the products produced in the process unit group are subject to 40 CFR part 63, subpart GGG (Pharmaceuticals MACT), the owner or operator may elect to comply with the requirements of subpart GGG for the PAI process unit(s) within the process unit group, except for the following:

(i) The emission limit standard for process vents in §63.1362(b)(2)(i) shall apply in place of §63.1254(a)(1) of subpart GGG of this part;

(ii) When the date of April 2, 1997 is provided in §63.1254(a)(iii) of subpart GGG of this part, the date of June 23, 1999 shall apply for purposes of this subpart; and

(iii) Requirements in §63.1367(a)(5) regarding application for approval of construction or reconstruction shall apply in place of the provisions in §63.1259(a)(5) of subpart GGG of this part.

(2) If the primary product of a process unit group is determined to be a material that is subject to another subpart of 40 CFR part 63 on June 23, 1999 or startup of the process unit group, whichever is later, the owner or operator may elect to comply with the other subpart for any PAI process unit within the process unit group.

(3) The primary product of the process unit group shall be determined according to paragraphs (h)(3)(i) and (ii) of this section.

(i) The primary product is the product that is produced for the greatest operating time over a 5 year period, based on expected utilization for the 5 years following the compliance date or following initial startup of the process unit group, whichever is later; or
(ii) If the process unit group produces multiple products equally based on operating time, then the product with the greatest production on a mass basis over 5 years shall represent the primary product of the process unit, based on expected utilization for the 5 years following the compliance date or following initial startup of the unit or unit group, whichever is later.

(i) Overlap with other regulations. (1) Overlap with other MACT standards. After the compliance dates specified in §63.1364, an affected source subject to the provisions of this subpart that is also subject to the provisions of any other subpart of 40 CFR part 63 may elect, to the extent the subparts are consistent, under which subpart to maintain records and report to EPA. The affected source shall identify in the Notification of Compliance Status report required by §63.1368(f) under which authority such records will be maintained.

(2) Overlap with RCRA subparts AA, BB, and/or CC. After the compliance dates specified in §63.1364, if any affected source subject to this subpart is also subject to monitoring, recordkeeping, and reporting requirements in 40 CFR part 264, subpart AA, BB, or CC, or is subject to monitoring and recordkeeping requirements in 40 CFR part 265, subpart AA, BB, or CC, and the owner or operator complies with the periodic reporting requirements under 40 CFR part 264, subpart AA, BB, or CC that would apply to the device if the facility had final-permitted status, the owner or operator may elect to comply with either the provisions of this subpart MMM or the provisions of subpart H of this part. The owner or operator shall identify in the Notification of Compliance Status report required by §63.1368(f) under which authority such records will be maintained.

(3) Overlap with NSPS subpart Kb. After the compliance dates specified in §63.1364, a Group 1 or Group 2 storage vessel that is also subject to the provisions of 40 CFR part 60, subpart Kb, is required to comply only with the provisions of this subpart MMM.

(4) Overlap with subpart I. After the compliance dates specified in §63.1364, for all equipment within a process unit that contains equipment subject to subpart I of this part, an owner or operator may elect to comply with either the provisions of this subpart MMM or the provisions of subpart H of this part. The owner or operator shall identify in the Notification of Compliance Status report required by §63.1368(f) the provisions with which the owner or operator elects to comply.

(5) Overlap with RCRA regulations for wastewater. After the compliance dates specified in §63.1364, the owner or operator of an affected wastewater stream that is also subject to provisions in 40 CFR parts 260 through 272 shall comply with the more stringent control requirements (e.g., waste management units, numerical treatment standards, etc.) and the more stringent testing, monitoring, recordkeeping, and reporting requirements that overlap between the provisions of this subpart and the provisions of 40 CFR parts 260 through 272. The owner or operator shall keep a record of the information used to determine which requirements were the most stringent and shall submit this information if requested by the Administrator.

(6) Overlap with NSPS subparts III, NNN, and RRR. After the compliance dates specified in §63.1364, if an owner or operator of a process vent subject to this subpart MMM that is also subject to the provisions of 40 CFR part 60, subpart III, or subpart NNN, or subpart RRR, elects to reduce organic HAP emissions from the process vent by 98 percent as specified in §63.1362(b)(2)(iii)(A), then the owner or operator is required to comply only with the provisions of this subpart MMM. Otherwise, the owner or operator shall comply with the provisions
in both this subpart MMM and the provisions in 40 CFR part 60, subparts III, NNN, and RRR, as applicable.

(j) Meaning of periods of time. All terms in this subpart MMM that define a period of time for completion of required tasks (e.g., weekly, monthly, quarterly, annual), unless specified otherwise in the section or subsection that imposes the requirement, refer to the standard calendar periods.

(1) Notwithstanding time periods specified in the subpart MMM for completion of required tasks, such time periods may be changed by mutual agreement between the owner and operator and the Administrator, as specified in subpart A of this part (e.g., a period could begin on the compliance date or another date, rather than on the first day of the standard period). For each time period that is changed by agreement, the revised period shall remain in effect until it is changed. A new request is not necessary for each recurring period.

(2) Where the period specified for compliance is a standard calendar period, if the initial compliance date occurs after the beginning of the period, compliance shall be required according to the schedule specified in paragraph (j)(1)(i) or (ii) of this section, as appropriate.

(i) Compliance shall be required before the end of the standard calendar period within which the compliance deadline occurs, if there remain at least 3 days for tasks that must be performed weekly, at least 2 weeks for tasks that must be performed monthly, at least 1 month for tasks that must be performed each quarter, or at least 3 months for tasks that must be performed annually; or

(ii) In all other cases, compliance shall be required before the end of the first full standard calendar period within which the initial compliance deadline occurs.

(3) In all instances where a provision of this subpart MMM requires completion of a task during each of multiple successive periods, an owner or operator may perform the required task at any time during the specified period, provided the task is conducted at a reasonable interval after completion of the task in the previous period.

§ 63.1361 Definitions.

Terms used in this subpart are defined in the CAA, in subpart A of this part, or in this section. If the same term is defined in subpart A of this part and in this section, it shall have the meaning given in this section for the purposes of this subpart MMM.

Air pollution control device or control device means equipment installed on a process vent, storage vessel, wastewater treatment exhaust stack, or combination thereof that reduces the mass of HAP emitted to the air. The equipment may consist of an individual device or a series of devices. Examples include incinerators, carbon adsorption units, condensers, flares, boilers, process heaters, and gas absorbers. Process condensers are not considered air pollution control devices or control devices.

Bag dump means equipment into which bags or other containers containing a powdered, granular, or other solid feedstock material are emptied. A bag dump is part of the process.

Batch emission episode means a discrete venting episode that is associated with a single unit operation. A unit operation may have more than one batch emission episode. For example, a batch distillation unit operation may consist of batch emission episodes associated with charging and heating. Charging the vessel with HAP will result in one discrete batch emission episode that will last through the duration of the charge and will have an average flowrate equal to the rate of the charge. Another discrete batch emission episode will result from the expulsion of expanded vapor as the contents of the vessel are heated.

Batch operation means a noncontinuous operation involving intermittent or discontinuous feed into PAI or integral intermediate manufacturing equipment, and, in general, involves the emptying of the equipment after the batch operation ceases and prior to beginning a new operation. Addition of raw material and withdrawal of product do not occur simultaneously in a batch operation. A batch process consists of a series of batch operations.

Bench-scale batch process means a batch process (other than a research
and development facility) that is capable of being located on a laboratory bench top. This bench-scale equipment will typically include reagent feed vessels, a small reactor and associated product separator, recovery and holding equipment. These processes are only capable of producing small quantities of product.

Block means a time period equal to, at a maximum, the duration of a single batch.

Car seal means a seal that is placed on a device that is used to change the position of a valve (e.g., from opened to closed) in such a way that the position of the valve cannot be changed without breaking the seal.

Cleaning operation means routine rinsing, washing, or boil-off of equipment in batch operations between batches.

Closed-loop system means an enclosed system that returns process fluid to the process and is not vented to the atmosphere except through a closed-vent system.

Closed-purge system means a system or combination of system and portable containers, to capture purged liquids. Containers must be covered or closed when not being filled or emptied.

Closed-vent system means a system that is not open to the atmosphere and is composed of piping, ductwork, connections, and, if necessary, flow inducing devices that transport gas or vapor from an emission point to a control device.

Combustion device means an individual unit of equipment, such as a flare, incinerator, process heater, or boiler, used for the combustion of organic HAP vapors.

Connector means flanged, screwed, or other joined fittings used to connect two pipe lines or a pipe line and a piece of equipment. A common connector is a flange. J oined fittings welded completely around the circumference of the interface are not considered connectors for the purpose of this regulation. For the purpose of reporting and record keeping, connector means joined fittings that are not inaccessible, ceramic, or ceramic-lined as described in §63.1255(b)(1)(vii) and 63.1255(f)(3).

Construction means the onsite fabrication, erection, or installation of an affected source or PAI process unit. Addition of new equipment to an existing PAI process unit does not constitute construction.

Consumption means the makeup quantity of HAP entering a process that is not used as reactant. The quantity of material used as reactant is the theoretical amount needed assuming a 100 percent stoichiometric conversion. Makeup is the net amount of material that must be added to the process to replenish losses.

Container, as used in the wastewater provisions, means any portable waste management unit that has a capacity greater than or equal to 0.1 m$^3$ in which a material is stored, transported, treated, or otherwise handled. Examples of containers are drums, barrels, tank trucks, barges, dumpsters, tank cars, dump trucks, and ships.

Continuous process means a process where the inputs and outputs flow continuously throughout the duration of the process. Continuous processes typically approach steady state.

Continuous seal means a seal that forms a continuous closure that completely covers the space between the wall of the storage vessel and the edge of the floating roof. A continuous seal may be a vapor-mounted, liquid-mounted, or metallic shoe seal.

Controlled HAP emissions means the quantity of HAP components discharged to the atmosphere from an air pollution control device.

Cover, as used in the wastewater provisions, means a device or system which is placed on or over a waste management unit containing wastewater or residuals so that the entire surface area is enclosed to minimize air emissions. A cover may have openings necessary for operation, inspection, and maintenance of the waste management unit such as access hatches, sampling ports, and gauge wells provided that each opening is closed when not in use. Examples of covers include a fixed roof installed on a wastewater tank, a lid installed on a container, and an air-supported enclosure installed over a waste management unit.
Double block and bleed system means two block valves connected in series with a bleed valve or line that can vent the line between the two block valves.

Duct work means a conveyance system such as those commonly used for heating and ventilation systems. It is often made of sheet metal and often has sections connected by screws or crimping. Hard-piping is not ductwork.

Equipment, for purposes of §63.1363, means each pump, compressor, agitator, pressure relief device, sampling connection system, open-ended valve or line, valve, connector, and instrumentation system in organic hazardous air pollutant service.

External floating roof means a pontoon-type or double-deck type cover that rests on the liquid surface in a storage tank or waste management unit with no fixed roof.


Fill or filling means the introduction of organic HAP into a storage tank or the introduction of a wastewater stream or residual into a waste management unit, but not necessarily to complete capacity.

First attempt at repair means to take action for the purpose of stopping or reducing leakage of organic material to the atmosphere.

Fixed roof means a cover that is mounted on a waste management unit or storage tank in a stationary manner and that does not move with fluctuations in liquid level.

Flame ionization detector (FID) means a device in which the measured change in conductivity of a standard flame (usually hydrogen) due to the insertion of another gas or vapor is used to detect the gas or vapor.

Floating roof means a cover consisting of a double deck, pontoon single deck, internal floating cover or covered floating roof, which rests upon and is supported by the liquid being contained, and is equipped with a continuous seal or seals to close the space between the roof edge and waste management unit or storage vessel wall.

Flow indicator means a device that indicates whether gas flow is, or whether the valve position would allow gas flow to be, present in a line.

Group 1 process vent means any process vent from a process at an existing or new affected source for which the uncontrolled organic HAP emissions from the sum of all process vents are greater than or equal to 0.15 Mg/yr and/or the uncontrolled hydrogen chloride (HCl) and chlorine emissions from the sum of all process vents are greater than or equal to 6.8 Mg/yr.

Group 2 process vent means any process vent that does not meet the definition of a Group 1 process vent.

Group 1 storage vessel means a storage vessel at an existing affected source with a capacity equal to or greater than 75 m³ and storing material with a maximum true vapor pressure greater than or equal to 3.45 kPa, or a storage vessel at a new affected source with a capacity equal to or greater than 40 m³ and storing material with a maximum true vapor pressure greater than or equal to 16.5 kPa and with a capacity greater than or equal to 75 m³ and storing material with a maximum true vapor pressure greater than or equal to 3.45 kPa.

Group 2 storage vessel means a storage vessel that does not meet the definition of a Group 1 storage vessel.

Group 1 wastewater stream means process wastewater at an existing or new source that meets the criteria for Group 1 status in §63.132(c) of subpart G of this part for compounds in Table 9 of subpart G of this part or a maintenance wastewater stream that contains 5.3 Mg of HAP per discharge event.

Group 2 wastewater stream means any wastewater stream that does not meet the definition of a Group 1 wastewater stream.

Group of processes means all of the equipment associated with processes in a building, processing area, or facility-wide. A group of processes may consist of a single process.

Halogenated compounds means organic compounds that contain chlorine atoms.

Halogenated vent stream means a process, storage vessel, or waste management unit vent stream determined to have a concentration of halogenated compounds of greater than 20 ppmv, as determined through process knowledge, test results using Method 18 of 40 CFR part 60, appendix A, or test results.
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using any other test method that has been validated according to the procedures in Method 301 of appendix A of this part.

Hard-piping means piping or tubing that is manufactured and properly installed using good engineering judgment and standards, such as ANSI B31-3.

Impurity means a substance that is produced coincidentally with the product(s), or is present in a raw material. An impurity does not serve a useful purpose in the production or use of the product(s) and is not isolated.

In gas/vapor service means that a piece of equipment in organic HAP service contains a gas or vapor at operating conditions.

In heavy liquid service means that a piece of equipment in organic HAP service is not in gas/vapor service or in light liquid service.

In light liquid service means that a piece of equipment in organic HAP service contains a liquid that meets the following conditions:

(1) The vapor pressure of one or more of the organic compounds is greater than 0.3 kPa at 20°C.

(2) The total concentration of the pure organic compounds constituents having a vapor pressure greater than 0.3 kPa at 20°C is equal to or greater than 20 percent by weight of the total process stream; and

(3) The fluid is a liquid at operating conditions.

NOTE: To definition of "In light liquid service: Vapor pressures may be determined by the methods described in 40 CFR 60.485(e)(1).

In liquid service means that a piece of equipment in organic HAP service is not in gas/vapor service.

In organic hazardous air pollutant or in organic HAP service means that a piece of equipment either contains or contacts a fluid (liquid or gas) that is at least 5 percent by weight of total organic HAP as determined according to the provisions of §63.1380(d) of subpart H of this part. The provisions of §63.1380(d) of subpart H of this part also specify how to determine that a piece of equipment is not in organic HAP service.

In vacuum service means that equipment is operating at an internal pressure which is at least 5 kPa below ambient pressure.

In situ sampling systems means non-extractive samplers or in-line samplers.

Individual drain system means the stationary system used to convey wastewater streams or residuals to a waste management unit or to discharge or disposal. The term includes: hard piping; all process drains and junction boxes; and associated sewer lines, other junction boxes, manholes, sumps, and lift stations conveying wastewater streams or residuals. A segregated stormwater sewer system, which is a drain and collection system designed and operated for the sole purpose of collecting rainfall-runoff at a facility, and which is segregated from all other individual drain systems, is excluded from this definition.

Instrumentation system means a group of equipment components used to condition and convey a sample of the process fluid to analyzers and instruments for the purpose of determining process operating conditions (e.g., composition, pressure, flow, etc.). Valves and connectors are the predominant type of equipment used in instrumentation systems; however, other types of equipment may also be included in these systems. Only valves nominally 0.5 inches and smaller and connectors nominally 0.75 inches and smaller in diameter are considered instrumentation systems for the purposes of this subpart. Valves greater than nominally 0.5 inches and connectors greater than nominally 0.75 inches associated with instrumentation systems are not considered part of instrumentation systems and must be monitored individually.

Integral intermediate means an intermediate for which 50 percent or more of the annual production is used in on-site production of any PAI(s) and that is not stored before being used in the production of another integral intermediate or the PAI(s). For the purposes of this definition, an intermediate is stored if it is discharged to a storage vessel and at least one of the following conditions is met: the processing equipment that discharges to the storage vessel is shutdown; during an annual period, the material must be
stored in the vessel for at least 30 days before being used to make a PAI; or the processing equipment that discharges to the storage vessel is located in a separate building (or processing area) of the plant than the processing equipment that uses material from the storage vessel as a feedstock, and control equipment is not shared by the two processing areas. Any process unit that produces an intermediate and is subject to subpart F of this part is not an integral intermediate.

Intermediate means an organic compound that is produced by chemical reaction and that is further processed or modified in one or more additional chemical reaction steps to produce another intermediate or a PAI.

Internal floating roof means a cover that rests or floats on the liquid surface (but not necessarily in complete contact with it) inside a storage tank or waste management unit that has a permanently affixed roof.

Junction box means a manhole or access point to a wastewater sewer system line or a lift station.

Large control device means a control device that controls process vents, and the total HAP emissions into the control device from all sources are greater than or equal to 10 tons/yr.

Liquid-mounted seal means a foam- or liquid-filled seal mounted in contact with the liquid between the wall of the storage vessel or waste management unit and the floating roof. The seal is mounted continuously around the tank or unit.

Liquids dripping means any visible leakage from the seal including dripping, spraying, misting, clouding, and ice formation. Indications of liquid dripping include puddling or new stains that are indicative of an existing evaporated drip.

Maintenance wastewater means wastewater generated by the draining of process fluid from components in the PAI process unit into an individual drain system prior to or during maintenance activities. Maintenance wastewater can be generated through planned or unplanned shutdowns and during periods not associated with a shutdown. Examples of activities that can generate maintenance wastewaters include descaling of heat exchanger tubing bundles, cleaning of distillation column traps, draining of low legs and high point bleeds, draining of pumps into an individual drain system, and draining of portions of the PAI process unit for repair.

Malfunction means any sudden, infrequent, and not reasonably preventable failure of air pollution control equipment, emissions monitoring equipment, process equipment, or a process to operate in a normal or usual manner. Failures that are caused all or in part by poor maintenance or careless operation are not malfunctions.

Maximum true vapor pressure means the equilibrium partial pressure exerted by the total organic HAP stored or transferred liquid at the temperature equal to the highest calendar-month average of the liquid storage or transferred temperature for liquids stored or transferred above or below the ambient temperature or at the local maximum monthly average temperature as reported by the National Weather Service for liquids stored or transferred at the ambient temperature, as determined:

(1) In accordance with methods described in Chapter 19.2 of the American Petroleum Institute's Manual of Petroleum Measurement Standards, Evaporative Loss From Floating-Roof Tanks (incorporated by reference as specified in §63.14 in subpart A of this part); or

(2) As obtained from standard reference texts; or

(3) As determined by the American Society for Testing and Materials Method D2879-97, Test Method for Vapor Pressure-Temperature Relationship and Initial Decomposition Temperature of Liquids by Isoteniscope (incorporated by reference as specified in §63.14 of subpart A of this part); or

(4) Any other method approved by the Administrator.

Metallic shoe seal or mechanical shoe seal means metal sheets that are held vertically against the wall of the storage tank by springs, weighted levers, or other mechanisms and connected to the floating roof by braces or other means. A flexible coated fabric (envelope) spans the annular space between the metal sheet and the floating roof.

Nonrepairable means that it is technically infeasible to repair a piece of
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equipment from which a leak has been detected without a process shutdown.

Open-ended valve or line means any valve, except pressure relief valves, having one side of the valve seat in contact with process fluid and one side open to atmosphere, either directly or through open piping.

Operating scenario, for the purposes of reporting and recordkeeping, means a description of a PAI process unit, including: identification of each wastewater point of determination (POD) and their associated emissions episodes and durations, and their associated level of control and control devices; calculations and engineering analyses required to demonstrate compliance; a description of operating and/or testing conditions for any associated control device.

Organic compound, as used in the definitions of intermediate and PAI, means any compound that contains both carbon and hydrogen with or without other elements.

Organic HAP means those HAP listed in section 112(b) of the CAA that are measured according to the procedures of Method 18 or Method 25A, 40 CFR part 60, appendix A.

Pesticide active ingredient or PAI means any material that is an active ingredient within the meaning of FIFRA section 2(a); that is used to produce an insecticide, herbicide, or fungicide end use pesticide product; that consists of one or more organic compounds; and that must be labeled in accordance with 40 CFR part 156 for transfer, sale, or distribution. These materials are typically described by North American Industrial Classification System (NAICS) Codes 325199 and 32532 (i.e., previously known as Standard Industrial Classification System Codes 2869 and 2879). These materials are identified by product classification codes 01, 21, 02, 04, 44, 07, 08, and 16 in block 19 on EPA form 3540-16, the Pesticides Report for Pesticide-Producing Establishments.

Pesticide active ingredient manufacturing process unit (PAI process unit) means a process unit that is used to produce a material that is primarily used as a PAI or integral intermediate. A PAI process unit consists of: the process, as defined in this subpart; associated storage vessels, as determined by the procedures in §63.1360(f); equipment identified in §63.1362(l); connected piping and ducts; and components such as pumps, compressors, agitators, pressure relief devices, sampling connection systems, open-ended valves or lines, valves, connectors, and instrumentation systems. A material is primarily used as a PAI or integral intermediate if more than 50 percent of the projected annual production from a process unit in the 3 years after June 23, 1999 or startup, whichever is later, is used as a PAI or integral intermediate; recordkeeping is required if the material is used as a PAI or integral intermediate, but not as the primary use. If the primary use changes to a PAI or integral intermediate, the process unit becomes a PAI process unit unless it is already subject to the HON. If the primary use changes from a PAI or integral intermediate to another use, the process unit remains a PAI process unit. Any process tank containing an integral intermediate is part of the PAI process unit used to produce the integral intermediate. A process unit that produces an intermediate that is not an integral intermediate may be designated as a PAI process unit according to the procedures of §63.1360(g). Formulation of pesticide products is not considered part of a PAI process unit. Quality assurance and quality control laboratories are not considered part of a PAI process unit.

Plant site means all contiguous or adjoining property that is under common control, including properties that are separated only by a road or other public right-of-way. Common control includes properties that are owned, leased, or operated by the same entity, parent entity, subsidiary, or any combination thereof.

Point of determination (POD) means each point where a wastewater stream exits the PAI process unit.

NOTE to definition of "point of determination": The regulation allows determination of the characteristics of a wastewater stream: at the point of determination; or downstream of the point of determination if corrections are made for changes in flow rate and
annual average concentration of Table 9 compounds as determined in §63.144 of subpart G of this part. Such changes include: losses by air emissions, reduction of annual average concentration or changes in flow rate by mixing with other water or wastewater streams, and reduction in flow rate or annual average concentration by treating or otherwise handling the wastewater stream to remove or destroy HAP.

Pressure release means the emission of materials resulting from the system pressure being greater than the set pressure of the pressure relief device. This release can be one release or a series of releases over a short time period due to a malfunction in the process.

Pressure relief device or valve means a safety device used to prevent operating pressures from exceeding the maximum allowable working pressure of the process equipment. A common pressure relief device is a spring-loaded pressure relief valve. Devices that are actuated either by a pressure of less than or equal to 25 pounds per square inch gauge or by a vacuum are not pressure relief devices.

Process means a logical grouping of processing equipment which collectively function to produce a product. For the purpose of this subpart, a PAI process includes all, or a combination of, reaction, recovery, separation, purification, treatment, cleaning, and other activities or unit operations, which are used to produce a PAI or integral intermediate. A PAI process and all integral intermediate processes for which 100 percent of the annual production is used in the production of the PAI may be linked together and defined as a single PAI process unit.

Process condenser means a condenser whose primary purpose is to recover material as an integral part of a unit operation. The condenser must cause a vapor-to-liquid phase change for periods during which the temperature of liquid in the process equipment is at or above its boiling or bubble point. Examples of process condensers include distillation condensers, reflux condensers, and condensers used in stripping or flushing operation. In a series of condensers, all condensers up to and including the first condenser with an exit gas temperature below the boiling or bubble point of the liquid in the process equipment are considered to be process condensers. All condensers in line prior to the vacuum source are included in this definition.

Process shutdown means a work practice or operational procedure that stops production from a process or part of a process during which it is technically feasible to clear process material from a process or part of a process consistent with safety constraints and during which repairs can be effected. An unscheduled work practice or operational procedure that stops production from a process or part of a process for less than 24 hours is not a process shutdown. An unscheduled work practice or operational procedure that would stop production from a process or part of a process for a shorter period of time than would be required to clear the process or part of the process of materials and start up the process, and would result in greater emissions than delay of repair of leaking components until the next scheduled process shutdown, is not a process shutdown. The use of spare equipment and technically feasible bypassing of equipment without stopping production are not process shutdowns.

Process tank means a tank that is used to collect material discharged from a feedstock storage vessel or equipment within the process and transfer of this material to other equipment within the process or a product storage vessel. Processing steps occur both upstream and downstream of the tank within a given process unit. Surge control vessels and bottoms receivers that fit these conditions are considered process tanks.

Process unit means the equipment assembled and connected by pipes or ducts to process raw materials and to manufacture an intended product.

Process unit group means a group of process units that manufacture PAI's and products other than PAI's by alternating raw materials or operating conditions, or by reconfiguring process equipment. Only process equipment that has been or could be part of a PAI process unit, because of its function or capacity, is included in a process unit group.
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Process vent means a point of emission from processing equipment to the atmosphere or a control device. The vent may be the release point for an emission stream associated with an individual unit operation, or it may be the release point for emission streams from multiple unit operations that have been manifolded together into a common header. Examples of process vents include, but are not limited to, vents on condensers used for product recovery, bottom receivers, surge control vessels, reactors, filters, centrifuges, process tanks, and product dryers. A vent is not considered to be a process vent for a given emission episode if the undiluted and uncontrolled emission stream that is released through the vent contains less than 20 ppmv HAP, as determined through process knowledge that no HAP are present in the emission stream; using an engineering assessment as discussed in §63.1365(b)(2)(ii); from test data collected using Method 1818 of 40 CFR part 60, appendix A; or from test data collected using any other test method that has been validated according to the procedures in Method 301 of appendix A of this part. Process vents do not include vents on storage vessels regulated under §63.1362(c), vents on wastewater emission sources regulated under §63.1362(d), or pieces of equipment regulated under §63.1363.

Process wastewater means wastewater which, during manufacturing or processing, comes into direct contact with, or results from, the production or use of any raw material, intermediate product, finished product, by-product, or waste product. Examples include: product tank drawdown or feed tank drawdown; water formed during a chemical reaction or used as a reactant; water used to wash impurities from organic products or reactants; water used to clean process equipment; water used to cool or quench vapor streams through direct contact; and condensed steam from jet ejector systems pulling vacuum on vessels containing organics.

Product means the compound(s) or chemical(s) that are produced or manufactured as the intended output of a process unit. Impurities and wastes are not considered products.

Product dryer means equipment that is used to remove moisture or other liquid from granular, powdered, or other solid PAI or integral intermediate products prior to storage, formulation, shipment, or other uses. The product dryer is part of the process.

Product dryer vent means a process vent from a product dryer through which a gas stream containing gaseous pollutants (i.e., organic HAP, HCl, or chlorine), particulate matter, or both are released to the atmosphere or are routed to a control device.

Production-indexed HAP consumption factor (HAP factor) is the result of dividing the annual consumption of total HAP by the annual production rate, per process.

Production-indexed VOC consumption factor (VOC factor) is the result of dividing the annual consumption of total VOC by the annual production rate, per process.

Publicly owned treatment works (POTW) is defined at 40 CFR part 403.3(0).

Reactor means a device or vessel in which one or more chemicals or reactants, other than air, are combined or decomposed in such a way that their molecular structures are altered and one or more new organic compounds are formed.

Recovery device, as used in the wastewater provisions, means an individual unit of equipment capable of, and normally used for the purpose of, recovering chemicals for fuel value (i.e., net positive heating value), use, reuse, or for sale for fuel value, use, or reuse. Examples of equipment that may be recovery devices include organic removal devices such as decanters, strippers, or thin-film evaporation units. To be a recovery device, a decanter and any other equipment based on the operating principle of gravity separation must receive only two-phase liquid streams.

Repaired means that equipment is adjusted, or otherwise altered, to eliminate a leak as defined in the applicable paragraphs of §63.1363.

Research and development facility means any stationary source whose primary purpose is to conduct research and development, where the operations
are under the close supervision of technically trained personnel, and is not engaged in the manufacture of products for commercial sale, except in a de minimis manner.

Residual means any liquid or solid material containing Table 9 compounds (as defined in §63.111 of subpart G of this part) that is removed from a wastewater stream by a waste management unit or treatment process that does not destroy organics (non-destructive unit). Examples of residuals from nondestructive wastewater management units include the organic layer and bottom residue removed by a decanter or organic-water separator and the overheads from a steam stripper or air stripper. Examples of materials which are not residuals include: silt; mud; leaves; bottoms from a steam stripper or air stripper; and sludges, ash, or other materials removed from wastewater being treated by destructive devices such as biological treatment units and incinerators.

Safety device means a closure device such as a pressure relief valve, frangible disc, fusible plug, or any other type of device which functions exclusively to prevent physical damage or permanent deformation to a unit or its air emission control equipment by venting gases or vapors directly to the atmosphere during unsafe conditions resulting from an unplanned, accidental, or emergency event. For the purposes of this subpart, a safety device is not used for routine venting of gases or vapors from the vapor headspace underneath a cover such as during filling of the unit or to adjust the pressure in this vapor headspace in response to normal daily diurnal ambient temperature fluctuations. A safety device is designed to remain in a closed position during normal operations and open only when the internal pressure, or another relevant parameter, exceeds the device threshold setting applicable to the air emission control equipment as determined by the owner or operator based on manufacturer recommendations, applicable regulations, fire protection and prevention codes, standard engineering codes and practices, or other requirements for the safe handling of flammable, combustible, explosive, reactive, or hazardous materials.

Sampling connection system means an assembly of equipment within a process unit used during periods of representative operation to take samples of the process fluid. Equipment used to take nonroutine grab samples is not considered a sampling connection system.

Sensor means a device that measures a physical quantity or the change in a physical quantity, such as temperature, pressure, flow rate, pH, or liquid level.

Set pressure means the pressure at which a properly operating pressure relief device begins to open to relieve atypical process system operating pressure.

Sewer line means a lateral, trunk line, branch line, or other conduit including, but not limited to, grates, trenches, etc., used to convey wastewater streams or residuals to a downstream waste management unit.

Shutdown means the cessation of operation of a continuous PAI process unit for any purpose. Shutdown also means the cessation of a batch PAI process unit or any related individual piece of equipment required or used to comply with this part or for emptying and degassing storage vessels for periodic maintenance, replacement of equipment, repair, or any other purpose not excluded from this definition. Shutdown does not apply to cessation of a batch PAI process unit at the end of a campaign or between batches (e.g., for rinsing or washing equipment), for routine maintenance, or for other routine operations.

Small control device means a control device that controls process vents, and the total HAP emissions into the control device from all sources are less than 10 tons of HAP per year.

Startup means the setting in operation of a continuous PAI process unit for any purpose, the first time a new or reconstructed batch PAI process unit begins production, or, for new equipment added, including equipment used to comply with this subpart, the first time the equipment is put into operation. For batch process units, startup does not apply to the first time the equipment is put into operation at the start of a campaign to produce a product that has been produced in the past.
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after a shutdown for maintenance, or when the equipment is put into operation as part of a batch within a campaign. As used in §63.1363, startup means the setting in operation of a piece of equipment or a control device that is subject to this subpart.

Startup means the setting in operation of a piece of equipment or a control device that is subject to this subpart.

Storage vessel means a tank or other vessel that is used to store organic liquid that contain one or more HAP and that has been assigned, according to the procedures in §63.1360(f) or (g), to a PAI process unit that is subject to this subpart MMM. The following are not considered storage vessels for the purposes of this subpart:

1. Vessels permanently attached to motor vehicles such as trucks, railcars, barges, or ships;
2. Pressure vessels designed to operate in excess of 204.9 kilopascals and without emissions to the atmosphere;
3. Vessels storing material that contains no organic HAP or contains organic HAP only as impurities;
4. Wastewater storage tanks;
5. Process tanks; and

Supplemental gases mean any non-affected gaseous streams (streams that are not from process vents, storage vessels, equipment or waste management units) that contain less than 20 ppmv TOC and less than 20 ppmv total HCl and chlorine, as determined through process knowledge, and are combined with an affected vent stream. Supplemental gases are often used to maintain pressures in manifolds or for fire and explosion protection and prevention. Air required to operate combustion device burner(s) is not considered a supplemental gas.

Surface impoundment means a waste management unit which is a natural topographic depression, manmade excavation, or diked area formed primarily of earthen materials (although it may be lined with manmade materials), which is designed to hold an accumulation of liquid wastes or waste containing free liquids. A surface impoundment is used for the purpose of treating, storing, or disposing of wastewater or residuals, and is not an injection well. Examples of surface impoundments are equalization, settling, and aeration pits, ponds, and lagoons.

Total organic compounds (TOC) means those compounds measured according to the procedures of Method 18 or Method 25A, 40 CFR part 60, appendix A.

Treatment process means a specific technique that removes or destroys the organics in a wastewater or residual stream such as a steam stripping unit, thin-film evaporation unit, waste incinerator, biological treatment unit, or any other process applied to wastewater streams or residuals to comply with §63.138 of subpart G of this part. Most treatment processes are conducted in tanks. Treatment processes are a subset of waste management units.

Uncontrolled HAP emissions mean a gas stream containing HAP which has exited the process (or process condenser, if any), but which has not yet been introduced into an air pollution control device to reduce the mass of HAP in the stream. If the process vent is not routed to an air pollution control device, uncontrolled emissions are those HAP emissions released to the atmosphere.

Unit operation means those processing steps that occur within distinct equipment that are used, among other things, to prepare reactants, facilitate reactions, separate and purify products, and recycle materials. Equipment used for these purposes includes, but is not limited to, reactors, distillation units, extraction columns, absorbers, decanters, dryers, condensers, and filtration equipment.

Vapor-mounted seal means a continuous seal that completely covers the annular space between the wall of the storage tank or waste management unit and the edge of the floating roof, and is mounted such that there is a vapor space between the stored liquid and the bottom of the seal.

Volatile organic compounds are defined in 40 CFR 51.100.

Waste management unit means the equipment, structure(s), and/or device(s) used to convey, store, treat, or dispose of wastewater streams or residuals. Examples of waste management units include wastewater tanks, surface impoundments, individual drain systems, and biological wastewater treatment units. Examples of
equipment that may be waste management units include containers, air flotation units, oil-water separators or organic-water separators, or organic removal devices such as decanters, strippers, or thin-film evaporation units. If such equipment is a recovery device, then it is part of a PAI process unit and is not a waste management unit.

Wastewater means water that meets either of the conditions described in paragraph (1) or (2) of this definition and is discarded from a PAI process unit that is at an affected source:

(1) Is generated from a PAI process and contains either:

(i) An annual average concentration of compounds in Table 9 of subpart G of this part of at least 5 ppmw and has an average flow rate of 0.02 L/min or greater; or

(ii) An annual average concentration of compounds in Table 9 of subpart G of this part of at least 10,000 ppmw at any flow rate;

(2) Is generated from a PAI process unit as a result of maintenance activities and contains at least 5.3 Mg of HAP per individual discharge event.

Wastewater tank means a stationary waste management unit that is designed to contain an accumulation of wastewater or residuals and is constructed primarily of nonearthen materials (e.g., wood, concrete, steel, plastic) which provide structural support. Wastewater tanks used for flow equalization are included in this definition.

Water seal controls means a seal pot, p-leg trap, or other type of trap filled with water (e.g., flooded sewers that maintain water levels adequate to prevent air flow through the system) that creates a water barrier between the sewer line and the atmosphere. The water level of the seal must be maintained in the vertical leg of a drain in order to be considered a water seal.

§ 63.1362 Standards.

(a) On and after the compliance dates specified in §63.1364, each owner or operator of an affected source subject to the provisions of this subpart shall control HAP emissions to the levels specified in this section and in §63.1363, as summarized in Table 2 of this subpart.

(b) Process vents. (1) The owner or operator of an existing source shall comply with the requirements of paragraphs (b)(2) and (3) of this section. The owner or operator of a new source shall comply with the requirements of paragraphs (b)(4) and (5) of this section. Compliance with paragraphs (b)(2) through (b)(5) of this section shall be demonstrated through the applicable test methods and initial compliance procedures in §63.1365 and the monitoring requirements in §63.1366.

(2) Organic HAP emissions from existing sources. The owner or operator of an existing affected source must comply with the requirements in either paragraph (b)(2)(i) of this section or with the requirements in paragraphs (b)(2)(ii) through (iv) of this section.

(i) The uncontrolled organic HAP emission rate shall not exceed 0.15 Mg/yr from the sum of all process vents within a process.

(ii) (A) Except as provided in paragraph (b)(2)(ii)(B) of this section, uncontrolled organic HAP emissions from a process vent shall be reduced by 98 percent by weight or greater if the flow-weighted average flowrate for the vent as calculated using Equation 1 of this subpart is less than or equal to the flowrate calculated using Equation 2 of this subpart.

\[
FR_a = \frac{\sum_{i=1}^{n} (D_i)(FR_i)}{\sum_{i=1}^{n} D_i} \quad (\text{Eq. 1})
\]

\[
FR = 0.02 \ast (HL) - 1,000 \quad (\text{Eq. 2})
\]

Where:

- \( FR_a \) = flow-weighted average flowrate for the vent, scfm
- \( D_i \) = duration of each emission event, min
- \( FR_i \) = flowrate of each emission event, scfm
- \( n \) = number of emission events
- \( HL \) = annual uncontrolled organic HAP emissions, lb/yr, as defined in §63.1361

(B) If the owner or operator can demonstrate that a control device, installed on or before November 10, 1997 on a process vent otherwise subject to the requirements of paragraph (b)(2)(iii)(A) of this section, reduces
inlet emissions of total organic HAP by greater than or equal to 90 percent by weight but less than 98 percent by weight, then the control device must be operated to reduce inlet emissions of total organic HAP by 90 percent by weight or greater.

(iii) Excluding process vents that are subject to the requirements in paragraph (b)(2)(ii) of this section, uncontrolled organic HAP emissions from the sum of all process vents within a process shall be reduced by 90 percent or greater by weight.

(iv) As an alternative to the requirements in paragraphs (b)(2)(ii) and (iii) of this section, uncontrolled organic HAP emissions from any process vent may be reduced in accordance with any of the provisions in paragraphs (b)(2)(i), (b)(2)(ii), or (b)(2)(iii) of this section. All remaining process vents within a process must be controlled in accordance with paragraphs (b)(2)(ii) and (iii) of this section.

(A) To outlet concentrations less than or equal to 20 ppmv as TOC; or

(B) By a flare that meets the requirements of §63.11(b); or

(C) By a control device specified in §63.1365(a)(4); or

(D) In accordance with the alternative standard specified in paragraph (b)(6) of this section.

(3) HCl and Cl₂ emissions from existing sources. For each process, the owner or operator of an existing source shall comply with the requirements of paragraph (b)(3)(ii) or (iii).

(i) The uncontrolled HCl and Cl₂ emissions, including HCl generated from the combustion of halogenated process vent emissions, from the sum of all process vents within a process shall not exceed 6.8 Mg/yr.

(ii) HCl and Cl₂ emissions, including HCl generated from combustion of halogenated process vent emissions, from the sum of all process vents within a process shall be reduced by 99 percent or greater to an outlet concentration less than or equal to 20 ppmv.

(iii) If HCl and Cl₂ emissions, including HCl generated from combustion of halogenated process vent emissions, from the sum of all process vents within a process are greater than 191 Mg/yr, these HCl and Cl₂ emissions shall be reduced by 99 percent or greater or to an outlet concentration less than or equal to 20 ppmv.

(4) Organic HAP emissions from new sources. For each process, the owner or operator of a new source shall comply with the requirements of either paragraph (b)(4)(i) or (ii) of this section.

(i) The uncontrolled organic HAP emissions shall not exceed 0.15 Mg/yr from the sum of all process vents within a process.

(ii) The uncontrolled organic HAP emissions from the sum of all process vents within a process at a new affected source that are not controlled according to any of the requirements of paragraphs (b)(4)(i), (b)(4)(ii), or (b)(6) of this section shall be reduced by 98 percent or greater.

(A) To outlet concentrations less than or equal to 20 ppmv as TOC; or

(B) By a flare that meets the requirements of §63.11(b); or

(C) By a control device specified in §63.1365(a)(4).

(5) HCl and Cl₂ emissions from new sources. For each process, the owner or operator of a new source shall comply with the requirements of either paragraph (b)(5)(i), (ii), or (iii).

(i) The uncontrolled HCl and Cl₂ emissions, including HCl generated from combustion of halogenated process vent emissions, from the sum of all process vents within a process shall not exceed 6.8 Mg/yr.

(ii) If HCl and Cl₂ emissions, including HCl generated from combustion of halogenated process vent emissions, from the sum of all process vents within a process are greater than or equal to 6.8 Mg/yr and less than 191 Mg/yr, these HCl and Cl₂ emissions shall be reduced by 94 percent or to an outlet concentration less than or equal to 20 ppmv.

(iii) If HCl and Cl₂ emissions, including HCl generated from combustion of halogenated process vent emissions, from the sum of all process vents within a process are greater than 191 Mg/yr, these HCl and Cl₂ emissions shall be reduced by 99 percent or greater or to an outlet concentration less than or equal to 20 ppmv.

(6) Alternative standard. As an alternative to the provisions in paragraphs (b)(2) through (5) of this section, the owner or operator may route emissions from a process vent to a control device or series of control devices achieving an outlet TOC concentration, as calibrated on methane or the predominant HAP, of 20 ppmv or less, and an outlet concentration of HCl and Cl₂ of 20 ppmv.
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or less. Any process vents within a process that are not routed to such a control device or series of control devices must be controlled in accordance with the provisions of paragraphs (b)(2)(ii), (b)(2)(iii), (b)(2)(iv), (b)(3)(ii), (b)(3)(iii), (b)(4)(ii), (b)(5)(ii), or (b)(5)(iii) of this section, as applicable.

(c) Storage vessels. (1) The owner or operator shall either determine the group status of a storage vessel or designate it as a Group 1 storage vessel. If the owner or operator elects to designate the storage vessel as a Group 1 storage vessel, the owner or operator is not required to determine the maximum true vapor pressure of the material stored in the storage vessel.

(2) Standard for existing sources. Except as specified in paragraphs (c) (4) and (5) of this section, the owner or operator of a Group 1 storage vessel at an existing affected source, as defined in § 63.1361, shall equip the affected storage vessel with one of the following:

(i) A fixed roof and internal floating roof, or

(ii) An external floating roof, or

(iii) An external floating roof converted to an internal floating roof, or

(iv) A closed vent system meeting the conditions of paragraph (k) of this section and a control device that meets any of the following conditions:

(A) Reduces organic HAP emissions by 95 percent by weight or greater; or

(B) Reduces organic HAP emissions to outlet concentrations of 20 ppmv or less as TOC; or

(C) Is a flare that meets the requirements of § 63.11(b); or

(D) Is a control device specified in § 63.1365(a)(4).

(3) Standard for new sources. Except as specified in paragraphs (c)(4) and (5) of this section, the owner or operator of a Group 1 storage vessel at a new source, as defined in § 63.1361, shall equip the affected storage vessel in accordance with any one of paragraphs (c)(2)(i) through (iv) of this section.

(4) Alternative standard. As an alternative to the provisions in paragraphs (c)(2) and (3) of this section, the owner or operator of an existing or new affected source may route emissions from storage vessels to a control device or series of control devices achieving an outlet TOC concentration, as calibrated on methane or the predominant HAP, of 20 ppmv or less, and an outlet concentration of hydrogen chloride and chlorine of 20 ppmv or less.

(5) Planned routine maintenance. The owner or operator is exempt from the specifications in paragraphs (c)(2) through (4) of this section during periods of planned routine maintenance of the control device that do not exceed 240 hr/yr.

(6) Compliance with the provisions of paragraphs (c)(2) and (3) of this section is demonstrated using the initial compliance procedures in § 63.1365(d) and the monitoring requirements in § 63.1366. Compliance with the outlet concentrations in paragraph (c)(4) of this section shall be determined by the initial compliance provisions in § 63.1365(a)(5) and the continuous emission monitoring requirements of § 63.1366(b)(5).

(d) Wastewater. The owner or operator of each affected source shall comply with the requirements of §§ 63.131 through 63.147 of subpart G of this part, with the differences noted in paragraphs (d)(1) through (13) of this section for the purposes of this subpart.

(1) When the determination of equivalence criteria in § 63.102(b) is referred to in §§ 63.132, 63.133, and 63.137 of subpart G of this part, the provisions in § 63.6(g) of subpart A of this part shall apply.

(2) When the storage tank requirements contained in §§ 63.119 through 63.123 of subpart G of this part are referred to in §§ 63.132 through 63.148 of subpart G of this part, §§ 63.119 through 63.123 of subpart G of this part are applicable, with the exception of the differences noted in paragraphs (d)(2)(i) through (v) of this section.

(i) When the term ‘‘storage vessel’’ is used in §§ 63.119 through 63.123 of subpart G of this part, the definition of the term ‘‘storage vessel’’ in § 63.1361 shall apply for the purposes of this subpart.

(ii) When December 31, 1992, is referred to in § 63.119 of subpart G of this part, November 10, 1997 shall apply for the purposes of this subpart.

(iii) When April 22, 1994 is referred to in § 63.119 of subpart G of this part, June 23, 1999 shall apply for the purposes of this subpart.
iv) When the phrase “the compliance date specified in §63.100 of subpart F of this part” is referred to in §63.120 of subpart G of this part, the phrase “the compliance date specified in §63.1364” shall apply for the purposes of this subpart.

v) When the phrase “the maximum true vapor pressure of the total organic HAP in the stored liquid falls below the values defining Group 1 storage vessels specified in Table 5 or Table 6 of this subpart” is referred to in §63.120(b)(1)(iv) of subpart G of this part, the phrase, “the maximum true vapor pressure of the total organic HAP in the stored liquid falls below the values defining Group 1 storage vessels specified in §63.1361” shall apply for the purposes of this subpart.

3) To request approval to monitor alternative parameters, as referred to in §63.146(a) of subpart G of this part, the owner or operator shall comply with the procedures in §63.8(f) of subpart A of this part, as referred to in §63.1366(b)(4), instead of the procedures in §63.151(f) or (g) of subpart G of this part.

4) When the Notification of Compliance Status report requirements contained in §63.152(b) of subpart G of this part are referred to in §63.146 of subpart G of this part, the Notification of Compliance Status report requirements in §63.1368(f) shall apply for the purposes of this subpart.

5) When the recordkeeping requirements contained in §63.152(f) of subpart G of this part are referred to in §63.147(d) of subpart G of this part, the recordkeeping requirements in §63.1367 shall apply for the purposes of this subpart.

6) When the Periodic report requirements contained in §63.152(c) of subpart G of this part are referred to in §63.146 and §63.147 of subpart G of this part, the Periodic report requirements contained in §63.1368(g) shall apply for the purposes of this subpart.

7) When the term “process wastewater” is referred to in §§63.132 through 63.147 of subpart G of this part, the term “wastewater” as defined in §63.1361 shall apply for the purposes of this subpart.

8) When the term “Group 1 wastewater stream” is used in §§63.132 through 63.147 of subpart G of this part, the definition of the term “Group 1 wastewater stream” in §63.1361 shall apply for both new sources and existing sources for the purposes of this subpart.

9) The requirements in §§63.132 through 63.147 for compounds listed on Table 8 of subpart G of this part shall not apply for the purposes of this subpart.

10) When the total load of Table 9 compounds in the sum of all process wastewater from PAI process units at a new affected source is 2,100 Mg/yr (2,300 tons/yr) or more, the owner or operator shall reduce, by removal or destruction, the mass flow rate of all compounds in Table 9 of subpart G of this part in all wastewater (process and maintenance wastewater) by 99 percent or more. Alternatively, the owner or operator may treat the wastewater in a unit identified in and complying with §63.138(h) of subpart G of this part. The removal/destruction efficiency shall be determined by the procedures specified in §63.145(c) of subpart G of this part, for noncombustion processes, or §63.145(d) of subpart G of this part, for combustion processes.

11) The compliance date for the affected source subject to the provisions of this section is specified in §63.1364.

12) The option in §63.139 of subpart G of this part to reduce emissions from a control device to an outlet HAP concentration of 20 ppmv shall not apply for the purposes of this subpart.

13) The requirement to correct outlet concentrations from combustion devices to 3 percent oxygen in §63.139(c)(1)(ii) of subpart H of this part shall apply only if supplemental gases are combined with affected vent streams. If emissions are controlled with a vapor recovery system as specified in §63.139(c)(2) of subpart H of this part, the owner or operator must correct for supplemental gases as specified in §63.1365(a)(7)(ii).

14) If wastewater is sent offsite for biological treatment, the waste management units up to the activated sludge unit must be covered, or the owner or operator must demonstrate that less than 5 percent of the total HAP on list 1 in §63.145(h) of subpart H...
of this part is emitted from these units.

(e) Bag dumps and product dryers. (1) The owner or operator shall reduce particulate matter emissions to a concentration not to exceed 0.01 gr/dscf from product dryers that dry a PAI or integral intermediate that is a HAP.

(2) The owner or operator shall reduce particulate matter emissions to a concentration not to exceed 0.01 gr/dscf from bag dumps that introduce to a PAI process unit a feedstock that is a solid material and a HAP, excluding bag dumps where the feedstock contains HAP only as impurities.

(3) Gaseous HAP emissions from product dryers and bag dumps shall be controlled in accordance with the provisions for process vent emissions in paragraph (b) of this section.

(f) Heat exchange systems. Unless one or more of the conditions specified in §63.104(a)(1) through (6) of subpart F of this part are met, an owner or operator shall monitor each heat exchange system that is used to cool process equipment in PAI process units that are part of an affected source as defined in §63.1360(a) according to the provisions in either §63.104(b) or (c) of subpart F of this part. When the term “chemical manufacturing process unit” is used in §63.104(c) of subpart F of this part, the term “PAI process unit” shall apply for the purposes of this subpart. Whenever a leak is detected, the owner or operator shall comply with the requirements in §63.104(d) of subpart F of this part. Delay of repair of heat exchange systems for which leaks have been detected is allowed in accordance with the provisions of §63.104(e) of subpart F of this part.

(g) Pollution prevention alternative. Except as provided in paragraph (g)(1) of this section, for a process that has an initial startup before November 10, 1997, an owner or operator may choose to meet the pollution prevention alternative requirement specified in either paragraph (g)(2) or (3) of this section for any PAI process unit, in lieu of the requirements specified in paragraphs (b), (c), (d), and (e) of this section and in §63.1363. Compliance with the requirements of paragraphs (g)(2) and (3) of this section shall be demonstrated through the procedures in §§63.1365(g) and 63.1366(f).

(1) A HAP must be controlled according to the requirements of paragraphs (b), (c), (d), and (e) of this section and §63.1363 if it is generated in the PAI process unit or an associated control device and it is not part of the production-indexed HAP consumption factor (HAP factor).

(2) The HAP factor shall be reduced by at least 85 percent from a 3-year average baseline beginning no earlier than the 1987 through 1989 calendar years. Alternatively, for a process that has been operating for less than 3 years but more than 1 year, the baseline factor may be calculated for the time period from startup of the process until the present. For any reduction in the HAP factor achieved by reducing a HAP that is also a VOC, an equivalent reduction in the production-indexed VOC consumption factor (VOC factor) is also required (the equivalence is determined on a mass basis, not a percentage basis). For any reduction in the HAP factor that is achieved by reducing a HAP that is not a VOC, the VOC factor may not be increased.

(3) As an alternative to the provisions in paragraph (g)(2) of this section, the owner or operator may combine pollution prevention with emissions control as specified in paragraphs (g)(3)(i) and (ii) of this section.

(i) The HAP factor shall be reduced as specified in paragraph (g)(2) of this section except that a reduction of at least 50 percent shall apply for the purposes of this paragraph.

(ii) The total annual HAP emissions from the PAI process unit shall be reduced by an amount that, when divided by the annual production rate and added to the reduction of the HAP factor yields a value of at least 85 percent of the baseline HAP factor. The total annual VOC emissions from the process unit must be reduced by an amount equivalent to the reduction in HAP emissions for each HAP that is a VOC (the equivalence is determined on a mass basis). For HAP emissions reductions that are achieved by reducing a HAP that is not a VOC, the total annual VOC emissions may not be increased. The reduction in HAP air
emissions must be achieved using one of the following control devices:

(A) Combustion control devices such as incinerators, flares, or process heaters.

(B) Control devices such as condensers and carbon adsorbers whose recovered product is destroyed or shipped offsite for destruction.

(C) Any control device that does not ultimately allow for recycling of material back to the PAI process unit.

(D) Any control device for which the owner or operator can demonstrate that the use of the device in controlling HAP emissions will have no effect on the HAP factor for the PAI process unit.

(h) Emissions averaging provisions. Except as provided in paragraphs (h)(1) through (7) of this section, the owner or operator of an existing affected facility may choose to comply with the emission standards in paragraphs (b), (c), and (d) of this section by using emissions averaging procedures specified in §63.1365(h) for organic HAP emissions from any storage vessel, process, or waste management unit that is part of an affected source subject to this subpart.

(i) A State may restrict the owner or operator of an existing source to use only the procedures in paragraphs (b), (c), and (d) of this section to comply with the emission standards where State authorities prohibit averaging of HAP emissions.

(2) Emission points that are controlled as specified in paragraphs (h)(2)(i) through (iii) may not be used to calculate emissions averaging credits, unless a nominal efficiency has been assigned according to the procedures in §63.133(h) of subpart G of this part. The nominal efficiency must exceed the percent reduction required by paragraphs (b) and (c) of this section for process vents and storage vessels, respectively, and exceed the percent reduction required in §63.138(e) or (f) of subpart G of this part for wastewater streams.

(i) Group 1 storage vessels controlled with an internal floating roof meeting the specifications of §63.119(b) of subpart G of this part, an external floating roof meeting the specifications of §63.119(c) of subpart G of this part, or an external floating roof converted to an internal floating meeting the specifications of §63.119(d) of subpart G of this part.

(ii) Emission points controlled with a flare.

(iii) Wastewater controlled as specified in paragraphs (h)(2)(iii)(A) or (B) of this section.

(A) With controls specified in §63.133 through §63.137 of subpart G of this part;

(B) With a steam stripper meeting the specifications of §63.138(d) of subpart G of this part.

(3) Process vents and storage vessels controlled with a control device to an outlet concentration of 20 ppmv and wastewater streams controlled in a treatment unit to an outlet concentration of 50 ppmv may not be used in any averaging group.

(4) Maintenance wastewater streams and wastewater streams treated in biological treatment units may not be included in any averaging group.

(5) Processes which have been permanently shut down and storage vessels permanently taken out of HAP service may not be included in any averaging group.

(6) Emission points already controlled on or before November 15, 1990 may not be used to generate emissions averaging credits, unless the level of control has been increased after November 15, 1990. In these cases, credit will be allowed only for the increase in control after November 15, 1990.

(7) Emission points controlled to comply with a State or Federal rule other than this subpart may not be included in any emissions averaging group, unless the level of control has been increased above what is required by the other State or Federal rule. Only the control above what is required by the other State or Federal rule will be credited. However, if an emission point has been used to generate emissions averaging credit in an approved emissions average, and the point is subsequently made subject to a State or Federal rule other than this subpart, the point can continue to generate emissions averaging credit for the purpose of complying with the previously approved average.
(i) Opening of a safety device. Opening of a safety device, as defined in §63.1361, is allowed at any time conditions require it to avoid unsafe conditions.

(j) Closed-vent systems. The owner or operator of a closed-vent system that contains bypass lines that could divert a vent stream away from a control device used to comply with the requirements in paragraphs (b) through (d) of this section shall comply with the requirements of Table 3 of this subpart and paragraph (j)(1) or (2) of this section. Equipment such as low leg drains, high point bleeds, analyzer vents, open-ended valves or lines, rupture disks and pressure relief valves needed for safety purposes are not subject to this paragraph.

(1) Install, calibrate, maintain, and operate a flow indicator that determines whether vent stream flow is present at least once every 15 minutes. Records shall be maintained as specified in §63.1367(f)(1). The flow indicator shall be installed at the entrance to any bypass line that could divert the vent stream away from the control device to the atmosphere; or

(2) Secure the bypass line valve in the closed position with a car seal or lock and key type configuration. A visual inspection of the seal or closure mechanism shall be performed at least once every month to ensure that the valve is maintained in the closed position and the vent stream is not diverted through the bypass line. Records shall be maintained as specified in §63.1367(f)(2).

(k) Control requirements for certain liquid streams in open systems within a PAI process unit. (1) The owner or operator shall comply with the provisions of Table 4 of this subpart, for each item of equipment meeting all the criteria specified in paragraphs (k)(2) through (4) of this section and either paragraph (k)(5)(i) or (ii) of this section.

(2) The item of equipment is of a type identified in Table 4 of this subpart;

(3) The item of equipment is part of a PAI process unit as defined in §63.1361;

(4) The item of equipment is controlled less stringently than in Table 4 of this subpart, and the item of equipment is not otherwise exempt from controls by the provisions of this subpart or subpart A of this part;

(5) The item of equipment:

(i) Is a drain, drain hub, manhole, lift station, trench, pipe, or oil/water separator that conveys water with a total annual average concentration greater than or equal to 10,000 ppm by weight of compounds in Table 9 of subpart G of this part at any flowrate; or a total annual average concentration greater than or equal to 1,000 ppm by weight of compounds in Table 9 of subpart G of this part at an annual average flow rate greater than or equal to 10 liters per minute; or

(ii) Is a tank that receives one or more streams that contain water with a total annual average concentration greater than or equal to 1,000 ppm by weight at an annual average flow rate greater than or equal to 10 liters per minute. The owner or operator of the source shall determine the characteristics of the stream as specified in paragraphs (k)(5)(ii)(A) and (B) of this section.

(A) The characteristics of the stream being received shall be determined at the inlet to the tank.

(B) The characteristics shall be determined according to the procedures in §63.144(b) and (c) of subpart G of this part.

(l) Exemption for RCRA treatment units. An owner or operator shall be exempt from the initial compliance demonstrations and monitoring provisions in §§63.1365 and 63.1366 and the associated recordkeeping and reporting requirements in §§63.1367 and 63.1368 for emissions from process vents, storage vessels, and waste management units that are discharged to the following devices:

(1) A boiler or process heater burning hazardous waste for which the owner or operator:

(i) Has been issued a final permit under 40 CFR part 270 and complies with the requirements of 40 CFR part 266, subpart H; or

(ii) Has certified compliance with the interim status requirements of 40 CFR part 266, subpart H.

(2) A hazardous waste incinerator for which the owner or operator has been issued a final permit under 40 CFR part
and complies with the requirements of 40 CFR part 264, subpart O, or has certified compliance with the interim status requirements of 40 CFR part 265, subpart O.

§ 63.1363 Standards for equipment leaks.

(a) General equipment leak requirements. (1) The provisions of this section apply to "equipment" as defined in § 63.1361 and any closed-vent systems and control devices required by this subpart.

(2) Consistency with other regulations. After the compliance date for a process, equipment subject to both this section and either of the following will be required to comply only with the provisions of this subpart:

(i) 40 CFR part 60.

(ii) 40 CFR part 61.

(3) [Reserved]

(4) The provisions in § 63.1(a)(3) of subpart A of this part do not alter the provisions in paragraph (a)(2) of this section.

(5) Lines and equipment not containing process fluids are not subject to the provisions of this section. Utilities, and other non-process lines, such as heating and cooling systems which do not combine their materials with those in the processes they serve, are not considered to be part of a process.

(6) The provisions of this section do not apply to bench-scale processes, regardless of whether the processes are located at the same plant site as a process subject to the provisions of this subpart MMM.

(7) Each piece of equipment to which this section applies shall be identified such that it can be distinguished readily from equipment that is not subject to this section. Identification of the equipment does not require physical tagging of the equipment. For example, the equipment may be identified on a plant site plan, in log entries, or by designation of process boundaries by some form of weatherproof identification. If changes are made to the affected source subject to the leak detection requirements, equipment identification for each type of component shall be updated, if needed, within 15 calendar days of the end of each monitoring period for that component.

(b) References. The owner or operator shall comply with the provisions of subpart H of this part as specified in paragraphs (b)(1) through (3) of this section. When the term "process unit" is used in subpart H of this part, it shall mean any group of processes for the purposes of this subpart. Groups of processes as used in this subpart may be any individual process or combination of processes.

(1) Sections 63.160, 63.161, 63.162, 63.163, 63.166, 63.168, 63.170, 63.173, 63.175, 63.176, 63.181, and 63.182 of subpart H of this part shall not apply for the purposes of this subpart MMM. The owner or operator shall comply with the provisions specified in paragraphs (b)(1)(i) through (vii) of this section.

(i) Sections 63.160 and 63.162 of subpart H of this part shall not apply, instead the owner or operator shall comply with paragraph (a) of this section.

(ii) Section 63.161 of subpart H of this part shall not apply, instead the owner or operator shall comply with § 63.1361;
(iii) Sections 63.163 and 63.173 of subpart H of this part shall not apply, instead the owner or operator shall comply with paragraph (c) of this section;

(iv) Section 63.167 of subpart H of this part shall not apply, instead the owner or operator shall comply with paragraph (d) of this section;

(v) Section 63.168 of subpart H of this part shall not apply, instead the owner or operator shall comply with paragraph (e) of this section;

(vi) Section 63.170 of subpart H of this part shall not apply, instead the owner or operator shall comply with §63.1362(b);

(vii) Section 63.181 of subpart H of this part shall not apply, instead the owner or operator shall comply with paragraph (f) of this section.

(2) The owner or operator shall comply with §§63.164, 63.165, 63.166, 63.169, 63.177, and 63.179 of subpart H of this part in their entirety, except that when these sections reference other sections of subpart H of this part, the owner or operator shall comply with the revised sections as specified in paragraphs (b)(1) and (3) of this section. Section 63.164 of subpart H of this part applies to compressors. Section 63.165 of subpart H of this part applies to pressure relief devices in gas/vapor service. Section 63.166 of subpart H of this part applies to sampling connection systems. Section 63.169 of subpart H of this part applies to control devices used to comply with §§63.164, 63.165, 63.166, 63.169, 63.177, and 63.179 of subpart H of this part in their entirety, except that when these sections reference other sections of subpart H of this part, the owner or operator shall comply with the revised sections as specified in paragraphs (b)(1) and (3) of this section.

(3) The owner or operator shall comply with §§63.171, 63.172, 63.174, 63.178, and 63.180 of subpart H of this part with the differences specified in paragraphs (b)(3)(i) through (v) of this section.

(i) Section 63.171, Delay of repair, shall apply except §63.171(a) shall not apply. Delay of repair of equipment for which leaks have been detected is allowed if one of the following conditions exist:

(A) The repair is technically infeasible without a process shutdown. Repair of this equipment shall occur by the end of the next scheduled process shutdown.

(B) The owner or operator determines that repair personnel would be exposed to an immediate danger if attempting to repair without a process shutdown. Repair of this equipment shall occur by the end of the next scheduled process shutdown.

(ii) Section 63.172, Closed-vent systems and control devices, shall apply for closed-vent systems used to comply with this section, and for control devices used to comply with this section only, except:

(A) Section 63.172(k) and (I) shall not apply. The owner or operator shall instead comply with paragraph (f) of this section.

(B) Owners or operators may, instead of complying with the provisions of §63.172(f), design a closed-vent system to operate at a pressure below atmospheric pressure. The system shall be equipped with at least one pressure gauge or other pressure measurement device that can be read from a readily accessible location to verify that negative pressure is being maintained in the closed-vent system when the associated control device is operating.

(iii) Section 63.174, Connectors, shall apply except:

(A) Section 63.174(f) and (g) shall not apply. Instead of §63.174(f) and (g), the owner or operator shall comply with paragraph (f) of this section.

(B) Days that the connectors are not in organic HAP service shall not be considered part of the 3-month period in §63.174(e).

(C) Section 63.174(b)(3)(ii) of subpart H of this part shall not apply. Instead, if the percent leaking connectors in the group of process units was less than 0.5 percent, but equal to or greater than 0.25 percent, during the last required monitoring period, monitoring shall be performed once every 4 years. An owner or operator may comply with the requirements of this paragraph by monitoring at least 40 percent of the connectors in the first 2 years and the
remainder of the connectors within the next 2 years. The percent leaking connectors will be calculated for the total of all monitoring performed during the 4-year period.

(D) Section 63.174(b)(3)(iv) of subpart H of this part shall not apply. Instead, the owner or operator shall increase the monitoring frequency to once every 2 years for the next monitoring period if leaking connectors comprise at least 0.5 percent but less than 1.0 percent of the connectors monitored within the 4 years specified in paragraph (b)(3)(iii)(C) of this section, or the first 4 years specified in §63.174(b)(3)(iii) of subpart H of this part. At the end of that 2-year monitoring period, the owner or operator shall monitor once per year while the percent leaking connectors is greater than or equal to 0.5 percent; if the percent leaking connectors is less than 0.5 percent, the owner or operator may return to monitoring once every 4 years or may monitor in accordance with §63.174(b)(3)(iii) of subpart H of this part, if appropriate.

(E) Section 63.174(b)(3)(v) of subpart H of this part shall not apply. Instead, if an owner or operator complying with the requirements of paragraph (b)(3)(iii)(C) and (D) of this section or §63.174(b)(3)(iii) of subpart H of this part for a group of process units determines that 1 percent or greater of the connectors are leaking, the owner or operator shall increase the monitoring frequency to one time per year. The owner or operator may again elect to use the provisions of paragraphs (b)(3)(iii)(C) or (D) of this section after a monitoring period in which less than 0.5 percent of the connectors are determined to be leaking.

(F) Section 63.174(b)(3)(iii) of subpart H of this part shall not apply. Instead, monitoring shall be required once every 8 years, if the percent leaking connectors in the group of process units was less than 0.25 percent during the last required monitoring period. An owner or operator shall monitor at least 50 percent of the connectors in the first 4 years and the remainder of the connectors within the next 4 years. If the percent leaking connectors in the first 4 years is equal to or greater than 0.35 percent, the monitoring program shall revert at that time to the appropriate monitoring frequency specified in paragraphs (b)(3)(iii)(C), (D), or (E) of this section.

(iv) Section 63.178 of subpart H of this part, Alternative means of emission limitation: Batch processes, shall apply except that §63.178(b) of subpart H of this part, requirements for pressure testing, shall apply to all processes, not just batch processes;

(v) Section 63.180 of subpart H of this part, Test methods and procedures, shall apply except §63.180(b)(4)(ii)(A) through (C) of subpart H of this part shall not apply. Calibration gases shall be a mixture of methane and air at a concentration of approximately, but less than, 10,000 parts per million methane for agitators, 2,000 parts per million for pumps, and 500 parts per million for all other equipment, except as provided in §63.180(b)(4)(iii) of subpart H of this part.

(c) standards for pumps in light liquid service and agitators in gas/vapor service and in light liquid service. (1) The provisions of this section apply to each pump that is in light liquid service, and to each agitator in gas/vapor service or in light liquid service.

(2)(i) Monitoring. Each pump and agitator subject to this section shall be monitored quarterly to detect leaks by the method specified in §63.180(b) of subpart H of this part, except as provided in §63.177 of subpart H of this part, paragraph (f) of this section, and paragraphs (c)(5) through (c)(9) of this section.

(ii) Leak definition. The instrument reading, as determined by the method as specified in §63.180(b) of subpart H of this part, that defines a leak is:

(A) For agitators, an instrument reading of 10,000 parts per million or greater.

(B) For pumps, an instrument reading of 2,000 parts per million or greater.

(iii) Visual inspections. Each pump and agitator shall be checked by visual inspection each calendar week for indications of liquids dripping from the pump or agitator seal. If there are indications of liquids dripping from the seal, a leak is detected.

(3) Repair provisions. (i) When a leak is detected, it shall be repaired as soon as practicable, but not later than 15
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calendar days after it is detected, except as provided in paragraph (b)(3)(i) of this section.

(ii) A first attempt at repair shall be made no later than 5 calendar days after the leak is detected. First attempts at repair include, but are not limited to, the following practices where practicable:

(A) Tightening of packing gland nuts.

(B) Ensuring that the seal flush is operating at design pressure and temperature.

(4) Calculation of percent leakers. (i) The owner or operator shall decide no later than the end of the first monitoring period what groups of processes will be developed. Once the owner or operator has decided, all subsequent percent calculations shall be made on the same basis.

(ii) If, calculated on a 1 year rolling average, the greater of either 10 percent or three of the pumps in a group of processes leak, the owner or operator shall monitor each pump once per month.

(iii) The number of pumps in a group of processes shall be the sum of all the pumps in organic HAP service, except that pumps found leaking in a continuous process within 1 quarter after startup of the pump shall not count in the percent leaking pumps calculation for that one monitoring period only.

(iv) Percent leaking pumps shall be determined using Equation 3 of this subpart:

\[
\%P_L = \left(\frac{P_L - P_S}{P_T - P_S}\right) \times 100 \quad \text{(Eq. 3)}
\]

where:

\(\%P_L\) = percent leaking pumps

\(P_L\) = number of pumps found leaking as determined through quarterly monitoring as required in paragraphs (c)(2)(i) and (ii) of this section.

\(P_T\) = total pumps in organic HAP service, including those meeting the criteria in paragraphs (c)(5) and (6) of this section.

\(P_S\) = number of pumps in a continuous process leaking within 1 quarter of startup during the current monitoring period.

(5) Exemptions. Each pump or agitator equipped with a dual mechanical seal system that includes a barrier fluid system is exempt from the requirements of paragraphs (c)(1) through (c)(4)(iii) of this section, provided the following requirements are met:

(i) Each dual mechanical seal system is:

(A) Operated with the barrier fluid at a pressure that is at all times greater than the pump/agitator stuffing box pressure; or

(B) Equipped with a barrier fluid degassing reservoir that is connected by a closed-vent system to a control device that complies with the requirements of paragraph (b)(3)(ii) of this section; or

(C) Equipped with a closed-loop system that purges the barrier fluid into a process stream.

(ii) The barrier fluid is not in light liquid service.

(iii) Each barrier fluid system is equipped with a sensor that will detect failure of the seal system, the barrier fluid system, or both.

(iv) Each pump/agitator is checked by visual inspection each calendar week for indications of liquids dripping from the pump/agitator seal.

(A) If there are indications of liquids dripping from the pump/agitator seal at the time of the weekly inspection, the pump/agitator shall be monitored as specified in §63.180(b) of subpart H of this part to determine if there is a leak of organic HAP in the barrier fluid.

(B) If an instrument reading of 2,000 parts per million or greater is measured for pumps, or 10,000 parts per million or greater is measured for agitators, a leak is detected.

(v) Each sensor as described in paragraph (c)(5)(iii) of this section is observed daily or is equipped with an alarm unless the pump is located within the boundary of an unmanned plant site.

(vi)(A) The owner or operator determines, based on design considerations and operating experience, criteria applicable to the presence and frequency of drips and to the sensor that indicate
failure of the seal system, the barrier fluid system, or both.

(B) If indications of liquids dripping from the pump/agitator seal exceed the criteria established in paragraph (c)(5)(vi)(A) of this section, or if, based on the criteria established in paragraph (c)(5)(vi)(A) of this section, the sensor indicates failure of the seal system, the barrier fluid system, or both, a leak is detected.

(C) When a leak is detected, it shall be repaired as soon as practicable, but not later than 15 calendar days after it is detected, except as provided in paragraph (b)(3)(i) of this section.

(D) A first attempt at repair shall be made no later than 5 calendar days after each leak is detected.

(6) Any pump/agitator that is designed with no externally actuated shaft penetrating the pump/agitator housing is exempt from the requirements of paragraphs (c)(1) through (4) of this section, except for the requirements of paragraph (c)(2)(iii) of this section and, for pumps, paragraph (c)(4)(iv) of this section.

(7) Any pump/agitator equipped with a closed-vent system capable of capturing and transporting any leakage from the seal or seals back to the process or to a control device that complies with the requirements of paragraph (b)(3)(ii) of this section is exempt from the requirements of paragraphs (c)(2) through (5) of this section.

(8) Any pump/agitator that is located within the boundary of an unmanned plant site is exempt from the weekly visual inspection requirement of paragraphs (c)(2)(iii) and (c)(5)(iv) of this section, and the daily requirements of paragraph (c)(5)(v) of this section, provided that each pump/agitator is visually inspected as often as practicable and at least monthly.

(9) If more than 90 percent of the pumps in a group of processes meet the criteria in either paragraph (c)(5) or (6) of this section, the process is exempt from the requirements of paragraph (c)(4) of this section.

(d) Standards: open-ended valves or lines. (1)(i) Each open-ended valve or line shall be equipped with a cap, blind flange, plug, or a second valve, except as provided in §63.177 of subpart H of this part and paragraphs (d)(4) through (6) of this section.

(ii) The cap, blind flange, plug, or second valve shall seal the open end at all times except during operations requiring process fluid flow through the open-ended valve or line, or during maintenance or repair. The cap, blind flange, plug, or second valve shall be in place within 1 hour of cessation of operations requiring process fluid flow through the open-ended valve or line, or within 1 hour of cessation of maintenance or repair.

(2) Each open-ended valve or line equipped with a second valve shall be operated in a manner such that the valve on the process fluid end is closed before the second valve is closed.

(3) When a double block and bleed system is being used, the bleed valve or line may remain open during operations that require venting the line between the block valves but shall comply with paragraph (d)(1) of this section at all other times.

(4) Open-ended valves or lines in an emergency shutdown system which are designed to open automatically in the event of a process upset are exempt from the requirements of paragraphs (d)(1) through (3) of this section.

(5) Open-ended valves or lines containing materials which would autocatalytically polymerize are exempt from the requirements of paragraphs (d)(1) through (3) of this section.

(6) Open-ended valves or lines containing materials which could cause an explosion, serious overpressure, or other safety hazard if capped or equipped with a double block and bleed system as specified in paragraphs (d)(1) through (3) of this section are exempt from the requirements of paragraphs (d)(1) through (3) of this section.

(e) Standards: valves in gas/vapor service and in light liquid service.

(1) The provisions of this section apply to valves that are either in gas/vapor service or in light liquid service.

(2) For existing and new affected sources, all valves subject to this section shall be monitored, except as provided in paragraph (f) of this section and in §63.177 of subpart H of this part, by no later than 1 year after the compliance date.
(3) Monitoring. The owner or operator of a source subject to this section shall monitor all valves, except as provided in paragraph (f) of this section and in §63.177 of subpart H of this part, at the intervals specified in paragraph (e)(4) of this section and shall comply with all other provisions of this section, except as provided in paragraph (b)(3)(i) of this section and §§63.178 and 63.179 of subpart H of this part.

(i) The valves shall be monitored to detect leaks by the method specified in §63.180(b) of subpart H of this part.

(ii) An instrument reading of 500 parts per million or greater defines a leak.

(4) Subsequent monitoring frequencies. After conducting the initial survey required in paragraph (e)(2) of this section, the owner or operator shall monitor valves for leaks at the intervals specified below:

(i) For a group of processes with 2 percent or greater leaking valves, calculated according to paragraph (e)(6) of this section, the owner or operator shall monitor each valve once per month, except as specified in paragraph (e)(9) of this section.

(ii) For a group of processes with less than 2 percent leaking valves, the owner or operator shall monitor each valve once each quarter, except as provided in paragraphs (e)(4)(iii) through (v) of this section.

(iii) For a group of processes with less than 1 percent leaking valves, the owner or operator may elect to monitor each valve once every 2 quarters.

(iv) For a group of processes with less than 0.5 percent leaking valves, the owner or operator may elect to monitor each valve once every 4 quarters.

(v) For a group of processes with less than 0.25 percent leaking valves, the owner or operator may elect to monitor each valve once every 2 years.

(5) Calculation of percent leakers. For a group of processes to which this subpart applies, the owner or operator may choose to subdivide the valves in the applicable group of processes and apply the provisions of paragraph (e)(4) of this section to each subgroup. If the owner or operator elects to subdivide the valves in the applicable group of processes, then the provisions of paragraphs (e)(5)(i) through (viii) of this section apply.

(i) The overall performance of total valves in the applicable group of processes must be less than 2 percent leaking valves, as detected according to paragraphs (e)(3)(i) and (ii) of this section and as calculated according to paragraphs (e)(6)(ii) and (iii) of this section.

(ii) The initial assignment or subsequent reassignment of valves to subgroups shall be governed by the provisions of paragraphs (e)(5)(ii) (A) through (C) of this section.

(A) The owner or operator shall determine which valves are assigned to each subgroup. Valves with less than 1 year of monitoring data or valves not monitored within the last 12 months must be placed initially into the most frequently monitored subgroup until at least 1 year of monitoring data have been obtained.

(B) Any valve or group of valves can be reassigned from a less frequently monitored subgroup to a more frequently monitored subgroup provided that the valves to be reassigned were monitored during the most recent monitoring period for the less frequently monitored subgroup. The monitoring results must be included with the less frequently monitored subgroup's monitoring event and associated next percent leaking valves calculation for that group.

(C) Any valve or group of valves can be reassigned from a more frequently monitored subgroup to a less frequently monitored subgroup provided that the valves to be reassigned have not leaked for the period of the less frequently monitored subgroup (e.g., for the last 12 months, if the valve or group of valves is to be reassigned to a subgroup being monitored annually). Nonrepairable valves may not be reassigned to a less frequently monitored subgroup.

(iii) The owner or operator shall determine every 6 months if the overall performance of total valves in the applicable group of processes is less than 2 percent leaking valves and so indicate the performance in the next Periodic report. If the overall performance of total valves in the applicable group of processes is 2 percent leaking valves
or greater, the owner or operator shall revert to the program required in paragraphs (e)(2) through (4) of this section. The overall performance of total valves in the applicable group of processes shall be calculated as a weighted average of the percent leaking valves of each subgroup according to Equation 4 of this subpart:

\[
%V_{LO} = \frac{\sum_{i=1}^{n} (\%V_{L,i} \times V_i)}{\sum_{i=1}^{n} V_i} \quad \text{(Eq. 4)}
\]

where:

- \(\%V_{LO}\) = overall performance of total valves in the applicable group of processes
- \(\%V_{L,i}\) = percent leaking valves in subgroup \(i\), most recent value calculated according to the procedures in paragraphs (e)(6)(ii) and (iii) of this section
- \(V_i\) = number of valves in subgroup \(i\)
- \(n\) = number of subgroups

(iv) Records. In addition to records required by paragraph (g) of this section, the owner or operator shall maintain records specified in paragraphs (e)(5)(iv)(A) through (D) of this section.

(A) Which valves are assigned to each subgroup,

(B) Monitoring results and calculations made for each subgroup for each monitoring period,

(C) Which valves are reassigned and when they were reassigned, and

(D) The results of the semiannual overall performance calculation required in paragraph (e)(5)(iii) of this section.

(v) The owner or operator shall notify the Administrator no later than 30 days prior to the beginning of the next monitoring period of the decision to subgroup valves. The notification shall identify the participating processes and the valves assigned to each subgroup.

(vi) Semiannual reports. In addition to the information required by paragraph (h)(3) of this section, the owner or operator shall submit in the Periodic reports the information specified in paragraphs (e)(5)(vi)(A) and (B) of this section.

(A) Valve reassignments occurring during the reporting period, and

(B) Results of the semiannual overall performance calculation required by paragraph (e)(5)(iii) of this section.

(vii) To determine the monitoring frequency for each subgroup, the calculation procedures of paragraph (e)(6)(iii) of this section shall be used.

(viii) Except for the overall performance calculations required by paragraphs (e)(5)(i) and (iii) of this section, each subgroup shall be treated as if it were a process for the purposes of applying the provisions of this section.

(B) Monitoring results and calculations made for each subgroup for each monitoring period.

(i) Percent leaking valves for each group of processes or subgroup shall be determined using Equation 5 of this subpart:

\[
%V_L = \left\lfloor \frac{V_L}{V_T} \right\rfloor \times 100 \quad \text{(Eq. 5)}
\]

Where:

- \(\%V_L\) = percent leaking valves
- \(V_L\) = number of valves found leaking excluding nonrepairables as provided in paragraph (e)(6)(iv)(A) of this section
- \(V_T\) = total valves monitored, in a monitoring period excluding valves monitored as required by paragraph (e)(7)(iii) of this section

(ii) When determining monitoring frequency for each group of processes or subgroup subject to monthly, quarterly, or semiannual monitoring frequencies, the percent leaking valves shall be the arithmetic average of the percent leaking valves from the last two monitoring periods. When determining monitoring frequency for each group of processes or subgroup subject to annual or biennial (once every 2 years) monitoring frequencies, the percent leaking valves shall be the arithmetic average of the percent leaking valves from the last three monitoring periods.

(iv)(A) Nonrepairable valves shall be included in the calculation of percent leaking valves the first time the valve is identified as leaking and nonrepairable and as required to comply with paragraph (e)(6)(iv)(B) of this section.
Otherwise, a number of nonrepairable valves (identified and included in the percent leaking calculation in a previous period) up to a maximum of 1 percent of the total number of valves in organic HAP service at a process may be excluded from calculation of percent leaking valves for subsequent monitoring periods.

(B) If the number of nonrepairable valves exceeds 1 percent of the total number of valves in organic HAP service at a process, the number of nonrepairable valves exceeding 1 percent of the total number of valves in organic HAP service shall be included in the calculation of percent leaking valves.

(7) Repair provisions. (i) When a leak is detected, it shall be repaired as soon as practicable, but no later than 15 calendar days after the leak is detected, except as provided in paragraph (b)(3)(i) of this section.

(ii) A first attempt at repair shall be made no later than 5 calendar days after each leak is detected.

(iii) When a leak is repaired, the valve shall be monitored at least once within the first 3 months after its repair. Days that the valve is not in organic HAP service shall not be considered part of this 3-month period.

(8) First attempts at repair include, but are not limited to, the following practices where practicable:

(i) Tightening of bonnet bolts,

(ii) Replacement of bonnet bolts,

(iii) Tightening of packing gland nuts, and

(iv) Injection of lubricant into lubricated packing.

(9) Any equipment located at a plant site with fewer than 250 valves in organic HAP service in the affected source is exempt from the requirements for monthly monitoring specified in paragraph (e)(4)(i) of this section. Instead, the owner or operator shall monitor each valve in organic HAP service for leaks once each quarter, or comply with paragraphs (e)(4)(ii) through (iv) of this section.

(f) Unsafe to monitor, difficult to monitor, and inaccessible equipment. (1) Equipment that is designated as unsafe to monitor, difficult to monitor, or inaccessible is exempt from the requirements specified in paragraphs (f)(1)(i) through (iv) of this section provided the owner or operator meets the requirements specified in paragraph (f)(2), (3), and (4) of this section, as applicable. Ceramic or ceramic-lined connectors are subject to the same requirements as inaccessible connectors.

(i) For pumps and agitators, paragraphs (c) (2), (3), and (4) of this section do not apply.

(ii) For valves, paragraphs (e)(2) through (7) of this section do not apply.

(iii) For closed-vent systems, §63.172(f)(1), (f)(2), and (g) of subpart H of this part do not apply.

(iv) For connectors, §63.174(b) through (e) of subpart H of this part do not apply.

(2) Equipment that is unsafe to monitor. (i) Equipment may be designated as unsafe to monitor if the owner or operator determines that monitoring personnel would be exposed to an immediate danger as a consequence of complying with the monitoring requirements identified in paragraphs (f)(1)(i) through (iv) of this section.

(ii) The owner or operator of equipment that is designated as unsafe-to-monitor must have a written plan that requires monitoring of the equipment as frequently as practicable during safe-to-monitor times, but not more frequently than the periodic monitoring schedule otherwise applicable.

(3) Equipment that is difficult to monitor. (i) Equipment may be designated as difficult to monitor if the owner or operator determines that the equipment cannot be monitored without elevating the monitoring personnel more than 2 meters above a support surface or the equipment is not accessible at anytime in a safe manner.

(ii) At an existing source, any equipment within a group of processes that meets the criteria of paragraph (f)(3)(i) of this section may be designated as difficult to monitor. At a new affected source, an owner or operator may designate no more than 3 percent of each type of equipment as difficult to monitor.

(iii) The owner or operator of equipment designated as difficult to monitor must follow a written plan that requires monitoring of the equipment at least once per calendar year.
Inaccessible equipment and ceramic or ceramic-lined connectors. (i) A connector, agitator, or valve may be designated as inaccessible if it is:
(A) Buried;
(B) Insulated in a manner that prevents access to the equipment by a monitor probe;
(C) Obstructed by equipment or piping that prevents access to the equipment by a monitor probe;
(D) Unable to be reached from a wheeled scissor-lift or hydraulic-type scaffold which would allow access to equipment up to 7.6 meters above the ground; or
(E) Not able to be accessed at any time in a safe manner to perform monitoring. Unsafe access includes, but is not limited to, the use of a wheeled scissor-lift on unstable or uneven terrain, the use of a motorized man-lift basket in areas where an ignition potential exists, or access would require near proximity to hazards such as electrical lines, or would risk damage to equipment.

(ii) At an existing source, any connector, agitator, or valve that meets the criteria of paragraph (f)(4)(i) of this section may be designated as inaccessible. At a new affected source, an owner or operator may designate no more than 3 percent of each type of equipment as inaccessible.

(iii) If any inaccessible equipment or ceramic or ceramic-lined connector is observed by visual, audible, olfactory, or other means to be leaking, the leak shall be repaired as soon as practicable, but no later than 15 calendar days after the leak is detected, except as provided in paragraph (b)(3)(i) of this section.

(g) Recordkeeping requirements. (1) An owner or operator of more than one group of processes subject to the provisions of this section may comply with the recordkeeping requirements for the groups of processes in one recordkeeping system if the system identifies with each record the program being implemented (e.g., quarterly monitoring) for each type of equipment. All records and information required by this section shall be maintained in a manner that can be readily accessed at the plant site. This could include physically locating the records at the plant site or accessing the records from a central location by computer at the plant site.

(2) General recordkeeping. Except as provided in paragraph (g)(5) of this section, the following information pertaining to all equipment subject to the requirements in this section shall be recorded:

(i)(A) A list of identification numbers for equipment (except instrumentation systems) subject to the requirements of this section. Connectors, except those subject to paragraph (f) of this section, need not be individually identified if all connectors in a designated area or length of pipe subject to the provisions of this section are identified as a group, and the number of subject connectors is indicated. The list for each type of equipment shall be completed no later than the completion of the initial survey required for that component. The list of identification numbers shall be updated, if needed, to incorporate equipment changes within 15 calendar days of the completion of each monitoring survey for the type of equipment component monitored.

(B) A schedule for monitoring connectors subject to the provisions of §63.174(a) of subpart H of this part and valves subject to the provisions of paragraph (e)(4) of this section.

(C) Physical tagging of the equipment is not required to indicate that it is in organic HAP service. Equipment subject to the provisions of this section may be identified on a plant site plan, in log entries, or by other appropriate methods.

(ii)(A) A list of identification numbers for equipment that the owner or operator elects to equip with a closed-vent system and control device, under the provisions of paragraph (c)(7) of this section or §§63.164(h) or 63.165(c) of subpart H of this part.

(B) A list of identification numbers for compressors that the owner or operator elects to designate as operating with an instrument reading of less than 500 parts per million above background, under the provisions of §63.164(i) of subpart H of this part.

(iii)(A) A list of identification numbers for pressure relief devices subject to the provisions in §63.165(a) of subpart H of this part.
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(B) A list of identification numbers for pressure relief devices equipped with rupture disks, under the provisions of §63.165(d) of subpart H of this part.

(iv) Identification of instrumentation systems subject to the provisions of this section. Individual components in an instrumentation system need not be identified.

(v) The following information shall be recorded for each dual mechanical seal system:

(A) Design criteria required by paragraph (c)(5)(vi)(A) of this section and §63.164(e)(2) of subpart H of this part, and an explanation of the design criteria; and

(B) Any changes to these criteria and the reasons for the changes.

(vi) A list of equipment designated as unsafe to monitor, difficult to monitor, or inaccessible under paragraphs (f) or (b)(3)(i)(B) of this section and a copy of the plan for monitoring or inspecting this equipment.

(vii) A list of connectors removed from and added to the process, as described in §63.174(i)(1) of subpart H of this part, and documentation of the integrity of the weld for any removed connectors, as required in §63.174(j) of subpart H of this part. This is not required unless the net credits for removed connectors is expected to be used.

(viii) For batch processes that the owner or operator elects to monitor as provided under §63.178(c) of subpart H of this part, a list of equipment added to batch product processes since the last monitoring period required in §63.178(c)(3)(iii) and (iii) of subpart H of this part. This list must be completed for each type of equipment within 15 calendar days of the completion of the each monitoring survey for the type of equipment monitored.

(3) Records of visual inspections. For visual inspections of equipment subject to the provisions of paragraphs (c)(2)(iii) and (c)(5)(iv) of this section, the owner or operator shall document that the inspection was conducted and the date of the inspection. The owner or operator shall maintain records as specified in paragraph (g)(4) of this section for leaking equipment identified in this inspection, except as provided in paragraph (g)(5) of this section. These records shall be retained for 5 years.

(4) Monitoring records. When each leak is detected as specified in paragraphs (c) and (e) of this section and §§63.164, 63.169, 63.172, and 63.174 of subpart H of this part, the owner or operator shall record the information specified in paragraphs (g)(4)(i) through (ix) of this section. All records shall be retained for 5 years, in accordance with the requirements of §63.10(b)(1) of subpart A of this part.

(i) The instrument and the equipment identification number and the operator name, initials, or identification number.

(ii) The date the leak was detected and the date of first attempt to repair the leak.

(iii) The date of successful repair of the leak.

(iv) If postrepair monitoring is required, maximum instrument reading measured by Method 21 of 40 CFR part 60, appendix A, after it is successfully repaired or determined to be nonrepairable.

(v) “Repair delayed” and the reason for the delay if a leak is not repaired within 15 calendar days after discovery of the leak.

(A) The owner or operator may develop a written procedure that identifies the conditions that justify a delay of repair. The written procedures may be included as part of the startup/shutdown/malfunction plan, required by §63.1367(a), for the source or may be part of a separate document that is maintained at the plant site. Reasons for delay of repair may be documented by citing the relevant sections of the written procedure.

(B) If delay of repair was caused by depletion of stocked parts, there must be documentation that the spare parts were sufficiently stocked onsite before depletion and the reason for depletion.

(vi) If repairs were delayed, dates of process shutdowns that occur while the equipment is unrepaired.

(vii) (A) If the alternative in §63.174(c)(1)(ii) of subpart H of this part is not in use for the monitoring period, identification, either by list, location
(area or grouping), or tagging of connectors disturbed since the last monitoring period required in §63.174(b) of subpart H of this part, as described in §63.174(c)(1) of subpart H of this part.

(B) The date and results of follow-up monitoring as required in §63.174(c) of subpart H of this part. If identification of disturbed connectors is made by location, then all connectors within the designated location shall be monitored.

(viii) The date and results of the monitoring required in §63.178(c)(3)(i) of subpart H of this part for equipment added to a batch process since the last monitoring period required in §63.178(c)(3)(ii) and (iii) of subpart H of this part. If no leaking equipment is found in this monitoring, the owner or operator shall record that the inspection was performed. Records of the actual monitoring results are not required.

(ix) Copies of the periodic reports as specified in paragraph (h)(3) of this section, if records are not maintained on a computerized data base capable of generating summary reports from the records.

(5) Records of pressure tests. The owner or operator who elects to pressure test a process equipment train and supply lines between storage and processing areas to demonstrate compliance with this section is exempt from the requirements of paragraphs (g)(2), (3), (4), and (6) of this section. Instead, the owner or operator shall maintain records of the following information:

(i) The identification of each product, or product code, produced during the calendar year. It is not necessary to identify individual items of equipment in the process equipment train.

(ii) Records demonstrating the proportion of the time during the calendar year the equipment is in use in the process that is subject to the provisions of this subpart. Examples of suitable documentation are records of time in use for individual pieces of equipment or average time in use for the process unit. These records are not required if the owner or operator does not adjust monitoring frequency by the time in use, as provided in §63.178(c)(3)(ii) of subpart H of this part.

(iii) Physical tagging of the equipment to identify that it is in organic HAP service and subject to the provisions of this section is not required. Equipment in a process subject to the provisions of this section may be identified on a plant site plan, in log entries, or by other appropriate methods.

(iv) The dates of each pressure test required in §63.178(b) of subpart H of this part, the test pressure, and the pressure drop observed during the test.

(v) Records of any visible, audible, or olfactory evidence of fluid loss.

(vi) When a process equipment train does not pass two consecutive pressure tests, the following information shall be recorded in a log and kept for 2 years:

(A) The date of each pressure test and the date of each leak repair attempt.

(B) Repair methods applied in each attempt to repair the leak.

(C) The reason for the delay of repair.

(D) The expected date for delivery of the replacement equipment and the actual date of delivery of the replacement equipment.

(E) The date of successful repair.

(6) Records of compressor and pressure relief valve compliance tests. The dates and results of each compliance test required for compressors subject to the provisions in §63.164(i) of subpart H of this part and the dates and results of the monitoring following a pressure release for each pressure relief device subject to the provisions in §63.165(a) and (b) of subpart H of this part. The results shall include:

(i) The background level measured during each compliance test.

(ii) The maximum instrument reading measured at each piece of equipment during each compliance test.

(7) Records for closed-vent systems. The owner or operator shall maintain records of the information specified in paragraphs (g)(7)(i) through (iii) of this section for closed-vent systems and control devices subject to the provisions of paragraph (b)(3)(ii) of this section. The records specified in paragraph (g)(7)(i) of this section shall be retained for the life of the equipment. The records specified in paragraphs (g)(7)(ii) and (iii) of this section shall be retained for 5 years.
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(i) The design specifications and performance demonstrations specified in paragraphs (g)(7)(i)(A) through (D) of this section.

(A) Detailed schematics, design specifications of the control device, and piping and instrumentation diagrams.

(B) The dates and descriptions of any changes in the design specifications.

(C) The flare design (i.e., steam assisted, air assisted, or nonassisted) and the results of the compliance demonstration required by § 63.11(b) of subpart A of this part.

(D) A description of the parameter or parameters monitored, as required in paragraph (b)(3)(ii) of this section, to ensure that control devices are operated and maintained in conformance with their design and an explanation of why that parameter (or parameters) was selected for the monitoring.

(ii) Records of operation of closed-vent systems and control devices.

(A) Dates and durations when the closed-vent systems and control devices required in paragraph (c) of this section and §§ 63.164 through 63.166 of subpart H of this part are not operated as designed as indicated by the monitored parameters, including periods when a flare pilot light system does not have a flame.

(B) Dates and durations during which the monitoring system or monitoring device is inoperative.

(C) Dates and durations of startups and shutdowns of control devices required in paragraph (c) of this section and §§ 63.164 through 63.166 of subpart H of this part.

(iii) Records of inspections of closed-vent systems subject to the provisions of § 63.172 of subpart H of this part.

(A) For each inspection conducted in accordance with the provisions of § 63.172(f)(1) or (2) of subpart H of this part during which no leaks were detected, a record that the inspection was performed, the date of the inspection, and a statement that no leaks were detected.

(B) For each inspection conducted in accordance with the provisions of § 63.172(f)(1) or (f)(2) of subpart H of this part during which leaks were detected, the information specified in paragraph (g)(4) of this section shall be recorded.

(8) Records for components in heavy liquid service. Information, data, and analysis used to determine that a piece of equipment or process is in heavy liquid service shall be recorded. Such a determination shall include an analysis or demonstration that the process fluids do not meet the criteria of “in light liquid or gas/vapor service.” Examples of information that could document this include, but are not limited to, records of chemicals purchased for the process, analyses of process stream composition, engineering calculations, or process knowledge.

(9) Records of exempt components. Identification, either by list, location (area or group), or other method of equipment in organic HAP service less than 300 hr/yr subject to the provisions of this section.

(10) Records of alternative means of compliance determination. Owners and operators choosing to comply with the requirements of § 63.179 of subpart H of this part shall maintain the following records:

(i) Identification of the process(es) and the organic HAP they handle.

(ii) A schematic of the process, enclosure, and closed-vent system.

(iii) A description of the system used to create a negative pressure in the enclosure to ensure that all emissions are routed to the control device.

(h) Reporting Requirements. (1) Each owner or operator of a source subject to this section shall submit the reports listed in paragraphs (h)(1)(i) and (ii) of this section.

(i) A Notification of Compliance Status report described in paragraph (h)(3) of this section.

(ii) Periodic reports described in paragraph (h)(3) of this section.

(2) Notification of compliance status report. Each owner or operator of a source subject to this section shall submit the information specified in paragraphs (h)(2)(ii) through (iii) of this section in the Notification of Compliance Status report described in § 63.1368(f). Section 63.9(j) of subpart A of this part shall not apply to the Notification of Compliance Status report.

(i) The notification shall provide the information listed in paragraphs (h)(2)(ii)(A) through (C) of this section for each group of processes subject to
the requirements of paragraphs (b) through (g) of this section.

(A) Identification of the group of processes.

(B) Approximate number of each equipment type (e.g., valves, pumps) in organic HAP service, excluding equipment in vacuum service.

(C) Method of compliance with the standard (for example, “monthly leak detection and repair” or “equipped with dual mechanical seals”).

(i) The notification shall provide the information listed in paragraphs (h)(2)(ii)(A) and (B) of this section for each process subject to the requirements of paragraph (b)(3)(iv) of this section and §63.178(b) of subpart H of this part.

(A) Products or product codes subject to the provisions of this section, and

(B) Planned schedule for pressure testing when equipment is configured for production of products subject to the provisions of this section.

(ii) The notification shall provide the information listed in paragraphs (h)(2)(ii)(A) and (B) of this section for each process subject to the requirements in §63.179 of subpart H of this part.

(A) Process identification.

(B) A description of the system used to create a negative pressure in the enclosure and the control device used to comply with the requirements of paragraph (b)(3)(ii) of this section.

(3) Periodic reports. The owner or operator of a source subject to this section shall submit Periodic reports.

(i) A report containing the information in paragraphs (h)(3)(iii), (iii), and (iv) of this section shall be submitted semiannually. The first Periodic report shall be submitted no later than 240 days after the date the Notification of Compliance Status report is due and shall cover the 6-month period beginning on the date the Notification of Compliance Status report is due. Each subsequent Periodic report shall cover the 6-month period following the preceding period.

(ii) For equipment complying with the provisions of paragraphs (b) through (g) of this section, the Periodic report shall contain the summary information listed in paragraphs (h)(3)(iii)(A) through (L) of this section for each monitoring period during the 6-month period.

(A) The number of valves for which leaks were detected as described in paragraph (e)(2) of this section, the percent leakers, and the total number of valves monitored;

(B) The number of valves for which leaks were not repaired as required in paragraph (e)(7) of this section, identifying the number of those that are determined nonrepairable;

(C) The number of pumps and agitators for which leaks were detected as described in paragraph (c)(2) of this section, the percent leakers, and the total number of pumps and agitators monitored;

(D) The number of pumps and agitators for which leaks were not repaired as required in paragraph (c)(3) of this section;

(E) The number of compressors for which leaks were detected as described in §63.164(f) of subpart H of this part;

(F) The number of compressors for which leaks were not repaired as required in §63.164(g) of subpart H of this part;

(G) The number of connectors for which leaks were detected as described in §63.174(a) of subpart H of this part, the percent of connectors leaking, and the total number of connectors monitored;

(H) The number of connectors for which leaks were not repaired as required in §63.174(d) of subpart H of this part, identifying the number of those that are determined nonrepairable;

(I) The facts that explain any delay of repairs and, where appropriate, why a process shutdown was technically infeasible.

(J) The results of all monitoring to show compliance with §§63.164(i), 63.165(a), and 63.172(f) of subpart H of this part conducted within the semiannual reporting period.

(K) If applicable, the initiation of a monthly monitoring program under either paragraph (c)(4)(ii) or paragraph (e)(4)(ii)(A) of this section.

(L) If applicable, notification of a change in connector monitoring alternatives as described in §63.174(c)(1) of subpart H of this part.

(iii) For owners or operators electing to meet the requirements of §63.178(b)
§ 63.1364 Compliance dates.

(a) Compliance dates for existing sources. (1) An owner or operator of an existing affected source must comply with the provisions of this subpart within 3 years after June 23, 1999.

(2) Pursuant to section 112(i)(3)(B) of the CAA, an owner or operator of an existing source may request an extension of up to 1 additional year to comply with the provisions of this subpart if the additional time is needed for the installation of controls.

(i) For purposes of this subpart, a request for an extension shall be submitted no later than 120 days prior to the compliance date specified in paragraph (a)(1) of this section, except as provided in paragraph (a)(2)(ii) of this section. The dates specified in §63.6(i) of subpart A of this part for submittal of requests for extensions shall not apply to sources subject to this subpart.

(ii) An owner or operator may submit a compliance extension request after the date specified in paragraph (a)(1)(i) of this section provided the need for the compliance extension arose after that date and before the otherwise applicable compliance date, and the need arose due to circumstances beyond reasonable control of the owner or operator. This request shall include the data described in §63.6(i)(8)(A), (B), and (D) of subpart A of this part.

(b) Compliance dates for new and reconstructed sources. An owner or operator of a new or reconstructed affected source must comply with the provisions of this subpart on June 23, 1999 or upon startup, whichever is later.

§ 63.1365 Test methods and initial compliance procedures.

(a) General. Except as specified in paragraph (a)(4) of this section, the procedures specified in paragraphs (c), (d), (e), (f), and (g) of this section are required to demonstrate initial compliance with §63.1362(b), (c), (d), (f), and (g), respectively. The provisions in paragraph (a)(1) of this section apply to design evaluations that are used to demonstrate compliance with the standards for process vents and storage vessels. The provisions in paragraph (a)(2) of this section apply to performance tests that are specified in paragraphs (c), (d), and (e) of this section. The provisions in paragraph (a)(3) of this section describe initial compliance procedures for flares. The provisions in paragraph (a)(5) of this section are used to demonstrate initial compliance with the alternative standards specified in §63.1362(b)(6) and (c)(4). The provisions in paragraph (a)(6) of this section are used to comply with the outlet concentration requirements specified in §63.1362(b)(2)(iv)(A), (b)(3)(ii), (b)(4)(ii)(A), (b)(5)(ii), and (b)(5)(iii).

(1) Design evaluation. To demonstrate that a control device meets the required control efficiency, a design evaluation must address the composition and HAP concentration of the vent stream entering the control device. A design evaluation also must address other vent stream characteristics and control device operating parameters as specified in any one of paragraphs (a)(1)(i) through (vii) of this section, depending on the type of control device that is used. If the vent stream is not the only inlet to the control device, the efficiency demonstration also must consider all other vapors, gases, and liquids, other than fuels, received by the control device.

(i) For an enclosed combustion device used to comply with the provisions of §63.1362(b)(2)(iv), (b)(4)(ii), (c)(2)(iv)(B), or (c)(3) with a minimum residence time of 0.5 seconds and a minimum
temperature of 760 °C, the design evaluation must document that these conditions exist.

(ii) For a combustion control device that does not satisfy the criteria in paragraph (a)(1)(i) of this section, the design evaluation must document control efficiency and address the following characteristics, depending on the type of control device:

(A) For a thermal vapor incinerator, the design evaluation must consider the autoignition temperature of the organic HAP, must consider the vent stream flow rate, and must establish the design minimum and average temperature in the combustion zone and the combustion zone residence time.

(B) For a catalytic vapor incinerator, the design evaluation must consider the vent stream flow rate and must establish the design minimum and average temperatures across the catalyst bed inlet and outlet.

(C) For a boiler or process heater, the design evaluation must consider the vent stream flow rate and must establish the design minimum and average flame zone temperatures and combustion zone residence time, and must describe the method and location where the vent stream is introduced into the flame zone.

(iii) For a condenser, the design evaluation must consider the vent stream flow rate, relative humidity, and temperature, and must establish the design outlet organic HAP compound concentration level, design average temperature of the condenser exhaust vent stream, and the design average temperatures of the coolant fluid at the condenser inlet and outlet. The temperature of the gas stream exiting the condenser must be measured and used to establish the outlet organic HAP concentration.

(iv) For a carbon adsorption system that regenerates the carbon bed directly onsite in the control device such as a fixed-bed adsorber, the design evaluation must consider the vent stream flow rate, relative humidity, and temperature, and must establish the design exhaust vent stream organic compound concentration level, adsorption cycle time, number of carbon beds and their capacities, type and working capacity of activated carbon used for the carbon beds, design total regeneration stream mass or volumetric flow over the period of each complete carbon bed regeneration cycle, design carbon bed temperature after regeneration, design carbon bed regeneration time, and design service life of carbon. For vacuum desorption, the pressure drop must be included.

(v) For a carbon adsorption system that does not regenerate the carbon bed directly onsite in the control device such as a carbon canister, the design evaluation must consider the vent stream mass or volumetric flow rate, relative humidity, and temperature, and must establish the design exhaust vent stream organic compound concentration level, capacity of the carbon bed, type and working capacity of activated carbon used for the carbon bed, and design carbon replacement interval based on the total carbon working capacity of the control device and source operating schedule.

(vi) For a scrubber, the design evaluation must consider the vent stream composition, constituent concentrations, liquid-to-vapor ratio, scrubbing liquid flow rate and concentration, temperature, and the reaction kinetics of the constituents with the scrubbing liquid. The design evaluation must establish the design exhaust vent stream organic compound concentration level and must include the additional information in paragraphs (a)(1)(vi)(A) and (B) of this section for trays and a packed column scrubber.

(A) Type and total number of theoretical and actual trays;

(B) Type and total surface area of packing for entire column, and for individual packed sections if column contains more than one packed section.

(vii) For fabric filters, the design evaluation must include the pressure drop through the device and the net gas-to-cloth ratio (i.e., cubic feet of gas per square feet of cloth).

(2) Calculation of TOC or total organic HAP concentration. The TOC concentration or total organic HAP concentration is the sum of the concentrations of the individual components. If compliance is being determined based on TOC, the owner or operator shall compute TOC for each run using Equation 6 of this subpart. If compliance with the
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percent reduction format of the standard is being determined based on total organic HAP, the owner or operator shall compute total organic HAP using Equation 6 of this subpart, except that only organic HAP compounds shall be summed; when determining compliance with the wastewater provisions of § 63.1363(d), the organic HAP compounds shall consist of the organic HAP compounds in Table 9 of subpart G of this part.

\[
CG_T = \frac{1}{m} \sum_{j=1}^{m} \left( \sum_{i=1}^{n} CGS_{i,j} \right)
\]  
(Eq. 6)

Where:

- \( CG_T \) = total concentration of TOC in vented gas stream, average of samples, dry basis, ppmv
- \( CGS_{i,j} \) = concentration of sample components in vented gas stream for sample \( j \), dry basis, ppmv
- \( n \) = number of compounds in the sample
- \( m \) = number of samples in the sample run

(3) Initial compliance using flares. When a flare is used to comply with the standards, the owner or operator shall comply with the provisions in §63.11(b) of subpart A of this part.

(i) The initial compliance determination shall consist of a visible emissions determination using Method 22 of 40 CFR part 60, appendix A, as described in §63.11(b)(4) of subpart A of this part, and a determination of net heating value of gas being combusted and exit velocity to comply with the requirements of §63.11(b)(6) through (8) of subpart A of this part. The net heating value and exit velocity shall be based on the results of performance testing under the conditions described in paragraphs (b)(10) and (11) of this section.

(ii) An owner or operator is not required to conduct a performance test to determine percent emission reduction or outlet organic HAP or TOC concentration when a flare is used.

(4) Exemptions from compliance demonstrations. An owner or operator using any control device specified in paragraphs (a)(4)(i) through (ii) of this section is exempt from the initial compliance provisions in paragraphs (c), (d), and (e) of this section.

(i) A boiler or process heater with a design heat input capacity of 44 megawatts or greater.

(ii) A boiler or process heater into which the emission stream is introduced with the primary fuel.

(5) Initial compliance with alternative standard. Initial compliance with the alternative standards in §63.1362(b)(6) and (c)(4) is demonstrated when the outlet TOC concentration is 20 ppmv or less, and the outlet HCl and chlorine concentration is 20 ppmv or less. To demonstrate initial compliance, the owner or operator shall be in compliance with the monitoring provisions in §63.1366(b)(5) on the initial compliance date. The owner or operator shall use Method 18 of 40 CFR part 60, appendix A to determine the predominant organic HAP in the emission stream if the TOC monitor is calibrated on the predominant HAP.

(6) Initial compliance with the 20 ppmv outlet limit. Initial compliance with the 20 ppmv TOC and HCl and chlorine concentration is demonstrated when the outlet TOC concentration is 20 ppmv or less, and the outlet HCl and chlorine concentration is 20 ppmv or less. To demonstrate initial compliance, the owner or operator shall comply with the monitoring provisions in §63.1366(b)(1) through (5) on the initial compliance date.

(7) Outlet concentration correction for supplemental gases. If supplemental gases are added to a vent stream for which compliance with an outlet concentration standard in §63.1362 or 63.1363 will be demonstrated, the owner or operator must correct the outlet concentration as specified in paragraphs (a)(7)(i) and (ii) of this section.

(i) Combustion device. If the vent stream is controlled with a combustion device, the owner or operator must comply with the provisions in paragraphs (a)(7)(ii)(A) through (C) of this section.

(A) To comply with a TOC outlet concentration standard in §63.1362(b)(2)(iv)(A), (b)(4)(ii)(A), (b)(6), (c)(2)(iv)(B), (c)(4), (d)(13), or §63.172 of
subpart H of this part, the actual TOC outlet concentration must be corrected to 3 percent oxygen.

(B) If the inlet stream to the combustion device contains any HCl, chlorine, or halogenated compounds, and the owner or operator elects to comply with a total HCl and chlorine outlet concentration standard in §63.1362(b)(3)(ii), (b)(5)(ii), (b)(5)(iii), (b)(6), or (c)(4), the actual total HCl and chlorine outlet concentration must be corrected to 3 percent oxygen.

(C) The integrated sampling and analysis procedures of Method 3B of 40 CFR part 60, appendix A shall be used to determine the actual oxygen concentration (%O<sub>2d</sub>). The samples shall be taken during the same time that the TOC and HCl and chlorine samples are taken. The concentration corrected to 3 percent oxygen (C<sub>C</sub>) shall be computed using Equation 7 of this subpart:

\[
C_c = C_m \left( \frac{17.9}{20.9 - %O_{2d}} \right) \quad (Eq. 7)
\]

Where:
- \(C_m\) = concentration of TOC or total HCl and chlorine corrected to 3 percent oxygen, dry basis, ppmv
- \(C_c\) = total concentration of TOC or total HCl and chlorine in the vented gas stream, average of samples, dry basis, ppmv
- \%O<sub>2d</sub> = concentration of oxygen measured in vented gas stream, dry basis, percent by volume

(ii) Noncombustion devices. If a control device other than a combustion device, and not in series with a combustion device, is used to comply with a TOC or total HCl and chlorine outlet concentration standard, the owner or operator must correct the actual concentration for supplemental gases using Equation 8 of this subpart:

\[
C_a = C_m \left( \frac{V_s + V_a}{V_a} \right) \quad (Eq. 8)
\]

Where:
- \(C_a\) = corrected outlet TOC or total HCl and chlorine concentration, dry basis, ppmv
- \(C_m\) = actual TOC or total HCl and chlorine concentration measured at control device outlet, dry basis, ppmv
- \(V_a\) = total volumetric flow rate of affected streams vented to the control device
- \(V_s\) = total volumetric flow rate of supplemental gases

(b) Test methods and conditions. When testing is conducted to measure emissions from an affected source, the test methods specified in paragraphs (b)(1) through (9) of this section shall be used. Compliance tests shall be performed under conditions specified in paragraphs (b)(10) and (11) of this section. Testing requirements for condensers are specified in paragraph (b)(12) of this section.

(1) Method 1 or 1A of appendix A of 40 CFR part 60 shall be used for sample and velocity traverses.

(2) Method 2, 2A, 2C, or 2D of appendix A of 40 CFR part 60 shall be used for velocity and volumetric flow rates.

(3) Method 3 of appendix A of 40 CFR part 60 shall be used for gas analysis.

(4) Method 4 of appendix A of 40 CFR part 60 shall be used for stack gas moisture.

(5) Concentration measurements shall be adjusted to negate the dilution effects of introducing nonaffected gaseous streams into the vent streams prior to control or measurement. The following methods are specified for concentration measurements of organic compounds:

(i) Method 18 of appendix A of 40 CFR part 60 may be used to determine HAP concentration in any control device efficiency determination.

(ii) Method 25 of appendix A of 40 CFR part 60 may be used to determine total gaseous nonmethane organic concentration for control efficiency determinations in combustion devices.

(iii) Method 25A of appendix A of 40 CFR part 60 may be used to determine total gaseous nonmethane organic concentration for control efficiency determinations in noncombustion devices.

(iv) Method 25A of appendix A of 40 CFR part 60 may be used to determine the concentration of TOC for the 20 ppmv standard, the instrument shall be calibrated on methane or the predominant HAP. If Method 25A of appendix A of 40 CFR part 60 is used to determine the concentration of TOC for the 20 ppmv standard, the instrument shall be calibrated on methane or the predominant HAP.
CFR part 60 shall comply with paragraphs (b)(5)(i)(A) through (C) of this section.

(A) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A, shall be the single organic HAP representing the largest percent by volume.

(B) The use of Method 25A, 40 CFR part 60, appendix A, is acceptable if the response from the high level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(C) The span value of the analyzer must be less than 100 ppmv.

(6) The methods in either paragraph (b)(5)(i) or (ii) of this section shall be used to determine the concentration, in mg/dscm, of total HCl and chlorine. Concentration measurements shall be adjusted to negate the dilution effects of introducing nonaffected gaseous streams into the vent streams prior to control or measurement.

(i) Method 26 or 26A of 40 CFR part 60, appendix A.

(ii) Any other method if the method or data have been validated according to the applicable procedures of Method 301 of appendix A of this part.

(7) Method 5 of appendix A of 40 CFR part 60 shall be used to determine the concentration of particulate matter in exhaust gas streams from bag dumps and product dryers.

(8) Wastewater analysis shall be conducted in accordance with §63.144(b)(5)(i) through (iii) of subpart G of this part.

(9) Method 22 of appendix A of 40 CFR part 60 shall be used to determine visible emissions from flares.

(10) Testing conditions for continuous processes. Testing of process vents on equipment operating as part of a continuous process shall consist of three one-hour runs. Gas stream volumetric flow rates shall be measured every 15 minutes during each 1-hour run. Organic HAP concentration shall be determined from samples collected in an integrated sample over the duration of each one-hour test run, or from grab samples collected simultaneously with the flow rate measurements (every 15 minutes). If an integrated sample is collected for laboratory analysis, the sampling rate shall be adjusted proportionally to reflect variations in flow rate. For continuous gas streams, the emission rate used to determine compliance shall be the average emission rate of the three test runs.

(11) Testing conditions for batch processes. Except as provided in paragraph (b)(12) of this section for condensers, testing of emissions on equipment where the flow of gaseous emissions is intermittent (batch operations) shall be conducted at absolute peak-case conditions or hypothetical peak-case conditions, as specified in paragraphs (b)(11)(i) and (ii) of this section, respectively. Gas stream volumetric flow rates shall be measured at 15-minute intervals. Organic HAP, TOC, or HCl and chlorine concentration shall be determined from samples collected in an integrated sample over the duration of the test, or from grab samples collected simultaneously with the flow rate measurements (every 15 minutes).

(i) Absolute peak-case. If the most challenging conditions for the control device occur under maximum HAP load, the absolute peak-case conditions shall be characterized by the criteria presented in paragraph (b)(11)(i)(A) or (B) of this section. Otherwise, absolute peak-case conditions are defined by the conditions in paragraph (b)(11)(i)(C) of this section.

(A) The period in which the inlet to the control device will contain at least 50 percent of the maximum HAP mass load that may be vented to the control device over any 8-hour period. An emission profile as described in paragraph (b)(11)(i)(ii) of this section.
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(b)(11)(iii)(A) of this section shall be used to identify the 8-hour period that includes the maximum projected HAP load.

(B) A 1-hour period of time in which the inlet to the control device will contain the highest hourly HAP mass load. An emission profile as described in paragraph (b)(11)(iii)(A) of this section shall be used to identify the 1-hour period of maximum HAP loading.

(C) The period of time when a condition other than the maximum HAP load is most challenging for the control device. These conditions include, but are not limited to the following:

1. Periods when the streams contain the highest combined VOC and HAP hourly load, as described by the emission profiles in paragraph (b)(11)(iii) of this section; or
2. Periods when the streams contain HAP constituents that approach the limits of solubility for scrubbing media; or
3. Periods when the streams contain HAP constituents that approach the limits of adsorptivity for carbon adsorption systems.

(ii) Hypothetical peak-case. Hypothetical peak-case conditions are simulated test conditions that, at a minimum, contain the highest total average hourly HAP load of emissions that would be predicted to be vented to the control device from the emissions profile described in either paragraph (b)(11)(iii)(B) or (C) of this section.

(iii) Emissions profile. The owner or operator may choose to perform tests only during those periods of the peak-case episodes that the owner or operator selects to control as part of achieving the required emission reduction. The owner or operator shall develop an emission profile for the vent to the control device that describes the characteristics of the vent stream at the inlet to the control device under either absolute or hypothetical peak-case conditions. The emissions profile shall be developed based on the applicable procedures described in paragraphs (b)(11)(iii)(A) through (C) of this section, as required by paragraphs (b)(11)(i) and (ii) of this section.

(A) Emissions profile by process. The emissions profile must consider all emission episodes that could contribute to the vent stack for a period of time that is sufficient to include all processes venting to the stack and shall consider production scheduling. The profile shall describe the HAP load to the device that equals the highest sum of emissions from the episodes that can vent to the control device during the period of absolute peak-case conditions specified in paragraph (b)(11)(i)(A), (B), or (C) as appropriate. Emissions per episode shall be calculated using the procedures specified in paragraph (c)(2) of this section. When complying with paragraph (b)(11)(i)(B) of this section, emissions per episode shall be divided by the duration of the episode if the duration of the episode is longer than 1 hour.

(B) Emission profile by equipment. The emission profile must consist of emissions that meet or exceed the highest hourly HAP load that would be expected under actual processing conditions. The profile shall describe equipment configurations used to generate the emission events, volatility of materials processed in the equipment, and the rationale used to identify and characterize the emission events. The emissions may be based on using a compound more volatile than compounds actually used in the process(es), and the emissions may be generated from all equipment in the process(es) or only selected equipment.

(C) Emission profile by capture and control device limitation. The emission profile shall consider the capture and control system limitations and the highest hourly emissions that can be routed to the control device, based on the maximum flow rate and concentrations possible because of limitations on conveyance and control equipment (e.g., fans, LEL alarms and safety bypasses).

(iv) Test duration. Three runs, at a minimum of 1 hour each, are required for performance testing. Each run must occur over the same absolute or hypothetical peak-case conditions, as defined in paragraph (b)(11)(i) or (ii) of this section.

(12) Testing requirements for condensers. For emission streams controlled using condensers, the owner or
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operator shall calculate the condenser outlet gas temperature that is needed to meet the required percent reduction.

(c) Initial compliance with process vent provisions. The owner or operator of an affected source shall demonstrate compliance with the process vent standards in §63.1362(b) using the procedures described in paragraphs (c)(1) through (3) of this section.

(1) Compliance with the process vent standards in §63.1362(b) shall be demonstrated in accordance with the provisions specified in paragraphs (c)(1)(i) through (viii) of this section.

(i) Initial compliance with the emission limit cutoffs in §63.1362(b)(2)(i) and (b)(4)(i) is demonstrated when the uncontrolled organic HAP emissions from the sum of all process vents within a process are less than or equal to 0.15 Mg/yr. Uncontrolled HAP emissions shall be determined using the procedures described in paragraph (c)(2) of this section.

(ii) Initial compliance with the emission limit cutoffs in §63.1362(b)(3)(i) and (b)(5)(i) is demonstrated when the uncontrolled HCl and Cl₂ emissions from the sum of all process vents within a process are less than or equal to 6.8 Mg/yr. Initial compliance with the emission limit cutoffs in §63.1362(b)(3)(ii) and (iii) is demonstrated when the uncontrolled HCl and Cl₂ emissions are greater than or equal to 6.8 Mg/yr or greater than or equal to 191 Mg/yr, respectively. Uncontrolled emissions shall be determined using the procedures described in paragraph (c)(2) of this section.

(iii) Initial compliance with the organic HAP percent reduction requirements specified in §63.1362(b)(2)(ii), (b)(2)(iii), and (b)(4)(i) is demonstrated by determining controlled HAP emissions using the procedures described in paragraph (c)(3) of this section, determining uncontrolled emissions of HCl and Cl₂ using the procedures described in paragraph (c)(2) of this section, and calculating the applicable percent reduction.

(iv) Initial compliance with the HCl and Cl₂ percent reduction requirements specified in §63.1362(b)(3)(ii), (b)(5)(ii), and (b)(5)(iii) is demonstrated by determining controlled emissions of HCl and Cl₂ using the procedures described in paragraph (c)(3) of this section, determining uncontrolled emissions of HCl and Cl₂ using the procedures described in paragraph (c)(2) of this section, and calculating the applicable percent reduction.

(v) Initial compliance with the outlet concentration limits in §63.1362(b)(2)(iv)(A), (b)(2)(v)(A), (b)(3)(ii), (b)(4)(ii)(A), (b)(5)(ii), and (b)(5)(iii) is demonstrated when the outlet TOC concentration is 20 ppmv or less and the outlet HCl and chlorine concentration is 20 ppmv or less. The owner or operator shall demonstrate compliance by fulfilling the requirements in paragraph (a)(6) of this section. If an owner or operator elects to develop an emissions profile by process as described in paragraph (b)(11)(iii)(A) of this section, uncontrolled emissions shall be determined using the procedures in paragraph (c)(2) of this section.

(vi) Initial compliance with the alternative standard in §63.1362(b)(6) is demonstrated by fulfilling the requirements in paragraph (a)(5) of this section.

(vii) Initial compliance when using a flare is demonstrated by fulfilling the requirements in paragraph (a)(3) of this section.

(viii) No initial compliance demonstration is required for control devices specified in §63.1362(l).

(2) Uncontrolled emissions. The owner or operator referred to from paragraphs (c)(3)(i) through (v) of this section shall calculate uncontrolled emissions according to the procedures described in paragraph (c)(2) or (ii) of this section, as appropriate.

(i) Emission estimation procedures. The owner or operator shall determine uncontrolled HAP emissions using emission measurements and/or calculations for each batch emission episode according to the engineering evaluation methodology in paragraphs (c)(2)(i)(A) through (H) of this section.

(A) Individual HAP partial pressures in multicomponent systems shall be determined in accordance with the methods specified in paragraphs (c)(2)(i)(A)(i) through (3) of this section. Chemical property data may be obtained from standard references.
(1) If the components are miscible in one another, use Raoult’s law to calculate the partial pressures;
(2) If the solution is a dilute aqueous mixture, use Henry’s law constants to calculate partial pressures;
(3) If Raoult’s law or Henry’s law are not appropriate or available, use any of the methods specified in paragraphs (c)(2)(i)(A)(3)(i) through (iii) of this section.
   (i) Use experimentally obtained activity coefficients;
   (ii) Use models such as the group-contribution models to predict activity coefficients;
   (iii) Assume the components of the system behave independently and use the summation of all vapor pressures from the HAP as the total HAP partial pressure;
(B) Charging or filling. Emissions from vapor displacement due to transfer of material to a vessel shall be calculated using Equation 9 of this subpart:
\[ E = \sum_{i=1}^{n} P_i \times \left( \frac{V}{(R)(T)} \times \left( \sum_{i=1}^{n} \frac{P_i}{P_T} \right) \right) \]  
Where:
- \( E \) = mass of HAP emitted
- \( V \) = volume of gas displaced from the vessel
- \( R \) = ideal gas law constant
- \( T \) = temperature of the vessel vapor space; absolute
- \( P_i \) = partial pressure of the individual HAP
- \( MW_i \) = molecular weight of the individual HAP

(C) Purging. Emissions from purging shall be calculated using Equation 10 of this subpart, except that for purge flow rates greater than 100 scfm, the mole fraction of HAP will be assumed to be 25 percent of the saturated value.
\[ E = \sum_{i=1}^{n} P_i MW_i \times \left( \frac{V}{(R)(T)} \right) \times \left( \frac{P_T}{P_T - \sum_{j=1}^{m} \frac{P_j}{P_T}} \right) \]  
Where:
- \( E \) = mass of HAP emitted
- \( V \) = purge flow rate at the temperature and pressure of the vessel vapor space
- \( R \) = ideal gas law constant
- \( T \) = temperature of the vessel vapor space; absolute
- \( P_i \) = partial pressure of the individual HAP
- \( MW_i \) = molecular weight of the individual HAP
- \( P_T \) = pressure of the vessel vapor space
- \( t \) = time of purge
- \( n \) = number of HAP compounds in the emission stream
- \( m \) = number of condensable VOC compounds (including HAP) in the emission stream
(D) Heating. Emissions caused by heating the contents of a vessel to a temperature less than the boiling point shall be calculated using procedures in either paragraph (c)(2)(i)(D)(1), (2), or (4) of this section, as appropriate. If the contents of a vessel are heated to the boiling point, emissions while boiling are assumed to be zero if the owner or operator is complying with the provisions in paragraph (d)(2)(i)(C)(3) of this section.
   (1) If the final temperature to which the vessel contents are heated is lower than 50 K below the boiling point of the HAP in the vessel, then emissions shall be calculated using Equations 11 through 14 of this subpart.
   (i) The mass of HAP emitted per episode shall be calculated using Equation 11 of this subpart:
\[ E = \frac{\sum_{i=1}^{n} (P_i)_{T_1} + \sum_{i=1}^{n} (P_i)_{T_2}}{2} \times \Delta \eta \times MW_{HAP} \quad \text{(Eq. 11)} \]

Where:
- \( E \) is the mass of HAP vapor displaced from the vessel being heated
- \((P_i)_{T_n}\) is the partial pressure of each HAP in the vessel headspace at initial \((n = 1)\) and final \((n = 2)\) temperatures
- \(P_{a_1}\) is the initial noncondensable gas pressure in the vessel, as calculated using Equation 13 of this subpart
- \(P_{a_2}\) is the final noncondensable gas pressure in the vessel, as calculated using Equation 13 of this subpart
- \(\Delta \eta\) is the number of moles of noncondensable gas displaced, as calculated using Equation 12 of this subpart
- \(MW_{HAP}\) is the average molecular weight of HAP present in the vessel, as calculated using Equation 14 of this subpart:

\[ MW_{HAP} = \frac{\sum_{i=1}^{n} \left( (P_i)_{T_1} + (P_i)_{T_2} \right) \cdot MW_i}{\sum_{i=1}^{n} \left( (P_i)_{T_1} + (P_i)_{T_2} \right)} \quad \text{(Eq. 14)} \]

Where:
- \(MW_{HAP}\) is the average molecular weight of HAP in the displaced gas
- \((P_i)_{T_n}\) is the partial pressure of each HAP in the vessel headspace at the initial \((T_{1})\) and final \((T_{2})\) temperatures
- \(MW_i\) is the molecular weight of each HAP
- \(n\) is the number of HAP compounds in the emission stream

(ii) The moles of noncondensable gas displaced shall be calculated using Equation 12 of this subpart:

\[ \Delta \eta = V \left[ \frac{P_{a_1}}{R \left( \frac{T_1}{T_2} \right)} - \frac{P_{a_2}}{R \left( \frac{T_1}{T_2} \right)} \right] \quad \text{(Eq. 12)} \]

where:
- \(\Delta \eta\) is the number of moles of noncondensable gas displaced
- \(V\) is the volume of free space in the vessel
- \(R\) is the ideal gas law constant

(iii) The initial and final pressure of the noncondensable gas in the vessel shall be calculated according to Equation 13 of this subpart:

\[ P_{a_n} = P_{a_{\text{atm}}} - \sum_{j=1}^{m} \left( P_j \right)_{T_n} \quad \text{(Eq. 13)} \]

Where:
- \(P_{a_n}\) is the partial pressure of noncondensable gas in the vessel headspace at initial \((n = 1)\) and final \((n = 2)\) temperatures
- \(P_{a_{\text{atm}}}\) is the atmospheric pressure
- \((P_j)_{T_n}\) is the partial pressure of each condensable volatile organic compound (including HAP) in the vessel headspace at the initial temperature \((n = 1)\) and final \((n = 2)\) temperature

(iv) The average molecular weight of HAP in the displaced gas shall be calculated using Equation 14 of this subpart:

\[ MW_{HAP} = \frac{\sum_{i=1}^{n} \left( (P_i)_{T_1} + (P_i)_{T_2} \right) \cdot MW_i}{\sum_{i=1}^{n} \left( (P_i)_{T_1} + (P_i)_{T_2} \right)} \quad \text{(Eq. 14)} \]

Where:
- \(MW_{HAP}\) is the average molecular weight of HAP in the displaced gas
- \((P_i)_{T_n}\) is the partial pressure of each HAP in the vessel headspace at the initial \((T_{1})\) and final \((T_{2})\) temperatures
- \(MW_i\) is the molecular weight of each HAP
- \(n\) is the number of HAP compounds in the emission stream

(2) If the vessel contents are heated to a temperature greater than 50 K below the boiling point, then emissions from the heating of a vessel shall be calculated as the sum of the emissions calculated in accordance with paragraphs (c)(2)(i)(D)(2)(i) and (ii) of this section.
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(i) For the interval from the initial temperature to the temperature 50 K below the boiling point, emissions shall be calculated using Equation 11 of this subpart, where \( T_2 \) is the temperature 50 K below the boiling point.

(ii) For the interval from the temperature 50 K below the boiling point to the final temperature, emissions shall be calculated as the summation of emissions for each 5 K increment, where the emission for each increment shall be calculated using Equation 11 of this subpart. If the final temperature of the heatup is lower than 5 K below the boiling point, the final temperature for the last increment shall be the final temperature of the heatup, even if the last increment is less than 5 K. If the final temperature of the heatup is higher than 5 K below the boiling point, the final temperature for the last increment shall be the temperature 5 K below the boiling point, even if the last increment is less than 5 K.

(3) While boiling, the vessel must be operated with a properly operated process condenser. An initial demonstration that a process condenser is properly operated is required for vessels that operate process condensers without secondary condensers that are air pollution control devices. The owner or operator must either measure the condenser exhaust gas temperature and show it is less than the boiling point of the substance(s) in the vessel, or perform a material balance around the vessel and condenser to show that at least 99 percent of the material vaporized while boiling is condensed. Uncontrolled emissions are assumed to be zero under these conditions. The initial demonstration shall be conducted for all appropriate operating scenarios and documented in the Notification of Compliance Status report as specified in §63.1368(f).

(4)(i) As an alternative to the procedures described in paragraphs (c)(2)(i)(D)(1) and (2) of this section, emissions caused by heating a vessel to any temperature less than the boiling point may be calculated using Equation 15 of this subpart.

\[
E = \text{MW}_{\text{HAP}} \times \left( N_{\text{avg}} \times \ln \frac{P_T - \sum_{j=1}^{m} (P_{i,j})}{P_T - \sum_{j=1}^{m} (P_{i,j})} \right) - \left( n_{\text{HAP},2} - n_{\text{HAP},1} \right) \quad \text{(Eq. 15)}
\]

Where:

- \( E \) = mass of HAP vapor displaced from the vessel being heated
- \( N_{\text{avg}} \) = average gas space molar volume during the heating process, as calculated using Equation 16 of this subpart
- \( P_T \) = total pressure in the vessel
- \( P_{i,j} \) = partial pressure of the individual HAP compounds at \( T_i \)
- \( \text{MW}_{\text{HAP}} \) = average molecular weight of the HAP compounds, as calculated using Equation 14 of this subpart
- \( n_{\text{HAP},1} \) = number of moles of total HAP in the vessel headspace at \( T_1 \)
- \( n_{\text{HAP},2} \) = number of moles of total HAP in the vessel headspace at \( T_2 \)
- \( m \) = number of condensable VOC compounds (including HAP) in the emission stream

(ii) The average gas space molar volume during the heating process is calculated using Equation 16 of this subpart.

\[
N_{\text{avg}} = \frac{V P_T}{2 R} \left( \frac{1}{T_1} + \frac{1}{T_2} \right) \quad \text{(Eq. 16)}
\]

Where:

- \( N_{\text{avg}} \) = average gas space molar volume during the heating process
- \( V \) = volume of free space in vessel
- \( P_T \) = total pressure in the vessel
- \( R \) = ideal gas law constant
- \( T_1 \) = initial temperature of the vessel contents, absolute
- \( T_2 \) = final temperature of the vessel contents, absolute
(iii) The difference in the number of moles of total HAP in the vessel headspace between the initial and final temperatures is calculated using Equation 17 of this subpart.

\[
\left(n_{\text{HAP,2}} - n_{\text{HAP,1}}\right) = \frac{V}{R(T_2)} \sum_{i=1}^{n} P_{i,2} - \frac{V}{R(T_1)} \sum_{i=1}^{n} P_{i,1} \quad (\text{Eq. 17})
\]

Where:
- \(n_{\text{HAP,2}}\) = number of moles of total HAP in the vessel headspace at \(T_2\)
- \(n_{\text{HAP,1}}\) = number of moles of total HAP in the vessel headspace at \(T_1\)
- \(V\) = volume of free space in vessel
- \(R\) = ideal gas law constant
- \(T_1\) = initial temperature of the vessel contents, absolute
- \(T_2\) = final temperature of the vessel contents, absolute
- \(P_{i,1}\) = partial pressure of the individual HAP compounds at \(T_1\)
- \(P_{i,2}\) = partial pressure of the individual HAP compounds at \(T_2\)
- \(n\) = number of HAP compounds in the emission stream

(E) Depressurization. Emissions from depressurization shall be calculated using the procedures in paragraphs (c)(2)(i)(E)(1) through (5) of this section. Alternatively, the owner or operator may elect to calculate emissions from depressurization using the procedures in paragraph (c)(2)(i)(E)(6) of this section.

(1) The moles of HAP vapor initially in the vessel are calculated using Equation 18 of this subpart:

\[
n_{\text{HAP}} = \frac{V}{RT} \times \sum_{i=1}^{n} P_i \quad (\text{Eq. 18})
\]

Where:
- \(n_{\text{HAP}}\) = moles of HAP vapor in the vessel
- \(P_i\) = partial pressure of each HAP in the vessel vapor space
- \(V\) = free volume in the vessel being depressurized
- \(R\) = ideal gas law constant
- \(T\) = absolute temperature in vessel
- \(n\) = number of HAP compounds in the emission stream

(2) The initial and final moles of noncondensable gas present in the vessel are calculated using Equations 19 and 20 of this subpart:

\[
n_1 = \frac{V P_{n_{\text{nc1}}}}{RT} \quad (\text{Eq. 19})
\]

\[
n_2 = \frac{V P_{n_{\text{nc2}}}}{RT} \quad (\text{Eq. 20})
\]

Where:
- \(n_1\) = initial number of moles of noncondensable gas in the vessel
- \(n_2\) = final number of moles of noncondensable gas in the vessel
- \(V\) = free volume in the vessel being depressurized
- \(P_{n_{\text{nc1}}}\) = initial partial pressure of the noncondensable gas, as calculated using Equation 21 of this subpart
- \(P_{n_{\text{nc2}}}\) = final partial pressure of the noncondensable gas, as calculated using Equation 22 of this subpart
- \(R\) = ideal gas law constant
- \(T\) = temperature, absolute

(3) The initial and final partial pressures of the noncondensable gas in the vessel are determined using Equations 21 and 22 of this subpart:

\[
P_{n_{\text{nc1}}} = P_1 - \sum_{j=1}^{m} \left( P_j^* \right) x_j \quad (\text{Eq. 21})
\]

\[
P_{n_{\text{nc2}}} = P_2 - \sum_{j=1}^{m} \left( P_j^* \right) x_j \quad (\text{Eq. 22})
\]

Where:
- \(P_{n_{\text{nc1}}}\) = initial partial pressure of the noncondensable gas
- \(P_{n_{\text{nc2}}}\) = final partial pressure of the noncondensable gas
- \(P_1\) = initial vessel pressure
- \(P_2\) = final vessel pressure
- \(P_j^*\) = vapor pressure of each condensable VOC (including HAP) in the emission stream
- \(x_j\) = mole fraction of each condensable VOC (including HAP) in the emission stream
- \(m\) = number of condensable VOC compounds (including HAP) in the emission stream
(4) The moles of HAP emitted during the depressurization are calculated by taking an approximation of the average ratio of moles of HAP to moles of noncondensable and multiplying by the total moles of noncondensables released during the depressurization, using Equation 23 of this subpart:

Where:

\[ n_{HAP,e} = \left( \frac{n_{HAP,1} + n_{HAP,2}}{n_1 + n_2} \right) \left[ n_1 - n_2 \right] \]  
(Eq. 23)

\( n_{HAP,1} \) = moles of HAP vapor in vessel at the initial pressure, as calculated using Equation 18 of this subpart

\( n_{HAP,2} \) = moles of HAP vapor in vessel at the final pressure, as calculated using Equation 18 of this subpart

\( n_1 \) = initial number of moles of noncondensable gas in the vessel, as calculated using Equation 19 of this subpart

\( n_2 \) = final number of moles of noncondensable gas in the vessel, as calculated using Equation 19 of this subpart

(5) Use Equation 24 of this subpart to calculate the mass of HAP emitted:

\[ E = n_{HAP,e} \times MW_{HAP} \]  
(Eq. 24)

\[ E = \frac{V}{R(T)} \times \ln \left( \frac{P_1 - \sum_{j=1}^{m} P_j}{P_2 - \sum_{j=1}^{m} P_j} \right) \times \sum_{i=1}^{n} \left( P_i \right) \left( MW_i \right) \]  
(Eq. 25)

where:

\( V \) = free volume in vessel being depressurized

\( R \) = ideal gas law constant

\( T \) = temperature of the vessel, absolute

\( P_1 \) = initial pressure in the vessel

\( P_2 \) = final pressure in the vessel

\( P_i \) = partial pressure of the individual HAP compounds

\( P_j \) = partial pressure of individual condensable VOC compounds (including HAP)

\( MW_i \) = molecular weight of the individual HAP compounds

\( n \) = number of HAP compounds in the emission stream

\( m \) = number of condensable VOC compounds (including HAP) in the emission stream

(6) As an alternative to the procedures in paragraphs (c)(2)(i)(E)(1) through (5) of this section, emissions from depressurization may be calculated using Equation 25 of this subpart:

(F) Vacuum systems. Calculate emissions from vacuum systems using Equation 26 of this subpart:
Where:

\[ E = \frac{(MW_s)(La)(t)}{MW_{nc}} \left( \frac{\sum_{i=1}^{n} P_i}{P_T - \sum_{j=1}^{m} P_j} \right) \]  

(Eq. 26)

\[ m = \text{number of condensable VOC compounds (including HAP) in the emission stream} \]

(G) Gas evolution. Emissions from gas evolution shall be calculated using Equation 10 of this subpart with \( V \) calculated using Equation 27 of this subpart:

\[ V = \frac{W_g(R)(T)}{(P_T)(MW_g)} \]  

(Eq. 27)

Where:

\( V \) = volumetric flow rate of gas evolution
\( W_g \) = mass flow rate of gas evolution
\( R \) = ideal gas law constant
\( T \) = temperature at the exit, absolute
\( P_T \) = vessel pressure
\( MW_g \) = molecular weight of the evolved gas

(H) Air drying. Use Equation 28 of this subpart to calculate emissions from air drying:

\[ E = B \times \left( \frac{PS_1}{100 - PS_1} - \frac{PS_2}{100 - PS_2} \right) \]  

(Eq. 28)

Where:

\( E \) = mass of HAP emitted
\( B \) = mass of dry solids
\( PS_1 \) = HAP in material entering dryer, weight percent
\( PS_2 \) = HAP in material exiting dryer, weight percent.

(ii) Engineering assessments. The owner or operator shall conduct an engineering assessment to determine uncontrolled HAP emissions for each emission episode that is not due to vapor displacement, purging, heating, depressurization, vacuum systems, gas evolution, or air drying. For a given emission episode caused by any of these seven types of activities, the owner or operator also may request approval to determine uncontrolled HAP emissions based on an engineering assessment. All data, assumptions, and procedures used in the engineering assessment shall be documented in the Precompliance plan in accordance with §63.1367(b). An engineering assessment includes, but is not limited to, the information and procedures described in paragraphs (c)(2)(ii)(A) through (D) of this section:

(A) Test results, provided the tests are representative of current operating practices at the process unit. If test data show a greater than 20 percent discrepancy between the test value and
the estimated value, the owner or operator may estimate emissions based on the test data, and the results of the engineering assessment shall be included in the Notification of Compliance Status report.

(B) Bench-scale or pilot-scale test data representative of the process under representative operating conditions.

(C) Maximum flow rate, HAP emission rate, concentration, or other relevant parameter specified or implied within a permit limit applicable to the process vent.

(D) Design analysis based on accepted chemical engineering principles, measurable process parameters, or physical or chemical laws or properties. Examples of analytical methods include, but are not limited to:

1. Use of material balances based on process stoichiometry to estimate maximum organic HAP concentrations;
2. Estimation of maximum flow rate based on physical equipment design such as pump or blower capacities; and
3. Estimation of HAP concentrations based on saturation conditions.

(3) Controlled emissions. Except for condensers, the owner or operator shall determine controlled emissions using the procedures in either paragraph (c)(3)(i) or (ii) of this section, as applicable. For condensers, controlled emissions shall be calculated using the emission estimation equations described in paragraph (c)(3)(iii) of this section. The owner or operator is not required to calculate controlled emissions from devices described in paragraph (a)(4) of this section or from flares for which compliance is demonstrated in accordance with paragraph (a)(3) of this section. If the owner or operator is not complying with an outlet concentration standard and the control device uses supplemental gases, the outlet concentrations shall be corrected in accordance with the procedures described in paragraph (a)(7) of this section.

(i) Small control devices, except condensers. Controlled emissions for each process vent that is controlled using a small control device, except for a condenser, shall be determined by applying the control efficiency of the large control device to the estimated uncontrolled emissions. The control efficiency shall be determined by conducting a performance test on the control device as described in paragraphs (c)(3)(ii)(A) through (C) of this section, or by using the results of a previous performance test as described in paragraph (c)(3)(ii)(D) of this section. If the control device is intended to control only HCl and chlorine, the owner or operator may assume the control efficiency for organic HAP is 0 percent. If the control device is intended to control only organic HAP, the owner or operator may assume the control efficiency for HCl and chlorine is 0 percent.

(A) Except for control devices that are intended to meet outlet TOC or HCl and chlorine concentrations of 20 ppmv, the performance test shall be conducted by performing emission testing on the inlet and outlet of the control device following the test methods and procedures of paragraph (b) of this

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For control devices that meet outlet TOC or HCl and chlorine concentrations of 20 ppmv, the performance testing shall be conducted by performing emission testing on the outlet of the control device following the test methods and procedures of paragraph (b) of this section. Concentrations shall be calculated from the data obtained through emission testing according to the procedures in paragraph (a)(2) of this section.

(b) Performance testing shall be conducted under absolute or hypothetical peak-case conditions, as defined in paragraphs (b)(11)(i) and (ii) of this section.

(c) The owner or operator may elect to conduct more than one performance test on the control device for the purpose of establishing more than one operating condition at which the control device achieves the required control efficiency.

(d) The owner or operator is not required to conduct a performance test for any control device for which a previous performance test was conducted, provided the test was conducted using the same procedures specified in paragraphs (b)(1) through (11) of this section over conditions typical of the absolute or hypothetical peak-case, as defined in paragraphs (b)(11)(i) and (ii) of this section. The results of the previous performance test shall be used to demonstrate compliance.

(iii) Condensers. The owner or operator using a condenser as a control device shall determine controlled emissions using exhaust gas temperature measurements and calculations for each batch emission episode according to the engineering methodology in paragraphs (c)(3)(iii)(A) through (G) of this section. Individual HAP partial pressures shall be calculated as specified in paragraph (c)(2)(i) of this section.

(A) Emissions from vapor displacement due to transfer of material to a vessel shall be calculated using Equation 9 of this subpart with T set equal to the temperature of the receiver and the HAP partial pressures determined at the temperature of the receiver.

(B) Emissions from purging shall be calculated using Equation 10 of this subpart with T set equal to the temperature of the receiver and the HAP partial pressures determined at the temperature of the receiver.

(C) Emissions from heating shall be calculated using Equation 29 of this subpart. In Equation 29 of this subpart, \( \Delta \eta \) is equal to the number of moles of noncondensable gas displaced from the vessel, as calculated using Equation 12 of this subpart. In Equation 29 of this subpart, the HAP average molecular weight shall be calculated using Equation 14 with the HAP partial pressures determined at the temperature of the receiver.

\[
E = \Delta \eta \times \frac{\sum_{i=1}^{n} P_i}{P_T - \sum_{j=1}^{m} P_j} \times MW_{HAP} \quad \text{(Eq. 29)}
\]

Where:
- \( E \) = mass of HAP emitted
- \( \Delta \eta \) = moles of noncondensable gas displaced
- \( P_T \) = pressure in the receiver
- \( P_i \) = partial pressure of the individual HAP at the receiver temperature
- \( P_j \) = partial pressure of the individual condensable VOC (including HAP) at the receiver temperature
- \( MW_{HAP} \) = the average molecular weight of HAP in vapor exiting the receiver, as calculated using Equation 14 of this subpart
- \( n \) = number of HAP compounds in the emission stream
- \( m \) = number of condensable VOC (including HAP) in the emission stream

(D)(1) Emissions from depressurization shall be calculated using Equation 30 of this subpart.
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\[ E = (\sum_{i=1}^{n} P_i) \times \frac{\sum_{j=1}^{m} P_j}{P_T - \sum_{j=1}^{m} P_j} \times \frac{P_T}{RT} \times MW_{HAP} \]  

(Eq. 30)

Where:

- \( E \) = mass of HAP vapor emitted
- \( V_{nc1} \) = initial volume of noncondensable in the vessel, corrected to the final pressure, as calculated using Equation 31 of this subpart
- \( V_{nc2} \) = final volume of noncondensable in the vessel, as calculated using Equation 32 of this subpart
- \( P_i \) = partial pressure of each individual HAP at the receiver temperature
- \( P_j \) = partial pressure of each condensable VOC (including HAP) at the receiver temperature
- \( P_T \) = receiver pressure
- \( T \) = temperature of the receiver, absolute
- \( R \) = ideal gas law constant
- \( MW_{HAP} \) = the average molecular weight of HAP calculated using Equation 14 of this subpart with partial pressures determined at the receiver temperature
- \( n \) = number of HAP compounds in the emission stream
- \( m \) = number of condensable VOC (including HAP) in the emission stream

(3) Initial and final partial pressures of the noncondensable gas in the vessel are determined using Equations 33 and 34 of this subpart.

\[ P_{nc1} = P_1 - \sum_{j=1}^{m} P_j \]  

(Eq. 33)

\[ P_{nc2} = P_2 - \sum_{j=1}^{m} P_j \]  

(Eq. 34)

Where:

- \( P_{nc1} \) = initial partial pressure of the noncondensable gas in the vessel
- \( P_{nc2} \) = final partial pressure of the noncondensable gas in the vessel
- \( P_1 \) = initial vessel pressure
- \( P_2 \) = final vessel pressure
- \( P_j \) = partial pressure of each condensable VOC (including HAP) in the vessel
- \( m \) = number of condensable VOC (including HAP) in the emission stream

(E) Emissions from vacuum systems shall be calculated using Equation 26 of this subpart.

(F) Emissions from gas evolution shall be calculated using Equation 8 with \( V \) calculated using Equation 27 of this subpart, \( T \) set equal to the receiver temperature, and the HAP partial pressures determined at the receiver temperature. The term for time, \( t \), in Equation 10 of this subpart is not needed for the purposes of this calculation.

(G) Emissions from air drying shall be calculated using Equation 9 of this subpart with \( V \) equal to the air flow rate and \( P_i \) determined at the receiver temperature.

(d) Initial compliance with storage vessel provisions. The owner or operator of an existing or new affected source shall demonstrate initial compliance with the storage vessel standards in §63.1362(c)(2) through (4) by fulfilling the requirements in either paragraph.
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(d)(1), (2), (3), (4), (5), or (6) of this section, as applicable. The owner or operator shall demonstrate initial compliance with the planned routine maintenance provision in §63.1362(c)(5) by fulfilling the requirements in paragraph (d)(7) of this section.

(1) Percent reduction requirement for control devices. If the owner or operator equips a Group 1 storage vessel with a closed vent system and control device, the owner or operator shall demonstrate initial compliance with the percent reduction requirement of §63.1362(c)(2)(iv)(A) or (c)(3) either by calculating the efficiency of the control device using performance test data as specified in paragraph (d)(1)(i) of this section, or by preparing a design evaluation as specified in paragraph (d)(1)(ii) of this section.

(i) Performance test option. If the owner or operator elects to demonstrate initial compliance based on performance test data, the efficiency of the control device shall be calculated as specified in paragraphs (d)(3)(i)(A) through (D) of this subpart.

(A) At the reasonably expected maximum filling rate, Equations 35 and 36 of this subpart shall be used to calculate the mass rate of total organic HAP at the inlet and outlet of the control device.

\[
E_i = K_2 \left( \sum_{j=1}^{n} C_{ij} M_{ij} \right) Q_i \quad \text{(Eq. 35)}
\]

\[
E_o = K_2 \left( \sum_{j=1}^{n} C_{oj} M_{oj} \right) Q_o \quad \text{(Eq. 36)}
\]

Where:

- \( C_{ij} \) = concentration of sample component j of the gas stream at the inlet and outlet of the control device, respectively, dry basis, ppmv
- \( E_i \) = mass rate of total organic HAP at the inlet and outlet of the control device, respectively, dry basis, kg/hr
- \( M_{ij} \) = molecular weight of sample component j of the gas stream at the inlet and outlet of the control device, respectively, g/mole
- \( Q_i \), \( Q_o \) = flow rate of gas stream at the inlet and outlet of the control device, respectively, dscmm
- \( K_2 \) = constant, \( 2.494 \times 10^{-6} \) (parts per million)\(^{-1}\) (gram-mole per standard cubic meter) (kilogram/gram) (minute/hour), where standard temperature is 20 °C

(B) The percent reduction in total organic HAP shall be calculated using Equation 37 of this subpart:

\[
R = \frac{E_i - E_o}{E_i} \times 100 \quad \text{(Eq. 37)}
\]

Where:

- \( R \) = control efficiency of control device, percent
- \( E_i \) = mass rate of total organic HAP at the inlet to the control device calculated under paragraph (d)(3)(i)(A) of this section, kilograms organic HAP per hour
- \( E_o \) = mass rate of total organic HAP at the outlet of the control device, as calculated under paragraph (d)(3)(i)(A) of this section, kilograms organic HAP per hour

(C) A performance test is not required to be conducted if the control device used to comply with §63.1362(c) (storage tank provisions) is also used to comply with §63.1362(b) (process vent provisions), provided compliance with §63.1362(b) is demonstrated in accordance with paragraph (c) of this section and the demonstrated percent reduction is equal to or greater than 95 percent.

(D) A performance test is not required for any control device for which a previous test was conducted, provided the test was conducted using the same procedures specified in paragraph (b) of this section.

(ii) Design evaluation option. If the owner or operator elects to conduct a design evaluation, the owner or operator shall prepare documentation in accordance with the design evaluation provisions in paragraph (a)(1) of this section, as applicable. The design evaluation shall demonstrate that the control device being used achieves the required control efficiency when the storage vessel is filled at the reasonably expected maximum filling rate.

(2) Outlet concentration requirement for control devices. If the owner or operator equips a Group 1 storage vessel with a closed vent system and control device,
the owner or operator shall demonstrate initial compliance with the outlet concentration requirements of §63.1362(c)(2)(iv)(B) or (c)(3) by fulfilling the requirements of paragraph (a)(6) of this section.

(3) Floating roof. If the owner or operator equips a Group 1 storage vessel with a floating roof to comply with the provisions in §63.1362(c)(2) or (c)(3), the owner or operator shall demonstrate initial compliance by complying with the procedures described in paragraphs (d)(3)(i) and (ii) of this section.

(i) Comply with §63.119(b), (c), or (d) of subpart G of this part, as applicable, with the differences specified in §63.1362(d)(2)(i) through (iii).

(ii) Comply with the procedures described in §63.120(a), (b), or (c) of subpart G of this part, as applicable, with the differences specified in §63.1362(d)(2)(ii), (iv), and (v).

(4) Flares. If the owner or operator controls the emissions from a Group 1 storage vessel with a flare, initial compliance is demonstrated by fulfilling the requirements in paragraph (a)(3) of this section.

(5) Exemptions from initial compliance. No initial compliance demonstration is required for control devices specified in paragraph (a)(4) of this section.

(6) Initial compliance with alternative standard. If the owner or operator equips a Group 1 storage vessel with a closed-vent system and control device, the owner or operator shall demonstrate initial compliance with the alternative standard in §63.1362(c)(4) by fulfilling the requirements of paragraph (a)(5) of this section.

(7) Planned maintenance. The owner or operator shall demonstrate initial compliance with the planned maintenance provisions of §63.1362(c)(5) by including the anticipated periods of planned maintenance for the first reporting period in the Notification of Compliance Status report as specified in §63.1368(f).

(e) Initial compliance with wastewater provisions. The owner or operator shall demonstrate initial compliance with the wastewater requirements by complying with the applicable provisions in §63.145 of subpart G of this part, except that the owner or operator need not comply with the requirement to determine visible emissions that is specified in §63.145(j)(1) of subpart G of this part, and references to compounds in Table 8 of subpart G of this part are not applicable for the purposes of this subpart.

(f) Initial compliance with the bag dump and product dryer provisions. Compliance with the particulate matter concentration limits specified in §63.1362(e) is demonstrated when the concentration of particulate matter is less than 0.01 gr/dscf, as measured using the method described in paragraph (b)(7) of this section.

(g) Initial compliance with the pollution prevention alternative standard. The owner or operator shall demonstrate initial compliance with §63.1362(h)(2) and (3) for a PAI process unit by preparing the demonstration summary in accordance with paragraph (g)(1) of this section and by calculating baseline and target annual HAP and VOC factors in accordance with paragraphs (g)(2) and (3) of this section. To demonstrate initial compliance with §63.1362(h)(3), the owner or operator must also comply with the procedures for add-on control devices that are specified in paragraph (g)(4) of this section.

(1) Demonstration summary. The owner or operator shall prepare a pollution prevention demonstration summary that shall contain, at a minimum, the information in paragraphs (g)(1)(i) through (iii) of this section. The demonstration summary shall be included in the Precompliance report as specified in §63.1368(e)(4).

(i) Descriptions of the methodologies and forms used to measure and record consumption of HAP and VOC compounds.

(ii) Descriptions of the methodologies and forms used to measure and record production of the product(s).

(iii) Supporting documentation for the descriptions provided in accordance with paragraphs (g)(1)(i) and (ii) of this section including, but not limited to, operator log sheets and copies of daily, monthly, and annual inventories of materials and products. The owner or operator must show how this documentation will be used to calculate the annual factors required in §63.1368(f)(1).

(2) Baseline factors. The baseline HAP and VOC factors shall be calculated by
dividing the consumption of total HAP and total VOC by the production rate, per process, for the first 3-year period in which the process was operational, beginning no earlier than the period consisting of the 1987 through 1989 calendar years. Alternatively, for a process that has been operational for less than 3 years, but more than 1 year, the baseline factors shall be established for the time period from startup of the process until the present.

(3) Target annual factors. The owner or operator must calculate target annual factors in accordance with either paragraph (g)(3)(i) or (ii) of this section.

(i) To demonstrate initial compliance with §63.1362(h)(2), the target annual HAP factor must be equal to or less than 15 percent of the baseline HAP factor. For each reduction in a HAP that is also a VOC, the target annual VOC factor must be lower than the baseline VOC factor by an equivalent amount on a mass basis. For each reduction in a HAP that is not a VOC, the target annual factor must be equal to or less than the baseline VOC factor.

(ii) To demonstrate initial compliance with §63.1362(h)(3)(i), the target annual HAP and VOC factors must be calculated as specified in paragraph (g)(3)(i) of this section, except that when “15 percent” is referred to in paragraph (g)(3)(i) of this section, “50 percent” shall apply for the purposes of this paragraph.

(4) Requirements for add-on control devices. Initial compliance with the requirements for add-on control devices in §63.1362(h)(3)(ii) is demonstrated when the requirements in paragraphs (g)(4)(i) through (iii) of this section are met.

(i) The yearly reductions associated with add-on controls that meet the criteria of §63.1362(h)(3)(ii)(A) through (D), must be equal to or greater than the amounts calculated using Equations 38 and 39 of this subpart:

\[
\text{HAP reduced} = \left( \text{HF}_{\text{base}} \right) \left( 0.85 - R_{p2} \right) M_{\text{prod}} \quad \text{(Eq. 38)}
\]

\[
\text{VOC reduced} = \left( \text{VF}_{\text{base}} - \text{VF}_{p2} - \text{VF}_{\text{annual}} \right) \times M_{\text{prod}} \quad \text{(Eq. 39)}
\]

Where:

- HAP reduced = the annual HAP emissions reduction required by add-on controls, kg/yr
- HF base = the baseline HAP factor, kg HAP consumed/kg product
- R p2 = the fractional reduction in the annual HAP factor achieved using pollution prevention where R p2 is ≥0.5
- VOC reduced = required VOC emission reduction from add-on controls, kg/yr
- VF base = baseline VOC factor, kg VOC emitted/kg production
- VF p2 = reduction in VOC factor achieved by pollution prevention, kg VOC emitted/kg production
- VF annual = target annual VOC factor, kg VOC emitted/kg production
- M prod = production rate, kg/yr

(ii) Demonstration that the criteria in §63.1362(h)(3)(ii)(A) through (D) are met shall be accomplished through a description of the control device and of the material streams entering and exiting the control device.

(iii) The annual reduction achieved by the add-on control shall be quantified using the methods described in paragraph (c) of this section.

(h) Compliance with emissions averaging provisions. An owner or operator shall demonstrate compliance with the emissions averaging provisions of §63.1362(h) by fulfilling the requirements of paragraphs (h)(1) through (6) of this section.

(1) The owner or operator shall develop and submit for approval an Emissions Averaging Plan containing all the information required in §63.1367(d). The Emissions Averaging Plan shall be submitted no later than 18 months prior to the compliance date of the standard. The Administrator shall determine within 120 calendar days whether the Emissions Averaging Plan submitted by sources using emissions averaging presents sufficient information. The Administrator shall either
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approve the Emissions Averaging Plan, request changes, or request that the owner or operator submit additional information. Once the Administrator receives sufficient information, the Administrator shall approve, disapprove, or request changes to the plan within 120 days. If the Emissions Averaging Plan is disapproved, the owner or operator must still be in compliance with the standard by the compliance date.

(2) For all points included in an emissions average, the owner or operator shall comply with the procedures that are specified in paragraphs (h)(2)(i) through (v) of this section.

(i) Calculate and record monthly debits for all Group 1 emission points that are controlled to a level less stringent than the standard for those emission points. Equations in paragraph (h)(5) of this section shall be used to calculate debits.

(ii) Calculate and record monthly credits for all Group 1 and Group 2 emission points that are overcontrolled to compensate for the debits. Equations in paragraph (h)(6) of this section shall be used to calculate credits.

(iii) Demonstrate that annual credits calculated according to paragraph (h)(5) of this section is greater than or equal to debits calculated according to paragraph (h)(5) of this section for the same annual compliance period. The initial demonstration in the Emissions Averaging Plan or operating permit application that credit-generating emission points will be capable of generating sufficient credits to offset the debit-generating emission points shall be made under representative operating conditions. After the compliance date, actual operating data shall be used for all debit and credit calculations.

(iv) Demonstrate that debits calculated for a quarterly (3-month) period according to paragraph (h)(5) of this section are not more than 1.30 times the credits for the same period calculated according to paragraph (h)(6) of this section. Compliance for the quarter shall be determined based on the ratio of credits and debits from that quarter, with 30 percent more debits than credits allowed on a quarterly basis.

(v) Record and report quarterly and annual credits and debits as required in §§ 63.1367(d) and 63.1368(d).

(3) Credits and debits shall not include emissions during periods of malfunction. Credits and debits shall not include periods of startup and shutdown for continuous processes.

(4) During periods of monitoring excursions, credits and debits shall be adjusted as specified in paragraphs (h)(4)(i) through (iii) of this section.

(i) No credits shall be assigned to the credit-generating emission point.

(ii) Maximum debits shall be assigned to the debit-generating emission point.

(iii) The owner or operator may demonstrate to the Administrator that full or partial credits or debits shall be assigned using the procedures in § 63.150(l) of subpart G of this part.

(5) Debits are generated by the difference between the actual emissions from a Group 1 emission point that is uncontrolled or controlled to a level less stringent than the applicable standard and the emissions allowed for the Group 1 emission point. Debits shall be calculated in accordance with the procedures specified in paragraphs (h)(5)(i) through (iv) of this section.

(i) Source-wide debits shall be calculated using Equation 40 of this subpart.

Debits and all terms of Equation 40 of this subpart are in units of Mg/month.

Where:

\[
\text{Debits} = \sum_{i}^{n} [\text{EPV}_{iA} - (0.10)(\text{EPV}_{iU})] + \sum_{i}^{n} [\text{ES}_{iA} - (0.05)(\text{ES}_{iU})] + \sum_{i}^{n} [\text{EWWW}_{iA} - (\text{EWWW}_{iC})] \quad (\text{Eq. 40})
\]
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EPV_i = uncontrolled emissions from process i calculated according to the procedures specified in paragraph (h)(5)(ii) of this section

EPV_A = actual emissions from each Group 1 process i that is uncontrolled or is controlled to a level less stringent than the applicable standard. EPV_A is calculated using the procedures in paragraph (h)(5)(ii) of this section

ES_i = uncontrolled emissions from storage vessel i calculated according to the procedures specified in paragraph (h)(5)(iii) of this section

ES_A = actual emissions from each Group 1 storage vessel i that is uncontrolled or is controlled to a level less stringent than the applicable standard. ES_A is calculated using the procedures in paragraph (h)(5)(iii) of this section

EWW_i = uncontrolled emissions from wastewater stream i calculated according to the procedures specified in paragraph (h)(5)(iv) of this section

EWW_A = actual emissions from each Group 1 wastewater stream i that is uncontrolled or is controlled to a level less stringent than the applicable standard. EWW_A is calculated using the procedures in paragraph (h)(5)(iv) of this section

n = the number of emission points being included in the emissions average; the value of n is not necessarily the same for process vents, storage tanks, and wastewater

(ii) Emissions from process vents shall be calculated in accordance with the procedures specified in paragraphs (h)(5)(ii)(A) through (C) of this section.

(A) Except as provided in paragraph (h)(5)(ii)(C) of this section, uncontrolled emissions for process vents shall be calculated using the procedures specified in paragraphs (h)(5)(ii)(A) through (C) of this section, as applicable.

(B) Except as provided in paragraph (h)(5)(ii)(C) of this section, actual emissions for process vents shall be calculated using the procedures specified in paragraphs (c)(2) and (c)(3) of this section, as applicable.

(C) As an alternative to the procedures described in paragraphs (h)(5)(ii)(A) and (B) of this section, for continuous processes, uncontrolled and actual emissions may be calculated by the procedures described in §63.150(g)(2)

of subpart G of this part. For purposes of complying with this paragraph, a 90 percent reduction shall apply instead of the 98 percent reduction in §63.150(g)(2)(iii) of subpart G of this part, and the term “process condenser” shall apply instead of the term “recovery device” in §63.150(g)(2) for the purposes of this subpart.

(iii) Uncontrolled emissions from storage vessels shall be calculated in accordance with the procedures described in paragraph (d)(1) of this section. Actual emissions from storage vessels shall be calculated using the procedures specified in §63.150(g)(3)(ii), (iii), or (iv) of subpart G of this subpart, as appropriate, except that when §63.150(g)(3)(ii)(B) refers to the procedures in §63.120(d) for determining percent reduction for a control device, §63.1365(d)(2) or (3) shall apply for the purposes of this subpart.

(iv) Emissions from wastewater shall be calculated using the procedures specified in §63.150(g)(5) of subpart G of this part.

(6) Credits are generated by the difference between emissions that are allowed for each Group 1 and Group 2 emission point and the actual emissions from that Group 1 or Group 2 emission point that have been controlled after November 15, 1990 to a level more stringent than what is required in this subpart or any other State or Federal rule or statute. Credits shall be calculated in accordance with the procedures specified in paragraphs (h)(6)(i) through (v) of this section.

(i) Source-wide credits shall be calculated using Equation 41 of this subpart. Credits and all terms in Equation 41 of this subpart are in units of Mg/month, the baseline date is November 15, 1990, the terms consisting of a constant multiplied by the uncontrolled emissions are the emissions from each emission point subject to the standards in §63.1362(b) and (c) that is controlled to a level more stringent than the standard.

Where:
Credits = \[ D \sum_{i=1}^{n} [0.10(EPV_{1 \text{IA}}) - EPV_{1 \text{U}}] + D \sum_{i=1}^{m} (EPV_{2 \text{IB}} - EPV_{2 \text{IA}}) + D \sum_{i=1}^{n} [0.05(ES_{1 \text{IB}}) - ES_{1 \text{IA}}] +
\]
\[ D \sum_{i=1}^{m} (ES_{2 \text{IB}} - ES_{2 \text{IA}}) + D \sum_{i=1}^{n} (EWW_{1 \text{IC}} - EWW_{1 \text{IA}}) + D \sum_{i=1}^{m} (EWW_{2 \text{IB}} - EWW_{2 \text{IA}}) \]  \hspace{1cm} (Eq. 41)

EPV_{1 \text{U}} = uncontrolled emissions from each Group 1 process i calculated according to the procedures in paragraph (h)(6)(iii)(A) of this section

EPV_{1 \text{IA}} = actual emissions from each Group 1 process i that is controlled to a level more stringent than the applicable standard. EPV_{1 \text{IA}} is calculated according to the procedures in paragraph (h)(6)(iii)(B) of this section

EPV_{2 \text{IB}} = emissions from each Group 2 process i at the baseline date. EPV_{2 \text{IB}} is calculated according to the procedures in paragraph (h)(6)(iii)(C) of this section

EPV_{2 \text{IA}} = actual emissions from each Group 2 process i that is controlled. EPV_{2 \text{IA}} is calculated according to the procedures in paragraph (h)(6)(iii)(C) of this section

ES_{1 \text{IB}} = uncontrolled emissions from each Group 1 storage vessel i calculated according to the procedures in paragraph (h)(6)(iv) of this section

ES_{1 \text{IA}} = actual emissions from each Group 1 storage vessel i that is controlled to a level more stringent that the applicable standard. ES_{1 \text{IA}} is calculated according to the procedures in paragraph (h)(6)(iv) of this section

ES_{2 \text{IB}} = emissions from each Group 2 storage vessel i at the baseline date. ES_{2 \text{IB}} is calculated according to the procedures in paragraph (h)(6)(iv) of this section

ES_{2 \text{IA}} = actual emissions from each Group 2 storage vessel i that is controlled. ES_{2 \text{IA}} is calculated according to the procedures in paragraph (h)(6)(iv) of this section

EWW_{1 \text{IC}} = emissions from each Group 1 wastewater stream i if the standard had been applied to the uncontrolled emissions. EWW_{1 \text{IC}} is calculated according to the procedures in paragraph (h)(6)(v) of this section

EWW_{1 \text{IA}} = actual emissions from each Group 1 wastewater stream i that is controlled to a level more stringent that the applicable standard. EWW_{1 \text{IA}} is calculated according to the procedures in paragraph (h)(6)(v) of this section

EWW_{2 \text{IB}} = emissions from each Group 2 wastewater stream i at the baseline date. EWW_{2 \text{IB}} is calculated according to the procedures in paragraph (h)(6)(v) of this section

EWW_{2 \text{IA}} = actual emissions from each Group 2 wastewater stream i that is controlled. EWW_{2 \text{IA}} is calculated according to the procedures in paragraph (h)(6)(v) of this section

\( n \) = number of Group 1 emission points that are included in the emissions average. The value of \( n \) is not necessarily the same for process vents, storage tanks, and wastewater

\( m \) = number of Group 2 emission points included in the emissions average. The value of \( m \) is not necessarily the same for process vents, storage tanks, and wastewater

\( D \) = discount factor equal to 0.9 for all credit-generating emission points except those controlled by a pollution prevention measure, which will not be discounted

\( (ii) \) For an emission point controlled using a pollution prevention measure, the nominal efficiency for calculating credits shall be as determined as described in §63.150(j) of subpart G of this part.

\( (iii) \) Emissions from process vents shall be calculated in accordance with the procedures specified in paragraphs (h)(6)(iii)(A) through (C) of this section.

(A) Uncontrolled emissions from Group 1 process vents shall be calculated according to the procedures in paragraph (h)(5)(iii)(A) through (C) of this section.

(B) Actual emissions from Group 1 process vents with a nominal efficiency greater than the applicable standard or a pollution prevention measure that achieves reductions greater than the applicable standard shall be calculated using Equation 42 of this subpart:

\[ EPV_{1 \text{IA}} = EPV_{1 \text{IU}} \times [1 - N_{\text{eff}} / 100] \]  \hspace{1cm} (Eq. 42)
§ 63.1366 Monitoring and inspection requirements.

(a) To provide evidence of continued compliance with the standard, the owner or operator of any existing or new affected source shall install, operate, and maintain monitoring devices as specified in this section. During the initial compliance demonstration, maximum or minimum operating parameter levels, or other design and operating characteristics, as appropriate, shall be established for emission sources that will indicate the source is in compliance. Test data, calculations, or information from the evaluation of the control device design, as applicable, shall be used to establish the operating parameter level or characteristic.

(b) Monitoring for control devices. (1) Parameters to monitor. Except as specified in paragraph (b)(1)(i) of this section, for each control device, the owner or operator shall install and operate monitoring devices and operate within the established parameter levels to ensure continued compliance with the standard. Monitoring parameters are specified for control scenarios in paragraphs (b)(1)(ii) through (xii) of this section, and are summarized in Table 3 of this subpart.

(i) Periodic verification. For control devices that control vent streams containing total HAP emissions less than 0.91 Mg/yr, before control, monitoring shall consist of a periodic verification that the device is operating properly. This verification shall include, but not be limited to, a daily or more frequent demonstration that the unit is working as designed and may include the daily measurements of the parameters described in paragraphs (b)(1)(ii) through (xii) of this section. This demonstration shall be included in the Precompliance plan, to be submitted 6 months prior to the compliance date of the standard.

(ii) Scrubbers. For affected sources using liquid scrubbers, the owner or operator shall establish a minimum scrubber liquid flow rate or pressure drop as a site-specific operating parameter which must be measured and recorded at least once every 15 minutes during the period in which the scrubber is controlling HAP from an emission stream as required by the standards in § 63.1362. If the scrubber uses a caustic solution to remove acid emissions, the pH of the effluent scrubber liquid shall also be monitored once a day. The minimum scrubber liquid flow rate or pressure drop shall be based on the conditions under which the initial compliance demonstration was conducted.

(A) The monitoring device used to determine the pressure drop shall be certified by the manufacturer to be accurate to within a gage pressure of ±10 percent of the maximum pressure drop measured.

(B) The monitoring device used for measurement of scrubber liquid flow rate shall be certified by the manufacturer to be accurate to within ±10 percent of the design scrubber liquid flow rate.
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(C) The monitoring device shall be calibrated annually.

(iii) Condensers. For each condenser, the owner or operator shall establish the maximum condenser outlet gas temperature as a site-specific operating parameter which must be measured and recorded at least once every 15 minutes during the period in which the condenser is controlling HAP from an emission stream as required by the standards in §63.1362.

(A) The temperature monitoring device must be accurate to within ±2 percent of the temperature measured in degrees Celsius or ±2.5°C, whichever is greater.

(B) The temperature monitoring device must be calibrated annually.

(iv) Regenerative carbon adsorbers. For each regenerative carbon adsorber, the owner or operator shall comply with the provisions in paragraphs (b)(1)(iv)(A) through (F) of this section.

(A) Establish the regeneration cycle characteristics specified in paragraphs (b)(1)(iv)(A) (1) through (4) of this section under absolute or hypothetical peak-case conditions, as defined in §63.1365(b)(11)(i) or (ii).

(1) Minimum regeneration frequency (i.e., operating time since last regeneration);

(2) Minimum temperature to which the bed is heated during regeneration;

(3) Maximum temperature to which the bed is cooled, measured within 15 minutes of completing the cooling phase; and

(4) Minimum regeneration stream flow.

(B) Monitor and record the regeneration cycle characteristics specified in paragraphs (b)(1)(iv)(B) (1) through (4) of this section for each regeneration cycle.

(1) Regeneration frequency (i.e., operating time since end of last regeneration);

(2) Temperature to which the bed is heated during regeneration;

(3) Temperature to which the bed is cooled, measured within 15 minutes of the completion of the cooling phase; and

(4) Regeneration stream flow.

(C) Use a temperature monitoring device that is accurate to within ±2 percent of the temperature measured in degrees Celsius or ±2.5°C, whichever is greater.

(D) Use a regeneration stream flow monitoring device capable of recording the total regeneration stream flow to within ±10 percent of the established value (i.e., accurate to within ±10 percent of the reading).

(E) Calibrate the temperature and flow monitoring devices annually.

(F) Conduct an annual check for bed poisoning in accordance with manufacturer’s specifications.

(v) Nonregenerative carbon adsorbers. For each nonregenerative carbon adsorption system such as a carbon canister that does not regenerate the carbon bed directly onsite in the control device, the owner or operator shall replace the existing carbon bed in the control device with fresh carbon on a regular schedule based on one of the following procedures:

(A) Monitor the TOC concentration level in the exhaust vent stream from the carbon adsorption system on a regular schedule, and replace the existing carbon with fresh carbon immediately when carbon breakthrough is indicated. The monitoring frequency shall be daily or at an interval no greater than 20 percent of the time required to consume the total carbon working capacity under absolute or hypothetical peak-case conditions as defined in §63.1365(b)(11)(i) or (ii).

(1) Minimum replacement frequency (i.e., operating time since last replacement);

(2) Temperature to which the bed is heated during replacement;

(3) Temperature to which the bed is cooled, measured within 15 minutes of the completion of the cooling phase; and

(4) Minimum replacement stream flow.

(B) Establish the maximum time interval between replacement, and replace the existing carbon before this time interval elapses. The time interval shall be established based on the conditions anticipated under absolute or hypothetical peak-case, as defined in §63.1365(b)(11)(i) or (ii), whichever is longer.

(B) Establish the maximum time interval between replacement, and replace the existing carbon before this time interval elapses. The time interval shall be established based on the conditions anticipated under absolute or hypothetical peak-case, as defined in §63.1365(b)(11)(i) or (ii).

(vi) Flares. For each flare, the presence of the pilot flame shall be monitored at least once every 15 minutes during the period in which the flare is controlling HAP from an emission stream subject to the standards in §63.1362. The monitoring device shall be calibrated annually.

(vii) Thermal incinerators. For each thermal incinerator, the owner or operator shall monitor the temperature of the gases exiting the combustion chamber as the site-specific operating parameter which must be measured...
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and recorded at least once every 15 minutes during the period in which the combustion device is controlling HAP from an emission stream subject to the standards in §63.1362.

(A) The temperature monitoring device must be accurate to within ±0.75 percent of the temperature measured in degrees Celsius or ±2.5°C, whichever is greater.

(B) The monitoring device must be calibrated annually.

(viii) Catalytic incinerators. For each catalytic incinerator, the parameter levels that the owner or operator shall establish are the minimum temperature of the gas stream immediately before the catalyst bed and the minimum temperature difference across the catalyst bed. The owner or operator shall monitor the temperature of the gas stream immediately before and after the catalyst bed, and calculate the temperature difference across the catalyst bed, at least once every 15 minutes during the period in which the catalytic incinerator is controlling HAP from an emission stream subject to the standards in §63.1362.

(A) The temperature monitoring devices must be accurate to within ±0.75 percent of the temperature measured in degrees Celsius or ±2.5°C, whichever is greater.

(B) The temperature monitoring devices must be calibrated annually.

(ix) Process heaters and boilers. (A) Except as specified in paragraph (b)(1)(ix)(B) of this section, for each boiler or process heater, the owner or operator shall monitor the temperature of the gases exiting the combustion chamber as the site-specific operating parameter which must be monitored and recorded at least every 15 minutes during the period in which the boiler or process heater is controlling HAP from an emission stream subject to the standards in §63.1362.

(1) The temperature monitoring device must be accurate to within ±0.75 percent of the temperature measured in degrees Celsius or ±2.5°C, whichever is greater.

(2) The temperature monitoring device must be calibrated annually.

(B) The owner or operator is exempt from the monitoring requirements specified in paragraph (b)(1)(ix)(A) of this section if either:

(1) All vent streams are introduced with primary fuel; or

(2) The design heat input capacity of the boiler or process heater is 44 megawatts or greater.

(x) Continuous emission monitor. As an alternative to the parameters specified in paragraphs (b)(1)(ii) through (ix) of this section, an owner or operator may monitor and record the outlet HAP concentration or both the outlet TOC concentration and outlet total HCl and chlorine concentration at least every 15 minutes during the period in which the control device is controlling HAP from an emission stream subject to the standards in §63.1362. The owner or operator need not monitor the total HCl and chlorine concentration if the owner or operator determines that the emission stream does not contain HCl or chlorine. The owner or operator need not monitor the TOC concentration if the owner or operator determines the emission stream does not contain organic compounds. The HAP or TOC monitor must meet the requirements of Performance Specification 8 or 9 of appendix B of part 60 and must be installed, calibrated, and maintained, according to §63.8 of subpart A of this part. As part of the QA/QC Plan, calibration of the device must include, at a minimum, quarterly cylinder gas audits. If supplemental gases are introduced before the control device, the monitored concentration shall be corrected as specified in §63.1365(a)(7).

(xi) Fabric filters. For each fabric filter used to control particulate matter emissions from bag dumps and product dryers subject to §63.1362(e), the owner or operator shall install, calibrate, maintain, and continuously operate a bag leak detection system that meets the requirements in paragraphs (b)(1)(xi)(A) through (G) of this section.

(A) The bag leak detection system sensor must provide output of relative particulate matter emissions.

(B) The bag leak detection system must be equipped with an alarm system that will sound when an increase in particulate matter emissions over a preset level is detected.
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(C) For positive pressure fabric filters, a bag leak detector must be installed in each fabric filter compartment or cell. If a negative pressure or induced air filter is used, the bag leak detector must be installed downstream of the fabric filter. Where multiple bag leak detectors are required (for either type of fabric filter), the system instrumentation and alarm may be shared among detectors.

(D) The bag leak detection system shall be installed, operated, calibrated and maintained in a manner consistent with available guidance from the U.S. Environmental Protection Agency or, in the absence of such guidance, the manufacturer’s written specifications and instructions.

(E) Calibration of the system shall, at a minimum, consist of establishing the relative baseline output level by adjusting the range and the averaging period of the device and establishing the alarm set points and the alarm delay time.

(F) Following initial adjustment, the owner or operator shall not adjust the sensitivity or range, averaging period, alarm set points, or alarm delay time, except as established in an operation and maintenance plan that is to be submitted with the Precompliance plan. In no event shall the sensitivity be increased more than 100 percent or decreased by more than 50 percent over a 365-day period unless such adjustment follows a complete baghouse inspection which demonstrates the baghouse is in good operating condition.

(G) If the alarm on a bag leak detection system is triggered, the owner or operator shall, within 1 hour of an alarm, initiate the procedures to identify the cause of the alarm and take corrective action as specified in the corrective action plan.

(xiii) Closed-vent system visual inspections. The owner or operator shall perform monthly visual inspections of each closed vent system as specified in §63.1362(j).

(2) Averaging periods. Averaging periods for parametric monitoring levels shall be established according to paragraphs (b)(2)(i) through (iii) of this section.

(i) Except as provided in paragraph (b)(2)(iii) of this section, a daily (24-hour) or block average shall be calculated as the average of all values for a monitored parameter level set according to the procedures in (b)(3)(iii) of this section recorded during the operating day or block.

(ii) The operating day or block shall be defined in the Notification of Compliance Status report. The operating day may be from midnight to midnight or another continuous 24-hour period. The operating block may be used as an averaging period only for vents from batch operations, and is limited to a period of time that is, at a maximum, equal to the time from the beginning to end of a series of consecutive batch operations.

(iii) Monitoring values taken during periods in which the control devices are not controlling HAP from an emission stream subject to the standards in §63.1362, as indicated by periods of no flow or periods when only streams that are not subject to the standards in §63.1362 are controlled, shall not be considered in the averages. Where flow to the device could be intermittent, the owner or operator shall install, calibrate and operate a flow indicator at the inlet or outlet of the control device to identify periods of no flow.

(3) Procedures for setting parameter levels for control devices used to control emissions from process vents. (i) Small control devices. Except as provided in paragraph (b)(1)(i) of this section, for devices controlling less than 10 tons/yr of HAP for which a performance test is not required, the parametric levels shall be set based on the design evaluation required in §63.1365(c)(3)(i)(A). If a performance test is conducted, the
monitoring parameter level shall be established according to the procedures in paragraph (b)(3)(ii) of this section.

(ii) Large control devices. For devices controlling greater than or equal to 10 tons/yr of HAP for which a performance test is required, the parameter level must be established as follows:

(A) If the operating parameter level to be established is a maximum or minimum, it must be based on the average of the average values from each of the three test runs.

(B) The owner or operator may establish the parametric monitoring level(s) based on the performance test supplemented by engineering assessments and/or manufacturer’s recommendations. Performance testing is not required to be conducted over the entire range of expected parameter values. The rationale for the specific level for each parameter, including any data and calculations used to develop the level(s) and a description of why the level indicates proper operation of the control device shall be provided in the Precompliance plan. Determination of the parametric monitoring level using these procedures is subject to review and approval by the Administrator.

(iii) Parameter levels for control devices controlling batch process vents. For devices controlling batch process vents alone or in combination with other streams, the level(s) shall be established in accordance with paragraph (b)(3)(iii)(A) or (B) of this section.

(A) A single level for the batch process(es) shall be calculated from the initial compliance demonstration.

(B) The owner or operator may establish separate levels for each batch emission episode or combination of emission episodes selected to be controlled. If separate monitoring levels are established, the owner or operator must provide a record indicating at what point in the daily schedule or log of processes required to be recorded per the requirements of §63.1367(b)(7), the parameter being monitored changes levels and must record at least one reading of the new parameter level, even if the duration of monitoring for the new parameter level is less than 15 minutes.

(4) Requesting approval to monitor alternative parameters. The owner or operator may request approval to monitor parameters other than those required by paragraphs (b)(1)(ii) through (xiii) of this section. The request shall be submitted according to the procedures specified in §63.8(f) of subpart A of this part or in the Precompliance report (as specified in §63.1368(e)).

(5) Monitoring for the alternative standards. For control devices that are used to comply with the provisions of §63.1362(b)(6) and (c)(4), the owner or operator shall monitor and record the outlet TOC concentration and the outlet total HCl and chlorine concentration at least once every 15 minutes during the period in which the device is controlling HAP from emission streams subject to the standards in §63.1362. A TOC monitor meeting the requirements of Performance Specification 8 or 9 of appendix B of 40 CFR part 60 shall be installed, calibrated, and maintained, according to §63.8 of subpart A of this part. The owner or operator need not monitor the total HCl and chlorine concentration if the owner or operator determines that the emission stream does not contain HCl or chlorine. The owner or operator need not monitor for TOC concentration if supplemental gases are introduced before the control device, the monitored concentration shall be corrected as specified in §63.1365(a)(7).

(6) Exceedances of operating parameters. An exceedance of an operating parameter is defined as one of the following:

(i) If the parameter level, averaged over the operating day or block, is below a minimum value established during the initial compliance demonstration.

(ii) If the parameter level, averaged over the operating day or block, is above the maximum value established during the initial compliance demonstration.

(iii) A loss of all pilot flames for a flare during an operating day or block. Multiple losses of all pilot flames during an operating day constitutes one exceedance.
(iv) Each operating day or block for which the time interval between replacement of a nonregenerative carbon adsorber exceeds the interval established in paragraph (b)(1)(iv) of this section.

(v) Each instance in which procedures to initiate the response to a bag leak detector alarm within 1 hour of the alarm as specified in the corrective action plan.

(7) Excursions. Excursions are defined by either of the two cases listed in paragraph (b)(7)(i) or (ii) of this section. An excursion also occurs if the periodic verification for a small control device is not conducted as specified in paragraph (b)(1)(i) of this section.

(i) When the period of control device operation is 4 hours or greater in an operating day or block and monitoring data are insufficient to constitute a valid hour of data, as defined in paragraph (b)(7)(iii) of this section, for at least 75 percent of the operating hours.

(ii) When the period of control device operation is less than 4 hours in an operating day or block and more than 1 of the hours during the period of operation does not constitute a valid hour of data due to insufficient monitoring data.

(iii) Monitoring data are insufficient to constitute a valid hour of data, as used in paragraphs (b)(7)(i) and (ii) of this section, if measured values are unavailable for any of the required 15-minute periods within the hour.

(8) Violations. Exceedances of parameters monitored according to the provisions of paragraphs (b)(1)(ii) and (b)(1)(iv) through (ix) of this section or excursions as defined by paragraphs (b)(7)(i) and (ii) of this section constitute violations of the operating limit according to paragraphs (b)(8)(i), (ii), and (iv) of this section. Exceedances of the temperature limit monitored according to the provisions of paragraph (b)(1)(iii) of this section or exceedances of the outlet concentrations monitored according to the provisions of paragraph (b)(1)(x) of this section constitute violations of the emission limit according to paragraphs (b)(8)(i), (ii), and (iv) of this section. Exceedances of the outlet concentrations monitored according to the provisions of paragraph (b)(5) of this section constitute violations of the emission limit according to the provisions of paragraphs (b)(8)(iii) and (iv) of this section.

(i) Except as provided in paragraph (b)(8)(iv) of this section, for episodes occurring more than once per day, exceedances of established parameter limits or excursions will result in no more than one violation per operating day for each monitored item of equipment utilized in the process.

(ii) Except as provided in paragraph (b)(8)(iv) of this section, for control devices used for more than one process in the course of an operating day, exceedances or excursions will result in no more than one violation per operating day, per control device, for each process for which the control device is in service.

(iii) Except as provided in paragraph (b)(8)(iv) of this section, exceedances of the 20 ppmv TOC outlet emission limit, averaged over the operating day, will result in no more than one violation per day per control device. Except as provided in paragraph (b)(8)(iv) of this section, exceedances of the 20 ppmv HCl and chlorine outlet emission limit, averaged over the operating day, will result in no more than one violation per day per control device.

(iv) Periods of time when monitoring measurements exceed the parameter values as well as periods of inadequate monitoring data do not constitute a violation if they occur during a startup, shutdown, or malfunction, and the facility follows its startup, shutdown, and malfunction plan.

(c) Monitoring for uncontrolled emission rates. The owner or operator shall demonstrate continuous compliance with the emission limit in §63.1362 (b)(2)(i) or (b)(4)(i) by calculating daily a 365-day rolling summation of uncontrolled emissions based on the uncontrolled emissions per emission episode, as calculated using the procedures in §63.1365(c)(2), and records of the number of batches produced. Each day that the summation for a process exceeds 0.15 Mg/yr is considered a violation of the emission limit.

(d) Monitoring for equipment leaks. The standard for equipment leaks is based
§ 63.1367 Recordkeeping requirements.

(a) Requirements of subpart A of this part. The owner or operator of an affected source shall comply with the recordkeeping requirements in subpart A of this part as specified in Table 1 of this subpart and in paragraphs (a)(1) through (5) of this section.

(1) Data retention. Each owner or operator of an affected source shall keep copies of all records and reports required by this subpart for at least 5 years, as specified in §63.10(b)(1) of subpart A of this part.

(2) Records of applicability determinations. The owner or operator of a stationary source that is not subject to this subpart shall keep a record of the applicability determination, as specified in §63.10(b)(3) of subpart A of this part.

(3) Startup, shutdown, and malfunction plan. The owner or operator of an affected source shall develop and implement a written startup, shutdown, and malfunction plan as specified in §63.6(e)(3) of subpart A of this part. This plan shall describe, in detail, procedures for operating and maintaining the affected source during periods of startups, shutdowns, and malfunctions and a program for corrective action for a malfunctioning process, air pollution control, and monitoring equipment used to comply with this subpart. The owner or operator of an affected source shall keep current and superseded versions of this plan onsite, as specified in §63.6(e)(3)(v) of subpart A of this part. The owner or operator shall keep the startup, shutdown, and malfunction records specified in paragraphs (b)(3)(i) through (iii) of this section. Reports related to the plan shall be submitted as specified in §63.1368(1).

(i) The owner or operator shall record the occurrence and duration of each malfunction of air pollution control equipment used to comply with this subpart, as specified in §63.6(e)(3)(iii) of subpart A of this part.

(4) Monitoring for emissions averaging. The owner or operator of an affected source that chooses to comply with the requirements of §63.1362(h) shall meet all monitoring requirements specified in paragraph (b) of this section, as applicable, for all processes, storage tanks, and waste management units included in the emissions average.

§ 63.1367 Monitoring requirements.

(e) Monitoring for heat exchanger systems. The standard for heat exchanger systems is based on monitoring. All monitoring requirements for heat exchanger systems are specified in §63.1362(f).

(f) Monitoring for the pollution prevention alternative standard. The owner or operator of an affected source that chooses to comply with the requirements of §63.1362(g) (2) or (3) shall calculate annual rolling average values of the HAP and VOC factors in accordance with the procedures specified in paragraph (f)(1) of this section. If complying with §63.1362(g)(3), the owner or operator shall also comply with the monitoring requirements specified in paragraph (b) of this section for the applicable add-on air pollution control device.

(1) Annual factors. The annual HAP and VOC factors shall be calculated in accordance with the procedures specified in paragraphs (f)(1) (i) through (iii) of this section.

(i) The consumption of both total HAP and total VOC shall be divided by the production rate, per process, for 12-month periods at the frequency specified in either paragraph (f)(1) (ii) or (iii) of this section, as applicable.

(ii) For continuous processes, the annual factors shall be calculated every 30 days for the 12-month period preceding the 30th day (annual rolling average calculated every 30 days). A process with both batch and continuous operations is considered a continuous process for the purposes of this section.

(iii) For batch processes, the annual factors shall be calculated every 10 batches for the 12-month period preceding the 10th batch (annual rolling average calculated every 10 batches). Additional annual factors shall be calculated every 12 months during the period before the 10th batch if more than 12 months elapse before the 10th batch is produced.

(2) Violations. Each rolling average that exceeds the target value established in §63.1365(g)(3) is considered a violation of the emission limit.

(g) Monitoring for emissions averaging. The owner or operator of an affected source that chooses to comply with the requirements of §63.1362(h) shall meet all monitoring requirements specified in paragraph (b) of this section, as applicable, for all processes, storage tanks, and waste management units included in the emissions average.
(ii) The owner or operator shall record the occurrence and duration of each malfunction of continuous monitoring systems used to comply with this subpart.

(iii) For each startup, shutdown, or malfunction, the owner or operator shall record all information necessary to demonstrate that the procedures specified in the affected source's startup, shutdown, and malfunction plan were followed, as specified in §63.6(e)(3)(iii) of subpart A of this part; alternatively, the owner or operator shall record any actions taken that are not consistent with the plan, as specified in §63.6(e)(3)(iv) of subpart A of this part.

(4) Recordkeeping requirements for sources with continuous monitoring systems. The owner or operator of an affected source who installs a continuous monitoring system to comply with the alternative standards in §63.1362(b)(6) or (c)(4) shall maintain records specified in §63.10(c)(1) through (14) of subpart A of this part.

(5) Application for approval of construction or reconstruction. For new affected sources, each owner or operator shall comply with the provisions regarding construction and reconstruction in §63.5 of subpart A of this part.

(b) Records of equipment operation. The owner or operator must keep the following records up-to-date and readily accessible:

(1) Each measurement of a control device operating parameter monitored in accordance with §63.1366 and each measurement of a treatment process parameter monitored in accordance with the provisions of §63.1362(d).

(2) For processes subject to §63.1362(g), records of consumption, production, and the rolling average values of the HAP and VOC factors.

(3) For each continuous monitoring system used to comply with the alternative standards in §63.1362(b)(6) and (c)(4), records documenting the completion of calibration checks and maintenance of the continuous monitoring systems.

(4) For processes in compliance with the 0.15 Mg/yr emission limit of §63.1362(b)(2)(i) or (b)(4)(i), records of the rolling annual calculations of uncontrolled emissions.

(5) For each bag leak detector used to monitor particulate HAP emissions from a fabric filter, the owner or operator shall maintain records of any bag leak detection alarm, including the date and time, with a brief explanation of the cause of the alarm and the corrective action taken.

(6) The owner or operator of an affected source that complies with the standards for process vents, storage tanks, and wastewater systems shall maintain up-to-date, readily accessible records of the information contained in paragraphs (b)(6)(i) through (vii) of this section to document that HAP emissions or HAP loadings (for wastewater) are below the limits specified in §63.1362:

(i) The initial calculations of uncontrolled and controlled emissions of gaseous organic HAP and HCl per batch for each process.

(ii) The wastewater concentrations and flow rates per POD and process.

(iii) The number of batches per year for each batch process.

(iv) The operating hours per year for continuous processes.

(v) The number of batches and the number of operating hours for processes that contain both batch and continuous operations.

(vi) The number of tank turnovers per year, if used in an emissions average or for determining applicability of a new PAI process unit.

(vii) A description of absolute or hypothetical peak-case operating conditions as determined using the procedures in §63.1365(b)(11).

(viii) Periods of planned routine maintenance as described in §63.1362(c)(9).

(7) Daily schedule or log of each operating scenario prior to its operation.

(c) Records of equipment leak detection and repair. The owner or operator of an affected source subject to the equipment leak standards in §63.1363 shall implement the recordkeeping requirements specified in §63.1363(g). All records shall be retained for a period of 5 years, in accordance with the requirements of §63.10(b)(1) of subpart A of this part.

(d) Records of emissions averaging. The owner or operator of an affected source
that chooses to comply with the requirements of §63.1362(h) shall maintain up-to-date records of the following information:

(1) An Emissions Averaging Plan which shall include in the plan, for all emission points included in each of the emissions averages, the information listed in paragraphs (d)(1)(i) through (v) of this section.

(i) The identification of all emission points in each emissions average.

(ii) The values of all parameters needed for input to the emission debits and credits equations in §63.1365(h).

(iii) The calculations used to obtain the debits and credits.

(iv) The estimated values for all parameters required to be monitored for input to the emission debits and credits equations in §63.1365(h).

(v) A statement that the compliance demonstration, monitoring, inspection, recordkeeping and reporting provisions in §63.104(f)(1)(i) through (iv) of subpart G of this part.

(2) The Emissions Averaging Plan shall demonstrate that the emissions from the emission points proposed to be included in the average will not result in greater hazard or, at the option of the operating permit authority, greater risk to human health or the environment than if the emission points were controlled according to the provisions in §63.1362(b) through (d).

(i) This demonstration of hazard or risk equivalency shall be made to the satisfaction of the operating permit authority.

(A) The Administrator may require an owner or operator to use specific methodologies and procedures for making a hazard or risk determination.

(B) The demonstration and approval of hazard or risk equivalency shall be made according to any guidance that the Administrator makes available for use or any other technically sound information or methods.

(ii) An Emissions Averaging Plan that does not demonstrate hazard or risk equivalency to the satisfaction of the Administrator shall not be approved. The Administrator may require such adjustments to the Emissions Averaging Plan as are necessary in order to ensure that the average will not result in greater hazard or risk to human health or the environment than would result if the emission points were controlled according to §63.1362(b) through (d).

(iii) A hazard or risk equivalency demonstration must satisfy the requirements specified in paragraphs (d)(2)(iii) (A) through (C) of this section.

(A) Be a quantitative, comparative chemical hazard or risk assessment;

(B) Account for differences between averaging and nonaveraging options in chemical hazard or risk to human health or the environment; and

(C) Meet any requirements set by the Administrator for such demonstrations.

(3) Records as specified in paragraphs (a) and (b) of this section.

(4) A calculation of the debits and credits as specified in §63.1365(h) for the last quarter and the prior four quarters.

(e) The owner or operator of an affected source subject to the requirements for heat exchanger systems in §63.1362(g) shall retain the records as specified in §63.104(f)(1)(i) through (iv) of subpart G of this part.

(f) For each vapor collection system or closed-vent system that contains bypass lines that could divert a vent stream away from the control device and to the atmosphere, the owner or operator shall keep a record of the information specified in either paragraph (f)(1) or (2) of this section.

(1) Hourly records of whether the flow indicator specified under §63.1362(j)(1) was operating and whether a diversion was detected at any time during the hour, as well as records of the times and durations of all periods when the vent stream is diverted from the control device or the flow indicator is not operating.
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(2) Where a seal mechanism is used to comply with §63.1362(j)(2), hourly records of flow are not required. In such cases, the owner or operator shall record that the monthly visual inspection of the seals or closure mechanism has been done, and shall record the occurrence of all periods when the seal mechanism is broken, the bypass line valve position has changed, or the key for a lock-and-key type lock has been checked out, and records of any car-seal that has broken.

(g) Records of primary use. For a PAI process unit that is used to produce a given material for use as a PAI as well as for other purposes, the owner or operator shall keep records of the total production and the production for use as a PAI on a semiannual or more frequent basis if the use as a PAI is not the primary use.

§ 63.1368 Reporting requirements.

(a) The owner or operator of an affected source shall comply with the reporting requirements of paragraphs (b) through (l) of this section. The owner or operator shall also comply with applicable paragraphs of §§63.9 and 63.10 of subpart A of this part, as specified in Table 1 of this subpart.

(b) Initial notification. The owner or operator shall submit the applicable initial notification in accordance with §63.9(b) or (d) of subpart A of this part.

(c) Application for approval of construction or reconstruction. The owner or operator who is subject to §63.5(b)(3) of subpart A of this part shall submit to the Administrator an application for approval of the construction of a new major source, the reconstruction of a major affected source, or the reconstruction of a major affected source subject to the standards. The application shall be prepared in accordance with §63.5(d) of subpart A of this part.

(d) Notification of continuous monitoring system performance evaluation. An owner or operator who is required by the Administrator to conduct a performance evaluation for a continuous monitoring system that is used to comply with the alternative standard in §63.1362(b)(6) or (c)(4) shall notify the Administrator of the date of the performance evaluation as specified in §63.8(e)(2) of subpart A of this part.

(e) Precompliance plan. The Precompliance plan shall be submitted at least 6 months prior to the compliance date of the standard. For new sources, the Precompliance plan shall be submitted to the Administrator with the application for approval of construction or reconstruction. The Administrator shall have 90 days to approve or disapprove the Precompliance plan. The Precompliance plan shall be considered approved if the Administrator either approves it in writing, or fails to disapprove it in writing within the 90-day time period. The 90-day period shall begin when the Administrator receives the Precompliance plan. If the Precompliance plan is disapproved, the owner or operator must still be in compliance with the standard by the compliance date. To change any of the information submitted in the Precompliance plan, the owner or operator shall notify the Administrator at least 90 days before the planned change is to be implemented; the change shall be considered approved if the Administrator either approves the change in writing, or fails to disapprove the change in writing within 90 days of receipt of the change. The Precompliance plan shall include the information specified in paragraphs (e)(1) through (5) of this section.

(1) Requests for approval to use alternative monitoring parameters or requests to set monitoring parameters according to §63.1366(b)(4).

(2) Descriptions of the daily or per batch demonstrations to verify that control devices subject to §63.1366(b)(1)(i) are operating as designed.

(3) Data and rationale used to support the parametric monitoring level(s) that are set according to §63.1366(b)(3)(ii)(B).

(4) For owners and operators complying with the requirements of §63.1362(i), the pollution prevention demonstration summary required in §63.1365(g)(3).

(5) Data and rationale used to support an engineering assessment to calculate uncontrolled emissions from process vents as required in §63.1365(c)(2)(ii).
(6) For fabric filters that are monitored with bag leak detectors, an operation and maintenance plan that describes proper operation and maintenance procedures, and a corrective action plan that describes corrective actions to be taken, and the timing of those actions, when the particulate matter concentration exceeds the setpoint and activates the alarm.

(f) Notification of compliance status report. The Notification of Compliance Status report required under §63.9(h) shall be submitted no later than 150 calendar days after the compliance date and shall include the information specified in paragraphs (f)(1) through (7) of this section.

(1) The results of any applicability determinations, emission calculations, or analyses used to identify and quantify HAP emissions from the affected source.

(2) The results of emissions profiles, performance tests, engineering analyses, design evaluations, or calculations used to demonstrate compliance. For performance tests, results should include descriptions of sampling and analysis procedures and quality assurance procedures.

(3) Descriptions of monitoring devices, monitoring frequencies, and the values of monitored parameters established during the initial compliance determinations, including data and calculations to support the levels established.

(4) Operating scenarios.

(5) Descriptions of absolute or hypothetical peak-case operating and/or testing conditions for control devices.

(6) Identification of emission points subject to overlapping requirements described in §63.1360(h) and the authority under which the owner or operator will comply, and identification of emission sources discharging to devices described by §63.1362(l).

(7) Anticipated periods of planned routine maintenance during which the owner or operator would not be in compliance with the provisions in §63.1362(c)(1) through (4).

(8) Percentage of total production from a PAI process unit that is anticipated to be produced for use as a PAI in the 3 years after either June 23, 1999 or startup, whichever is later.

(g) Periodic reports. The owner or operator shall prepare Periodic reports in accordance with paragraphs (g)(1) and (2) of this section and submit them to the Administrator.

(1) Submittal schedule. Except as provided in paragraphs (g)(3)(i) and (ii) of this section, the owner or operator shall submit Periodic reports semi-annually, beginning 60 operating days after the end of the applicable reporting period. The first report shall be submitted no later than 240 days after the date the Notification of Compliance Status report is due and shall cover the 6-month period beginning on the date the Notification of Compliance Status report is due.

(i) The Administrator may determine on a case-by-case basis that more frequent reporting is necessary to accurately assess the compliance status of the affected source.

(ii) Quarterly reports shall be submitted when the monitoring data are used to comply with the alternative standards in §63.1362(b)(6) or (c)(4) and the source experiences excess emissions. Once an affected source reports excess emissions, the affected source shall follow a quarterly reporting format until a request to reduce reporting frequency is approved. If an owner or operator submits a request to reduce the frequency of reporting, the provisions in §63.10(e)(3)(ii) and (iii) of subpart A of this part shall apply, except that the term “excess emissions and continuous monitoring system performance report and/or summary report” shall mean “Periodic report” for the purposes of this section.

(2) Content of periodic report. The owner or operator shall include the information in paragraphs (g)(2)(i) through (vi) of this section, as applicable.

(i) Each Periodic report must include the information in §63.10(e)(3)(vi)(A) through (M) of subpart A of this part, as applicable.

(ii) If the total duration of excess emissions, parameter exceedances, or excursions for the reporting period is 1 percent or greater of the total operating time for the reporting period, or the total continuous monitoring system downtime for the reporting period
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is 5 percent or greater of the total operating time for the reporting period, the Periodic report must include the information in paragraphs (g)(2)(iii)(A) through (D) of this section.

(A) Monitoring data, including 15-minute monitoring values as well as daily average values of monitored parameters, for all operating days when the average values were outside the ranges established in the Notification of Compliance Status report or operating permit.

(B) Duration of excursions, as defined in §63.1366(b)(7).

(C) Operating logs and operating scenarios for all operating days when the values are outside the levels established in the Notification of Compliance Status report or operating permit.

(D) When a continuous monitoring system is used, the information required in §63.10(c)(5) through (13) of subpart A of this part.

(iii) For each vapor collection system or closed vent system with a bypass line subject to §63.1362(j)(1), records required under §63.1366(f) of all periods when the vent stream is diverted from the control device through a bypass line. For each vapor collection system or closed vent system with a bypass line subject to §63.1362(j)(2), records required under §63.1366(f) of all periods in which the seal mechanism is broken, the bypass valve position has changed, or the key to unlock the bypass line valve was checked out.

(iv) The information in paragraphs (g)(2)(iv)(A) through (D) of this section shall be stated in the Periodic report, when applicable.

(A) No excess emissions.

(B) No exceedances of a parameter.

(C) No excursions.

(D) No continuous monitoring system has been inoperative, out of control, repaired, or adjusted.

(v) For each storage vessel subject to control requirements:

(A) Actual periods of planned routine maintenance during the reporting period in which the control device does not meet the specifications of §63.1362(c)(5); and

(B) Anticipated periods of planned routine maintenance for the next reporting period.

(vi) For each PAI process unit that does not meet the definition of primary use, the percentage of the production in the reporting period produced for use as a PAI.

(viii) Updates to the corrective action plan.

(h) Notification of process change. (1) Except as specified in paragraph (h)(2) of this section, whenever a process change is made, or any of the information submitted in the Notification of Compliance Status report changes, the owner or operator shall submit a report quarterly. The report may be submitted as part of the next Periodic report required under paragraph (g) of this section. The report shall include:

(i) A brief description of the process change;

(ii) A description of any modifications to standard procedures or quality assurance procedures;

(iii) Revisions to any of the information reported in the original Notification of Compliance Status report under paragraph (f) of this section; and

(iv) Information required by the Notification of Compliance Status report under paragraph (f) of this section for changes involving the addition of processes or equipment.

(2) The owner or operator must submit a report 60 days before the scheduled implementation date of either of the following:

(i) Any change in the activity covered by the Precompliance report.

(ii) A change in the status of a control device from small to large.

(i) Reports of startup, shutdown, and malfunction. For the purposes of this subpart, the startup, shutdown, and malfunction reports shall be submitted on the same schedule as the Periodic reports required under paragraph (g) of this section instead of the schedule specified in §63.10(d)(5)(i) of subpart A of this part. These reports shall include the information specified in §63.1367(a)(3)(i) through (iii) and shall contain the name, title, and signature of the owner or operator or other responsible official who is certifying its accuracy. Reports are only required if a startup, shutdown, or malfunction occurred during the reporting period. Any time an owner or operator takes an action that is not consistent with
the procedures specified in the affected source's startup, shutdown, and malfunction plan, the owner or operator shall submit an immediate startup, shutdown, and malfunction report as specified in §63.10(d)(5)(ii) of subpart A of this part.

(j) Reports of equipment leaks. The owner or operator of an affected source subject to the standards in §63.1363 shall implement the reporting requirements specified in §63.1363(h). Copies of all reports shall be retained as records for a period of 5 years, in accordance with the requirements of §63.10(b)(1) of subpart A of this part.

(k) Reports of emissions averaging. The owner or operator of an affected source that chooses to comply with the requirements of §63.1362(h) shall submit all information as specified in §63.1367(d) for all emission points included in the emissions average. The owner or operator shall also submit to the Administrator all information specified in paragraph (g) of this section for each emission point included in the emissions average.

(i) The reports shall also include the information listed in paragraphs (k)(1)(i) through (iv) of this section:

(i) Any changes to the processes, storage tanks, or waste management unit included in the average.

(ii) The calculation of the debits and credits for the reporting period.

(iii) Changes to the Emissions Averaging Plan which affect the calculation methodology of uncontrolled or controlled emissions or the hazard or risk equivalency determination.

(iv) Any changes to the parameters monitored according to §63.1368(g).

(2) Every second semiannual or fourth quarterly report, as appropriate, shall include the results according to §63.1367(d)(4) to demonstrate the emissions averaging provisions of §63.1362(h), §63.1365(h), §63.1368(g), and §63.1367(d) are satisfied.

(l) Reports of heat exchange systems. The owner or operator of an affected source subject to the requirements for heat exchange systems in §63.1362(f) shall submit information about any delay of repairs as specified in §63.104(f)(2) of subpart F of this part, except that when the phrase “periodic reports required by §63.152(c) of subpart G of this part” is referred to in §63.104(f)(2) of subpart F of this part, the periodic reports required in paragraph (g) of this section shall apply for the purposes of this subpart.

(m) Notification of performance test and test Plan. The owner or operator of an affected source shall notify the Administrator of the scheduled date of a performance test at least 60 days before the test in accordance with §63.7(b)(1) of subpart A of this part. The owner or operator also must submit the test Plan required by §63.7(c) of subpart A of this part and the emission profile required by §63.1365(b)(10)(ii) with the notification of the performance test.

(n) Request for extension of compliance. The owner or operator who submits an operating permit application before the date the Emissions Averaging Plan is due shall submit the information specified in paragraphs (o)(1) through (3) of this section with the operating permit application instead of the Emissions Averaging Plan.

(o) The owner or operator who submits an operating permit application before the date the Emissions Averaging Plan is due shall submit the information specified in paragraphs (o)(1) through (3) of this section with the operating permit application instead of the Emissions Averaging Plan:

(i) The information specified in §63.1367(d) for emission points included in the emissions average:

(ii) The information specified in §63.9(h) of subpart A of this part, as applicable; and

(iii) The information specified in paragraph (e) of this section, as applicable.

§63.1369 Delegation of authority.

(a) In delegating implementation and enforcement authority to a State under section 112(d) of the CAA, the authorities contained in paragraph (b) of this section shall be retained by the Administrator and not transferred to a State.

(b) The authority conferred in §63.177 of subpart H of this part, the authority to approve alternative test methods shall not be delegated to any State.
### TABLE 1 TO SUBPART MMM OF PART 63—GENERAL PROVISIONS APPLICABILITY TO SUBPART MMM

<table>
<thead>
<tr>
<th>Reference to subpart A</th>
<th>Applies to subpart MMM</th>
<th>Explanation</th>
</tr>
</thead>
<tbody>
<tr>
<td>§63.1(a)(1)</td>
<td>Yes</td>
<td>Additional terms are defined in §63.1361.</td>
</tr>
<tr>
<td>§63.1(a)(2)–(3)</td>
<td>Yes</td>
<td>Subpart MMM (this table) specifies applicability of each paragraph in subpart A to subpart MMM.</td>
</tr>
<tr>
<td>§63.1(a)(4)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§63.1(a)(5)</td>
<td>N/A</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§63.1(a)(5)–(7)</td>
<td>Yes</td>
<td>Discusses State programs.</td>
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<tr>
<td>§63.1(a)(9)</td>
<td>N/A</td>
<td>Reserved.</td>
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<tr>
<td>§63.1(a)(10)–(14)</td>
<td>Yes</td>
<td>§63.1360 specifies applicability.</td>
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<tr>
<td>§63.1(b)(1)</td>
<td>No</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§63.1(b)(2)–(3)</td>
<td>Yes</td>
<td>Subpart MMM (this table) specifies the applicability of each paragraph in subpart A to sources subject to subpart MMM.</td>
</tr>
<tr>
<td>§63.1(c)(2)</td>
<td>No</td>
<td>Area sources are not subject to subpart MMM.</td>
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<td>§63.1(c)(3)</td>
<td>N/A</td>
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<td>§63.1(c)(4)–(5)</td>
<td>Yes</td>
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<td>§63.1(d)</td>
<td>N/A</td>
<td>Reserved.</td>
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<td>§63.1(e)</td>
<td>Yes</td>
<td>Additional terms are defined in §63.1361; when overlap between subparts A and MMM occurs, subpart MMM takes precedence.</td>
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<td>§63.3</td>
<td>Yes</td>
<td>Other units used in subpart MMM are defined in that subpart.</td>
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<td>§63.4(a)(1)–(3)</td>
<td>Yes</td>
<td>§63.1364 specifies compliance dates.</td>
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<td>§63.4(a)(4)</td>
<td>N/A</td>
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<tr>
<td>§63.4(a)(5)–(c)</td>
<td>Yes</td>
<td>Except the term “affected source” shall apply instead of the terms “source” and “stationary source” in §63.5(a)(1) of subpart A.</td>
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<tr>
<td>§63.5(b)(1)</td>
<td>Yes</td>
<td>Reserved.</td>
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<td>§63.5(b)(2)</td>
<td>N/A</td>
<td>§63.1360(g) specifies requirements for determining applicability of added PAI equipment.</td>
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<td>§63.5(b)(3)–(5)</td>
<td>Yes</td>
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<td>§63.5(b)(6)</td>
<td>N/A</td>
<td>Except “affected source” shall apply instead of “source” in §63.5(f)(1) of subpart A.</td>
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<td>§63.5(f)(2)</td>
<td>Yes</td>
<td>§63.1364 specifies compliance dates.</td>
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<td>§63.6(a)</td>
<td>Yes</td>
<td>§63.1364 specifies compliance dates.</td>
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<tr>
<td>§63.6(b)(1)–(2)</td>
<td>No</td>
<td>§63.1364 specifies compliance dates.</td>
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<td>§63.6(b)(3)–(4)</td>
<td>Yes</td>
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<td>§63.6(b)(5)</td>
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<td>§63.6(b)(6)</td>
<td>N/A</td>
<td>§63.1364 specifies compliance dates.</td>
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<td>§63.6(b)(7)</td>
<td>Yes</td>
<td>§63.1364 specifies compliance dates.</td>
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<td>§63.6(c)(1)–(2)</td>
<td>Yes</td>
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<td>§63.6(c)(3)–(4)</td>
<td>Yes</td>
<td>§63.1364 specifies compliance dates.</td>
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<td>§63.6(c)(5)</td>
<td>Yes</td>
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<td>§63.6(d)</td>
<td>Yes</td>
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<td>§63.6(f)</td>
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<td>§63.6(g)</td>
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<td>§63.6(h)</td>
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<td>§63.6(i)(1)</td>
<td>Yes</td>
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<td>§63.6(i)(2)</td>
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<td>§63.6(i)(3)–(14)</td>
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<td>§63.1364 specifies compliance dates.</td>
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<td>§63.6(i)(15)</td>
<td>N/A</td>
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<td>§63.6(i)(16)</td>
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<td>§63.6(j)</td>
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<td>§63.7(a)(2)(i)–(vii)</td>
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<td>§63.7(a)(2)(viii)</td>
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<td>§63.1364 specifies compliance dates.</td>
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<td>§63.7(a)(2)(ix)–(c)</td>
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<td>§63.7(b)</td>
<td>Yes</td>
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<td>§63.7(d)</td>
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### TABLE 1 TO SUBPART MMM OF PART 63—GENERAL PROVISIONS APPLICABILITY TO SUBPART MMM—Continued

<table>
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<tr>
<th>Reference to subpart</th>
<th>Applies to subpart MMM</th>
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<td>§ 63.7(e)(3)</td>
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<td>§ 63.7(e)(4)</td>
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<td>§ 63.7(f)</td>
<td>Yes</td>
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<tr>
<td>§ 63.7(g)(1)</td>
<td>Yes</td>
<td>Except § 63.1360(a) specifies that the results of the performance test be submitted with the Notification of Compliance Status report.</td>
</tr>
<tr>
<td>§ 63.7(g)(2)</td>
<td>N/A</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.7(h)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>§ 63.8(a)(1)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>§ 63.8(a)(2)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>§ 63.8(a)(3)</td>
<td>N/A</td>
<td>Reserved.</td>
</tr>
<tr>
<td>§ 63.8(a)(4)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>§ 63.8(b)(1)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>§ 63.8(b)(2)</td>
<td>Yes</td>
<td>§ 63.1366 specifies CMS requirements.</td>
</tr>
<tr>
<td>§ 63.8(b)(3)−(c)(3)</td>
<td>Yes</td>
<td>Except the submittal date of the immediate startup, shutdown, and malfunction reports for CMS events shall be 2 days as in § 63.6(e)(3)(v).</td>
</tr>
<tr>
<td>§ 63.8(c)(4)</td>
<td>No</td>
<td>§ 63.1366 specifies monitoring frequencies.</td>
</tr>
<tr>
<td>§ 63.8(c)(5)−(8)</td>
<td>No</td>
<td>§ 63.1366 specifies data reduction procedures.</td>
</tr>
<tr>
<td>§ 63.8(d)(1)±(f)(3)</td>
<td>Yes</td>
<td>§ 63.1366 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.8(d)(4)</td>
<td>Yes</td>
<td>Except § 63.1366(b) specifies that requests may also be included in the Precompliance report.</td>
</tr>
<tr>
<td>§ 63.8(f)(4)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>§ 63.8(h)(5)</td>
<td>Yes</td>
<td>§ 63.1366 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.8(h)(6)</td>
<td>No</td>
<td>Subpart MMM does not require CEM's.</td>
</tr>
<tr>
<td>§ 63.8(g)</td>
<td>No</td>
<td>§ 63.1366 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.9(a)−(e)</td>
<td>No</td>
<td>Subpart MMM does not contain opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.9(f)</td>
<td>Yes</td>
<td>§ 63.1366 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(a)−(b)(1)</td>
<td>Yes</td>
<td>§ 63.1367 specifies recordkeeping requirements.</td>
</tr>
<tr>
<td>§ 63.10(b)(2)</td>
<td>No</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(b)(3)</td>
<td>Yes</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(c)</td>
<td>Yes</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(d)(1)</td>
<td>Yes</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(d)(2)</td>
<td>Yes</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(d)(3)</td>
<td>Yes</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(d)(4)</td>
<td>Yes</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(d)(5)</td>
<td>Yes</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(e)(1)−(2)(i)</td>
<td>Yes</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(e)(2)(ii)</td>
<td>No</td>
<td>§ 63.1367 specifies opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(e)(3)</td>
<td>Yes</td>
<td>Subpart MMM does not include opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(e)(4)</td>
<td>Yes</td>
<td>Subpart MMM does not include opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.10(f)</td>
<td>Yes</td>
<td>Subpart MMM does not include opacity and visible emission standards.</td>
</tr>
<tr>
<td>§ 63.11−§ 63.15</td>
<td>Yes</td>
<td>Subpart MMM does not include opacity and visible emission standards.</td>
</tr>
</tbody>
</table>

### TABLE 2 TO SUBPART MMM OF PART 63—STANDARDS FOR NEW AND EXISTING PAI SOURCES

<table>
<thead>
<tr>
<th>Emission source</th>
<th>Applicability</th>
<th>Requirement</th>
</tr>
</thead>
<tbody>
<tr>
<td>Process vents</td>
<td>Processes having uncontrolled organic HAP emissions ≥0.15 Mg/yr. Processes having uncontrolled HCl and chlorine emissions ≥6.8 Mg/yr.</td>
<td>90% for organic HAP per process or to outlet concentration of ≤20 ppmv TOC. 94% for HCl and chlorine per process or to outlet concentration of ≤20 ppmv.</td>
</tr>
</tbody>
</table>
### TABLE 2 TO SUBPART MMM OF PART 63—STANDARDS FOR NEW AND EXISTING PAI SOURCES—Continued

<table>
<thead>
<tr>
<th>Emission source</th>
<th>Applicability</th>
<th>Requirement</th>
</tr>
</thead>
<tbody>
<tr>
<td>Individual process vents meeting flow and mass emissions criteria that have gaseous organic HAP emissions controlled to less than 90% on or after November 10, 1997.</td>
<td>98% gaseous organic HAP control per vent or ≤20 ppmv TOC outlet limit.</td>
<td></td>
</tr>
<tr>
<td>New Processes having uncontrolled organic HAP emissions ≥0.15 Mg/yr. Processes having uncontrolled HCl and chlorine emissions ≥6.8 Mg/yr and &lt;191 Mg/yr. Processes having uncontrolled HCl and chlorine emissions ≥191 Mg/yr.</td>
<td>98% for organic HAP per process or ≤20 ppmv TOC. Reduce concentration of total Table 9 compounds to &lt;50 ppmw (or other options). 99% for HCl and chlorine per process or to outlet concentration of ≤20 ppmv HCl and chlorine.</td>
<td></td>
</tr>
<tr>
<td>Storage vessels Existing: &gt;75 m³ capacity and vapor pressure ≥3.45 kPa. New: ≥38 m³ capacity and vapor pressure ≥16.5 kPa.</td>
<td>Same as for existing sources. Reduce concentration of total Table 9 compounds to &lt;50 ppmw (or other options). 99% reduction of Table 9 compounds from all streams.</td>
<td></td>
</tr>
<tr>
<td>Wastewater Existing: Process wastewater with ≥10,000 ppmw Table 9 compounds at any flowrate or ≥1,000 ppmw Table 9 compounds at ≥10 L/min, and maintenance wastewater with HAP load ≥5.3 Mg per discharge event. New: Same criteria as for existing sources.</td>
<td>Reduce concentration of total Table 9 compounds to &lt;50 ppmw (or other options). Particle matter concentration not to exceed 0.01 gr/dscf.</td>
<td></td>
</tr>
<tr>
<td>Equipment leaks Subpart H</td>
<td>Subpart H with minor changes, including monitoring frequencies consistent with the proposed CAR. Particulate matter concentration not to exceed 0.01 gr/dscf. Monitoring and leak repair program as in HON.</td>
<td></td>
</tr>
<tr>
<td>Product dryers and bag dumps.</td>
<td>Dryers used to dry PAI that is also a HAP, and bag dumps used to introduce feedstock that is a solid and a HAP.</td>
<td></td>
</tr>
<tr>
<td>Heat exchange systems</td>
<td>Each heat exchange system used to cool process equipment in PAI manufacturing operations.</td>
<td></td>
</tr>
</tbody>
</table>

Note: Table 9 is listed in the appendix to subpart G of 40 CFR part 63.

### TABLE 3 TO SUBPART MMM OF PART 63—MONITORING REQUIREMENTS FOR CONTROL DEVICES

<table>
<thead>
<tr>
<th>Control device</th>
<th>Monitoring equipment required</th>
<th>Parameters to be monitored</th>
<th>Frequency</th>
</tr>
</thead>
<tbody>
<tr>
<td>All control devices</td>
<td>1. Flow indicator installed at all bypass lines to the atmosphere and equipped with continuous recorder or. 2. Valves sealed closed with car-seal or lock-and-key configuration.</td>
<td>1. Presence of flow diverted from the control device to the atmosphere or. 2. Monthly inspections of sealed valves.</td>
<td>Hourly records of whether the flow indicator was operating and whether a diversion was detected at any time during each hour. Monthly.</td>
</tr>
<tr>
<td>Scrubber</td>
<td>Liquid flow rate or pressure drop mounting device. Also a pH monitor if the scrubber is used to control acid emissions.</td>
<td>1. Liquid flow rate into or out of the scrubber or the pressure drop across the scrubber. 2. pH of effluent scrubber liquid.</td>
<td>1. Every 15 minutes. 2. Once a day.</td>
</tr>
<tr>
<td>Thermal incinerator</td>
<td>Temperature monitoring device installed in firebox or in ductwork immediately downstream of firebox.</td>
<td>Firebox temperature</td>
<td>Every 15 minutes.</td>
</tr>
<tr>
<td>Catalytic incinerator</td>
<td>Temperature monitoring device installed in gas stream immediately before and after catalyst bed.</td>
<td>Temperature difference across catalyst bed.</td>
<td>Every 15 minutes.</td>
</tr>
<tr>
<td>Control device</td>
<td>Monitoring equipment required</td>
<td>Parameters to be monitored</td>
<td>Frequency</td>
</tr>
<tr>
<td>--------------------------------------</td>
<td>---------------------------------------------------------------------</td>
<td>------------------------------------------------------------------------------------------</td>
<td>-------------------------</td>
</tr>
<tr>
<td>Flare</td>
<td>Heat sensing device installed at the pilot light.</td>
<td>Presence of a flame at the pilot light.</td>
<td>Every 15 minutes.</td>
</tr>
<tr>
<td></td>
<td>Temperature monitoring device installed in firebox.</td>
<td>Combustion temperature</td>
<td>Every 15 minutes.</td>
</tr>
<tr>
<td>Boiler or process heater &lt; 44</td>
<td>Temperature monitoring device installed at a condenser exit.</td>
<td>Condenser exit (product side) temperature.</td>
<td>Every 15 minutes.</td>
</tr>
<tr>
<td>megawatts and vent stream is not</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>mixed with the primary fuel.</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Condenser</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Carbon adsorber (nonregenerative)</td>
<td>Stream flow monitoring device, and.</td>
<td>Operating time since last replacement.</td>
<td></td>
</tr>
<tr>
<td>Carbon adsorber (regenerative)</td>
<td>Carbon bed temperature monitoring device.</td>
<td>1. Total regeneration stream mass or volumetric flow during carbon bed regeneration cycle(s).</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>2. Temperature of carbon bed after regeneration.</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>3. Temperature of carbon bed within 15 minutes of completing any cooling cycle(s).</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>4. Operating time since end of last regeneration.</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>5. Check for bed poisoning</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

*a* As an alternative to the monitoring requirements specified in this table, the owner or operator may use a CEM meeting the requirements of Performance Specifications 8 or 9 of appendix B of part 60 to monitor TOC every 15 minutes.

*b* Monitor may be installed in the firebox or in the ductwork immediately downstream of the firebox before any substantial heat exchange is encountered.

### Table 4 to Subpart MMM of Part 63—Control Requirements for Items of Equipment That Meet the Criteria of § 63.1362(k)

<table>
<thead>
<tr>
<th>Item of equipment</th>
<th>Control requirement</th>
</tr>
</thead>
<tbody>
<tr>
<td>Drain or drain hub</td>
<td>(a) Tightly fitting solid cover (TFSC); or</td>
</tr>
<tr>
<td></td>
<td>(b) TFSC with a vent to either a process, or to a control device meeting the requirements of § 63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(c) Water seal with submerged discharge or barrier to protect discharge from wind.</td>
</tr>
<tr>
<td>Manhole</td>
<td>(a) TFSC; or</td>
</tr>
<tr>
<td></td>
<td>(b) TFSC with a vent to either a process, or to a fuel gas system, or to a control device meeting the requirements of § 63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(c) If the item is vented to the atmosphere, use a TFSC with a properly operating water seal at the entrance or exit to the item to restrict ventilation in the collection system. The vent pipe shall be at least 90 cm in length and not exceeding 10.2 cm in nominal inside diameter.</td>
</tr>
<tr>
<td>Lift station</td>
<td>(a) TFSC; or</td>
</tr>
<tr>
<td></td>
<td>(b) TFSC with a vent to either a process, or to a control device meeting the requirements of § 63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(c) If the lift station is vented to the atmosphere, use a TFSC with a properly operating water seal at the entrance or exit to the item to restrict ventilation in the collection system. The vent pipe shall be at least 90 cm in length and not exceeding 10.2 cm in nominal inside diameter. The lift station shall be level controlled to minimize changes in the liquid level.</td>
</tr>
<tr>
<td>Trench</td>
<td>(a) TFSC; or</td>
</tr>
<tr>
<td></td>
<td>(b) TFSC with a vent to either a process, or to a control device meeting the requirements of § 63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(c) If the item is vented to the atmosphere, use a TFSC with a properly operating water seal at the entrance or exit to the item to restrict ventilation in the collection system. The vent pipe shall be at least 90 cm in length and not exceeding 10.2 cm in nominal inside diameter.</td>
</tr>
<tr>
<td>Pipe</td>
<td>Each pipe shall have no visible gaps in joints, seals, or other emission interfaces.</td>
</tr>
<tr>
<td>Oil/Water separator</td>
<td>(a) Equip with a fixed roof and route vapors to a process, or equip with a closed-vent system that routes vapors to a control device meeting the requirements of § 63.1256(h)(2); or</td>
</tr>
<tr>
<td></td>
<td>(b) Equip with a floating roof that meets the equipment specifications of § 60.693 (a)(1)(i), (a)(1)(ii), (a)(2), (a)(3), and (a)(4).</td>
</tr>
</tbody>
</table>
Environmental Protection Agency

§ 63.1381

TABLE 4 TO SUBPART MMM OF PART 63—CONTROL REQUIREMENTS FOR ITEMS OF EQUIPMENT THAT MEET THE CRITERIA OF § 63.1362(k)—Continued

<table>
<thead>
<tr>
<th>Item of equipment</th>
<th>Control requirement*</th>
</tr>
</thead>
<tbody>
<tr>
<td>Tank</td>
<td>Maintain a fixed roof. <strong>If the tank is sparged</strong> or used for heating or treating by means of an exothermic reaction, a fixed roof and a system shall be maintained that routes the organic hazardous air pollutants vapors to other process equipment or a fuel gas system, or a closed-vent system that routes vapors to a control device that meets the requirements of 40 CFR § 63.119(e)(1) or (e)(2).</td>
</tr>
</tbody>
</table>

*Where a tightly fitting solid cover is required, it shall be maintained with no visible gaps or openings, except during periods of sampling, inspection, or maintenance.
**Manhole includes sumps and other points of access to a conveyance system.
***A fixed roof may have openings necessary for proper venting of the tank, such as pressure/vacuum vent, j-pipe vent.

(d) The provisions of this part 63, subpart A that apply and those that do not apply to this subpart are specified in Table 1 of this subpart.

§ 63.1381 Definitions.

Terms used in this subpart are defined in the Clean Air Act, in § 63.2, or in this section as follows:

Bag leak detection system means systems that include, but are not limited to, devices using triboelectric, light scattering, and other effects to monitor relative or absolute particulate matter (PM) emissions.

Bonded means wool fiberglass to which a phenol-formaldehyde binder has been applied.

Building insulation means bonded wool fiberglass insulation, having a loss on ignition of less than 8 percent and a density of less than 32 kilograms per cubic meter (kg/m³) (2 pounds per cubic foot [lb/ft³]).

Cold top electric furnace means an all-electric glass-melting furnace that operates with a temperature of 120 °C (250 °F) or less as measured at a location 46 to 61 centimeters (18 to 24 inches) above the molten glass surface.

Flame attenuation means a process used to produce wool fiberglass where molten glass flows by gravity from melting furnaces, or pots, to form filaments that are drawn down and attenuated by passing in front of a high-velocity gas burner flame.

Glass-melting furnace means a unit comprising a refractory vessel in which raw materials are charged, melted at high temperature, refined, and conditioned to produce molten glass. The
unit includes foundations, superstructure and retaining walls, raw material charger systems, heat exchangers, melter cooling system, exhaust system, refractory brick work, fuel supply and electrical boosting equipment, integral control systems and instrumentation, and appendages for conditioning and distributing molten glass to forming processes. The forming apparatus, including flow channels, is not considered part of the glass-melting furnace.

Glass pull rate means the mass of molten glass that is produced by a single glass-melting furnace or that is used in the manufacture of wool fiberglass at a single manufacturing line in a specified time period.

Hazardous Air Pollutant (HAP) means any air pollutant listed in or pursuant to section 112(b) of the Clean Air Act.

Heavy-density product means bonded wool fiberglass insulation manufactured on a flame attenuation manufacturing line and having a loss on ignition of 11 to 25 percent and a density of 8 to 48 kg/m³ (0.5 to 3 lb/ft³).

Incinerator means an enclosed air pollution control device that uses controlled flame combustion to convert combustible materials to noncombustible gases.

Loss on ignition (LOI) means the percent decrease in weight of wool fiberglass after it has been ignited. The LOI is used to monitor the weight percent of binder in wool fiberglass.

Manufacturing line means the manufacturing equipment for the production of wool fiberglass that consists of a forming section where molten glass is fiberized and a fiberglass mat is formed and which may include a curing section where binder resin in the mat is thermally set and a cooling section where the mat is cooled.

New source means any affected source the construction or reconstruction of which is commenced after March 31, 1997.

Pipe product means bonded wool fiberglass insulation manufactured on a flame attenuation manufacturing line and having a loss on ignition of 8 to 14 percent and a density of 48 to 96 kg/m³ (3 to 6 lb/ft³).

Rotary spin means a process used to produce wool fiberglass building insulation by forcing molten glass through numerous small orifices in the side wall of a spinner to form continuous glass fibers that are then broken into discrete lengths by high-velocity air flow. Any process used to produce bonded wool fiberglass building insulation by a process other than flame attenuation is considered rotary spin.

Wool fiberglass means insulation materials composed of glass fibers made from glass produced or melted at the same facility where the manufacturing line is located.

Wool fiberglass manufacturing facility means any facility manufacturing wool fiberglass on a rotary spin manufacturing line or on a flame attenuation manufacturing line.

§ 63.1382 Emission standards

(a) Emission limits—(1) Glass-melting furnaces. On and after the date the initial performance test is completed or required to be completed under § 63.7 of this part, whichever date is earlier, the owner or operator shall not discharge or cause to be discharged into the atmosphere in excess of 0.25 kilogram (kg) of particulate matter (PM) per megagram (Mg) (0.5 pound [lb] of PM per ton) of glass pulled for each new or existing glass-melting furnace.

(ii) Rotary spin manufacturing lines. On and after the date the initial performance test is completed or required to be completed under § 63.7 of this part, whichever date is earlier, the owner or operator shall not discharge or cause to be discharged into the atmosphere in excess of:

(i) 0.6 kg of formaldehyde per megagram (1.2 lb of formaldehyde per ton) of glass pulled for each existing rotary spin manufacturing line; and

(ii) 0.4 kg of formaldehyde per megagram (0.8 lb of formaldehyde per ton) of glass pulled for each new rotary spin manufacturing line.

(3) Flame attenuation manufacturing lines. On and after the date the initial performance test is completed or required to be completed under § 63.7 of this part, whichever date is earlier, the owner or operator shall not discharge or cause to be discharged into the atmosphere in excess of:

(i) 3.9 kg of formaldehyde per megagram (7.8 lb of formaldehyde per ton) of glass pulled for each new flame attenuation manufacturing line; and

(ii) 0.6 kg of formaldehyde per megagram (1.2 lb of formaldehyde per ton) of glass pulled for each existing flame attenuation manufacturing line.
ton) of glass pulled for each new flame attenuation manufacturing line that produces heavy-density wool fiberglass; and

(ii) 3.4 kg of formaldehyde per megagram (6.8 lb of formaldehyde per ton) of glass pulled from each existing or new flame attenuation manufacturing line that produces pipe product wool fiberglass.

(b) Operating limits. On and after the date on which the performance test required to be conducted by §§63.7 and 63.1384 is completed, the owner or operator must operate all affected control equipment and processes according to the following requirements.

(1)(i) The owner or operator must initiate corrective action within 1 hour of an alarm from a bag leak detection system and complete corrective actions in a timely manner according to the procedures in the operations, maintenance, and monitoring plan.

(ii) The owner or operator must implement a Quality Improvement Plan (QIP) consistent with the compliance assurance monitoring provisions of 40 CFR part 64, subpart D when the bag leak detection system alarm is sounded for more than 5 percent of the total operating time in a 6-month block reporting period.

(2)(i) The owner or operator must initiate corrective action within 1 hour when any 3-hour block average of the monitored electrostatic precipitator (ESP) parameter is outside the limit(s) established during the performance test as specified in §63.1384 and complete corrective actions in a timely manner according to the procedures in the operations, maintenance, and monitoring plan.

(ii) The owner or operator must operate the cold top electric furnace such that the temperature does not exceed 120 °C (250 °F) as measured at a location 46 to 61 centimeters (18 to 24 inches) above the molten glass surface, for more than 10 percent of the total operating time in a 6-month reporting period.

(3)(i) The owner or operator must initiate corrective action within 1 hour when any 3-hour block average temperature of a cold top electric furnace as measured at a location 46 to 61 centimeters (18 to 24 inches) above the molten glass surface, exceeds 120 °C (250 °F) and complete corrective actions in a timely manner according to the procedures in the operations, maintenance, and monitoring plan.

(ii) The owner or operator of a cold top electric furnace must implement a QIP consistent with the compliance assurance monitoring provisions of 40 CFR part 64, subpart D when the temperature, as measured at a location 46 to 61 centimeters (18 to 24 inches) above the molten glass surface, exceeds 120 °C (250 °F) for more than 5 percent of the total operating time in a 6-month block reporting period.

(iii) The owner or operator must operate the cold top electric furnace such that the temperature does not exceed 120 °C (250 °F) as measured at a location 46 to 61 centimeters (18 to 24 inches) above the molten glass surface, for more than 10 percent of the total operating time in a 6-month reporting period.

(4)(i) The owner or operator must initiate corrective action within 1 hour when any 3-hour block average value for the monitored parameter(s) for a glass-melting furnace, which uses no add-on controls and which is not a cold top electric furnace, is outside the limit(s) established during the performance test as specified in §63.1384 and complete corrective actions in a timely manner according to the procedures in the operations, maintenance, and monitoring plan.

(ii) The owner or operator must implement a QIP consistent with the compliance assurance monitoring provisions of 40 CFR part 64, subpart D when the monitored parameter(s) is outside the limit(s) established during the performance test as specified in §63.1384 for more than 5 percent of the total operating time in a 6-month block reporting period.

(iii) The owner or operator must operate a glass-melting furnace, which
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uses no add-on controls and which is not a cold top electric furnace, such that the monitored parameter(s) is not outside the limit(s) established during the performance test as specified in § 63.1384 for more than 10 percent of the total operating time in a 6-month block reporting period.

(5)(i) The owner or operator must initiate corrective action within 1 hour when the average glass pull rate of any 4-hour block period for glass melting furnaces equipped with continuous monitors, or daily glass pull rate for glass melting furnaces not so equipped, exceeds the average glass pull rate established during the performance test as specified in § 63.1384, by greater than 20 percent and complete corrective actions in a timely manner according to the procedures in the operations, maintenance, and monitoring plan.

(ii) The owner or operator must implement a QIP consistent with the compliance assurance monitoring provisions of 40 CFR part 64, subpart D when any scrubber parameter is outside the limit(s) established during the performance test as specified in § 63.1384 for more than 5 percent of the total operating time in a 6-month block reporting period.

(iii) The owner or operator must operate each scrubber such that each monitored parameter is not outside the limit(s) established during the performance test as specified in § 63.1384 for more than 10 percent of the total operating time in a 6-month block reporting period.

(6) The owner or operator must operate each incinerator used to control formaldehyde emissions from forming or curing such that any 3-hour block average temperature in the firebox does not fall below the average established during the performance test as specified in § 63.1384 for more than 10 percent of the total operating time in a 6-month block reporting period.

(7)(i) The owner or operator must initiate corrective action within 1 hour when the average pressure drop, liquid flow rate, or chemical feed rate for any 3-hour block period is outside the limits established during the performance tests as specified in § 63.1384 for each wet scrubbing control device and complete corrective actions in a timely manner according to the procedures in the operations, maintenance, and monitoring plan.

(ii) The owner or operator must implement a QIP consistent with the compliance assurance monitoring provisions of 40 CFR part 64, subpart D when any scrubber parameter is outside the limit(s) established during the performance test as specified in § 63.1384 for more than 5 percent of the total operating time in a 6-month block reporting period.

(iii) The owner or operator must operate each scrubber such that each monitored parameter is not outside the limit(s) established during the performance test as specified in § 63.1384 for more than 10 percent of the total operating time in a 6-month block reporting period.

(8)(i) The owner or operator must initiate corrective action within 1 hour when the monitored process parameter level(s) is outside the limit(s) established during the performance test as specified in § 63.1384 for each process modification(s) used to control formaldehyde emissions and complete corrective actions in a timely manner according to the procedures in the operations, maintenance, and monitoring plan.

(ii) The owner or operator must implement a QIP consistent with the compliance assurance monitoring provisions of 40 CFR part 64, subpart D when the process parameter(s) is outside the limit(s) established during the performance test as specified in § 63.1384 for more than 5 percent of the total operating time in a 6-month block reporting period.

(iii) The owner or operator must operate the process modifications such that the monitored process parameter(s) is not outside the limit(s) established during the performance test as specified in § 63.1384 for more than 10 percent of the total operating time in a 6-month block reporting period.

(9) The owner or operator must use a resin in the formulation of binder such that the free-formaldehyde content of the resin used does not exceed the free-formaldehyde range contained in the specification for the resin used during
the performance test as specified in §63.1384.

(10) The owner or operator must use a binder formulation that does not vary from the specification and operating range established and used during the performance test as specified in §63.1384. For the purposes of this standard, adding or increasing the quantity of urea and/or lignin in the binder formulation does not constitute a change in the binder formulation.

§63.1383 Monitoring requirements.

On and after the date on which the performance test required to be conducted by §§63.7 and 63.1384 is completed, the owner or operator must monitor all affected control equipment and processes according to the following requirements.

(a) The owner or operator of each wool fiberglass manufacturing facility must prepare for each glass-melting furnace, rotary spin manufacturing line, and flame attenuation manufacturing line subject to the provisions of this subpart, a written operations, maintenance, and monitoring plan. The plan must include the following information:

(1) Procedures for the proper operation and maintenance of process modifications and add-on control devices used to meet the emission limits in §63.1382;

(2) Procedures for the proper operation and maintenance of monitoring devices used to determine compliance, including quarterly calibration and certification of accuracy of each monitoring device according to the manufacturer's instructions; and

(3) Corrective actions to be taken when process parameters or add-on control device parameters deviate from the limit(s) established during initial performance tests.

(b)(1) Where a baghouse is used to control PM emissions from a glass-melting furnace, the owner or operator shall install, calibrate, maintain, and continuously operate a bag leak detection system.

(1) The bag leak detection system must be certified by the manufacturer to be capable of detecting PM emissions at concentrations of 10 milligrams per actual cubic meter (0.0044 grains per actual cubic foot) or less.

(ii) The bag leak detection system sensor must produce output of relative PM emissions.

(iii) The bag leak detection system must be equipped with an alarm system that will sound automatically when an increase in relative PM emissions over a preset level is detected and the alarm must be located such that it can be heard by the appropriate plant personnel.

(iv) For positive pressure fabric filter systems, a bag leak detection system must be installed in each baghouse compartment or cell. If a negative pressure or induced air baghouse is used, the bag leak detection system must be installed downstream of the baghouse. Where multiple bag leak detection systems are required (for either type of baghouse), the system instrumentation and alarm may be shared among the monitors.

(v) A triboelectric bag leak detection system shall be installed, operated, adjusted, and maintained in a manner consistent with the U.S. Environmental Protection Agency guidance, “Fabric Filter Bag Leak Detection Guidance” (EPA-454/R-98-015, September 1997). Other bag leak detection systems shall be installed, operated, adjusted, and maintained in a manner consistent with the manufacturer's written specifications and recommendations.

(vi) Initial adjustment of the system shall, at a minimum, consist of establishing the baseline output by adjusting the range and the averaging period of the device and establishing the alarm set points and the alarm delay time.

(vii) Following the initial adjustment, the owner or operator shall not adjust the range, averaging period, alarm setpoints, or alarm delay time except as detailed in the approved operations, maintenance, and monitoring plan required under paragraph (a) of this section. In no event shall the range be increased by more than 300 percent or decreased more than 50 percent over a 365-day period unless a responsible official as defined in §63.2 of
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the general provisions in subpart A of this part certifies that the baghouse has been inspected and found to be in good operating condition.

(2) The operations, maintenance, and monitoring plan required by paragraph (a) of this section must specify corrective actions to be followed in the event of a bag leak detection system alarm. Example corrective actions that may be included in the plan include the following:

(i) Inspecting the baghouse for air leaks, torn or broken bags or filter media, or any other conditions that may cause an increase in emissions.

(ii) Sealing off defective bags or filter media.

(iii) Replacing defective bags or filter media.

(iv) Sealing off a defective baghouse compartment.

(v) Cleaning the bag leak detection system probe, or otherwise repairing the bag leak detection system.

(vi) Shutting down the process producing the particulate emissions.

(c)(1) Where an ESP is used to control PM emissions from a glass-melting furnace, the owner or operator must monitor the ESP according to the procedures in the operations, maintenance, and monitoring plan. (2) The operations, maintenance, and monitoring plan for the ESP must contain the following information:

(i) The ESP operating parameter(s), such as secondary voltage of each electrical field, to be monitored and the minimum and/or maximum value(s) that will be used to identify any operational problems;

(ii) A schedule for monitoring the ESP operating parameter(s);

(iii) Recordkeeping procedures, consistent with the recordkeeping requirements of §63.1386, to show that the glass-melting furnace parameter(s) is within the limit(s) established during the performance test; and

(iv) Procedures for the proper operation and maintenance of the ESP.

(d) The owner or operator must measure and record at least once per shift the temperature 46 to 61 centimeters (18 to 24 inches) above the surface of the molten glass in a cold top electric furnace that does not use any add-on controls to control PM emissions.

(e)(1) Where a glass-melting furnace is operated without an add-on control device to control PM emissions, the owner or operator must monitor the glass-melting furnace according to the procedures in the operations, maintenance, and monitoring plan.

(2) The operations, maintenance, and monitoring plan for the glass-melting furnace must contain the following information:

(i) The operating parameter(s) to be monitored and the minimum and/or maximum value(s) that will be used to identify any operational problems;

(ii) A schedule for monitoring the operating parameter(s) of the glass-melting furnace;

(iii) Recordkeeping procedures, consistent with the recordkeeping requirements of §63.1386, to show that the glass-melting furnace parameter(s) is within the limit(s) established during the performance test; and

(iv) Procedures for the proper operation and maintenance of the glass-melting furnace.

(f)(1) The owner or operator of an existing glass-melting furnace equipped with continuous glass pull rate monitors must monitor and record the glass pull rate on an hourly basis. For glass-melting furnaces that are not equipped with continuous glass pull rate monitors, the glass pull rate must be monitored and recorded once per day.

(2) On any new glass-melting furnace, the owner or operator must install, calibrate, and maintain a continuous glass pull rate monitor that monitors and records on an hourly basis the glass pull rate.

(g)(1) The owner or operator who uses an incinerator to control formaldehyde emissions from forming or curing shall install, calibrate, maintain, and operate a monitoring device that continuously measures and records the operating temperature in the firebox of each incinerator.

(2) The owner or operator must inspect each incinerator at least once per year according to the procedures in the operations, maintenance, and monitoring plan. At a minimum, an inspection must include the following:
(i) Inspect all burners, pilot assemblies, and pilot sensing devices for proper operation and clean pilot sensor, as necessary;
(ii) Ensure proper adjustment of combustion air and adjust, as necessary;
(iii) Inspect, when possible, internal structures, for example, baffles, to ensure structural integrity per the design specifications;
(iv) Inspect dampers, fans, and blowers for proper operation;
(v) Inspect for proper sealing;
(vi) Inspect motors for proper operation;
(vii) Inspect combustion chamber refractory lining and clean and repair/replace lining, as necessary;
(viii) Inspect incinerator shell for corrosion and/or hot spots;
(ix) For the burn cycle that follows the inspection, document that the incinerator is operating properly and make any necessary adjustments; and
(x) Generally observe that the equipment is maintained in good operating condition.
(xi) Complete all necessary repairs as soon as practicable.
(h) The owner or operator who uses a wet scrubbing control device to control formaldehyde emissions must install, calibrate, maintain, and operate monitoring devices that continuously monitor and record the gas pressure drop across each scrubber and scrubbing liquid flow rate to each scrubber according to the procedures in the operations, maintenance, and monitoring plan. The pressure drop monitor is to be certified by its manufacturer to be accurate within ±250 pascals (±1 inch water gauge) over its operating range, and the flow rate monitor is to be certified by its manufacturer to be accurate within ±5 percent over its operating range. The owner or operator must also continuously monitor and record the feed rate of any chemical(s) added to the scrubbing liquid.
(i) The owner or operator who uses process modifications to control formaldehyde emissions must establish a correlation between formaldehyde emissions and a process parameter(s) to be monitored.
(2) The owner or operator must monitor the established parameter(s) according to the procedures in the operations, maintenance, and monitoring plan.
(3) The owner or operator must include as part of their operations, maintenance, and monitoring plan the following information:
(i) Procedures for the proper operation and maintenance of the process;
(ii) Process parameter(s) to be monitored to demonstrate compliance with the applicable emission limits in §63.1382. Examples of process parameters include LOI, binder solids content, and binder application rate;
(iii) Correlation(s) between process parameter(s) to be monitored and formaldehyde emissions;
(iv) A schedule for monitoring the process parameter(s); and
(v) Recordkeeping procedures, consistent with the recordkeeping requirements of §63.1386, to show that the process parameter value(s) established during the performance test is not exceeded.
(j) The owner or operator must monitor and record the free-formaldehyde content of each resin shipment received and used in the formulation of binder.
(k) The owner or operator must monitor and record the formulation of each batch of binder used.
(l) The owner or operator must monitor and record at least once every 8 hours, the product LOI and product density of each bonded wool fiberglass product manufactured.
(m) For all control device and process operating parameters measured during the initial performance tests, the owners or operators of glass-melting furnaces, rotary spin manufacturing lines or flame attenuation manufacturing lines subject to this subpart may change the limits established during the initial performance test if additional performance testing is conducted to verify that, at the new control device or process parameter levels, they comply with the applicable emission limits in §63.1382. The owner or operator shall conduct all additional performance tests according to the procedures in this part 63, subpart A and in §63.1384.
§ 63.1384 Performance test requirements.

(a) The owner or operator subject to the provisions of this subpart shall conduct a performance test to demonstrate compliance with the applicable emission limits in §63.1382. Compliance is demonstrated when the emission rate of the pollutant is equal to or less than each of the applicable emission limits in §63.1382. The owner or operator shall conduct the performance test according to the procedures in 40 CFR part 63, subpart A and in this section.

(1) All monitoring systems and equipment must be installed, operational, and calibrated prior to the performance test.

(2) Unless a different frequency is specified in this section, the owner or operator must monitor and record process and/or add-on control device parameters at least every 15 minutes during the performance tests. The arithmetic average for each parameter must be calculated using all of the recorded measurements for the parameter.

(3) During each performance test, the owner or operator must monitor and record the glass pull rate for each glass-melting furnace and, if different, the glass pull rate for each rotary spin manufacturing line and flame attenuation manufacturing line. Record the glass pull rate every 15 minutes during any performance test required by this subpart and determine the arithmetic average of the recorded measurements for each test run and calculate the average of the three test runs.

(4) The owner or operator shall conduct a performance test for each existing and new glass-melting furnace.

(5) During the performance test, the owner or operator of a glass-melting furnace controlled by an ESP shall monitor and record the ESP parameter level(s), as specified in the operations, maintenance, and monitoring plan, and establish the minimum and/or maximum value(s) that will be used to demonstrate compliance after the initial performance test.

(6) During the performance test, the owner or operator of a glass-melting furnace not equipped with an add-on control device for PM emissions control, must monitor and record the temperature 46 to 61 centimeters (18 to 24 inches) above the molten glass surface to ensure that the maximum temperature does not exceed 120 °C (250 °F).

(7) During the performance test, the owner or operator of a glass melting furnace (other than a cold top electric furnace) that is not equipped with an add-on control device for PM emissions control, must monitor and record the furnace parameter level, and establish the minimum and/or maximum value(s) that will be used to demonstrate compliance after the initial performance test.

(8) The owner or operator must conduct a performance test for each rotary spin manufacturing line, subject to this subpart, while producing the building insulation with the highest LOI expected to be produced on that line; and for each flame attenuation manufacturing line, subject to this subpart, while producing the heavy-density product or pipe product with the highest LOI expected to be produced on the affected line.

(9) The owner or operator of each rotary spin manufacturing line and flame attenuation manufacturing line regulated by this subpart must conduct performance tests using the resin with the highest free-formaldehyde content. During the performance test of each rotary spin manufacturing line and flame attenuation manufacturing line regulated by this subpart, the owner or operator shall monitor and record the free-formaldehyde content of the resin, the binder formulation used, and the product LOI and density.

(10) During the performance test, the owner or operator of a rotary spin manufacturing line or flame attenuation manufacturing line who plans to use process modifications to comply with the emission limits in §63.1382 must monitor and record the process parameter level(s), as specified in the operations, maintenance, and monitoring plan, which will be used to demonstrate compliance after the initial performance test.

(11) During the performance test, the owner or operator of a rotary spin manufacturing line or flame attenuation manufacturing line who plans to use a wet scrubbing control device to
comply with the emission limits in §63.1382 must continuously monitor and record the pressure drop across the scrubber, the scrubbing liquid flow rate, and addition of any chemical to the scrubber, including the chemical feed rate, and establish the minimum and/or maximum value(s) that will be used to determine compliance after the initial performance test.

(12) During the performance test, the owner or operator of a rotary spin manufacturing line or affected flame attenuation manufacturing line shall continuously monitor and record the pressure drop across the scrubber, the scrubbing liquid flow rate, and addition of any chemical to the scrubber, including the chemical feed rate, and establish the minimum and/or maximum value(s) that will be used to determine compliance after the initial performance test.

(13) Unless disapproved by the Administrator, an owner or operator of a rotary spin or flame attenuation manufacturing line regulated by this subpart may conduct short-term experimental production runs using binder formulations or other process modifications where the process parameter values would be outside those established during performance tests without first conducting performance tests. Such runs must not exceed 1 week in duration unless the Administrator approves a longer period. The owner or operator must notify the Administrator and postmark or deliver the notification at least 15 days prior to commencement of the short-term experimental production runs. The Administrator must inform the owner or operator of a decision to disapprove or must request additional information prior to the date of the short-term experimental production runs. Notification of intent to perform an experimental short-term production run shall include the following information:

(i) The purpose of the experimental production run;
(ii) The affected line;
(iii) How the established process parameters will deviate from previously approved levels;
(iv) The duration of the experimental production run;
(v) The date and time of the experimental production run; and
(vi) A description of any emission testing to be performed during the experimental production run.

(b) To determine compliance with the PM emission limit for glass-melting furnaces, use the following equation:

\[ E = \frac{C \times Q \times K_1}{P} \]  
(Eq. 1)

Where:

- \( E \) = Emission rate of PM, kg/Mg (lb/ton) of glass pulled;
- \( C \) = Concentration of PM, g/dscm (gr/dscf);
- \( Q \) = Volumetric flow rate of exhaust gases, dscm/h (dscf/h);
- \( K_1 \) = Conversion factor, 1 kg/1,000 g (1 lb/7,000 gr); and
- \( P \) = Average glass pull rate, Mg/h (tons/h).

(c) To determine compliance with the emission limit for formaldehyde for rotary spin manufacturing lines and flame attenuation forming processes, use the following equation:

\[ E = \frac{C \times MW \times Q \times K_1 \times K_2}{K_3 \times P \times 10^6} \]  
(Eq. 2)

Where:

- \( E \) = Emission rate of formaldehyde, kg/Mg (lb/ton) of glass pulled;
- \( C \) = Measured volume fraction of formaldehyde, ppm;
- \( MW \) = Molecular weight of formaldehyde, 30.03 g/g-mol;
- \( Q \) = Volumetric flow rate of exhaust gases, dscm/h (dscf/h);
- \( K_1 \) = Conversion factor, 1 kg/1,000 g (1 lb/453.6 g);
- \( K_2 \) = Conversion factor, 1,000 L/m³ (28.3 L/ft³);
- \( K_3 \) = Conversion factor, 24.45 L/g-mol; and
- \( P \) = Average glass pull rate, Mg/h (tons/h).

§ 63.1385 Test methods and procedures.

(a) The owner or operator shall use the following methods to determine compliance with the applicable emission limits:

(1) Method 1 (40 CFR part 60, appendix A) for the selection of the sampling port location and number of sampling ports;
(2) Method 2 (40 CFR part 60, appendix A) for volumetric flow rate;
(3) Method 3 or 3A (40 CFR part 60, appendix A) for \( O_2 \) and \( CO_2 \) for diluent measurements needed to correct the concentration measurements to a standard basis;
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(4) Method 4 (40 CFR part 60, appendix A) for moisture content of the stack gas;  
(5) Method 5 (40 CFR part 60, appendix A) for the concentration of PM. Each run shall consist of a minimum run time of 2 hours and a minimum sample volume of 60 dry standard cubic feet (dscf). The probe and filter holder heating system may be set to provide a gas temperature no greater than 177 ±14 °C (350 ±25 °F);  
(6) Method 316 or Method 318 (appendix A of this part) for the concentration of formaldehyde. Each run shall consist of a minimum run time of 1 hour;  
(7) Method contained in appendix A of this subpart for the determination of product LOI;  
(8) Method contained in appendix B of this subpart for the determination of the free-formaldehyde content of resin;  
(9) Method contained in appendix C of this subpart for the determination of product density;  
(10) An alternative method, subject to approval by the Administrator.  
(b) Each performance test shall consist of 3 runs. The owner or operator shall use the average of the three runs in the applicable equation for determining compliance.

§ 63.1386  Notification, recordkeeping, and reporting requirements.

(a) Notifications. As required by §63.9(b) through (h) of this part, the owner or operator shall submit the following written initial notifications to the Administrator:

(1) Notification for an area source that subsequently increases its emissions such that the source is a major source subject to the standard;  
(2) Notification that a source is subject to the standard, where the initial startup is before June 14, 2002;  
(3) Notification that a source is subject to the standard, where the source is new or has been reconstructed, the initial startup is after June 14, 2002, and for which an application for approval of construction or reconstruction is not required;  
(4) Notification of intention to construct a new major source or reconstruct a major source; of the date construction or reconstruction commenced; of the anticipated date of startup; of the actual date of startup, where the initial startup of a new or reconstructed source occurs after June 14, 2002, and for which an application for approval or construction or reconstruction is required (See §63.9(b)(4) and (5) of this part);  
(5) Notification of special compliance obligations;  
(6) Notification of performance test; and  
(7) Notification of compliance status.

(b) Performance test report. As required by §63.10(d)(2) of the general provisions, the owner or operator shall report the results of the initial performance test as part of the notification of compliance status required in paragraph (a)(7) of this section.

(c) Startup, shutdown, and malfunction plan and reports. (1) The owner or operator shall develop and implement a written plan as described in §63.6(e)(3) of this part that contains specific procedures to be followed for operating the source and maintaining the source during periods of startup, shutdown, and malfunction and a program of corrective action for malfunctioning process modifications and control systems used to comply with the standard. In addition to the information required in §63.6(e)(3), the plan shall include:

(i) Procedures to determine and record the cause of the malfunction and the time the malfunction began and ended;  
(ii) Corrective actions to be taken in the event of a malfunction of a control device or process modification, including procedures for recording the actions taken to correct the malfunction or minimize emissions; and  
(iii) A maintenance schedule for each control device and process modification that is consistent with the manufacturer's instructions and recommendations for routine and long-term maintenance.

(2) The owner or operator shall also keep records of each event as required by §63.10(b) of this part and record and report if an action taken during a startup, shutdown, or malfunction is not consistent with the procedures in the plan as described in §63.10(e)(3)(iv) of this part.
(d) Recordkeeping. (1) As required by §63.10(b) of this part, the owner or operator shall maintain files of all information (including all reports and notifications) required by the general provisions and this subpart:

(i) The owner or operator must retain each record for at least 5 years following the date of each occurrence, measurement, maintenance, corrective action, report, or record. The most recent 2 years of records must be retained at the facility. The remaining 3 years of records may be retained off site;

(ii) The owner or operator may retain records on microfilm, on a computer, on computer disks, on magnetic tape, or on microfiche; and

(iii) The owner or operator may report required information on paper or on a labeled computer disk using commonly available and EPA-compatible computer software.

(2) In addition to the general records required by §63.10(b)(2) of this part, the owner or operator shall maintain records of the following information:

(i) Any bag leak detection system alarms, including the date and time of the alarm, when corrective actions were initiated, the cause of the alarm, an explanation of the corrective actions taken, and when the cause of the alarm was corrected;

(ii) ESP parameter value(s) used to monitor ESP performance, including any period when the value(s) deviated from the established limit(s), the date and time of the deviation, when corrective actions were initiated, the cause of the deviation, an explanation of the corrective actions taken, and when the cause of the deviation was corrected;

(iii) Air temperature above the molten glass in an uncontrolled cold top electric furnace, including any period when the temperature exceeded 120 °C (250 °F) at a location 46 to 61 centimeters (18 to 24 inches) above the molten glass surface, the date and time of the exceedance, when corrective actions were initiated, the cause of the exceedance, an explanation of the corrective actions taken, and when the cause of the exceedance was corrected;

(iv) Uncontrolled glass-melting furnace (that is not a cold top electric furnace) parameter value(s) used to monitor furnace performance, including any period when the value(s) exceeded the established limit(s), the date and time of the exceedance, when corrective actions were initiated, the cause of the exceedance, an explanation of the corrective actions taken, and when the cause of the exceedance was corrected;

(v) The formulation of each binder batch and the LOI and density for each product manufactured on a rotary spin manufacturing line or flame attenuation manufacturing line subject to the provisions of this subpart, and the free formaldehyde content of each resin shipment received and used in the binder formulation;

(vi) Process parameter level(s) for RS and FA manufacturing lines that use process modifications to comply with the emission limits, including any period when the parameter level(s) deviated from the established limit(s), the date and time of the deviation, when corrective actions were initiated, the cause of the deviation, an explanation of the corrective actions taken, and when the cause of the deviation was corrected;

(vii) Scrubber pressure drop, scrubbing liquid flow rate, and any chemical additive (including chemical feed rate to the scrubber), including any period when a parameter level(s) deviated from the established limit(s), the date and time of the deviation, when corrective actions were initiated, the cause of the deviation, an explanation of the corrective actions taken, and when the cause of the deviation was corrected;

(viii) Incinerator operating temperature and results of periodic inspection of incinerator components, including any period when the temperature fell below the established average or the inspection identified problems with the incinerator, the date and time of the problem, when corrective actions were initiated, the cause of the problem, an explanation of the corrective actions taken, and when the cause of the problem was corrected;

(ix) Glass pull rate, including any period when the pull rate exceeded the average pull rate established during the performance test by more than 20 percent, the date and time of the exceedance, when corrective actions were initiated, the cause of the exceedance,
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an explanation of the corrective actions taken, and when the cause of the exceedance was corrected.

(e) Excess emissions report. As required by §63.10(e)(3)(v) of this part, the owner or operator shall report semiannually if measured emissions are in excess of the applicable standard or a monitored parameter deviates from the levels established during the performance test. The report shall contain the information specified in §63.10(c) of this part as well as the additional records required by the recordkeeping requirements of paragraph (d) of this section. When no deviations have occurred, the owner or operator shall submit a report stating that no excess emissions occurred during the reporting period.

§ 63.1387 Compliance dates.

(a) Compliance dates. The owner or operator subject to the provisions of this subpart shall demonstrate compliance with the requirements of this subpart by no later than:

(1) June 14, 2002, for an existing glass-melting furnace, rotary spin manufacturing line, or flame attenuation manufacturing line; or

(2) Upon startup for a new glass-melting furnace, rotary spin manufacturing line, or flame attenuation manufacturing line.

(b) Compliance extension. The owner or operator of an existing source subject to this subpart may request from the Administrator an extension of the compliance date for the emission standards for one additional year if such additional period is necessary for the installation of controls. The owner or operator shall submit a request for an extension according to the procedures in §63.6(i)(3) of this part.

§§ 63.1388–63.1399 [Reserved]
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<td>63.6(b)(1)±(b)(5)</td>
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<td>63.6(b)(7)</td>
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<td>63.6(c)(1)</td>
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<td>Yes</td>
<td>§63.1387 specifies compliance dates.</td>
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<td>Yes</td>
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<td>63.6(g)(1)±(g)(3)</td>
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<td>63.6(h)</td>
<td></td>
<td>Yes</td>
<td>Subpart NNN-no COMS, VE or opacity standards.</td>
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<td>63.6(i)</td>
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<td>Yes</td>
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<td>63.6(k)(15)</td>
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<td>63.6(l)±(l)(16)</td>
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<td>Applies to subpart NNN</td>
<td>Explanation</td>
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<td>63.7(a)</td>
<td>Performance Testing Requirements</td>
<td>Yes</td>
<td>§63.1384 has specific requirements.</td>
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<td>63.7(h)</td>
<td>Notification</td>
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<td>Quality Assurance Program/Test Plan</td>
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<td>Performance Testing Facilities</td>
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<td>63.7(g)</td>
<td>Data Analysis</td>
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<td>63.7(h)</td>
<td>Waiver of Performance Tests</td>
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<td>63.8(b)</td>
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<td>Performance Evaluation for CMS</td>
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<td>63.8(e)</td>
<td>Alternative Monitoring Method</td>
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<td>63.8(f)</td>
<td>Reduction of Monitoring Data</td>
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<td>63.8(g)</td>
<td>Notification Requirements</td>
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<td>63.8(h)</td>
<td>Initial Notifications</td>
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<td>Request for Compliance Extension</td>
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<td>63.9(a)</td>
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<td>63.9(c)</td>
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<td>63.9(d)</td>
<td>Notification of Compliance Status</td>
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<td>63.9(e)</td>
<td>Adjustment of Deadlines</td>
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<td>63.9(f)</td>
<td>Change in Previous Information</td>
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<td>63.10(a)</td>
<td>General Requirements</td>
<td>Yes</td>
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<td>63.10(b)</td>
<td>Additional CMS Recordkeeping/Reporting</td>
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<td>63.10(c)(9)</td>
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<td>63.10(d)</td>
<td>General Reporting Requirements</td>
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<td>63.10(d)(2)</td>
<td>Performance Test Results</td>
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<td>63.10(d)(3)</td>
<td>Opacity or VE Observations</td>
<td>No</td>
<td>No limits for VE/opacity.</td>
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<td>63.10(d)(4)</td>
<td>Progress Reports</td>
<td>Yes</td>
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<td>63.10(d)(5)</td>
<td>Startup, Shutdown, Malfunction Reports</td>
<td>Yes</td>
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<td>Additional CMS Reports</td>
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<td>63.10(f)</td>
<td>Waiver of Recordkeeping/Reporting</td>
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<td>COM not required.</td>
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<td>Section</td>
<td>Requirement</td>
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<td>63.11(a)</td>
<td>Control Device Requirements</td>
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<td>63.11(b)</td>
<td>Flares</td>
<td>No</td>
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<td>63.12</td>
<td>State Authority and Delegations</td>
<td>Yes</td>
<td></td>
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<tr>
<td>63.13</td>
<td>State/Regional Addresses</td>
<td>Yes</td>
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<tr>
<td>63.14</td>
<td>Incorporation by Reference</td>
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<td>63.15</td>
<td>Availability of Information</td>
<td>Yes</td>
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APPENDIX A TO SUBPART NNN OF PART 63—METHOD FOR THE DETERMINATION OF LOI

1. Purpose
The purpose of this test is to determine the LOI of cured blanket insulation. The method is applicable to all cured board and blanket products.

2. Equipment
2.1 Scale sensitive to 0.1 gram.
2.2 Furnace designed to heat to at least 540 °C (1,000 °F) and controllable to ±10 °C (50 °F).
2.3 Wire tray for holding specimen while in furnace.

3. Procedure
3.1 Cut a strip along the entire width of the product that will weigh at least 10.0 grams. Sample should be free of dirt or foreign matter.
   NOTE: Remove all facing from sample.
3.2 Cut the sample into pieces approximately 12 inches long, weigh to the nearest 0.1 gram and record. Place in wire tray. Sample should not be compressed or overhang on tray edges.
   NOTE: On air duct products, remove shiplaps and overspray.
3.3 Place specimen in furnace at 540 °C (1,000 °F), ±10 °C (50 °F) for 15 to 20 minutes to insure complete oxidation. After ignition, fibers should be white and should not be fused together.
3.4 Remove specimen from the furnace and cool to room temperature.
3.5 Weigh cooled specimen and wire tray to the nearest 0.1 gram. Deduct the weight of the wire tray and then calculate the loss in weight as a percent of the original specimen weight.

APPENDIX B TO SUBPART NNN OF PART 63—FREE FORMALDEHYDE ANALYSIS OF INSULATION RESINS BY HYDROXYLAMINE HYDROCHLORIDE

1. Scope
This method was specifically developed for water-soluble phenolic resins that have a relatively high free-formaldehyde (FF) content such as insulation resins. It may also be suitable for other phenolic resins, especially those with a high FF content.

2. Principle
2.1 a. The basis for this method is the titration of the hydrochloric acid that is liberated when hydroxylamine hydrochloride reacts with formaldehyde to form formaldoxime:
\[
\text{HCHO} + \text{NH}_2\text{OH}:\text{HCl} \rightarrow \text{CH}_2\text{NOH} + \text{H}_2\text{O} + \text{HCl}
\]
b. Free formaldehyde in phenolic resins is present as monomeric formaldehyde, hemiformals, polyoxymethylene hemiformals, and polyoxymethylene glycols. Monomeric formaldehyde and hemiformals react rapidly with hydroxylamine hydrochloride, but the polymeric forms of formaldehyde must hydrolyze to the monomeric state before they can react. The greater the concentration of free formaldehyde in a resin, the more of that formaldehyde will be in the polymeric form. The hydrolysis of these polymers is catalyzed by hydrogen ions.

2.2 The resin sample being analyzed must contain enough free formaldehyde so that the initial reaction with hydroxylamine hydrochloride will produce sufficient hydrogen ions to catalyze the depolymerization of the polymeric formaldehyde within the time limits of the test method. The sample should contain approximately 0.3 grams free formaldehyde to ensure complete reaction within 5 minutes.

3. Apparatus
3.1 Balance, readable to 0.01 g or better.
3.2 pH meter, standardized to pH 4.0 with pH 4.0 buffer and pH 7 with pH 7.0 buffer.
3.3 50-mL burette for 1.0 N sodium hydroxide.
3.4 Magnetic stirrer and stir bars.
3.5 250-mL beaker.
3.6 50-mL graduated cylinder.
3.7 100-mL graduated cylinder.
3.8 Timer.

4. Reagents
4.1 Standardized 1.0 N sodium hydroxide solution.
4.2 Hydroxylamine hydrochloride solution, 100 grams per liter, pH adjusted to 4.00.
4.3 Hydrochloric acid solution, 1.0 N and 0.1 N.
4.4 Sodium hydroxide solution, 0.1 N.
4.5 50/50 v/v mixture of distilled water and methyl alcohol.

5. Procedure
5.1 Determine the sample size as follows:
   a. If the expected FF is greater than 2 percent, go to Part A to determine sample size.
   b. If the expected FF is less than 2 percent, go to Part B to determine sample size.
   c. Part A: Expected FF ≥2 percent.

   1. The following table shows example levels:
   
<table>
<thead>
<tr>
<th>Expected % free formaldehyde</th>
<th>Sample size, grams</th>
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<tbody>
<tr>
<td>2</td>
<td>30.0</td>
</tr>
<tr>
<td>5</td>
<td>10.0</td>
</tr>
<tr>
<td>8</td>
<td>7.5</td>
</tr>
<tr>
<td>10</td>
<td>6.0</td>
</tr>
<tr>
<td>12</td>
<td>5.0</td>
</tr>
</tbody>
</table>

   i. Grams resin = 60(expected percent FF)

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i. It is very important to the accuracy of the results that the sample size be chosen correctly. If the milliliters of titrant are less than 15 mL or greater than 30 mL, reestimate the needed sample size and repeat the tests.

1. Part A: Expected FF = 2 percent

Grams resin = \( \frac{30}{\text{expected percent FF}} \)

ii. If the milliliters of titrant are less than 5 mL or greater than 30 mL, reestimate the needed sample size and repeat the tests.

5. Weigh the resin sample to the nearest 0.01 grams into a 250-mL beaker. Record sample weight.

6. Add 100 mL of the methanol/water mixture and stir on a magnetic stirrer. Confirm that the resin has dissolved.

5. Adjust the resin/solvent solution to pH 4.0, using the prestandardized pH meter, 1.0 N hydrochloric acid, 0.1 N hydrochloric acid, and 0.1 N sodium hydroxide.

5. Add 50 mL of the hydroxylamine hydrochloride solution, measured with a graduated cylinder. Start the timer.

5. Stir for 5 minutes. Titrate to pH 4.0 with standardized 1.0 N sodium hydroxide. Record the milliliters of titrant and the normality.

6. Calculations

\[
\% \text{ FF} = \frac{\text{mL sodium hydroxide} \times \text{normality} \times 3.003}{\text{grams of sample}}
\]

7. Method Precision and Accuracy

Test values should conform to the following statistical precision:

- Variance = 0.005
- Standard deviation = 0.07
- 95% Confidence Interval, for a single determination = 0.2

8. Author

This method was prepared by K. K. Tutin and M. L. Foster, Tacoma R&D Laboratory, Georgia-Pacific Resins, Inc. (Principle written by R. R. Conner.)

9. References

9.1 GPAM 2221.2.
9.2 PR&CTM 2.035.

APPENDIX C TO SUBPART NNN OF PART 63—METHOD FOR THE DETERMINATION OF PRODUCT DENSITY

1. Purpose

The purpose of this test is to determine the product density of cured blanket insulation. The method is applicable to all cured board and blanket products.

2. Equipment

One square foot (12 in. by 12 in.) template, or templates that are multiples of one square foot, for use in cutting insulation samples.

3. Procedure

3.1 Obtain a sample at least 30 in. long across the machine width. Sample should be free of dirt or foreign matter.

3.2 Lay out the cutting pattern according to the plant’s written procedure for the designated product.

3.3 Cut samples using one square foot (or multiples of one square foot) template.

3.4 Weigh product and obtain area weight (lb/ft²).

3.5 Measure sample thickness.

3.6 Calculate the product density:

\[
\text{Density (lb/ft}^3\text{)} = \frac{\text{area weight (lb/ft}^2\text{)} \times \text{thickness (ft)}}
\]

Subpart OOO [Reserved]

Subpart PPP—National Emission Standards for Hazardous Air Pollutant Emissions for Polyether Polyols Production

SOURCE: 64 FR 29439, June 1, 1999, unless otherwise noted.

§ 63.1420 Applicability and designation of affected sources.

(a) Definition of affected source. The provisions of this subpart apply to each affected source. Affected sources are described in paragraphs (a)(1) through (4) of this section.
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(1) An affected source is either an existing affected source or a new affected source. Existing affected source is defined in paragraph (a)(2) of this section, and new affected source is defined in paragraph (a)(3) of this section.

(2) An existing affected source is defined as the group of one or more polyether polyol manufacturing process units (PMPUs) and associated equipment, as listed in paragraph (a)(4) of this section, that is not part of a new affected source, as defined in paragraph (a)(3) of this section, and that is located at a plant site that is a major source.

(3) A new affected source is defined as a source that meets the criteria of paragraph (a)(3)(i), (ii), or (iii) of this section. The situation described in paragraph (a)(3)(i) of this section is distinct from those situations described in paragraphs (a)(3)(ii) and (iii) of this section.

(i) At a site without organic HAP emission points before September 4, 1997 (i.e., a “greenfield” site), the group of one or more PMPUs and associated equipment, as listed in paragraph (a)(4) of this section, that is part of a major source, and on which construction for the PMPU(s) commenced after September 4, 1997;

(ii) The group of one or more PMPUs meeting the criteria in paragraph (g)(1)(i) of this section; or

(iii) A reconstructed affected source meeting the criteria in paragraph (g)(2)(i) of this section.

(4) The affected source also includes the emission points and equipment specified in paragraphs (a)(4)(i) through (vi) of this section that are associated with a PMPU (or a group of PMPUs) making up an affected source, as defined in §63.1423.

(i) Each waste management unit.

(ii) Maintenance wastewater.

(iii) Each heat exchange system.

(iv) Equipment required by or utilized as a method of compliance with this subpart which may include control techniques and recovery devices.

(v) Product finishing operation.

(vi) Each feed or catalyst operation.

(b) PMPUs without organic HAP. The owner or operator of a PMPU that is part of an affected source, as defined in paragraph (a) of this section, but that does not use or manufacture any organic HAP during the production of one or more products is only subject to the provisions of this subpart as specified in paragraph (b)(1) or (2) of this section, as applicable. Products or raw material(s) containing organic HAP as impurities only are not considered organic HAP for the purposes of this paragraph.

(1) If an organic HAP is not used or manufactured in the production of polyether polyls, the PMPU is not subject to any provisions of this subpart, except that the owner or operator shall comply with either paragraph (b)(1)(ii) or (ii) of this section. The owner or operator is not required to comply with the provisions of 40 CFR part 63, subpart A (the General Provisions) for that PMPU.

(i) Retain information, data, and analyses used to document the basis for the determination that the PMPU does not use or manufacture any organic HAP. Types of information that could document this determination include, but are not limited to, records of chemicals purchased for the process, analyses of process stream composition, engineering calculations, or process knowledge.

(ii) When requested by the Administrator, demonstrate that the PMPU does not use or manufacture any organic HAP.

(2) If an organic HAP is used or manufactured in the production of polyether polyls, but an organic HAP is not used in the production of one or more products that are not polyether polyls, the PMPU is not subject to any provision of this subpart other than paragraph (b)(1)(i) or (ii) of this section during the production of the non-polyether polyl products that do not use or manufacture any organic HAP.

(c) Emission points included in the affected source but not subject to the provisions of this subpart. The affected source includes the emission points listed in paragraphs (c)(1) through (12) of this section, but these emission points are not subject to the requirements of this subpart or the provisions of 40 CFR part 63, subpart A.

(1) Equipment that does not contain organic HAP or that contains organic...
HAP as impurities only and is located at a PMPU that is part of an affected source.

(2) Stormwater managed in segregated sewers.

(3) Water from fire-fighting and deluge systems in segregated sewers.

(4) Spills.

(5) Water from safety showers.

(6) Water from testing of deluge systems.

(7) Water from testing of firefighting systems.

(8) Vessels that store and/or handle material that contains no organic HAP or organic HAP as impurities only.

(9) Equipment that operates in organic HAP service for less than 300 hours during the calendar year.

(10) Loading racks, loading arms, or loading hoses that only transfer liquids containing HAP as impurities.

(11) Loading racks, loading arms, or loading hoses that vapor balance during all loading operations.

(12) Utility fluids, such as heat transfer fluids.

(d) Processes exempted from the affected source. The processes specified in paragraphs (d)(1) through (3) of this section are not part of the affected source and are exempted from the requirements of both this subpart and subpart A of this part.

(1) Research and development facilities.

(2) Solvent reclamation, recovery, or recycling operations at hazardous waste treatment, storage, and disposal facilities (TSDF) requiring a permit under 40 CFR part 270 that are not part of a PMPU to which this subpart applies.

(3) Reactions or processing that occur after the epoxide polymerization is complete and after all catalyst removal steps, if any, are complete.

(e) Primary product determination and applicability. An owner or operator of a process unit that produces or plans to produce a polyether polyol shall determine if the process unit is subject to this subpart in accordance with this paragraph.

(1) Initial primary product determination. The owner or operator shall initially determine the primary product of each process unit in accordance with paragraphs (e)(1)(i) through (iii) of this section.

(i) If a process unit manufactures only one product, then that product shall represent the primary product of the process unit.

(ii) If a process unit produces more than one intended product at the same time, the primary product shall be determined in accordance with paragraph (e)(1)(ii)(A) or (B) of this section.

(A) The product for which the process unit has the greatest annual design capacity on a mass basis shall represent the primary product of the process unit, or

(B) If a process unit has the same maximum annual design capacity on a mass basis for two or more products and if one of those products is a polyether polyol, then the polyether polyol shall represent the primary product of the process unit.

(iii) If a process unit is designed and operated as a flexible operation unit, the primary product shall be determined as specified in paragraph (e)(1)(iii)(A) or (B) of this section based on the anticipated operations for the 5 years following September 4, 1997 for existing process units, or for the first year after the process unit begins production of any product for the new process units. If operations cannot be anticipated sufficiently to allow the determination of the primary product for the specified period, applicability shall be determined in accordance with paragraph (e)(2) of this section.

(A) If the flexible operation unit will manufacture one product for the greatest operating time over the specified 5-year period for existing process units, or the specified 1-year period for new process units, then that product shall represent the primary product of the flexible operation unit.

(B) If the flexible operation unit will manufacture multiple products equally based on operating time, then the product with the greatest expected production on a mass basis over the specified 5-year period for existing process units, or the specified 1-year period for new process units shall represent the primary product of the flexible operation unit.

(iv) If, according to paragraph (e)(1)(i), (ii), or (iii) of this section, the
primary product of a process unit is a polyether polyol, then that process unit shall be designated as a PMPU. If the plant site is a major source, that PMPU and associated equipment, as listed in paragraph (a)(4) of this section, is either an affected source or part of an affected source comprised of one or more other PMPUs and associated equipment, as listed in paragraph (a)(4) of this section, and subject to this subpart. If the primary product of a process unit is not a polyether polyol, then that process unit is not a PMPU.

(2) Provisions if primary product cannot be determined. If the primary product cannot be determined for a flexible operation unit in accordance with paragraph (e)(1)(iii) of this section, applicability shall be determined in accordance with this paragraph.

(i) If the owner or operator can determine that a polyether polyol is not the primary product, then that flexible operation unit is not a PMPU.

(ii) If the owner or operator cannot determine that a polyether polyol is not the primary product as specified in paragraph (e)(2)(i) of this section, applicability shall be determined in accordance with paragraph (e)(2)(ii)(A) or (B) of this section.

(A) If the flexible operation unit is an existing process unit, the flexible operation unit shall be designated as a PMPU if a polyether polyol was produced for 5 percent or greater of the total operating time of the flexible operation unit since September 4, 1997.

(B) If the flexible operation unit is a new process unit, the flexible operation unit shall be designated as a PMPU if the owner or operator anticipates that a polyether polyol will be manufactured in the flexible operation unit at any time in the first year after the date the unit begins production of any product.

(3) Annual applicability determination for non-PMPUs that have produced a polyether polyol. Once per year beginning June 1, 2004 the owner or operator of each flexible operation unit that is not designated as a PMPU, but that has produced a polyether polyol at any time in the preceding 5-year period or since the date that the unit began production of any product, whichever is shorter, shall perform the evaluation described in paragraphs (e)(3)(i) through (iii) of this section.

(i) For each product produced in the flexible operation unit, the owner or operator shall calculate the percentage of total operating time over which the product was produced during the preceding 5-year period.

(ii) The owner or operator shall identify the primary product as the product with the highest percentage of total operating time for the preceding 5-year period.

(iii) If the primary product identified in paragraph (e)(3)(ii) is a polyether polyol, the flexible operation unit shall be designated as a PMPU. The owner or operator shall notify the Administrator no later than 45 days after determining that the flexible operation unit is a PMPU, and shall comply with the requirements of this subpart in accordance with paragraph (g)(1) of this section for the flexible operation unit.

(4) Applicability determination for non-PMPUs that have not produced a polyether polyol. The owner or operator that anticipates the production of a polyether polyol in a process unit that is not designated as a PMPU, and in which no polyether polyol products have been produced in the previous 5-year period or since the date that the process unit began production of any product, whichever is shorter, shall use the procedures in paragraph (e)(1) or (2) of this section to determine if the process unit is designated as a PMPU, with the exception that for existing process units, owners or operators shall project production for the 5 years following the date that the owner or operator anticipates initiating the production of a polyether polyol, instead of the 5 years following September 4, 1997. If the unit is designated as a PMPU, the owner or operator shall comply in accordance with paragraph (g)(1) of this section.

(5) Applicability of requirements for PMPUs that are flexible operation units. The owner or operator of PMPUs that are flexible operation units shall comply with the provisions of this subpart in accordance with paragraphs (e)(5)(i) through (iii) of this section.

(i) Control requirements. The owner or operator shall comply with the control
requirements of this subpart in accordance with paragraphs (e)(5)(i)(A) and (B) of this section.

(A) During periods when the PMPU produces polyether polyols, the owner or operator shall comply with the provisions of this subpart.

(B) During periods when the PMPU produces products other than polyether polyols, the owner or operator is not required to install additional combustion, recovery, or recapture devices to otherwise demonstrate compliance. However, the owner or operator shall continue to operate any existing combustion, recovery, or recapture devices that are required for compliance during the production of polyether polyols, with the exceptions provided in paragraph (e)(5)(iv) of this section. If extended cookout (ECO) is the control technique chosen for epoxide emission reduction, then ECO or a control technique providing an equivalent reduction in epoxide emissions should continue to be used for epoxide emission reduction, if the non-polyether polyol being produced uses epoxide monomers.

(iii) Monitoring requirements. The owner or operator shall comply with the monitoring requirements of this subpart in accordance with paragraphs (e)(5)(ii)(A) and (B) of this section, and paragraph (e)(5)(ii)(C) of this section if applicable.

(A) The owner or operator shall establish a single parameter monitoring level (for each parameter required to be monitored at each device subject to monitoring requirements) in accordance with §63.1438(a) based on emission point and control technique characteristics when polyether polyol is being produced.

(B) The owner or operator shall monitor each parameter at each device subject to monitoring requirements at all times (during periods when the PMPU produces polyether polyols, and during periods when the PMPU produces products other than polyether polyols), with the exceptions provided in paragraph (e)(5)(iv) of this section.

(C) If ECO is used to reduce epoxide emissions, a parameter monitoring level shall be established for the production of non-polyether polyol products as the average of the established parameter levels for all product classes produced. During periods when products other than polyether polyols are produced, the ECO shall be performed so that the parameter monitoring level established for the production of non-polyether polyol products is maintained when the ECO is used as a control technique.

(iii) Group determinations. For emission points where the owner or operator is required to determine if the emission point is Group 1 according the definitions in §63.1423 (storage vessels, process vents for nonepoxide organic HAP emissions used to make or modify the product, and wastewater), the owner or operator shall determine the group status based on emission point characteristics when polyether polyol is being manufactured. Group 1 emission points shall be controlled in accordance with paragraph (e)(5)(i) of this section.

(iv) Exceptions. During periods when products described in paragraphs (e)(5)(iv)(A) and (B) of this section are produced, the owner or operator is not required to comply with the provisions of this subpart.

(A) Products in which no organic HAP is used or manufactured, provided that the owner or operator comply with paragraph (b)(2) of this section.

(B) Products that make the PMPU subject to 40 CFR part 63, subpart GGG (Pharmaceuticals Production NESHAP).

(6)-(7) [Reserved]

(8) Requirements for process units that are not PMPUs. If it is determined that a process unit is not subject to this subpart, the owner or operator shall either retain all information, data, and analysis used to document the basis for the determination that the process unit is not a PMPU, or, when requested by the Administrator, demonstrate that the process unit is not a PMPU.

(9) PMPUs terminating production of polyether polyol products. If a PMPU terminates the production of polyether polyol and does not anticipate the production of a polyether polyol in the future, the process unit is no longer a PMPU and is not subject to this subpart after notification is made to the Administrator. This notification shall be accompanied by a rationale for why it is anticipated that no polyether
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polyol will be produced in the process unit in the future.

(10) Redetermination of applicability to PMPUs that are flexible operation units. Whenever changes in production occur that could reasonably be expected to change the primary product of a PMPU that is operating as a flexible operation unit from a polyether polyol to a product that would make the process unit subject to another subpart of this part, the owner or operator shall reevaluate the primary product in accordance with paragraphs (e)(3)(i) and (ii) of this section. If the conditions in paragraphs (e)(10)(i) through (iii) of this section are met, the flexible operation unit shall no longer be designated as a PMPU after the compliance date of the other subpart, and shall no longer be subject to the provisions of this subpart. If the conditions in paragraphs (e)(10)(i) through (iii) of this section are not met, the flexible operation unit shall continue to be considered a PMPU and subject to the requirements of this subpart.

(i) The product identified as the primary product is not polyether polyol;

(ii) The production of the product identified as the primary product is subject to another subpart of this part; and

(iii) The owner or operator submits a notification to the Administrator of the pending change in applicability.

(f) Storage vessel ownership determination. The owner or operator shall follow the procedures specified in paragraphs (f)(1) through (7) of this section to determine to which process unit a storage vessel shall be assigned.

(1) If a storage vessel is already subject to another subpart of 40 CFR part 63 (National Emission Standards for Hazardous Air Pollutants for Source Categories) on June 1, 1999, that storage vessel shall be assigned to the process unit subject to the other subpart, and none of the other provisions in this subpart shall apply to that storage vessel.

(2) If a storage vessel is shared among process units, then the storage vessel shall be assigned to that process unit located on the same plant site as the storage vessel that has the greatest input into or output from the storage vessel (i.e., the process unit that has the predominant use of the storage vessel.)

(3) If a storage vessel is shared among process units, then the storage vessel shall be assigned to that process unit located on the same plant site as the storage vessel that has the greatest input into or output from the storage vessel (i.e., the process unit that has the predominant use of the storage vessel.)

(4) If predominant use cannot be determined for a storage vessel that is shared among process units and if only one of those process units is a PMPU subject to this subpart, the storage vessel shall be assigned to that PMPU.

(5) If predominant use cannot be determined for a storage vessel that is shared among process units and if more than one of the process units are PMPUs that have different primary products and that are subject to this subpart, then the owner or operator shall assign the storage vessel to any one of the PMPUs sharing the storage vessel.

(6) If the predominant use of a storage vessel varies from year to year, then predominant use shall be determined based on the utilization that occurred during the year preceding June 1, 1999 or based on the expected utilization for the 5 years following June 1, 1999 for existing affected sources, whichever is more representative of the expected operations for that storage vessel, and based on the expected utilization for the 5 years after initial start-up for new affected sources. The determination of predominant use shall be reported in the Notification of Compliance Status, as required by §63.1439(e)(5)(v).

(7) Where a storage vessel is located at a major source that includes one or more process units which place material into or receive material from the storage vessel, but the storage vessel is located in a tank farm (including a marine tank farm), the applicability of this subpart shall be determined according to the provisions in paragraphs (f)(7)(i) through (iv) of this section.

(i) The storage vessel may only be assigned to a process unit that utilizes the storage vessel and does not have an intervening storage vessel for that product (or raw materials, as appropriate). With respect to any process unit, an intervening storage vessel
means a storage vessel connected by hard-piping to both the process unit and the storage vessel in the tank farm so that product or raw material entering or leaving the process unit flows into (or from) the intervening storage vessel and does not flow directly into (or from) the storage vessel in the tank farm.

(ii) If there is no process unit at the major source that meets the criteria of paragraph (f)(7)(i) of this section with respect to a storage vessel, this subpart does not apply to the storage vessel.

(iii) If there is only one process unit at the major source that meets the criteria of paragraph (f)(7)(i) of this section with respect to a storage vessel, the storage vessel shall be assigned to that process unit.

(iv) If there are two or more process units at the major source that meet the criteria of paragraph (f)(7)(i) of this section with respect to a storage vessel, the storage vessel shall be assigned to one of those process units according to the provisions of paragraphs (f)(3) through (6) of this section. The predominant use shall be determined among only those process units that meet the criteria of paragraph (f)(7)(i) of this section.

(g) Changes or additions to plant sites. The provisions of this paragraph apply to the owner or operator that changes or adds to their plant site or affected source.

(1) Adding a PMPU to a plant site. The provisions of paragraphs (g)(1)(i) and (ii) of this section apply to the owner or operator that adds one or more PMPUs to a plant site. A PMPU may be added to a plant site by constructing or reconstructing a process unit to produce polyether polyols. A PMPU may also be added to a plant site due to changes in production (anticipated production or actual past production) such that a polyether polyol becomes the primary product of a process unit that was not previously a PMPU.

(i) If a group of one or more PMPUs is added to a plant site, the added group of one or more PMPUs and their associated equipment, as listed in paragraph (a)(4) of this section, shall be a new affected source and shall comply with the requirements for a new affected source in this subpart upon initial start-up or by June 1, 1999, whichever is later, if the criteria specified in paragraph (g)(1)(i)(A) is met and either the criteria in paragraph (g)(1)(i)(B) or (C) of this section are met.

(A) The process units are new process units, as defined in §63.1423.

(B) The added group of one or more PMPUs and associated equipment, as listed in paragraph (a)(4) of this section, has the potential to emit 10 tons per year (9.1 megagrams per year) or more of any organic HAP or 25 tons per year (22.7 megagrams per year) or more of any combination of organic HAP, and polyether polyols are currently produced at the plant site as the primary product of an affected source.

(C) A polyether polyol is not currently produced at the plant site as the primary product of an affected source, and the plant site meets, or after the addition is constructed will meet, the General Provisions’ definition of a major source in §63.2.

(ii) If a group of one or more PMPUs is added to a plant site, and the added group of one or more PMPUs does not meet the criteria specified in paragraph (g)(1)(i)(A) of this section and one of the criteria specified in either paragraph (g)(1)(i)(B) or (C) of this section, and the plant site meets, or after the addition will meet, the definition of a major source, the owner or operator of the added group of one or more PMPUs and associated equipment, as listed in paragraph (a)(4) of this section, shall comply with the requirements for an existing affected source in this subpart upon initial start-up; by June 1, 2002; or by 6 months after notifying the Administrator that a process unit has been designated as a PMPU (in accordance with paragraph (g)(3) of this section), whichever is later.

(2) Adding emission points or making process changes to existing affected
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sources. The provisions of paragraphs (g)(2)(i) and (ii) of this section apply to the owner or operator that adds emission points or makes process changes to an existing affected source.

(i) If any process change or addition is made to an existing affected source that meets the criteria specified in paragraphs (g)(2)(i)(A) and (B) of this section, the entire affected source shall be a new affected source and shall comply with the requirements for a new affected source in this subpart upon initial start-up or by June 1, 1999.

(A) It is a process change or addition that meets the definition of reconstruction in §63.1423(b). For purposes of determining whether the fixed capital cost of the new components exceeds 50 percent of the fixed capital cost that would be required to construct an entire affected source, the equivalent capital cost shall be the entire potentially affected source; and

(B) Such reconstruction commenced after September 4, 1997.

(ii) If any process change is made or emission point is added to an existing affected source, and the process change or addition does not meet the criteria specified in paragraph (g)(2)(i)(A) of this section, the resulting emission point(s) shall be subject to the requirements for an existing affected source in this subpart. The resulting emission point(s) shall be in compliance upon initial start-up or by the appropriate compliance date specified in §63.1422 (i.e., December 1, 1999 for most equipment leak components, and June 1, 2002 for emission points other than equipment leaks).

(3) Determining what are and are not process changes. For purposes of paragraph (g) of this section, examples of process changes include, but are not limited to, additions in process equipment resulting in changes in production capacity; production of a product outside the scope of the compliance demonstration; or whenever there is a replacement, removal, or addition of recovery equipment. For purposes of paragraph (g) of this section, process changes do not include: Process upsets, unintentional temporary process changes, and changes that are within the equipment configuration and operating conditions documented in the Notification of Compliance Status report required by §63.1439(e)(5).

(4) Reporting requirements for owners or operators that change or add to their plant site or affected source. An owner or operator that changes or adds to their plant site or affected source, as discussed in paragraphs (g)(1) and (2) of this section, shall submit a report as specified in §63.1439(e)(7)(ii).

(h) Applicability of this subpart during periods of start-up, shutdown, malfunction, or non-operation. Paragraphs (h)(1) through (4) of this section shall be followed during periods of start-up, shutdown, malfunction, and non-operation of the affected source or any part thereof.

(1) The emission limitations set forth in this subpart and the emission limitations referred to in this subpart shall apply at all times except during periods of non-operation of the affected source (or specific portion thereof) resulting in cessation of the emissions to which this subpart applies. These emission limitations shall not apply during periods of start-up, shutdown, or malfunction, during which the owner or operator shall follow the applicable provisions of the start-up, shutdown, and malfunction plan required by §63.6(e)(3). However, if a start-up, shutdown, malfunction, or period of non-operation of one portion of an affected source does not affect the ability of a particular emission point to comply with the emission limitations to which it is subject, then that emission point shall still be required to comply with the applicable emission limitations of this subpart during the start-up, shutdown, malfunction, or period of non-operation. For example, if there is an overpressure in the reactor area, a storage vessel that is part of the affected source would still be required to be controlled in accordance with the storage tank provisions in §63.1432. Similarly, the degassing of a storage vessel would not affect the ability of a process vent to meet the emission limitations for process vents in §§63.1425 through 63.1430.

(2) The emission limitations set forth in 40 CFR part 63, subpart H, as referred to in the equipment leak provisions in §63.1434, shall apply at all
times except during periods of non-operation of the affected source (or specific portion thereof) in which the lines are drained and depressurized resulting in cessation of the emissions to which §63.1434 applies, or during periods of start-up, shutdown, malfunction, or process unit shutdown (as defined in §63.161).

(3) The owner or operator shall not shut down items of equipment that are required or utilized for compliance with this subpart during periods of start-up, shutdown, malfunction during times when emissions (or, where applicable, wastewater streams or residuals) are being routed to such items of equipment if the shutdown would contravene requirements applicable to such items of equipment. This paragraph does not apply if the item of equipment is malfunctioning. This paragraph also does not apply if the owner or operator shuts down the compliance equipment (other than monitoring systems) to avoid damage due to a contemporaneous start-up, shutdown, or malfunction of the affected source or portion thereof. If the owner or operator has reason to believe that monitoring equipment would be damaged due to a contemporaneous start-up, shutdown, or malfunction of the affected source or portion thereof, the owner or operator shall provide documentation supporting such a claim in the Precompliance Report or in a supplement to the Precompliance Report, as provided for in §63.1439(e)(4). Once approved by the Administrator in accordance with §63.1439(e)(4)(vii), the provision for ceasing to collect, during a start-up, shutdown, or malfunction, monitoring data that would otherwise be required by the provisions of this subpart shall be incorporated into the start-up, shutdown, malfunction plan for that affected source, as stated in §63.1439(b)(1).

(4) During start-ups, shutdowns, and malfunctions when the emission limitations of this subpart do not apply pursuant to paragraphs (h)(1) through (3) of this section, the owner or operator shall implement, to the extent reasonably available, measures to prevent or minimize excess emissions to the extent practicable. For purposes of this paragraph, the term “excess emissions” means emissions in excess of those that would have occurred if there were no start-up, shutdown, or malfunction and the owner or operator complied with the relevant provisions of this subpart. The measures to be taken shall be identified in the applicable start-up, shutdown, and malfunction plan, and may include, but are not limited to, air pollution control technologies, recovery technologies, work practices, pollution prevention, monitoring, and/or changes in the manner of operation of the affected source. Use of back-up control techniques is not required, but is allowed, if available.

§ 63.1421 Delegation of authority.

(a) In delegating implementation and enforcement authority to a State under section 112(l) of the Act, the authorities contained in paragraph (b) of this section shall be retained by the Administrator and not transferred to a State.

(b) Authorities which will not be delegated to the States: the permission to use an alternative means of emission limitation, from §63.6(g), and the authority of §63.177.

§ 63.1422 Compliance dates and relationship of this rule to existing applicable rules.

(a) [Reserved]

(b) New affected sources that commence construction or reconstruction after September 4, 1997 shall be in compliance with this subpart upon initial start-up or by June 1, 1999, whichever is later, as provided in §63.6(b).

(c) Existing affected sources shall be in compliance with this subpart (except for §63.1434 for which compliance is covered by paragraph (d) of this section) no later than June 1, 1999, unless an extension has been granted as specified in paragraph (e) of this section.

(d) Except as provided for in paragraphs (d)(1) through (5) of this section, existing affected sources shall be in compliance with §63.1434 no later than December 1, 1999 unless an extension has been granted as specified in paragraph (e) of this section.

(1) Compliance with the compressor provisions of §63.164 shall occur no
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later than June 1, 2000 for any compressor meeting one or more of the criteria in paragraphs (d)(1)(i) through (iv) of this section, if the work can be accomplished without a process unit shutdown, as defined in §63.161.

(i) The seal system will be replaced.
(ii) A barrier fluid system will be installed.
(iii) A new barrier fluid will be utilized which requires changes to the existing barrier fluid system.
(iv) The compressor shall be modified to permit connecting the compressor to a closed vent system.

(2) Compliance with the compressor provisions of §63.164 shall occur no later than December 1, 2000, for any compressor meeting all the criteria in paragraphs (d)(2)(i) through (iv) of this section.

(i) The compressor meets one or more of the criteria specified in paragraphs (d)(1)(i) through (iv) of this section.
(ii) The work can be accomplished without a process unit shutdown as defined in §63.161.
(iii) The additional time is necessary, due to the unavailability of parts beyond the control of the owner or operator.
(iv) The owner or operator submits the request for a compliance extension to the appropriate U.S. Environmental Protection Agency Regional Office at the addresses listed in §63.13 no later than 45 days before December 1, 1999. The request for a compliance extension shall contain the information specified in §63.6(i)(6)(i)(A), (B), and (D). Unless the EPA Regional Office objects to the request for a compliance extension within 30 days after receipt of the request, the request shall be deemed approved.

(3) If compliance with the compressor provisions of §63.164 cannot reasonably be achieved without a process unit shutdown, as defined in §63.161, the owner or operator shall achieve compliance no later than June 1, 2001. The owner or operator who elects to use this provision shall submit a request for an extension of compliance in accordance with the requirements of paragraph (d)(3)(ii) of this section.

(i) Compliance cannot be achieved without replacing the compressor.
(ii) Compliance cannot be achieved without recasting the distance piece.
(iii) Design modifications are required to connect to a closed-vent system.

(4) Compliance with the surge control vessel and bottoms receiver provisions of §63.170 shall occur no later than June 1, 2002.

(e) Pursuant to section 112(i)(3)(B) of the Act, an owner or operator may request an extension allowing the existing affected source up to 1 additional year to comply with section 112(d) standards. For purposes of this subpart, a request for an extension shall be submitted to the permitting authority as part of the operating permit application or to the Administrator as a separate submittal or as part of the Precompliance Report. Requests for extensions shall be submitted no later than 120 days prior to the compliance dates specified in paragraphs (b) through (d) of this section, except as discussed in paragraph (e)(3) of this section. The dates specified in §63.6(i) for submittal of requests for extensions shall not apply to this subpart.

(1) A request for an extension of compliance shall include the data described in §63.6(i)(6)(i)(A), (B), and (D).

(2) The requirements in §63.6(i)(8) through (14) shall govern the review and approval of requests for extensions of compliance with this subpart.

(3) An owner or operator may submit a compliance extension request after the date specified in paragraph (e) of this section, provided that the need for the compliance extension arose after that date, and the need arose due to circumstances beyond reasonable control of the owner or operator. This request shall include, in addition to the information specified in paragraph (e)(1) of this section, a statement of the reasons additional time is needed and
the date when the owner or operator first learned of the problem.

(f) Table 1 of this subpart specifies the requirements in 40 CFR part 63, subpart A (the General Provisions) that apply and those that do not apply to owners and operators of affected sources subject to this subpart. For the purposes of this subpart, Table 3 of 40 CFR part 63, subpart F is not applicable.

(g) Table 2 of this subpart summarizes the provisions of 40 CFR part 63, subparts F, G, and H (collectively known as the “HON”) that apply and those that do not apply to owners and operators of affected sources subject to this subpart.

(h)(1) After the compliance dates specified in this section, an affected source subject to this subpart that is also subject to the provisions of 40 CFR part 63, subpart I, is required to comply only with the provisions of this subpart.

(2) Sources subject to the provisions in 40 CFR part 63, subpart I, that have elected to comply through a quality improvement program, as specified in §63.175 or §63.176 or both, may elect to continue these programs without interruption as a means of complying with this subpart. In other words, becoming subject to this subpart does not restart or reset the “compliance clock” as it relates to reduced burden earned through a quality improvement program.

(i) After the compliance dates specified in this section, a storage vessel that is assigned to an affected source subject to this subpart that is also subject to the provisions of 40 CFR part 63, subpart Kb (Standards of Performance for Volatile Organic Liquid Storage Vessels (Including Petroleum Liquid Storage Vessels) for Which Construction, Reconstruction, or Modification Commenced after July 23, 1984) is required to comply only with the provisions of this subpart. After the compliance dates specified in this section, that storage vessel shall no longer be subject to 40 CFR part 63, subpart Kb.

(j) After the compliance dates specified in this subpart, if any combustion device, recovery device or recapture device subject to this subpart is also subject to monitoring, recordkeeping, and reporting requirements for hazardous waste, disposal, and treatment facilities in 40 CFR part 264, subpart AA (Air Emission Standards for Process Vents) or subpart CC (Air Emission Standards for Tanks, Surface Impoundments, and Containers), the owner or operator may comply with either paragraph (j)(1) or (2) of this section. If, after the compliance dates specified in this subpart, any combustion device, recovery device, or recapture device subject to this subpart is subject to monitoring and recordkeeping requirements hazardous waste treatment, storage, and disposal facilities in 40 CFR part 265, subpart AA (Air Emission Standards for Process Vents) or subpart CC (Air Emission Standards for Tanks, Surface Impoundments, and Containers), the owner or operator may comply with either paragraph (j)(1) or (3) of this section. If the owner or operator elects to comply with either paragraph (j)(2) or (3) of this section, the owner or operator shall notify the Administrator of this choice in the Notification of Compliance Status required by §63.1439(e)(5).

(1) The owner or operator shall comply with the monitoring, recordkeeping and reporting requirements of this subpart.

(2) The owner or operator shall comply with the monitoring, recordkeeping and reporting requirements in 40 CFR part 264, with the following exception. All excursions, as defined in §63.1438(f), shall be reported in the periodic report. Compliance with this paragraph shall constitute compliance with the monitoring, recordkeeping and reporting requirements of this subpart.

(3) The owner or operator shall comply with the monitoring and recordkeeping requirements of 40 CFR part 265, subpart AA or subpart CC, and the periodic reporting requirements under 40 CFR part 264, subpart AA or subpart CC, that would apply to the device if the facility had final-permitted status, with the following exception. All excursions, as defined in §63.1438(f), shall be reported in the periodic report. Compliance with this paragraph shall constitute compliance with the monitoring, recordkeeping and reporting requirements of this subpart.
(k) Paragraphs (k)(1) and (2) of this section address instances in which requirements from other regulations overlap for the same heat exchange system(s) or waste management unit(s) that are subject to this subpart.

(1) After the applicable compliance date specified in this subpart, if a heat exchange system subject to this subpart is also subject to a standard identified in paragraph (k)(1)(i) or (ii) of this section, compliance with the applicable provisions of the standard identified in paragraph (k)(1)(i) or (ii) shall constitute compliance with the applicable provisions of this subpart with respect to that heat exchange system.

(i) 40 CFR part 63, subpart F.

(ii) A subpart of this part which requires compliance with the HON heat exchange system requirements in §63.104 (e.g., 40 CFR part 63, subpart JJJ or U).

(2) After the applicable compliance date specified in this subpart, if any waste management unit subject to this subpart is also subject to a standard identified in paragraph (k)(2)(i) or (ii) of this section, compliance with the applicable provisions of the standard identified in paragraph (k)(2)(i) or (ii) shall constitute compliance with the applicable provisions of this subpart with respect to that waste management unit.

(i) 40 CFR part 63, subpart G.

(ii) A subpart of this part which requires compliance with the HON process wastewater provisions in §§63.132 through 63.147 (e.g., subpart JJJ or U).

(l) All terms in this subpart that define a period of time for completion of required tasks (e.g., monthly, quarterly, annually), unless specified otherwise in the section or subsection that imposes the requirement, refer to the standard calendar periods, unless altered by mutual agreement between the owner or operator and the Administrator, as specified in the General Provisions in 40 CFR part 63, subpart A (e.g., a period could begin on the compliance date or another date, rather than on the first day of the standard calendar period). For each time period that is changed by agreement, the revised period shall remain in effect until it is changed. A new request is not necessary for each recurring period.

(2) Where the period specified for compliance is a standard calendar period, if the initial compliance date occurs after the beginning of the period, compliance shall be required according to the schedule specified in paragraphs (l)(2)(i) or (ii) of this section, as appropriate.

(i) Compliance shall be required before the end of the standard calendar period within which the compliance deadline occurs, if there remains at least 2 weeks for tasks that shall be performed monthly, at least 1 month for tasks that shall be performed each quarter, or at least 3 months for tasks that shall be performed annually; or

(ii) In all other cases, compliance shall be required before the end of the first full standard calendar period after the period within which the initial compliance deadline occurs.

(3) In all instances where a provision of this subpart requires completion of a task during each of multiple successive periods, an owner or operator may perform the required task at any time during the specified period, provided that the task is conducted at a reasonable interval after completion of the task during the previous period.

§63.1423 Definitions.

(a) The following terms used in this subpart shall have the meaning given them in subparts A (§63.2), F (§63.101), G (§63.111), and H (§63.161) as specified after each term:

Act (subpart A)

Administrator (subpart A)

Automated monitoring and recording system (subpart G)

Boiler (subpart G)

Bottoms receiver (subpart H)

By-product (subpart F)

Car-seal (subpart G)

Closed-vent system (subpart G)

Combustion device (subpart G)

Commenced (subpart A)

Compliance date (subpart A)
Environmental Protection Agency

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Continuous monitoring system (subpart A)
Emission standard (subpart A)
EPA (subpart A)
Equipment (subpart H)
Flow indicator (subpart G)
Fuel gas (subpart F)
Fuel gas system (subpart F)
Hard-piping (subpart G)
Heat exchange system (subpart F)
Impurity (subpart F)
Incinerator (subpart G)
Major source (subpart A)
Malfunction (subpart A)
Open-ended valve or line (subpart H)
Operating permit (subpart F)
Organic monitoring device (subpart G)
Owner or operator (subpart A)
Performance evaluation (subpart A)
Performance test (subpart A)
Permitting authority (subpart A)
Plant site (subpart F)
Potential to emit (subpart A)
Primary fuel (subpart G)
Process heater (subpart G)
Process unit shutdown (subpart H)
Reactor (subpart G)
Recapture device (subpart G)
Relief valve (subpart G)
Research and development facility (subpart F)
Run (subpart A)
Secondary fuel (subpart G)
Sensor (subpart H)
Specific gravity monitoring device (subpart G)
Start-up, shutdown, and malfunction plan (subpart F)
State (subpart A)
Surge control vessel (subpart H)
Temperature monitoring device (subpart G)
Test method (subpart A)
Total resource effectiveness index value (subpart G)
Treatment process (subpart G)
Visible emission (subpart A)

(b) All other terms used in this subpart shall have the meaning given them in this section.

Annual average concentration, as used in conjunction with the wastewater provisions, means the flow-weighted annual average concentration and is determined by the procedures in §63.144(b), except as provided in §63.1433(a)(2).

Annual average flow rate, as used in conjunction with the wastewater provisions, is determined by the procedures in §63.144(c).

Batch cycle means the step or steps, from start to finish, that occur in a batch unit operation.

Batch unit operation means a unit operation involving intermittent or discontinuous feed into equipment, and, in general, involves the emptying of equipment after the batch cycle ceases and prior to beginning a new batch cycle. Mass, temperature, concentration and other properties of the process may vary with time. Addition of raw material and withdrawal of product do not simultaneously occur in a batch unit operation.

Catalyst extraction means the removal of the catalyst using either solvent or physical extraction method.

Construction means the on-site fabrication, erection, or installation of a facility whose principal purpose is the production of a product. Construction also means the on-site fabrication, erection, or installation of a process unit or a combination of process units which subsequently becomes an affected source or part of an affected source due to a change in primary product.

Continuous record means documentation, either in hard copy or computer readable form, of data values measured at least once during approximately equal intervals of 15 minutes and recorded at the frequency specified in §63.1439(d).

Continuous recorder is defined in §63.111, except that when the definition in §63.111 reads “or records 15-minute or more frequent block average values,” the phrase “or records 1-hour or more frequent block average values” shall apply for purposes of this subpart.

Continuous unit operation means a unit operation where the inputs and outputs flow continuously. Continuous unit operations typically approach steady-state conditions. Continuous unit operations typically involve the simultaneous addition of raw material and withdrawal of the product.

Control technique means any equipment or process control used for capturing, recovering, or oxidizing organic hazardous air pollutant vapors. Such equipment includes, but is not limited to, absorbers, adsorbers, boilers, condensers, flares, incinerators, process
heaters, and scrubbers, or any combination thereof. Process control includes extended cookout (as defined in this section). Condensers operating as reflux condensers that are necessary for processing, such as liquid level control, temperature control, or distillation operation, shall be considered inherently part of the process and will not be considered control techniques.

Emission point means an individual process vent, storage vessel, wastewater stream, or equipment leak.

Epoxide means a chemical compound consisting of a three-membered cyclic ether. Only emissions of epoxides listed in Table 4 of this subpart (i.e., ethylene oxide and propylene oxide) are regulated by the provisions of this subpart.

Equipment leak means emissions of organic HAP from a pump, compressor, agitator, pressure relief device, sampling connection system, open-ended valve or line, valve, surge control vessel, bottoms receiver, or instrumentation system in organic HAP service.

Extended Cookout (ECO) means a control technique that reduces the amount of unreacted ethylene oxide (EO) and/or propylene oxide (PO) in the reactor. This is accomplished by allowing the product to react for a longer time period, thereby having less unreacted epoxides and reducing epoxides emissions that may have otherwise occurred.

Flexible operation unit means a process unit that manufactures different chemical products by periodically alternating raw materials fed to the process unit or operating conditions at the process unit. These units are also referred to as campaign plants or blocked operations.

Group 1 combination of batch process vents means a collection of process vents in a PMPU from batch unit operations that are associated with the use of a nonepoxide organic HAP to make or modify the product that is not classified as a Group 1 combination of batch process vents.

Group 1 continuous process vent means a process vent from a continuous unit operation that is associated with the use of a nonepoxide organic HAP to make or modify the product that meets all of the following conditions:

1. Has a flow rate greater than or equal to 0.005 standard cubic meters per minute,
2. Has a total organic HAP concentration greater than or equal to 50 parts per million by volume, and
3. Has a total resource effectiveness index value, calculated in accordance with §63.1428(h)(3), less than or equal to 1.0.

Group 2 continuous process vent means a process vent from a continuous unit operation that is associated with the use of a nonepoxide organic HAP to make or modify the product that is not classified as a Group 1 continuous process vent.

Group 1 storage vessel means a storage vessel that meets the applicability criteria specified in Table 3 of this subpart.

Flexible operation unit means a storage vessel that does not fall within the definition of a Group 1 storage vessel.

Group 1 wastewater stream means a process wastewater stream at an existing or new affected source that meets the criteria for Group 1 status in §63.132(c), with the exceptions listed in §63.1433(a)(2) for the purposes of this subpart (i.e., for organic HAP listed on Table 4 of this subpart only).

Group 2 wastewater stream means any process wastewater stream as defined in §63.101 at an existing affected source that does not meet the definition (in this section) of a Group 1 wastewater stream.

Inorganic hazardous air pollutant service or in organic HAP service means that a piece of equipment either contains or contacts a fluid (liquid or gas) that is
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at least 5 percent by weight of total organic HAP (as defined in this section), as determined according to the provisions of §63.180(d). The provisions of §63.180(d) also specify how to determine that a piece of equipment is not in organic HAP service.

Initial start-up means the first time a new or reconstructed affected source begins production, or, for equipment added or changed as described in §63.1420(g), the first time the equipment is put into operation to produce a polyether polyl. Initial start-up does not include operation solely for testing equipment. Initial start-up does not include subsequent start-ups of an affected source or portion thereof following malfunctions or shutdowns or following changes in product for flexible operation units. Further, for purposes of §63.1422, initial start-up does not include subsequent start-ups of affected sources or portions thereof following malfunctions or process unit shutdowns.

Maintenance wastewater is defined in §63.101, except that the term “polyether polyl manufacturing process unit” shall apply whenever the term “chemical manufacturing process unit” is used. Further, the generation of wastewater from the routine rinsing or washing of equipment in batch operation between batches is not maintenance wastewater, but is considered to be process wastewater, for the purposes of this subpart.

Make or modify the product means to produce the polyether polyl by polymerization of epoxides or other cyclic ethers with compounds having one or more reactive hydrogens (i.e., a hydrogen atom bonded to nitrogen, oxygen, phosphorus, sulfur, etc.) to form polyethers (i.e., compounds with two or more ether bonds). This definition of “polyether polyl” excludes hydroxyethyl cellulose and materials regulated under 40 CFR part 63, subparts F, G, and H (the HON), such as glycols and glycol ethers.

Polyether polyl manufacturing process unit (PMPU) means a process unit that manufactures a polyether polyl as its primary product, or a process unit designated as a polyether polyl manufacturing unit in accordance with §63.1420(e)(2). A polyether polyl manufacturing process unit consists of more than one unit operation. This collection of equipment includes purification systems, reactors and their associated product separators and recovery devices, distillation units and their associated distillate receivers and recovery devices, distillation units and their associated distillate receivers and recovery
devices, other associated unit operations, storage vessels, surge control vessels, bottoms receivers, product transfer racks, connected ducts and piping, combustion, recovery, or recapture devices or systems, and the equipment (i.e., all pumps, compressors, agitators, pressure relief devices, sampling connection systems, open-ended valves or lines, valves, connectors, and instrumentation systems that are associated with the PMPU) that are subject to the equipment leak provisions as specified in §63.1434.

Pressure decay curve is the graph of the reactor pressure versus time from the point when epoxide feed is stopped until the reactor pressure is constant, indicating that most of the epoxide has reacted out of the vapor and liquid phases. This curve shall be determined with no leaks or vents from the reactor.

Primary product is defined in and determined by the procedures specified in §63.1420(e).

Process unit means a collection of equipment assembled and connected by pipes or ducts to process raw materials and to manufacture a product.

Process vent means a point of emission from a unit operation having a gaseous stream that is discharged to the atmosphere either directly or after passing through one or more combustion, recovery, or recapture devices. A process vent from a continuous unit operation is a gaseous emission stream containing more than 0.005 weight-percent total organic HAP. A process vent from a batch unit operation is a gaseous emission stream containing more than 225 kilograms per year (500 pounds per year) of organic HAP emissions. Unit operations that may have process vents are condensers, distillation units, reactors, or other unit operations within the PMPU. Process vents exclude pressure relief valve discharges, gaseous streams routed to a fuel gas system(s), and leaks from equipment regulated under §63.1434. A gaseous emission stream is no longer considered to be a process vent after the stream has been controlled and monitored in accordance with the applicable provisions of this subpart.

Reactor liquid means the compound or material made in the reactor, even though the substance may be transferred to another vessel. This material may require further modifications before becoming a final product, in which case the reactor liquid is classified as an “intermediate.” This material may be complete at this stage, in which case the reactor liquid is classified as a “product.”

Reconstruction means the replacement of components of an affected source or of a previously unaffected stationary source that becomes an affected source as a result of the replacement, to such an extent that:

Process wastewater means wastewater which, during manufacturing or processing, comes into direct contact with or results from the production or use of any raw material, intermediate product, finished product, by-product, or waste product. Examples are product tank drawdown or feed tank drawdown; water formed during a chemical reaction or used as a reactant; water used to wash impurities from organic products or reactants; equipment washes between batches in a batch process; water used to cool or quench organic vapor streams through direct contact; and condensed steam from jet ejector systems pulling vacuum on vessels containing organics.

Product means a compound or material which is manufactured by a process unit. By-products, isolated intermediates, impurities, wastes, and trace contaminants are not considered products.

Product class means a group of polyether polyols with a similar pressure decay curve (or faster pressure decay curves) that are manufactured within a given set of operating conditions representing the decline in pressure versus time. All products within a product class shall have an essentially similar pressure decay curve, and operate within a given set of operating conditions. These operating conditions are: a minimum reaction temperature; the number of -OH groups in the polyol; a minimum catalyst concentration; the type of catalyst (e.g., self-catalyzed, base catalyst, or acid catalyst); the epoxide ratio, or a range for that ratio; and the reaction conditions of the system (e.g., the size of the reactor, or the size of the batch).

Reactor liquid means the compound or material made in the reactor, even though the substance may be transferred to another vessel. This material may require further modifications before becoming a final product, in which case the reactor liquid is classified as an “intermediate.” This material may be complete at this stage, in which case the reactor liquid is classified as a “product.”

Reconstruction means the replacement of components of an affected source or of a previously unaffected stationary source that becomes an affected source as a result of the replacement, to such an extent that:
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(1) The fixed capital cost of the new components exceeds 50 percent of the fixed capital cost that would be required to construct a comparable new source; and

(2) It is technologically and economically feasible for the reconstructed source to meet the provisions of this subpart.

Recovery device means an individual unit of equipment capable of and normally used for the purpose of recovering chemicals for fuel value (i.e., net positive heating value), use, reuse, or for sale for fuel value, use, or reuse. Examples of equipment that may be recovery devices include absorbers, carbon absorbers, condensers (except reflux condensers), oil-water separators or organic-water separators, or organic removal devices such as decanters, strippers, or thin film evaporation units. For the purposes of the monitoring, recordkeeping, or reporting requirements of this subpart, recapture devices are considered to be recovery devices.

Residual is defined in §63.111, except that when the definition in §63.111 uses the term “Table 9 compounds,” the term “organic HAP listed in Table 9 of subpart G” shall apply, for the purposes of this subpart.

Shutdown means the cessation of operation of an affected source, a PMPU within an affected source, a waste management unit or unit operation within an affected source, equipment required or used to comply with this subpart, or the emptying or degassing of a storage vessel. The purposes for a shutdown may include, but are not limited to, periodic maintenance, replacement of equipment, or equipment repairs. Shutdown does not include the normal periods between batch cycles. For continuous unit operations, shutdown includes transitional conditions due to changes in product for flexible operation units. For batch unit operations, shutdown does not include transitional conditions due to changes in product for flexible operation units.

Steady-state conditions means that all variables (temperatures, pressures, volumes, flow rates, etc.) in a process do not vary significantly with time; minor fluctuations about constant mean values may occur.

Storage vessel means a tank or other vessel that is used to store liquids that contain one or more organic HAP. Storage vessels do not include:

1. Vessels permanently attached to motor vehicles such as trucks, railcars, barges, or ships;
2. Pressure vessels designed to operate in excess of 204.9 kilopascals and without emissions to the atmosphere;
3. Vessels with capacities smaller than 38 cubic meters;
4. Vessels and equipment storing and/or handling material that contains no organic HAP, or organic HAP as impurities only;
5. Surge control vessels and bottoms receiver tanks;
6. Wastewater storage tanks; and
7. Storage vessels assigned to another process unit regulated under another subpart of part 63.

Total organic compounds (TOC) are those compounds, excluding methane and ethane, measured according to the procedures of Method 18 or Method 25A of 40 CFR part 60, appendix A.

Unit operation means one or more pieces of process equipment used to make a single change to the physical or chemical characteristics of one or more process streams. Unit operations include, but are not limited to, reactors, distillation units, extraction columns, absorbers, decanters, condensers, and filtration equipment.
Vent stream, as used in reference to process vents, means the emissions from a process vent.

Waste management unit is defined in §63.111, except that when the definition in §63.111 uses the term "chemical manufacturing process unit," the term "PMPU" shall apply for the purposes of this subpart.

Wastewater means water that:

(1) Contains either
   (i) An annual average concentration of organic HAP listed in Table 4 of this subpart of at least 5 parts per million by weight and has an annual average flow rate of 0.02 liter per minute or greater, or
   (ii) An annual average concentration of organic HAP listed on Table 4 of this subpart of at least 10,000 parts per million by weight at any flow rate; and
(2) Is discarded from a PMPU that is part of an affected source. Wastewater is process wastewater or maintenance wastewater.

§63.1424 Emission standards.

(a) Except as provided under paragraph (b) of this section, the owner or operator of an existing or new affected source shall comply with the provisions in:
   (1) Sections 63.1425 through 63.1430 for process vents;
   (2) Section 63.1432 for storage vessels;
   (3) Section 63.1433 for wastewater;
   (4) Section 63.1434 for equipment leaks;
   (5) Section 63.1435 for heat exchangers;
   (6) Section 63.1437 for additional test methods and procedures;
   (7) Section 63.1438 for monitoring levels and excursions; and
   (8) Section 63.1439 for general reporting and recordkeeping requirements.

(b) When emissions of different kinds (i.e., emissions from process vents subject to §63.1425 through 63.1430, storage vessels subject to §63.1432, process wastewater, and/or in-process equipment subject to §63.1449) are combined, and at least one of the emission streams would require control according to the applicable provision in the absence of combination with other emission streams, the owner or operator shall comply with the requirements of either paragraph (b)(1) or (2) of this section.

(1) Comply with the applicable requirements of this subpart for each kind of emission in the stream as specified in paragraphs (a)(1) through (5) of this section; or

(2) Comply with the most stringent set of requirements that applies to any individual emission stream that is included in the combined stream, where either that emission stream would be classified as requiring control in the absence of combination with other emission streams, or the owner chooses to consider that emission stream to require control for the purposes of this paragraph.

§63.1425 Process vent control requirements.

(a) Applicability of process vent control requirements. For each process vent at an affected source, the owner or operator shall comply with the provisions of this section. Owners and operators of all affected sources using epoxides in the production of polyether polyols are subject to the requirements of paragraph (b) of this section. Owners or operators are subject to the requirements of paragraph (c) of this section only if epoxides are used in the production of polyether polyols and nonepoxide organic HAP are used to make or modify the product. Similarly, owners or operators are subject to the requirements of paragraph (d) of this section only if epoxides are used in the production of polyether polyols and organic HAP are used in catalyst extraction. The owner or operator of an affected source where polyether polyl products are produced using tetrahydrofuran shall comply with paragraph (f) of this section.

(b) Requirements for epoxide emissions. The owner or operator of an affected source where polyether polyl products are produced using epoxides shall reduce epoxide emissions from process vents from batch unit operations and continuous unit operations within each PMPU in accordance with either paragraph (b)(1) or (2) of this section.

(1) For new affected sources, the owner or operator shall comply with paragraph (b)(1)(i), (ii), or (iii) this section. The owner or operator also has
the option of complying with a combination of paragraphs (b)(1)(i) and (ii) of this section. If the owner or operator chooses to comply with a combination of paragraphs (b)(1)(i) and (ii) of this section, each process vent not controlled in accordance with paragraph (b)(1)(ii) of this section shall then comply with paragraph (b)(1)(i) of this section.

(i) Reduce the total epoxide emissions from each process vent using a flare;

(ii) Reduce the total epoxide emissions from the group of applicable process vents by an aggregated 99.9 percent;

(iii) Maintain an emission factor of no greater than 4.43 × 10^{-3} kilogram epoxide emissions per megagram of product (4.43 × 10^{-3} pounds epoxide emissions per 1,000 pounds of product) for all process vents in the PMPU.

(2) For existing affected sources, the owner or operator shall comply with either paragraph (b)(2)(i), (ii), (iii), or (iv) of this section. The owner or operator also has the option of complying with a combination of paragraphs (b)(2)(ii) and (iii) of this section. If the owner or operator chooses to comply with a combination of paragraphs (b)(2)(ii) and (iii) of this section, each process vent that is not controlled in accordance with paragraph (b)(2)(iii) of this section shall then comply with paragraph (b)(2)(ii) of this section.

(i) Reduce the total epoxide emissions from the group of applicable process vents by an aggregated 99.9 percent;

(ii) Maintain an outlet concentration of total epoxides or TOC after each combustion, recapture, or recovery device of 20 ppmv or less; or

(iii) Maintain an emission factor of no greater than 4.43 × 10^{-3} kilogram epoxide emissions per megagram of product (4.43 × 10^{-3} pounds epoxide emissions per 1,000 pounds of product) for all process vents in the PMPU.

(c) Requirements for nonepoxide organic HAP emissions from making or modifying the product. The owner or operator of a new or existing source where polyether polyols are produced using epoxides, and where nonepoxide organic HAP are used to make or modify the product, shall comply with this paragraph. For each process vent from a continuous unit operation that is associated with the use of nonepoxide organic HAP to make or modify the product, the owner or operator shall determine if the process vent is a Group 1 continuous process vent, as defined in §63.1423. For the combination of process vents from batch unit operations that are associated with the use of a nonepoxide organic HAP to make or modify the product, the owner or operator shall determine if the combination of process vents is a Group 1 combination of batch process vents, as defined in §63.1423.

(1) Requirements for Group 1 combinations of batch process vents. For each Group 1 combination of batch process vents, as defined in §63.1423, the owner or operator shall comply with either paragraph (c)(1)(i) or (ii) of this section.

(i) Reduce nonepoxide organic HAP emissions using a flare.

(ii) Reduce nonepoxide organic HAP emissions by 90 percent using a combustion, recovery, or recapture device.

(2) Requirements for Group 2 combinations of batch process vents. For each Group 2 combination of batch process vents, as defined in §63.1423, the owner or operator reassess the group status when process changes occur, in accordance with the provisions of §63.1428(g). No control requirements apply to these process vents.

(3) Requirements for Group 1 continuous process vents. For each Group 1 continuous process vent, as defined in §63.1423, the owner or operator shall comply with either paragraph (c)(3)(i) or (ii) of this section.

(i) Reduce nonepoxide organic HAP emissions using a flare.

(ii) Reduce nonepoxide organic HAP emissions by 98 percent using a combustion, recovery, or recapture device.
(4) Requirements for Group 2 continuous process vents. For each Group 2 continuous process vent, as defined in §63.1423, the owner or operator shall comply with either paragraph (c)(4)(i) or (ii) of this section.

(i) If the TRE for the process vent is greater than 1.0 but less than 4.0, the owner or operator shall comply with the monitoring provisions in §63.1429, the recordkeeping provisions in §63.1430(d), and recalculate the TRE index value when process changes occur, in accordance with the provisions in §63.1428(h)(2).

(ii) If the TRE for the process vent is greater than 4.0, the owner or operator shall recalculate the TRE index value when process changes occur, in accordance with the provisions in §63.1428(h)(2).

(d) Requirements for nonepoxide organic HAP emissions from catalyst extraction. The owner or operator of a new or existing affected source where polyether polyol products are produced using epoxide compounds shall comply with either paragraph (d)(1) or (2) of this section. A PMPU that does not use any nonepoxide organic HAP in catalyst extraction is exempt from the requirements of this paragraph.

(1) Reduce emissions of nonepoxide organic HAP from all process vents associated with catalyst extraction using a flare; or

(2) Reduce emissions of nonepoxide organic HAP from the sum total of all process vents associated with catalyst extraction by an aggregated 90 percent for each PMPU.

(e) [Reserved]

(f) Requirements for process vents at PMPUs that produce polyether polyol products using tetrahydrofuran. For each process vent in a PMPU that uses tetrahydrofuran (THF) to produce one or more polyether polyol products that is, or is part of, an affected source, the owner or operator shall comply with the HON process vent requirements in §63.113 through 63.118, except as provided for in paragraphs (f)(1) through (10) of this section.

(1) When December 31, 1992 is referred to in the HON process vent requirements in §63.113, it shall be replaced with September 4, 1997, for the purposes of this subpart.

(2) When §63.151(f), alternative monitoring parameters, and §63.152(e), submission of an operating permit application, are referred to in §§63.114(c) and 63.117(e), §63.1439(f), alternative monitoring parameters, and §63.1439(e)(18), submission of an operating permit application, respectively, shall apply for the purposes of this subpart.

(3) When the Notification of Compliance Status requirements contained in §63.152(b) are referred to in §§63.114, 63.117, and 63.118, the Notification of Compliance Status requirements contained in §63.1439(e)(5) shall apply for the purposes of this subpart.

(4) When the Periodic Report requirements contained in §63.152(c) are referred to in §§63.117 and 63.118, the Periodic Report requirements contained in §63.1439(e)(6) shall apply for the purposes of this subpart.

(5) When the definition of excursion in §63.152(c)(2)(ii)(A) is referred to in §63.118(f)(2), the definition of excursion in §63.1438(f) shall apply for the purposes of this subpart.

(6) When §63.114(e) specifies that an owner or operator shall submit the information required in §63.152(b) in order to establish the parameter monitoring range, the owner or operator shall comply with the provisions of §63.1438 for establishing the parameter monitoring level and shall comply with §63.1439(e)(5)(ii) or §63.1439(e)(6) for the purposes of reporting information related to the establishment of the parameter monitoring level, for the purposes of this subpart. Further, the term “level” shall apply whenever the term “range” is used in §§63.114, 63.117, and 63.118.

(7) When reports of process changes are required under §63.118(g), (h), (i), or (j), paragraphs (f)(7)(i) through (iv) of this section shall apply for the purposes of this subpart.

(i) For the purposes of this subpart, whenever a process change, as defined in §63.115(e), is made that causes a Group 2 process vent to become a Group 1 process vent, the owner or operator shall submit a report within 180 days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included...
in the next Periodic Report. A description of the process change shall be included in this report.

(ii) Whenever a process change, as defined in §63.115(e), is made that causes a Group 2 process vent with a TRE greater than 4.0 to become a Group 2 process vent with a TRE less than 4.0, the owner or operator shall submit a report within 180 days after the process change is made or the information regarding the process change is known to the owner or operator, unless the flow rate is less than 0.005 standard cubic meters per minute. This report may be included in the next Periodic Report. A description of the process change shall be included in this report.

(iii) Whenever a process change, as defined in §63.115(e), is made that causes a Group 2 process vent with a flow rate less than 0.005 standard cubic meter per minute (scmm) to become a Group 2 process vent with a flow rate of 0.005 scmm or greater and a TRE index value less than or equal to 4.0, the owner or operator shall submit a report within 180 days after the process change is made or the information regarding the process change is known to the owner or operator, unless the organic HAP concentration is less than 50 ppmv. This report may be included in the next Periodic Report. A description of the process change shall be submitted with this report.

(iv) Whenever a process change, as defined in §63.115(e), is made that causes a Group 2 process vent with an organic HAP concentration less than 50 parts per million by volume (ppmv) to become a Group 2 process vent with an organic HAP concentration of 50 ppmv or greater and a TRE index value less than or equal to 4.0, the owner or operator shall submit a report within 180 days after the process change is made or the information regarding the process change is known to the owner or operator, unless the flow rate is less than 0.005 standard cubic meters per minute. This report may be included in the next Periodic Report. A description of the process change shall be submitted with this report.

§63.1426 Process vent requirements for determining organic HAP concentration, control efficiency, and aggregated organic HAP emission reduction for a PMPU.

(a) Use of a flare. When a flare is used to comply with §63.1425(b)(1)(i) (in combination with other control techniques), (b)(2)(i), (c)(1)(i), (c)(3)(i), or (d)(1), the owner or operator shall comply with §63.1437(c), and is not required to demonstrate the control efficiency for the flare, if the owner or operator chooses to assume a 98 percent control efficiency for that flare, as allowed under paragraph (e)(2)(i) of this section. In order to use only a flare to comply with §63.1425(b)(1)(i), or to use a flare and apply a control efficiency greater than 98 percent, an owner or operator shall submit a request in accordance with §63.116(c)(3) and (4) specify that Method 18, 40 CFR part 60, appendix A shall be used, Method 18 or Method 25A, 40 CFR part 60, appendix A may be used for the purposes of this subpart. The use of Method 25A, 40 CFR part 60, appendix A shall comply with paragraphs (f)(10)(i) and (ii) of this section.

(i) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A shall be the single organic HAP representing the largest percent by volume of the emissions.

(ii) The use of Method 25A, 40 CFR part 60, appendix A is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(b) Exceptions to performance tests. An owner or operator is not required to conduct a performance test when a combustion, recovery, or recapture device specified in paragraphs (b)(1)
through (6) of this section is used to comply with §63.1425(b), (c), or (d).

(1) A boiler or process heater with a design heat input capacity of 44 megawatts or greater.

(2) A boiler or process heater where the process vent stream is introduced with the primary fuel or is used as the primary fuel.

(3) A combustion, recovery, or recapture device for which a performance test was conducted within the preceding 5-year period, using the same Methods specified in this section and either no deliberate process changes have been made since the test, or the owner or operator can demonstrate that the results of the performance test, with or without adjustments, reliably demonstrate compliance despite process changes. The operating parameters reported under the previous performance test shall be sufficient to meet the parameter monitoring requirements in this subpart.

(4) A boiler or process heater burning hazardous waste for which the owner or operator:
   (i) Has been issued a final hazardous waste permit under 40 CFR part 270 and complies with the requirements for hazardous waste burned in boilers and industrial furnaces in 40 CFR part 266, subpart H; or
   (ii) Has certified compliance with the interim status requirements for hazardous waste burned in boilers and industrial furnaces in of 40 CFR part 266, subpart H.

(5) A hazardous waste incinerator for which the owner or operator has been issued a final permit under 40 CFR part 270 and complies with the requirements for incinerators in 40 CFR part 264, subpart O. or has certified compliance with the interim status requirements for incinerators in 40 CFR part 265, subpart O.

(6) Combustion, recovery or recapture device (except for condensers) performance may be determined by using the design evaluation described in paragraph (f) of this section, provided that the combustion, recovery or recapture device receives less than 10 tons per year (9.1 megagrams per year) of uncontrolled organic HAP emissions from one or more PMPUs, determined in accordance with paragraph (d) of this section. If a combustion, recovery or recapture device exempted from testing in accordance with this paragraph receives more than 10 tons per year (9.1 megagrams per year) of uncontrolled organic HAP emissions from one or more PMPUs, the owner or operator shall comply with the performance test requirements in paragraph (c) of this section and shall submit the test report in the next Periodic Report.

(c) Determination of organic HAP concentration and control efficiency. Except as provided in paragraphs (a) and (b) of this section, an owner or operator using a combustion, recovery, or recapture device to comply with an epoxide or organic HAP percent reduction efficiency requirement in §63.1425(b)(1)(i), (b)(2)(ii), (c)(3)(ii), or (d)(2); an epoxide concentration limitation in §63.1425(b)(1)(i) or (b)(2)(ii); or an annual epoxide emission limitation in §63.1425(b)(1)(iii) or (b)(2)(iv), shall conduct a performance test using the applicable procedures in paragraphs (c)(1) through (4) of this section. The organic HAP or epoxide concentration and percent reduction may be measured as total epoxide, total organic HAP, or as TOC minus methane and ethane according to the procedures specified. When conducting testing in accordance with this section, the owner or operator is only required to measure HAP of concern for the specific requirement for which compliance is being determined. For instance, to determine compliance with the epoxide emission requirement of §63.1425(b), the owner or operator is only required to measure epoxide control efficiency or outlet concentration.

(1) Sampling site location. The sampling site location shall be determined as specified in paragraphs (c)(1)(i) and (ii) of this section.

   (i) For determination of compliance with a percent reduction of total epoxide requirement in §63.1425(b)(1)(i), (b)(2)(ii), or a percent reduction of total organic HAP requirement in §63.1425(c)(1)(ii), (c)(3)(ii), or (d)(2), sampling sites shall be located at the inlet of the combustion, recovery, or recapture device as specified in paragraphs (c)(1)(i)(A), (B), and (C) of this section, and at the outlet of the combustion, recovery, or recapture device.
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(A) For process vents from continuous unit operations, the inlet sampling site shall be determined in accordance with either paragraph (c)(1)(i)(A)(1) or (2) of this section.

(1) To demonstrate compliance with either the provisions for epoxide emissions in §63.1425(b) or the provisions for nonepoxide organic HAP emissions from catalyst extraction in §63.1425(d), the inlet sampling site shall be located after the exit from the continuous unit operation but before any recovery devices, or

(2) To demonstrate compliance with the requirements for nonepoxide organic HAP emissions from the use of nonepoxide organic HAP in making or modifying the product in §63.1425(c), the inlet sampling site shall be located after all control techniques to reduce epoxide emissions and after the final nonepoxide organic HAP recovery device.

(B) For process vents from batch unit operations, the inlet sampling site shall be determined in accordance with either paragraph (c)(1)(i)(B)(1) or (2) of this section.

(1) To demonstrate compliance with either the provisions for epoxide emissions in §63.1425(b) or the provisions for nonepoxide organic HAP emissions from catalyst extraction in §63.1425(d), the inlet sampling site shall be located after the exit from the batch unit operation but before any recovery device.

(2) To demonstrate compliance with the requirements for nonepoxide organic HAP emissions in making or modifying the product in §63.1425(c), the inlet sampling site shall be located after all control techniques to reduce epoxide emissions but before any nonepoxide organic HAP recovery device.

(C) If a process vent stream is introduced with the combustion air or as a secondary fuel into a boiler or process heater with a design capacity less than 44 megawatts, selection of the location of the inlet sampling sites shall ensure the measurement of total organic HAP or TOC (minus methane and ethane) concentrations in all process vent streams and primary and secondary fuels introduced into the boiler or process heater.

(i) To determine compliance with a parts per million by volume total epoxide or TOC limit in §63.1425(b)(1)(iii) or (b)(2)(iii), the sampling site shall be located at the outlet of the combustion, recovery, or recapture device.

(2) [Reserved]

(3) Testing conditions and calculation of TOC or total organic HAP concentration. (i) Testing conditions shall be as specified in paragraphs (c)(3)(i)(A) through (E) of this section, as appropriate.

(A) Testing of process vents from continuous unit operations shall be conducted at maximum representative operating conditions, as described in §63.1437(a)(1). Each test shall consist of three 1-hour runs. Gas stream volumetric flow rates shall be measured at approximately equal intervals of about 15 minutes during each 1-hour run. The organic HAP concentration (of the HAP of concern) shall be determined from samples collected in an integrated sample over the duration of the test, or from grab samples collected simultaneously with the flow rate measurements (at approximately equal intervals of about 15 minutes). If an integrated sample is collected for laboratory analysis, the sampling rate shall be adjusted proportionally to reflect variations in flow rate. For gas streams from continuous unit operations, the organic HAP concentration or control efficiency used to determine compliance shall be the average organic HAP concentration or control efficiency of the three test runs.

(B) Testing of process vents from batch unit operations shall be conducted at absolute worst-case conditions or hypothetical worst-case conditions, as defined in paragraphs (c)(3)(i)(B)(1) through (5) of this section. Worst-case conditions are limited to the maximum production allowed in a State or Federal permit or regulation and the conditions specified in §63.1437(a)(1). Gas stream volumetric flow rates shall be measured at 15-minute intervals, or at least once during the emission episode. The organic HAP or TOC concentration shall be determined from samples collected in an integrated sample over the duration of the test, or from grab samples collected simultaneously with the flow rate measurements (at approximately

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equal intervals of about 15 minutes). If an integrated sample is collected for laboratory analysis, the sampling rate shall be adjusted proportionally to reflect variations in flow rate.

(1) Absolute worst-case conditions are defined by the criteria presented in paragraph (c)(3)(i)(B)(1)(i) or (ii) of this section if the maximum load is the most challenging condition for the control device. Otherwise, absolute worst-case conditions are defined by the conditions in paragraph (c)(3)(i)(B)(1)(iii) of this section.

(i) The period in which the inlet to the control device will contain at least 50 percent of the maximum HAP load (in lbs) capable of being vented to the control device over any 8-hour period. An emission profile as described in paragraph (c)(3)(i)(B)(3)(i) of this section shall be used to identify the 8-hour period that includes the maximum projected HAP load.

(ii) A period of time in which the inlet to the control device will contain the highest HAP mass loading rate capable of being vented to the control device. An emission profile as described in paragraph (c)(3)(i)(B)(3)(i) of this section shall be used to identify the period of maximum HAP loading.

(iii) The period of time when the HAP loading or stream composition (including non-HAP) is most challenging for the control device. These conditions include, but are not limited to the following: periods when the stream contains the highest combined VOC and HAP load described by the emission profiles in paragraph (c)(3)(i)(B)(3) of this section; periods when the streams contain HAP constituents that approach limits of solubility for scrubbing media; or periods when the streams contain HAP constituents that approach limits of adsorptivity for carbon adsorption systems.

(2) Hypothetical worst-case conditions are simulated test conditions that, at a minimum, contain the highest hourly HAP load of emissions that would be predicted to be vented to the control device from the emissions profile described in paragraph (c)(3)(i)(B)(3)(ii) or (iii) of this section.

(3) The owner or operator shall develop an emission profile for the vent to the control device that describes the characteristics of the vent stream at the inlet to the control device under worst case conditions. The emission profile shall be developed based on any one of the procedures described in paragraphs (c)(3)(i)(B)(3)(i) through (iii) of this section, as required by paragraph (c)(3)(i)(B) of this section.

(i) The emission profile shall consider all emission episodes that could contribute to the vent stack for a period of time that is sufficient to include all processes venting to the stack and shall consider production scheduling. The profile shall describe the HAP load to the device that equals the highest sum of emissions from the episodes that can vent to the control device in any given period, not to exceed 1 hour. Emissions per episode shall be divided by the duration of the episode only if the duration of the episode is longer than 1 hour, and emissions per episode shall be calculated using the procedures specified in Equation 1:

\[
E = \sum_{i=1}^{n} P_i MW_i \times \frac{(V)(t)}{(R)(T)} \times \frac{P_T}{P_T - \sum_{i=1}^{n} P_i} \quad \text{[Equation 1]}
\]

Where:
- \(E\) = Mass of HAP emitted.
- \(V\) = Purge flow rate at the temperature and pressure of the vessel vapor space.
- \(R\) = Ideal gas law constant.
- \(T\) = Temperature of the vessel vapor space (absolute).
- \(P_i\) = Partial pressure of the individual HAP.
- \(P_T\) = Pressure of the vessel vapor space.
- \(MW_i\) = Molecular weight of the individual HAP.
- \(n\) = Number of HAP compounds in the emission stream.

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i = Identifier for a HAP compound.
j = Identifier for a condensable compound.
m = Number of condensable compounds (including HAP) in the emission stream.

(ii) The emission profile shall consist of emissions that meet or exceed the highest emissions that would be expected under actual processing conditions. The profile shall describe equipment configurations used to generate the emission events, volatility of materials processed in the equipment, and the rationale used to identify and characterize the emission events. The emissions may be based on using compounds more volatile than compounds actually used in the process(es), and the emissions may be generated from all equipment in the process(es) or only selected equipment.

(iii) The emission profile shall consider the capture and control system limitations and the highest emissions that can be routed to the control device, based on maximum flow rate and concentrations possible because of limitations on conveyance and control equipment (e.g., fans, LEL alarms and safety bypasses).

(4) Three runs, each at a minimum of the complete duration of the batch venting episode or 1 hour, whichever is shorter, and a maximum of 8 hours, are required for performance testing. Each run shall occur over the same worst-case conditions, as defined in paragraph (c)(3)(i)(B) of this section.

(5) If a condenser is used to control the process vent stream(s), the worst case emission episode(s) shall represent a period of time in which a process vent from the batch cycle or combination of cycles (if more than one cycle is vented through the same process vent) will require the maximum heat removal capacity, in Btu/hr, to cool the process vent stream to a temperature that, upon calculation of HAP concentration, will yield the required removal efficiency for the entire cycle. The calculation of maximum heat load shall be based on the emission profile described in paragraph (c)(3)(i)(B) of this section that will allow calculation of sensible and latent heat loads.

(ii) The concentration of either TOC (minus methane or ethane) or total organic HAP (of the HAP of concern) shall be calculated according to paragraph (c)(3)(ii)(A) or (B) of this section.

(A) The TOC concentration \( C_{TOC} \) is the sum of the concentrations of the individual components and shall be computed for each run using Equation 2:

\[
C_{TOC} = \sum_{i=1}^{x} \sum_{j=1}^{n} C_{ji} / n \tag{Equation 2}
\]

Where:
- \( C_{TOC} \) = Concentration of TOC (minus methane and ethane), dry basis, parts per million by volume.
- \( C_{ji} \) = Concentration of sample components \( j \) of sample \( i \), dry basis, parts per million by volume.
- \( n \) = Number of components in the sample.
- \( x \) = Number of samples in the sample run.

(B) The total organic HAP concentration \( C_{HAP} \) shall be computed according to Equation 2, except that only the organic HAP species shall be summed.

(iii) The concentration of TOC or total organic HAP shall be corrected to 3 percent oxygen if a combustion device is used.

(A) The emission rate correction factor or excess air, integrated sampling and analysis procedures of Method 3B of 40 CFR part 60, appendix A shall be used to determine the oxygen concentration \( \%O_{2d} \). The samples shall be taken during the same time that the TOC (minus methane or ethane) or total organic HAP samples are taken.

(B) The concentration corrected to 3 percent oxygen shall be computed using Equation 3, as follows:

\[
C_c = C_m \left( \frac{17.9}{20.9 - \%O_{2d}} \right) \tag{Equation 3}
\]

Where:
- \( C_c \) = Concentration of TOC or organic HAP corrected to 3 percent oxygen, dry basis, parts per million by volume.
- \( C_m \) = Concentration of TOC (minus methane and ethane) or organic HAP, dry basis, parts per million by volume.
- \( \%O_{2d} \) = Concentration of oxygen, dry basis, percent by volume.

(4) Test methods. When testing is conducted to measure emissions from an affected source, the test methods specified in paragraphs (c)(4)(i) through (iv)
of this section shall be used, as applicable.

(i) For sample and velocity traverses, Method 1 or 1A of appendix A of part 60 shall be used, as appropriate, except that references to particulate matter in Method 1A do not apply for the purposes of this subpart.

(ii) The velocity and gas volumetric flow rate shall be determined using Method 2, 2A, 2C, or 2D of 40 CFR part 60, appendix A, as appropriate.

(iii) The concentration measurements shall be determined using the methods described in paragraphs (c)(4)(iii) (A) through (C) of this section.

(A) Method 18 of appendix A of part 60 may be used to determine the HAP concentration in any control device efficiency determination.

(B) Method 25 of appendix A of part 60 may be used to determine total gaseous nonmethane organic concentration for control efficiency determinations in combustion devices.

(C) Method 25A of appendix A of part 60 may be used to determine the HAP or TOC concentration for control device efficiency determinations under the conditions specified in Method 25 of appendix A of part 60 for direct measurements of an effluent with a flame ionization detector, or in demonstrating compliance with the 20 ppmv standard, the instrument shall be calibrated on methane or the predominant HAP. If calibrating on the predominant HAP, the use of Method 25A of appendix A of part 60 shall comply with paragraphs (c)(4)(iii) (C) (1) through (3) of this section.

(1) The organic HAP used as the calibration gas for Method 25A of appendix A of part 60 shall be the single organic HAP representing the largest percent by volume.

(2) The use of Method 25A, 40 CFR part 60, appendix A, is acceptable if the response from the high level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(3) The span value of the analyzer shall be less than 100 ppmv.

(iv) Alternatively, any other method or data that have been validated according to the applicable procedures in 40 CFR part 63, appendix A, Method 301 may be used.

(5) Calculation of percent reduction efficiency. The following procedures shall be used to calculate percent reduction efficiency:

(i) Test duration shall be as specified in paragraphs (c)(3)(i) (A) through (B) of this section, as appropriate.

(ii) The mass rate of either TOC (minus methane and ethane) or total organic HAP of the HAP of concern \( E_i, E_o \) shall be computed.

(A) The following equations shall be used:

\[
E_i = K_2 \left( \sum_{j=1}^{n} C_{ij} M_{ij} \right) Q_i \quad \text{[Equation 4]}
\]

\[
E_o = K_3 \left( \sum_{j=1}^{n} C_{oj} M_{oj} \right) Q_o \quad \text{[Equation 5]}
\]

Where:

- \( C_{ij}, C_{oj} = \) Concentration of sample component \( j \) of the gas stream at the inlet and outlet of the combustion, recovery, or recapture device, respectively, dry basis, parts per million by volume.

- \( E_i, E_o = \) Mass rate of TOC (minus methane and ethane) or total organic HAP at the inlet and outlet of the combustion, recovery, or recapture device, respectively, dry basis, kilogram per hour.

- \( M_{ij}, M_{oj} = \) Molecular weight of sample component \( j \) of the gas stream at the inlet and outlet of the combustion, recovery, or recapture device, respectively, gram/gram-mole.

- \( Q_i, Q_o = \) Flow rate of gas stream at the inlet and outlet of the combustion, recovery, or recapture device, respectively, dry standard cubic meter per minute.

- \( K_2 = \) Constant, \( 2.494 \times 10^{-8} \) (parts per million)\(^{-1}\) (gram-mole per standard cubic meter) (kilogram/gram) (minute/hour), where standard temperature (gram-mole per standard cubic meter) is 20°C.

(B) Where the mass rate of TOC is being calculated, all organic compounds (minus methane and ethane) measured by Method 18 of 40 CFR part 60, appendix A are summed using Equations 4 and 5 in paragraph (c)(5)(ii)(A) of this section.

(C) Where the mass rate of total organic HAP is being calculated, only the organic HAP species shall be summed using Equations 4 and 5 in paragraph (c)(5)(ii)(A) of this section.
(iii) The percent reduction in TOC (minus methane and ethane) or total organic HAP shall be calculated using Equation 6 as follows:

\[
R = \frac{E_i - E_o}{E_i} \times 100 \quad \text{[Equation 6]}
\]

Where:

- \(R\) = Control efficiency of combustion, recovery, or recapture device, percent.
- \(E_i\) = Mass rate of TOC (minus methane and ethane) or total organic HAP at the inlet to the combustion, recovery, or recapture device as calculated under paragraph (c)(5)(ii) of this section, kilograms TOC per hour or kilograms organic HAP per hour.
- \(E_o\) = Mass rate of TOC (minus methane and ethane) or total organic HAP at the outlet of the combustion, recovery, or recapture device, as calculated under paragraph (c)(5)(ii) of this section, kilograms TOC per hour or kilograms organic HAP per hour.

(iv) If the process vent stream entering a boiler or process heater with a design capacity less than 44 megawatts is introduced with the combustion air or as a secondary fuel, the weight-percent reduction of total organic HAP or TOC (minus methane and ethane) across the device shall be determined by comparing the TOC (minus methane and ethane) or total organic HAP in all combusted process vent streams and primary and secondary fuels with the TOC (minus methane and ethane) or total organic HAP, respectively, exiting the combustion device.

(d) Determination of uncontrolled organic HAP emissions. For each process vent at a PMPU that is complying with the process vent control requirements in §63.1425(b)(1)(i), (b)(1)(iii), (b)(2)(ii), (b)(2)(iv), (c)(1)(ii), or (d)(2) using a combustion, recovery, or recapture device, the owner or operator shall determine the uncontrolled organic HAP emissions in accordance with the provisions of this paragraph, with the exceptions noted in paragraph (d)(1) of this section. The provisions of §63.1427(c)(1) shall be used to calculate uncontrolled epoxide emissions prior to the onset of an extended cook out.

(1) Exemptions. The owner or operator is not required to determine uncontrolled organic HAP emissions for process vents in a PMPU if the conditions in paragraph (d)(1)(i), (ii), or (iii) of this section are met.

(i) For PMPUs where all process vents subject to the epoxide emission reduction requirements of §63.1425(b) are controlled at all times using a combustion, recovery, or recapture device, or extended cookout, the owner or operator is not required to determine uncontrolled epoxide emissions.

(ii) For PMPUs where the combination of process vents from batch unit operations associated with the use of nonepoxide organic HAP to make or modify the product is subject to the Group 1 requirements of §63.1425(c)(1), the owner or operator is not required to determine uncontrolled nonepoxide organic HAP emissions for those process vents if every process vent from a batch unit operation associated with the use of nonepoxide organic HAP to make or modify the product in the PMPU is controlled at all times using a combustion, recovery, or recapture device.

(iii) For PMPUs where all process vents subject to either the provisions for epoxide emissions in §63.1425(b) or the provisions for organic
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HAP emissions from catalyst extraction in § 63.1425(d), uncontrolled emissions shall be determined after the exit from the continuous unit operation but before any recovery device.

(ii) The owner or operator shall determine the hourly uncontrolled organic HAP emissions from each process vent from a continuous unit operation in accordance with paragraph (c)(4)(ii) of this section, except that the emission rate shall be determined at the location specified in paragraph (d)(2)(i) of this section.

(e) Determination of organic HAP emission reduction for a PMPU. (1) The owner or operator shall determine the organic HAP emission reduction for process vents in a PMPU that are complying with § 63.1425(b)(1)(i), (b)(2)(ii), (c)(1)(iii), or (d)(2) using Equation 7. The organic HAP emission reduction shall be determined for each group of process vents subject to the same paragraph (i.e., paragraph (b), (c), or (d)) of § 63.1425. For instance, process vents that emit epoxides are subject to paragraph (b) of § 63.1425. Therefore, if the owner or operator of an existing affected source is complying with the 98 percent reduction requirement in § 63.1425(b)(2)(ii), the organic HAP (i.e., epoxide) emission reduction shall be determined for the group of vents in a PMPU that are subject to this paragraph.

\[
RED_{\text{PMPU}} = \frac{\sum_{i=1}^{n} (E_{\text{unc},i} \times \frac{R_i}{100})}{\sum_{i=1}^{n} E_{\text{unc},i} + \sum_{j=1}^{n} E_{\text{unc},j}} \times 100 \quad \text{[Equation 7]}
\]

Where:

- \( RED_{\text{PMPU}} \) = Organic HAP emission reduction for the group of process vents subject to the same paragraph of § 63.1425, percent.
- \( E_{\text{unc},i} \) = Uncontrolled organic HAP emissions from process vent \( i \) that is controlled using a combustion, recovery, or recapture device, or extended cookout, kg/batch cycle for process vents from batch unit operations, kg/hr for process vents from continuous unit operations.
- \( n \) = Number of process vents in the PMPU that are subject to the same paragraph of § 63.1425 and that are controlled using a combustion, recovery, or recapture device, or extended cookout.
- \( R_i \) = Control efficiency of the combustion, recovery, or recapture device, or extended cookout, used to control organic HAP emissions from vent \( i \), determined in accordance with paragraph (e)(2) of this section.
- \( E_{\text{unc},j} \) = Uncontrolled organic HAP emissions from process vent \( j \) that is not controlled using a combustion, recovery, or recapture device, kg/batch cycle for process vents from batch unit operations, kg/hr for process vents from continuous unit operations.
- \( m \) = Number of process vents in the PMPU that are subject to the same paragraph of § 63.1425 and that are not controlled using a combustion, recovery, or recapture device.

(2) The control efficiency, \( R_i \), shall be assigned as specified below in paragraph (e)(2)(i), (ii), (iii), or (iv) of this section.

(i) If the process vent is controlled using a flare (and the owner or operator has not previously obtained approval to assume a control efficiency greater than 98 percent in accordance with § 63.6(g)) or a combustion device specified in paragraph (b)(1), (2), (4), or (5) of this section, and a performance test has not been conducted, the control efficiency shall be assumed to be 98 percent.

(ii) If the process vent is controlled using a combustion, recovery, or recapture device for which a performance test has been conducted in accordance with the provisions of paragraph (c) of this section, or for which a performance test that meets the requirements of paragraph (b)(3) of this section has been previously performed, the control efficiency shall be the efficiency determined by the performance test.

(iii) If epoxide emissions from the process vent are controlled using extended cookout, the control efficiency...
shall be the efficiency determined in accordance with §63.1427(e).

(iv) If the process vent is controlled using a flare, and the owner or operator has obtained approval to assume a control efficiency greater than 98 percent in accordance with §63.6(g), the control efficiency shall be the efficiency approved in accordance with §63.6(g).

(f) Design evaluation. A design evaluation is required for those control techniques that receive less than 10 tons per year (9.1 megagrams per year) of uncontrolled organic HAP emissions from one or more PMPUs, if the owner or operator has chosen not to conduct a performance test for those control techniques in accordance with paragraph (b)(6) of this section. The design evaluation shall include documentation demonstrating that the control technique being used achieves the required control efficiency under worst-case conditions, as determined from the emission profile described in §63.1426(c)(3)(i)(A) through (C).

(i) For an enclosed combustion technique used to comply with the provisions of §63.1425(b)(1), (c)(1), or (d), with a minimum residence time of 0.5 seconds and a minimum temperature of 760°C, the design evaluation shall document that these conditions exist.

(ii) For a combustion control technique that does not satisfy the criteria in paragraph (f)(1)(i) of this section, the design evaluation shall document the control efficiency and address the characteristics listed in paragraphs (f)(1)(ii)(A) through (C) of this section, depending on the type of control technique.

(A) For a thermal vapor incinerator, in the design evaluation the owner or operator shall consider the autoignition temperature of the organic HAP, shall consider the vent stream flow rate, and shall establish the design minimum and average temperatures in the combustion zone and the combustion zone residence time.

(B) For a catalytic vapor incinerator, in the design evaluation the owner or operator shall consider the vent stream flow rate and shall establish the design minimum and average temperatures across the catalyst bed inlet and outlet.

(C) For a boiler or process heater, in the design evaluation the owner or operator shall consider the vent stream flow rate; shall establish the design minimum and average flame zone temperatures and combustion zone residence time; and shall describe the method and location where the vent stream is introduced into the flame zone.

(iii) For a condenser, in the design evaluation the owner or operator shall consider the vent stream flow rate, relative humidity, and temperature, and shall establish the design outlet organic HAP concentration level, design average temperature of the exhaust vent stream, and the design average temperatures of the coolant fluid at the condenser inlet and outlet. The temperature of the gas stream exiting the condenser shall be measured and used to establish the outlet organic HAP concentration.

(iv) For a carbon adsorption system that regenerates the carbon bed directly onsite as part of the control technique (such as a fixed-bed adsorber), in the design evaluation the owner or operator shall consider the vent stream flow rate, relative humidity, and temperature, and shall establish the design exhaust vent stream organic compound concentration level.
§ 63.1427 Process vent requirements for processes using extended cookout as an epoxide emission reduction technique.

(a) Applicability of extended cookout requirements. Owners or operators of affected sources that produce polyether polyols using epoxides, and that are using ECO as a control technique to reduce epoxide emissions in order to comply with percent emission reduction requirements in § 63.1425(b)(1)(i) or (b)(2)(ii) shall comply with the provisions of this section. The owner of operator that is using ECO in order to comply with the emission factor requirements in § 63.1425(b)(1)(iii) or § 63.1425(b)(2)(iv) shall demonstrate that the specified emission factor is achieved by following the requirements in § 63.1431. If additional control devices are used to further reduce the HAP emissions from a process vent already controlled by ECO, then the owner or operator shall also comply with the testing, monitoring, recordkeeping, and reporting requirements associated with the additional control device, as specified in §§ 63.1426, 63.1429, and 63.1430, respectively.

(1) For each product class, the owner or operator shall determine the batch cycle percent epoxide emission reduction for the most difficult to control product in the product class, where the most difficult to control product is the polyether polyol that is manufactured with the slowest pressure decay curve.

(2) The owner or operator may determine the batch cycle percent epoxide emission reduction by directly measuring the concentration of the unreacted epoxide, or by using process knowledge, reaction kinetics, and engineering knowledge, in accordance with paragraph (a)(2)(i) of this section.

(i) If the owner or operator elects to use any method other than direct measurement, the epoxide concentration shall be determined by direct measurement for one product from each product class and compared with the epoxide concentration determined using the selected estimation method, with the exception noted in paragraph (a)(2)(ii) of this section. If the difference between the directly determined epoxide concentration and the calculated epoxide concentration is...
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less than 25 percent, then the selected estimation method will be considered to be an acceptable alternative to direct measurement for that class.

(ii) If uncontrolled epoxide emissions prior to the end of the ECO are less than 10 tons per year (9.1 megagrams per year), the owner or operator is not required to perform the direct measurement required in paragraph (a)(2)(i) of this section. Uncontrolled epoxide emissions prior to the end of the ECO shall be determined by the procedures in paragraph (d)(1) of this section.

(b) Define the end of epoxy feed. The owner or operator shall define the end of the epoxy feed in accordance with paragraph (b)(1) or (2) of this section.

(1) The owner or operator shall determine the concentration of epoxide in the reactor liquid at the point in time when all epoxide has been added to the reactor and prior to any venting. This concentration shall be determined in accordance with the procedures in paragraph (f)(1)(i) of this section.

(2) If the conditions in paragraphs (b)(2)(i), (ii), and (iii) of this section are met, the end of the epoxy feed may be defined by the reactor epoxide partial pressure at the point in time when all epoxy reactants have been added to the reactor. This reactor epoxide partial pressure shall be determined in accordance with the procedures in paragraph (g) of this section.

(i) No epoxide is emitted before the end of the ECO;

(ii) Extended cookout is the only control technique to reduce epoxide emissions; and

(iii) The owner or operator elects to determine the percent epoxide emission reduction for the ECO using reactor epoxide partial pressure in accordance with paragraph (e)(2) of this section.

(c) Define the onset of the ECO. The owner or operator shall calculate the uncontrolled emissions for the batch cycle by calculating the epoxide emissions, if any, prior to the onset of the ECO, plus the epoxide emissions at the onset of the ECO. The onset of the ECO is defined as the point in time when the combined unreacted epoxide concentration in the reactor liquid is equal to 25 percent of the concentration of epoxides at the end of the epoxy feed, which was determined in accordance with paragraph (b) of this section.

(1) The uncontrolled epoxide emissions for the batch cycle shall be determined using Equation 8.

\[ E_{c,u} = (C_{liq,i})(V_{liq,i})(D_{liq,i}) + (C_{vap,i})(V_{vap,i})(D_{vap,i}) + E_{epox, bef} \]  

Where:

- \( E_{c,u} \) = Uncontrolled epoxide emissions at the onset of the ECO, kilograms per (kg/batch).
- \( C_{liq,i} \) = Concentration of epoxide in the reactor liquid at the onset of the ECO, which is equal to 25 percent of the concentration of epoxide at the end of the epoxy feed, determined in accordance with paragraph (b)(1) of this section, weight percent.
- \( V_{liq,i} \) = Volume of reactor liquid at the onset of the ECO, liters.
- \( D_{liq,i} \) = Density of reactor liquid, kg/liter.
- \( C_{vap,i} \) = Concentration of epoxide in the reactor vapor space at the onset of the ECO, determined in accordance with paragraph (f)(2) of this section, weight percent.
- \( V_{vap,i} \) = Volume of the reactor vapor space at the onset of the ECO, liters.
- \( D_{vap,i} \) = Vapor density of reactor vapor space at the onset of the ECO, kg/liter.
- \( E_{epox, bef} \) = Epoxide emissions that occur prior to the onset of the ECO, determined in accordance with the provisions of §63.1426(d), kilograms.

(2) If the conditions in paragraphs (b)(2)(i), (ii), and (iii) of this section are met, the owner or operator may define the onset of the ECO as the point in time when the reactor epoxide partial pressure equals 25 percent of the reactor epoxide partial pressure at the end of the epoxy feed, and is not required to determine the uncontrolled epoxide emissions in accordance with paragraph (c)(1) of this section.

(d) Determine emissions at the end of the ECO. The owner or operator shall calculate the epoxy emissions at the end of the ECO, where the end of the
ECO is defined as the point immediately before the time when the reactor contents are emptied and/or the reactor vapor space purged to the atmosphere or to a combustion, recovery, or recapture device.

(1) The epoxide emissions at the end of the ECO shall be determined using Equation 9.

\[
E_{c,E} = (C_{liq,f})(V_{liq,f})(D_{liq,f}) + (C_{vap,f})(V_{vap,f})(D_{vap,f})
\]  [Equation 9]

Where:

- \(E_{c,E}\) = Epoxide emissions at the end of the ECO, kg.
- \(C_{liq,f}\) = Concentration of epoxide in the reactor liquid at the end of the ECO, weight percent.
- \(V_{liq,f}\) = Volume of reactor liquid at the end of the ECO, liters.
- \(D_{liq,f}\) = Density of reactor liquid, kg/liter.
- \(C_{vap,f}\) = Concentration of epoxide in the reactor vapor space as it exits the reactor at the end of the ECO, determined in accordance with paragraph (f)(2) of this section, weight percent.
- \(V_{vap,f}\) = Volume of the reactor vapor space as it exits the reactor at the end of the ECO, liters.
- \(D_{vap,f}\) = Vapor density of reactor vapor space at the end of the ECO, kg/liter.

(2) If the conditions in paragraphs (b)(2)(i), (ii), and (iii) of this section are met, the owner or operator may determine the reactor epoxide partial pressure at the end of the ECO instead of determining the uncontrolled epoxide emissions at the end of the ECO in accordance with paragraph (d)(1) of this section.

(e) Determine percent epoxide emission reduction. (1) The owner or operator shall determine the percent epoxide emission reduction for the batch cycle using Equation 10.

\[
R_{batchcycle} = \frac{E_{c,E} - (E_{c,E})(1 - \frac{R_{addon,i}}{100}) + (E_{c,u})(1 - \frac{R_{addon,j}}{100})}{E_{c,u}} \times 100
\]  [Equation 10]

Where:

- \(R_{batchcycle}\) = Epoxide emission reduction for the batch cycle, percent.
- \(E_{c,E}\) = Epoxide emissions at the end of the ECO determined in accordance with paragraph (d)(1) of this section, kilograms.
- \(R_{addon,i}\) = Control efficiency of combustion, recovery, or recapture device that is used to control epoxide emissions after the ECO, determined in accordance with the provisions of §63.1426(c), percent.
- \(E_{c,u}\) = Uncontrolled epoxide emissions that occur before the end of the ECO, determined in accordance with the provisions of §63.1426(c), percent.
- \(R_{addon,j}\) = Control efficiency of combustion, recovery, or recapture device that is used to control epoxide emissions that occur before the end of the ECO, determined in accordance with the provisions of §63.1426(d), percent.

(2) If the conditions in paragraphs (b)(2)(i), (ii), and (iii) of this section are met, the owner or operator may determine the percent epoxide emission reduction for the batch cycle using reactor epoxide partial pressure and Equation 11, instead of using the procedures in paragraph (e)(1) of this section.
\[ R_{\text{batchcycle}} = \left[ 1 - \frac{P_{\text{epox,f}}}{P_{\text{epox,i}}} \right] \times 100 \]  

[Equation 11]

Where:

- \( R_{\text{batchcycle}} \) = Epoxide emission reduction for the batch cycle, percent.
- \( P_{\text{epox,i}} \) = Reactor epoxide partial pressure at the onset of the ECO, determined in accordance with paragraph (c)(2) of this section, mm Hg.
- \( P_{\text{epox,f}} \) = Reactor epoxide partial pressure at the end of the ECO, determined in accordance with paragraph (c)(2) of this section, mm Hg.

(f) Determination of epoxide concentrations. The owner or operator shall determine the epoxide concentrations in accordance with the procedures in this paragraph.

(1) The owner or operator shall determine the concentration of epoxide in the reactor liquid using either direct measurement in accordance with paragraph (f)(1)(i) of this section, or reaction kinetics in accordance with paragraph (f)(1)(ii) of this section. An owner or operator may also request to use an alternative methodology in accordance with paragraph (f)(1)(iii) of this section.

(i) The owner or operator shall submit a standard operating procedure for obtaining the liquid sample, along with the test method used to determine the epoxide concentration. This information shall be submitted in the Precompliance Report.

(ii) Determine the epoxide concentration in the reactor liquid using Equation 12. [Equation 12]

\[ C_{\text{liq,f}} = C_{\text{liq,i}} e^{-kt} \]  

\[ C_{\text{liq,i}} = \text{Concentration of epoxide in the reactor liquid at the beginning of the time period, weight percent.} \]

\[ C_{\text{liq,f}} = \text{Concentration of epoxide in the reactor liquid at the end of the time period, weight percent.} \]

\[ k = \text{Reaction rate constant, hour}^{-1}. \]

\[ t = \text{Time, hours.} \]

(g) Determination of pressure. The owner or operator shall determine the total pressure of the system using standard pressure measurement devices calibrated according to the manufacturer's specifications or other written procedures that provide adequate assurance that the equipment would reasonably be expected to monitor accurately.

(h) Determination if pressure decay curves are similar. The owner or operator shall determine the pressure decay curve as defined in §63.1423. Products with similar pressure decay curves constitute a product class. To determine if two pressure decay curves are similar when the pressure decay curves for products have different starting and finishing pressures, the owner or operator shall determine the time when the pressure has fallen to half its total pressure by using Equation 13:
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\[
\text{Time}\left(\frac{P_{\text{half}1}}{P_{\text{avg}}}\right) - \text{Time}\left(\frac{P_{\text{half}2}}{P_{\text{avg}}}\right) < 20\% \quad [\text{Equation 13}]
\]

Where:
- \(P_{\text{half}1}\) = Half the total pressure of the epoxide for product 1.
- \(\text{Time}\left(\frac{P_{\text{half}1}}{P_{\text{avg}}}\right)\) = Time when the pressure has fallen to half its total pressure for product 1.
- \(P_{\text{half}2}\) = Half the total pressure of the epoxide for product 2.
- \(\text{Time}\left(\frac{P_{\text{half}2}}{P_{\text{avg}}}\right)\) = Time when the pressure has fallen to half its total pressure for product 2.
- \(T_{\text{avg}}\) = The average time to cookout to the point where the epoxide pressure is 25 percent of the epoxide pressure at the end of the feed step for products 1 and 2.

(i) ECO monitoring requirements. The owner or operator using ECO shall comply with the monitoring requirements of this paragraph to demonstrate continuous compliance with this subpart. Paragraphs (i)(1) through (3) of this section address monitoring of the extended cookout.

(1) To comply with the provisions of this section, the owner or operator shall monitor one of the parameters listed in paragraphs (i)(1)(i) through (iii) of this section, or may utilize the provision in paragraph (i)(1)(iv) of this section.

(i) Time from the end of the epoxide feed;  
(ii) The epoxide partial pressure in the closed reactor;  
(iii) Direct measurement of epoxide concentration in the reactor liquid at the end of the ECO, when the reactor liquid is still in the reactor, or after the reactor liquid has been transferred to another vessel; or  
(iv) An owner or operator may submit a request to the Administrator to monitor a parameter other than the parameters listed in paragraphs (i)(1)(i) through (iii) of this section, as described in §63.1439(f).

(2) During the determination of the percent epoxide emission reduction in paragraphs (b) through (e) of this section, the owner or operator shall establish, as a level that shall be maintained during periods of operation, one of the parameters in paragraphs (i)(2)(i) through (iii) of this section, or may utilize the procedure in paragraph (i)(2)(iv) of this section, for each product class.

(i) The time from the end of the epoxide feed to the end of the ECO;  
(ii) The reactor epoxide partial pressure at the end of the ECO;  
(iii) The epoxide concentration in the reactor liquid at the end of the ECO, when the reactor liquid is still in the reactor, or after the reactor liquid has been transferred to another vessel; or  
(iv) An owner or operator may submit a request to the Administrator to monitor a parameter other than the parameters listed in paragraphs (i)(2)(i) through (iii) of this section, as described in §63.1439(f).

(3) For each batch cycle where ECO is used to reduce epoxide emissions, the owner or operator shall record the value of the monitored parameter at the end of the ECO. This parameter is then compared with the level established in accordance with paragraph (i)(2) of this section to determine if an excursion has occurred. An ECO excursion is defined as one of the situations described in paragraphs (i)(3)(i) through (v) of this section.

(i) When the time from the end of the epoxide feed to the end of the ECO is less than the time established in paragraph (i)(2)(i) of this section;  
(ii) When the reactor epoxide partial pressure at the end of the ECO is greater than the partial pressure established in paragraph (i)(2)(ii) of this section;  
(iii) When the epoxide concentration in the reactor liquid at the end of the ECO is greater than the epoxide concentration established in paragraph (i)(2)(iii) of this section;  
(iv) When the parameter is not measured and recorded at the end of the ECO; or  
(v) When the alternative monitoring parameter is outside the range established under §63.1439(f) for proper operation of the ECO as a control technique.

(j) Recordkeeping requirements. (1) The owner or operator shall maintain the records specified in paragraphs (j)(1)(i) and (ii) of this section, for each product.
class. The owner or operator shall also maintain the records related to the initial determination of the percent epoxide emission reduction specified in paragraphs (j)(1)(iii) through (x) of this section, as applicable, for each product class:

(i) Operating conditions of the product class, including:
   (A) Pressure decay curve;
   (B) Minimum reaction temperature;
   (C) Number of reactive hydrogens in the raw material;
   (D) Minimum catalyst concentration;
   (E) Ratio of EO/PO at the end of the epoxide feed; and
   (F) Reaction conditions, including the size of the reactor or batch.

(ii) A listing of all products in the product class, along with the information specified in paragraphs (j)(1)(i)(A) through (F) of this section, for each product.

(iii) The concentration of epoxide at the end of the epoxide feed, determined in accordance with paragraph (b)(1) of this section.

(iv) The concentration of epoxide at the onset of the ECO, determined in accordance with paragraph (c) of this section.

(v) The uncontrolled epoxide emissions at the onset of the ECO, determined in accordance with paragraph (c)(1) of this section. The records shall also include all the background data, measurements, and assumptions used to calculate the uncontrolled epoxide emissions.

(vi) The epoxide emissions at the end of the ECO, determined in accordance with paragraph (d)(1) of this section. The records shall also include all the background data, measurements, and assumptions used to calculate the epoxide emissions.

(vii) The percent epoxide reduction for the batch cycle, determined in accordance with paragraph (e)(1) of this section. The records shall also include all the background data, measurements, and assumptions used to calculate the percent reduction.

(viii) The parameter level, established in accordance with paragraph (i)(3) of this section.

(ix) If epoxide emissions occur before the end of the ECO, the owner or operator shall maintain records of the time and duration of all such emission episodes that occur during the initial demonstration of batch cycle efficiency.

(x) If the conditions in paragraphs (b)(2)(i), (ii), and (iii) of this section are met, the owner or operator is not required to maintain the records specified in paragraphs (j)(1)(i)(iii) through (iv) of this section, but shall maintain the records specified in paragraphs (j)(1)(x)(A), (B), and (C) of this section.

(A) The reactor epoxide partial pressure at the following times:
   (1) At end of the epoxide feed, determined in accordance with paragraph (b)(2) of this section;
   (2) At the onset of the ECO, established in accordance with paragraph (c)(2) of this section; or
   (3) At the end of the ECO, determined in accordance with paragraph (d)(2) of this section.

(B) The percent epoxide reduction for the batch cycle, determined in accordance with paragraph (e)(2) of this section. The records shall also include all the measurements and assumptions used to calculate the percent reduction.

(C) The reactor epoxide partial pressure at the end of the ECO.

(2) The owner or operator shall maintain the records specified in paragraphs (j)(1)(i) through (iv) of this section.

(i) For each batch cycle, the product being produced and the product class to which it belongs.

(ii) For each batch cycle, the owner or operator shall record the value of the parameter monitored in accordance with paragraph (i)(3) of this section.

(iii) If a combustion, recovery, or recapture device is used in conjunction with ECO, the owner or operator shall record the information specified in §63.1430(d) and comply with the monitoring provisions in §63.1429.

(iv) If a combustion, recovery, or recapture device is used to reduce emissions, the owner or operator shall maintain the records specified in §63.1430(d).

(v) If epoxide emissions occur before the end of the ECO, the owner or operator shall maintain records of the time and duration of all such emission episodes.
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(k) Reporting requirements. The owner or operator shall comply with the reporting requirements in this paragraph.

(1) The information specified in paragraphs (k)(1)(i) through (ii) of this section shall be provided in the Precompliance Report, as specified in §63.1439(e)(4).

(i) A standard operating procedure for obtaining the reactor liquid sample and a method that will be used to determine the epoxide concentration in the liquid, in accordance with paragraph (f)(1)(i) of this section.

(ii) A request to monitor a parameter other than those specified in paragraph (i)(1)(i), (ii), or (iii) of this section, as provided for in paragraph (i)(1)(iv) of this section.

(2) The information specified in paragraphs (k)(2)(i) through (iv) of this section shall be provided in the Notification of Compliance Status, as specified in §63.1439(e)(5).

(i) For each product class, the information specified in paragraphs (k)(2)(i)(A) through (C) of this section.

(A) The operating conditions of this product class, as specified in paragraph (j)(1)(i) of this section.

(B) A list of all products in the product class.

(C) The percent epoxide emission reduction, determined in accordance with paragraph (e) of this section.

(ii) The parameter for each product class, as determined in accordance with paragraph (i)(2) of this section.

(iii) If a combustion, recovery, or re-capture device is used in addition to ECO to reduce emissions, the information specified in §63.1430(h).

(iv) If epoxide emissions occur before the end of the ECO, recorded in accordance with paragraph (j)(2)(iv) of this section, exceed the time and duration of the emission episodes during the initial epoxide emission percentage reduction determination, as recorded in paragraph (j)(1)(viii) of this section.

(3) The information specified in paragraphs (k)(3)(i) through (iii) of this section shall be provided in the Periodic Report, as specified in §63.1439(e)(6).

(i) Reports of each batch cycle for which an ECO excursion occurred, as defined in paragraph (i)(3)(iii) of this section.

(ii) Notification of each batch cycle when the time and duration of epoxide emissions before the end of the ECO, recorded in accordance with paragraph (j)(2)(iv) of this section, exceed the time and duration of the emission episodes during the initial epoxide emission percentage reduction determination, as recorded in paragraph (j)(1)(viii) of this section.

(iii) If a combustion, recovery, or re-capture device is used to reduce emissions, the information specified in §63.1430(h).

(l) New polyether polyol products. If an owner or operator wishes to utilize ECO as a control option for a polyether polyol not previously assigned to a product class and reported to the Agency in accordance with either paragraph (k)(2)(i)(B), (l)(1)(ii), or (l)(2)(iii) of this section, the owner or operator shall comply with the requirements in paragraphs (l)(1)(i) and (ii) of this section.

(1) If the operating conditions of the new polyether polyol are consistent with the operating conditions for an existing product class, the owner or operator shall update the list of products for the product class.

(ii) Within 180 days after the production of the new polyether polyol, the owner or operator shall submit a report updating the product list previously submitted for the product class. This information may be submitted along with the next Periodic Report.

(2) If the operating conditions of the new polyether polyol do not conform with the operating characteristics of an existing product class, the owner or operator shall establish a new product class and shall comply with provisions of paragraphs (l)(2)(i) through (iii) of this section.

(i) The owner or operator shall update the list of products for the product class required by paragraph (j)(1)(ii) of this section, and shall record the information in paragraphs (j)(1)(ii)(A) through (F) of this section for the new product.

(ii) Within 180 days after the production of the new polyether polyol, the owner or operator shall submit a report updating the product list previously submitted for the product class. This information may be submitted along with the next Periodic Report.

(iii) The owner or operator shall establish the batch cycle percent epoxide emission reduction in accordance with paragraphs (b) through (g) of this section for the product class.
(ii) The owner or operator shall establish the records specified in paragraph (j)(1) of this section for the product class.

(iii) Within 180 days of the production of the new polyether polyol, the owner or operator shall submit a report containing the information specified in paragraphs (k)(2)(i) and (ii) of this section.

(m) Polyether polyol product changes. If a change in operation, as defined in paragraph (m)(1) of this section, occurs for a polyether polyol that has been assigned to a product class and reported to the Agency in accordance with paragraph (k)(2)(i), (l)(1)(ii), or (l)(2)(iii) of this section, the owner or operator shall comply with the provisions of paragraphs (m)(2) through (3) of this section.

(1) A change in operation for a polyether polyol is defined as a change in any one of the parameters listed in paragraphs (m)(2)(i) through (ix) of this section.

(i) A significant change in reaction kinetics;
(ii) Use of a different oxide reactant;
(iii) Use of a different EO/PO ratio;
(iv) A lower reaction temperature;
(v) A lower catalyst feed on a mole/mole fraction OH basis;
(vi) A shorter cookout;
(vii) A lower reactor pressure;
(viii) A different type of reaction, (e.g., a self-catalyzed vs. catalyzed reaction); or
(ix) A marked change in reaction conditions (e.g., a markedly different liquid level).

(2) If the operating conditions of the product after the change in operation remain within the operating conditions of the product class to which the product was assigned, the owner or operator shall update the records specified in paragraphs (j)(3)(i)(A) through (F) of this section for the product.

(3) If the operating conditions of the product after the change in operation are outside of the operating conditions of the product class to which the product was assigned, the owner or operator shall comply with the requirements in paragraphs (m)(3)(i) or (ii) of this section, as appropriate.

(i) If the new operating conditions of the polyether polyol are consistent with the operating conditions for another existing product class, the owner or operator shall comply with the requirements in paragraphs (m)(3)(i)(A) and (B) of this section.

(A) The owner or operator shall update the list of products for the product class that the product is entering, and for the product class that the product is leaving, and shall record the new information in paragraphs (j)(1)(i)(A) through (F) of this section for the product.

(B) Within 180 days after the change in operating conditions for the polyether polyol product, the owner or operator shall submit a report updating the product lists previously submitted for the product class. This information may be submitted along with the next Periodic Report.

(ii) If the new operating conditions of the polyether polyol product do not conform with the operating characteristics of an existing product class, the owner or operator shall establish a new product class and shall comply with provisions of paragraphs (m)(3)(i)(A) through (C) of this section.

(A) The owner or operator shall establish the batch cycle percent epoxide emission reduction in accordance with paragraphs (b) through (g) of this section for the product class.

(B) The owner or operator shall establish the records specified in paragraph (j)(1) of this section for the product class.

(C) Within 180 days of the change in operating conditions for the polyether polyol, the owner or operator shall submit a report containing the information specified in paragraphs (k)(2)(i) and (ii) of this section.

[64 FR 29439, June 1, 1999; 64 FR 31895, June 14, 1999]
modify the product is a Group 1 combination of batch process vents, as defined in §63.1423. The annual uncontrolled nonepoxide organic HAP emissions, determined in accordance with paragraph (b) of this section, and annual average flow rate, determined in accordance with paragraph (c) of this section, shall be determined for all process vents from batch unit operations associated with the use of a nonepoxide organic HAP to make or modify the product, with the exception of those vents specified in paragraph (i) of this section, at the location after all applicable control techniques have been applied to reduce epoxide emissions in accordance with paragraph (a)(1) or (2) of this section.

(1) If the owner or operator is using a combustion, recovery, or recapture device to reduce epoxide emissions, this location shall be at the exit of the combustion, recovery, or recapture device.

(2) If the owner or operator is using ECO to reduce epoxide emissions, this location shall be at the exit from the batch unit operation. For the purpose of these determinations, the primary condenser operating as a reflux condenser on a reactor or distillation column shall be considered part of the unit operation.

(b) Determination of annual nonepoxide organic HAP emissions. The owner or operator shall determine, for each PMPU, the total annual nonepoxide organic HAP emissions from the combination of all process vents from batch unit operations that are associated with the use of nonepoxide organic HAP to make or modify the product in accordance with paragraphs (b)(1) and (2) of this section.

(1) The annual nonepoxide organic HAP emissions for each process vent from a batch unit operation associated with the use of nonepoxide organic HAP to make or modify the product shall be determined using the batch process vent procedures in the NESHAP for Group I Polymers and Resins (40 CFR part 63, subpart U), §63.488(e).

(2) The owner or operator shall sum the annual nonepoxide organic HAP emissions from all individual process vents from batch unit operations in a PMPU, determined in accordance with paragraph (b)(1) of this section, to obtain the total nonepoxide organic HAP emissions from the combination of process vents associated with the use of a nonepoxide organic HAP to make or modify the product, for the PMPU.

(c) Minimum emission level exemption. If the annual emissions of TOC or nonepoxide organic HAP from the combination of process vents from batch unit operations that are associated with the use of nonepoxide organic HAP to make or modify a polyether polyol for a PMPU are less than 11,800 kg/yr, the owner or operator of that PMPU is not required to comply with the provisions in paragraphs (d) and (e) of this section.

(d) Determination of average flow rate and annual average flow rate. The owner or operator shall determine, for each PMPU, the total annual average flow rate for the combination of all process vents from batch unit operations that are associated with the use of a nonepoxide organic HAP to make or modify a product in accordance with paragraphs (d)(1) and (2) of this section.

(1) The annual average flow rate for each process vent from batch unit operations that is associated with the use of nonepoxide organic HAP to make or modify the product shall be determined using the batch process vent procedures in the NESHAP for Group I Polymers and Resins (40 CFR part 63, subpart U), §63.488(e).

(2) The owner or operator shall sum the annual average flow rates from the individual process vents from batch unit operations in a PMPU, determined in accordance with paragraph (d)(1) of this section, to obtain the total annual average flow rate for the combination of process vents associated with the use of a nonepoxide organic HAP to make or modify the product, for the PMPU.

(e) Determination of cutoff flow rate. For each PMPU at an affected source that uses nonepoxide organic HAP to make or modify the product, the owner or operator shall calculate the cutoff flow rate using Equation 14.
CFR = Cutoff flow rate, standard cubic meters per minute (scmm).

AE = Annual TOC or nonepoxide organic HAP emissions from the combination of process vents from batch unit operations that are associated with the use of nonepoxide organic HAP to make or modify the product, as determined in paragraph (b)(2) of this section, kg/yr.

(3) Based on the results of paragraph (g)(2) of this section, the owner or operator shall comply with either paragraph (g)(3)(i) or (ii) of this section.

(i) If the redetermination described in paragraph (g)(2) of this section indicates that the group status of the combination of process vents from batch unit operations in a PMPU that are associated with the use of nonepoxide organic HAP to make or modify the product changes from Group 2 to Group 1 as a result of the process change, the owner or operator shall submit a report as specified in §63.1439(e)(6)(iii)(D)(1) and shall comply with Group 1 combination of batch process vents provisions in this subpart, as specified in §63.1420(g)(3).

(ii) If the redetermination described in paragraph (g)(2) of this section indicates no change in group status, the owner or operator is not required to submit a report.

(h) Process vents from continuous unit operations. (1) The owner or operator shall determine the total resource effectiveness (TRE) index value for each process vent from a continuous unit operation that is associated with the use of nonepoxide organic HAP to make or modify the product. To determine the TRE index value, the owner or operator shall conduct a TRE determination and calculate the TRE index value according to the HON process vent group determination procedures in §63.115(d)(1) or (2) and the TRE equation in §63.115(d)(3). The TRE index value shall be determined at the location after all applicable control techniques have been applied to reduce epoxide emissions in accordance with paragraph (h)(1)(i), (ii), or (iii) of this section.

(i) If the owner or operator uses one or more nonepoxide recovery devices after all control techniques to reduce epoxide emissions, this location shall be after the last nonepoxide recovery device.

(ii) If the owner or operator does not use a nonepoxide recovery device after a combustion, recovery, or recapture device to reduce epoxide emissions,
§ 63.1429 Process vent monitoring requirements.

(a) Monitoring equipment requirements. The owner or operator of a process vent that uses a combustion, recovery, or recapture device to comply with the process vent control requirements in §63.1425(b)(1), (b)(2), (c)(1), (c)(3), or (d) shall install monitoring equipment as specified in paragraph (a)(1), (2), (3), (4), (5), (6), or (7) of this section, depending on the type of device used. Also, the owner or operator that uses a recovery or recapture device to comply with §63.1425(c)(4) shall install monitoring equipment as specified in paragraph (a)(4), (5), (6), or (7) of this section. All monitoring equipment shall be installed, calibrated, maintained, and operated according to manufacturers' specifications or other written procedures that provide adequate assurance describing compliance dates for sources subject to this subpart).

(iii) Where the recalculated TRE index value is greater than 4.0, the owner or operator is not required to submit a report.

(i) Combination of process vents from batch unit operations and process vents from continuous unit operations. If an owner or operator combines a process vent from a batch unit operation that is associated with the use of a non-epoxide organic HAP to make or modify the product with a process vent from a continuous unit operation that is associated with the use of a non-epoxide prior to the epoxide control technique, or prior to a nonepoxide recovery device that is after the epoxide control technique, then the provisions in paragraphs (i)(1) and (2) of this section shall apply.

(1) The process vent from the batch unit operation is not required to be included in the group determination required by paragraphs (a) through (e) of this section.

(2) The TRE index value of the combined stream shall be determined in accordance with paragraph (h) of this section, and the TRE index value shall be calculated during a period when nonepoxide organic HAP emissions are being generated by the batch unit operation.

§ 63.1429 Process vent monitoring requirements.

(a) Monitoring equipment requirements. The owner or operator of a process vent that uses a combustion, recovery, or recapture device to comply with the process vent control requirements in §63.1425(b)(1), (b)(2), (c)(1), (c)(3), or (d) shall install monitoring equipment specified in paragraph (a)(1), (2), (3), (4), (5), (6), or (7) of this section, depending on the type of device used. Also, the owner or operator that uses a recovery or recapture device to comply with §63.1425(c)(4) shall install monitoring equipment as specified in paragraph (a)(4), (5), (6), or (7) of this section. All monitoring equipment shall be installed, calibrated, maintained, and operated according to manufacturers’ specifications or other written procedures that provide adequate assurance describing compliance dates for sources subject to this subpart).

(iii) Where the recalculated TRE index value is greater than 4.0, the owner or operator is not required to submit a report.

(i) Combination of process vents from batch unit operations and process vents from continuous unit operations. If an owner or operator combines a process vent from a batch unit operation that is associated with the use of a non-epoxide organic HAP to make or modify the product with a process vent from a continuous unit operation that is associated with the use of a non-epoxide prior to the epoxide control technique, or prior to a nonepoxide recovery device that is after the epoxide control technique, then the provisions in paragraphs (i)(1) and (2) of this section shall apply.

(1) The process vent from the batch unit operation is not required to be included in the group determination required by paragraphs (a) through (e) of this section.

(2) The TRE index value of the combined stream shall be determined in accordance with paragraph (h) of this section, and the TRE index value shall be calculated during a period when nonepoxide organic HAP emissions are being generated by the batch unit operation.

§ 63.1429 Process vent monitoring requirements.

(a) Monitoring equipment requirements. The owner or operator of a process vent that uses a combustion, recovery, or recapture device to comply with the process vent control requirements in §63.1425(b)(1), (b)(2), (c)(1), (c)(3), or (d) shall install monitoring equipment specified in paragraph (a)(1), (2), (3), (4), (5), (6), or (7) of this section, depending on the type of device used. Also, the owner or operator that uses a recovery or recapture device to comply with §63.1425(c)(4) shall install monitoring equipment as specified in paragraph (a)(4), (5), (6), or (7) of this section. All monitoring equipment shall be installed, calibrated, maintained, and operated according to manufacturers’ specifications or other written procedures that provide adequate assurance describing compliance dates for sources subject to this subpart).

(iii) Where the recalculated TRE index value is greater than 4.0, the owner or operator is not required to submit a report.

(i) Combination of process vents from batch unit operations and process vents from continuous unit operations. If an owner or operator combines a process vent from a batch unit operation that is associated with the use of a non-epoxide organic HAP to make or modify the product with a process vent from a continuous unit operation that is associated with the use of a non-epoxide prior to the epoxide control technique, or prior to a nonepoxide recovery device that is after the epoxide control technique, then the provisions in paragraphs (i)(1) and (2) of this section shall apply.

(1) The process vent from the batch unit operation is not required to be included in the group determination required by paragraphs (a) through (e) of this section.

(2) The TRE index value of the combined stream shall be determined in accordance with paragraph (h) of this section, and the TRE index value shall be calculated during a period when nonepoxide organic HAP emissions are being generated by the batch unit operation.

§ 63.1429 Process vent monitoring requirements.

(a) Monitoring equipment requirements. The owner or operator of a process vent that uses a combustion, recovery, or recapture device to comply with the process vent control requirements in §63.1425(b)(1), (b)(2), (c)(1), (c)(3), or (d) shall install monitoring equipment specified in paragraph (a)(1), (2), (3), (4), (5), (6), or (7) of this section, depending on the type of device used. Also, the owner or operator that uses a recovery or recapture device to comply with §63.1425(c)(4) shall install monitoring equipment as specified in paragraph (a)(4), (5), (6), or (7) of this section. All monitoring equipment shall be installed, calibrated, maintained, and operated according to manufacturers’ specifications or other written procedures that provide adequate assurance describing compliance dates for sources subject to this subpart).

(iii) Where the recalculated TRE index value is greater than 4.0, the owner or operator is not required to submit a report.

(i) Combination of process vents from batch unit operations and process vents from continuous unit operations. If an owner or operator combines a process vent from a batch unit operation that is associated with the use of a non-epoxide organic HAP to make or modify the product with a process vent from a continuous unit operation that is associated with the use of a non-epoxide prior to the epoxide control technique, or prior to a nonepoxide recovery device that is after the epoxide control technique, then the provisions in paragraphs (i)(1) and (2) of this section shall apply.

(1) The process vent from the batch unit operation is not required to be included in the group determination required by paragraphs (a) through (e) of this section.

(2) The TRE index value of the combined stream shall be determined in accordance with paragraph (h) of this section, and the TRE index value shall be calculated during a period when nonepoxide organic HAP emissions are being generated by the batch unit operation.

§ 63.1429 Process vent monitoring requirements.

(a) Monitoring equipment requirements. The owner or operator of a process vent that uses a combustion, recovery, or recapture device to comply with the process vent control requirements in §63.1425(b)(1), (b)(2), (c)(1), (c)(3), or (d) shall install monitoring equipment specified in paragraph (a)(1), (2), (3), (4), (5), (6), or (7) of this section, depending on the type of device used. Also, the owner or operator that uses a recovery or recapture device to comply with §63.1425(c)(4) shall install monitoring equipment as specified in paragraph (a)(4), (5), (6), or (7) of this section. All monitoring equipment shall be installed, calibrated, maintained, and operated according to manufacturers’ specifications or other written procedures that provide adequate assurance describing compliance dates for sources subject to this subpart).

(iii) Where the recalculated TRE index value is greater than 4.0, the owner or operator is not required to submit a report.

(i) Combination of process vents from batch unit operations and process vents from continuous unit operations. If an owner or operator combines a process vent from a batch unit operation that is associated with the use of a non-epoxide organic HAP to make or modify the product with a process vent from a continuous unit operation that is associated with the use of a non-epoxide prior to the epoxide control technique, or prior to a nonepoxide recovery device that is after the epoxide control technique, then the provisions in paragraphs (i)(1) and (2) of this section shall apply.

(1) The process vent from the batch unit operation is not required to be included in the group determination required by paragraphs (a) through (e) of this section.

(2) The TRE index value of the combined stream shall be determined in accordance with paragraph (h) of this section, and the TRE index value shall be calculated during a period when nonepoxide organic HAP emissions are being generated by the batch unit operation.
that the equipment would reasonably be expected to monitor accurately.

(1) Where an incinerator is used, a temperature monitoring device equipped with a continuous recorder is required.

(i) Where an incinerator other than a catalytic incinerator is used, a temperature monitoring device shall be installed in the firebox or in the ductwork immediately downstream of the firebox in a position before any substantial heat exchange occurs.

(ii) Where a catalytic incinerator is used, temperature monitoring devices shall be installed in the gas stream immediately before and after the catalyst bed.

(2) Where a flare is used, the following monitoring equipment is required: a device (including but not limited to a thermocouple, ultra-violet beam sensor, or infrared sensor) capable of continuously detecting the presence of a pilot flame.

(3) Where a boiler or process heater of less than 44 megawatts design heat input capacity is used, the following monitoring equipment is required: a temperature monitoring device in the firebox equipped with a continuous recorder. Any boiler or process heater in which all process vent streams are introduced with primary fuel or are used as the primary fuel is exempt from this requirement.

(4) Where an absorber is used, a scrubbing liquid flow rate meter or a pressure monitoring device is required and should be equipped with a continuous recorder. If an acid or base absorbent is used, a pH monitoring device to monitor scrubber effluent is also required. If two or more absorbers in series are used, a scrubbing liquid flow rate meter, or a pressure monitoring device, equipped with a continuous recorder, is required for each absorber in the series. An owner or operator may submit a request to instead install the scrubbing liquid flow rate meter, or a pressure monitoring device, equipped with a continuous recorder, on only the final absorber in a series, in accordance with the alternative parameter monitoring reporting requirements in §63.1439(f).

(5) Where a condenser is used, a condenser exit temperature (product side) monitoring device equipped with a continuous recorder is required.

(6) Where a carbon adsorber is used, an integrating regeneration stream flow monitoring device having an accuracy of ±10 percent or better, capable of recording the total regeneration stream mass or volumetric flow for each regeneration cycle, and a carbon bed temperature monitoring device, capable of recording the carbon bed temperature after each regeneration and within 15 minutes of completing any cooling cycle are required.

(7) As an alternative to paragraphs (a)(4) through (6) of this section, the owner or operator may install an organic monitoring device equipped with a continuous recorder.

(b) Alternative parameters. An owner or operator of a process vent may request approval to monitor parameters other than those listed in paragraph (a) of this section. The request shall be submitted according to the procedures specified in the process vent reporting and recordkeeping requirements in §63.1430(j) and the alternative parameter monitoring reporting requirements in §63.1439(f). Approval shall be requested if the owner or operator:

(1) Uses a combustion device other than an incinerator, boiler, process heater, or flare; or

(2) For a Group 2 continuous process vent, maintains a TRE greater than 1.0 but less than or equal to 4.0 without a recovery device or with a recovery device other than the recovery devices listed in paragraph (a) of this section; or

(3) Uses one of the combustion, recovery, or recapture devices listed in paragraph (a) of this section, but seeks to monitor a parameter other than those specified in paragraph (a) of this section.

(c) Monitoring of bypass lines. The owner or operator of a process vent using a process vent system that contains bypass lines that could divert a process vent stream away from the combustion, recovery, or recapture device used to comply with the process vent control requirements in §63.1425(b), (c), or (d) shall comply with paragraph (c)(1) or (2) of this section. Equipment such as low leg drains, high point bleeds, analyzer vents, open-
ended valves or lines, and pressure relief valves needed for safety purposes are not subject to paragraphs (c)(1) or (2) of this section.

(1) Properly install, maintain, and operate a flow indicator that takes a reading at least once at approximately equal intervals of about 15 minutes. Records shall be generated as specified in the process vent reporting and recordkeeping provisions in § 63.1430(d)(3). The flow indicator shall be installed at the entrance to any bypass line that could divert emissions away from the combustion, recovery, or recapture device and to the atmosphere; or

(2) Secure the bypass line valve in the non-diverting position with a car-seal or a lock-and-key type configuration. A visual inspection of the seal or closure mechanism shall be performed at least once every month to ensure that the valve is maintained in the non-diverting position and emissions are not diverted through the bypass line. Records shall be generated as specified in the process vent reporting and recordkeeping provisions in § 63.1430(d)(4)(i).

(d) Establishment of parameter monitoring levels. Parameter monitoring levels for process vents from continuous or batch unit operations using a combustion, recovery, or recapture device to comply with the process vent control requirements in § 63.1425(b), (c), or (d) shall be established as specified in paragraphs (d)(1) through (3) of this section.

(1) For each parameter monitored under paragraph (a) or (b) of this section, the owner or operator shall establish a level, defined as either a maximum or minimum operating parameter as denoted in Table 5 of this subpart (the table listing the monitoring, recordkeeping, and reporting requirements for process vents from batch unit operations), that indicates that the combustion, recovery, or recapture device is operated in a manner to ensure compliance with the provisions of this subpart. The level shall be established in accordance with the procedures specified in the process vent control requirements in § 63.1430(d). The level may be based upon a prior performance test conducted for determining compliance with a regulation promulgated by the EPA, and the owner or operator is not required to conduct a performance test under the process vent requirements for determining organic HAP concentration, control efficiency, and aggregated organic HAP emission reductions in § 63.1426, provided that the prior performance test meets the conditions of § 63.1426(b)(3).

(2) The established level, along with supporting documentation, shall be submitted in the Notification of Compliance Status or the operating permit application as required in the Notification of Compliance Status requirements in § 63.1439(e)(5) or in the operating permit application requirements in § 63.1439(e)(8), respectively.

(3) The operating day shall be defined as part of establishing the parameter monitoring level and shall be submitted with the information in paragraph (d)(2) of this section. The definition of operating day shall specify the time(s) at which an operating day begins and ends.

§ 63.1430 Process vent reporting and recordkeeping requirements.

(a) [Reserved]

(b) Records to demonstrate compliance.

The owner or operator complying with the process vent control requirements in § 63.1425(b), (c), or (d) shall keep the following records, as applicable, readily accessible:

(1) When using a flare to comply with the process vent control requirements in § 63.1425(b)(2)(i), (c)(1)(i), (c)(3)(i), or (d)(1):

(i) The flare design (i.e., steam-assisted, air-assisted, or non-assisted);

(ii) All visible emission readings, heat content determinations, flow rate determinations, and exit velocity determinations made during the flare specification determination required by § 63.1437(c); and

(iii) All periods during the flare specification determination required by § 63.1437(c) when all pilot flames are absent.

(2) The following information when using a combustion, recovery, or recapture device (other than a flare) to achieve compliance with the process vent control requirements in § 63.1425(b), (c), or (d):
(i) For a combustion, recovery, or recapture device being used to comply with a percent reduction requirement of §63.1425(b)(1)(i), (b)(2)(iii), (c)(1)(ii), (c)(3)(ii), or (d)(2), or the annual epoxide emission limitation in §63.1425(b)(1)(iii) or (b)(2)(iv), the percent reduction of organic HAP or TOC achieved, as determined using the procedures specified in the process vent requirements in §63.1426;

(ii) For a combustion device being used to comply with an outlet concentration limitation of §63.1425(b)(1)(ii) or (b)(2)(iii), the concentration of organic HAP or TOC outlet of the combustion device, as determined using the procedures specified in the process vent requirements in §63.1426;

(iii) For a boiler or process heater, a description of the location at which the process vent stream is introduced into the boiler or process heater;

(iv) For a boiler or process heater with a design heat input capacity of less than 44 megawatts and where the process vent stream is introduced with combustion air or is used as a secondary fuel and is not mixed with the primary fuel, the percent reduction of organic HAP or TOC achieved, as determined using the procedures specified in §63.1426.

(c) Records related to the establishment of parameter monitoring levels. For each parameter monitored according to the process vent monitoring requirements in §63.1429(a) and Table 5 of this subpart, or for alternate parameters and/or parameters for alternate control techniques monitored according to the alternative parameter monitoring reporting requirements in §63.1439(f) as allowed under §63.1429(b), maintain documentation showing the establishment of the level that indicates that the combustion, recovery, or recapture device is operated in a manner to ensure compliance with the provisions of this subpart, as required by the process vent monitoring requirements in §63.1429(d).

(d) Records to demonstrate continuous compliance. The owner or operator that uses a combustion, recovery, or recapture device to comply with the process vent control requirements in §63.1425(b), (c), or (d) shall keep the following records readily accessible:

(1) Continuous records of the equipment operating parameters specified to be monitored under the process vent monitoring requirements in §63.1429(a) as applicable, and listed in Table 5 of this subpart, or specified by the Administrator in accordance with the alternative parameter monitoring reporting requirements in §63.1439(f), as allowed under §63.1429(b). These records shall be kept as specified under §63.1439(d), except as specified in paragraphs (d)(1)(i) and (ii) of this section.

(i) For flares, the records specified in Table 5 of this subpart shall be maintained in place of continuous records.

(ii) For carbon adsorbers used for process vents from batch unit operations, the records specified in Table 5 of this subpart shall be maintained in place of daily averages.

(2) Records of the daily average value for process vents from continuous unit operations or batch unit operations of each continuously monitored parameter, except as provided in paragraphs (d)(2)(i) and (ii) of this section.

(i) Monitoring data recorded during periods of monitoring system breakdowns, repairs, calibration checks, and zero (low-level) and high-level adjustments shall not be included in computing the daily averages. In addition, monitoring data recorded during periods of non-operation of the process (or specific portion thereof) resulting in cessation of organic HAP emissions, (or periods of start-up, shutdown, or malfunction) shall not be included in computing the daily averages.

(ii) If all recorded values for a monitored parameter during an operating day are above the minimum or below the maximum parameter monitoring level established in accordance with the process vent monitoring requirements in §63.1429(d), the owner or operator may record that all values were above the minimum or below the maximum level established, rather than calculating and recording a daily average for that operating day.

(3) Hourly records of whether the flow indicator for bypass lines specified under §63.1429(c)(1) was operating and whether a diversion was detected at any time during the hour. Also, records
of the time(s) of all periods when the process vent was diverted from the combustion, recovery, or recapture device, or the flow indicator specified in §63.1429(c)(1) was not operating.

(4) Where a seal or closure mechanism is used to comply with the process vent monitoring requirements for bypass lines in §63.1429(c)(2), hourly records of flow are not required. For compliance with §63.1429(c)(2), the owner or operator shall record whether the monthly visual inspection of the seals or closure mechanism has been done, and shall record the occurrence of all periods when the seal mechanism is broken, the bypass line valve position has changed, or the key for a lock-and-key type configuration has been checked out, and records of any broken seal that has been broken.

(5) Records specifying the times and duration of periods of monitoring system breakdowns, repairs, calibration checks, and zero (low-level) and high level adjustments. In addition, records specifying any other periods of process or combustion, recovery, or recapture device operation when monitors are not operating.

(e) Records related to the group determination for process vents that are associated with the use of nonepoxide organic HAP to make or modify the product. (1) Process vents from batch unit operations. Except as provided in paragraphs (e)(1)(vi) and (vii) of this section, the owner or operator of an affected source shall maintain the records specified in paragraphs (e)(1)(i) through (v) of this section for each PMPU that uses a nonepoxide organic HAP to make or modify the product, as determined in accordance with the process vent requirements for group determinations in §63.1428(b).

(ii) Total annual uncontrolled TOC or nonepoxide organic HAP emissions from the combination of process vents from batch unit operations associated with the use of nonepoxide organic HAP to make or modify the product, as determined in accordance with the process vent requirements for group determinations in §63.1428(d).

(iv) The cutoff flow rate, determined in accordance with the process vent requirements for group determinations in §63.1428(e).

(v) The results of the PMPU group determination (i.e., whether the combination of process vents is Group 1 or Group 2).

(vi) If the combination of all process vents from batch unit operations associated with the use of an organic HAP to make or modify the product is subject to the Group 1 batch process vent control requirements for nonepoxide HAP emissions from making or modifying the product in §63.1425(c)(1), none of the records in paragraphs (b)(1)(i) through (v) of this section are required.

(vii) If the total annual emissions from the combination of process vents from batch unit operations associated with the use of an organic HAP to make or modify the product are less than 11,800 kg per year, only the records in paragraphs (b)(1)(i) and (ii) of this section are required.

(2) Process vents from continuous unit operations. The owner or operator of an affected source that uses nonepoxide organic HAP to make or modify the product in continuous unit operations...
shall keep records regarding the measurements and calculations performed to determine the TRE index value of each process vent stream. The owner or operator of Group 1 continuous process vents that are subject to the control requirements of §63.1425(c)(3) is not required to keep these records.

(f) Records for Group 2 process vents that are associated with the use of non-epoxide organic HAP to make or modify the product. The following records shall be maintained for PMPUs with a Group 2 combination of batch process vents and/or one or more Group 2 continuous process vents.

(1) Process vents from batch unit operations—emission records. The owner or operator shall maintain records of the combined total annual non-epoxide organic HAP emissions from process vents associated with the use of non-epoxide organic HAP to make or modify the product for each PMPU where the combination of these process vents is classified as Group 2.

(2) Process vents from continuous unit operations—monitoring records for vents with TRE between 1.0 and 4.0. The owner or operator using a recovery device or other means to achieve and maintain a TRE index value greater than 1.0 but less than 4.0 as specified in the HON process vent requirements in §63.113(a)(3) or §63.113(d) shall keep the following records readily accessible:

(i) Continuous records of the equipment operating parameters specified to be monitored under §63.114(b) and listed in Table 5 of this subpart or specified by the Administrator in accordance with §63.114(c) and §63.117(e); and

(ii) Records of the daily average value of each continuously monitored parameter for each operating day determined according to the procedures specified in §63.152(f). If carbon adsorber regeneration stream flow and carbon bed regeneration temperature are monitored, the records specified in Table 5 of this subpart shall be kept instead of the daily averages.

(3) Process vents from continuous unit operations—records related to process changes. The owner or operator subject to the provisions of this subpart who has elected to demonstrate compliance with the TRE index value greater than 4.0 under §63.113(e) or greater than 1.0 under §63.113(a)(3) or §63.113(d) shall keep readily accessible records of:

(i) Any process changes as defined in §63.115(e); and

(ii) Any recalculation of the TRE index value pursuant to §63.115(e).

(4) Process vents from continuous unit operations—records for vents with a flow rate less than 0.005 standard cubic meter per minute. The owner or operator who elects to comply by maintaining a flow rate less than 0.005 standard cubic meter per minute under §63.113(f), shall keep readily accessible records of:

(i) Any process changes as defined in §63.115(e) that increase the process vent stream flow rate;

(ii) Any recalculation of the flow rate pursuant to §63.115(e); and

(iii) If the flow rate increases to 0.005 standard cubic meter per minute or greater as a result of the process change, the TRE determination performed according to the procedures of §63.115(d).

(5) Process vents from continuous unit operations—records for vents with an organic HAP concentration less than 50 parts per million. The owner or operator who elects to comply by maintaining an organic HAP concentration less than 50 parts per million by volume or organic HAP concentration under §63.113(g) shall keep readily accessible records of:

(i) Any process changes as defined in §63.115(e) that increase the organic HAP concentration of the process vent stream;

(ii) Any recalculation of the concentration pursuant to §63.115(e); and

(iii) If the organic HAP concentration increases to 50 parts per million by volume or greater as a result of the process change, the TRE determination performed according to the procedures of §63.115(d).

(g) Notification of Compliance Status. The owner or operator of an affected source shall submit the information specified in paragraphs (g)(1) through (3) of this section, as appropriate, as part of the Notification of Compliance Status specified in §63.1439(e)(5).

(1) For the owner or operator complying with the process vent control requirements in §63.1425(b), (c)(1), (c)(3),
or (d), the information specified in paragraph (b) of this section related to the compliance demonstration, and the information specified in paragraph (c) of this section related to the establishment of parameter monitoring levels.

(2) For each PMPU where the combination of process vents from batch unit operations that are associated with the use of nonepoxide organic HAP to make or modify the product is Group 2, the information related to the group determination specified in paragraph (e)(1) of this section.

(3) For each process vent from a continuous unit operation that is associated with the use of nonepoxide organic HAP to make or modify the product that is Group 2, the information related to the group determination specified in paragraph (e)(2) of this section.

(h) Periodic Reports. The owner or operator of an affected source shall submit Periodic Reports of the recorded information specified in paragraphs (h)(1) through (6) of this section, as appropriate, according to the schedule for submitting Periodic Reports in §63.1439(e)(6)(i).

(1) Reports of daily average values of monitored parameters for all operating days when the daily average values recorded under paragraph (d)(2) of this section were above the maximum, or below the minimum, level established in the Notification of Compliance Status or operating permit.

(2) Reports of the duration of periods when monitoring data are not collected for each excursion caused by insufficient monitoring data as defined in §63.1438(f)(1)(iv), (f)(2)(i)(B), or (f)(3)(ii).

(3) Reports of the times and durations of all periods recorded under paragraph (d)(3) of this section when the process vent stream is diverted from the combustion, recovery, or recapture device through a bypass line.

(4) Reports of all periods recorded under paragraph (d)(4) of this section in which the seal mechanism is broken, the bypass line valve position has changed, or the key to unlock the bypass line valve was checked out.

(5) Reports of the times and durations of all periods recorded under paragraph (d)(3)(ii) of this section in which all pilot flames of a flare were absent.

(6) Reports of all carbon bed regeneration cycles during which the parameters recorded under paragraph (d)(1)(iii) of this section were above the maximum, or below the minimum, levels established in the Notification of Compliance Status or operating permit.

(i) Reports of process changes. Whenever a process change, as defined in §63.1420(g)(3), is made that causes a Group 2 combination of batch process vents at a PMPU that are associated with the use of nonepoxide organic HAP to make or modify the product to become Group 1, the owner or operator shall submit a report within 180 days after the process change is made or the information regarding the process change is known to the owner or operator. This report may be included in the next Periodic Report or in a separate submittal to the Administrator, as specified in §63.1439(e)(6)(iii)(D)(1). A description of the process change shall be submitted with the report.

(j) Reporting requirements for Group 2 continuous process vents. (1) Whenever a process change, as defined in §63.1420(g)(3), is made that causes a Group 2 continuous process vent with a TRE greater than 4.0 to become a Group 2 continuous process vent with a TRE less than 4.0, the owner or operator shall submit a report within 180 calendar days after the process change is made or the information regarding the process change is known, unless the flow rate is less than 0.005 standard cubic meters per minute. The report may be submitted as part of the next periodic report. The report shall include:

(i) A description of the process change;

(ii) The results of the recalculation of the TRE index value required under §63.1428(h)(2), and recorded under paragraph (f)(3) of this section; and

(iii) A statement that the owner or operator will comply with the process vent monitoring requirements specified in §63.1429, as appropriate.

(2) Whenever a process change, as defined in §63.1420(g)(3), is made that causes a Group 2 continuous process vent with a flow rate less than 0.005 standard cubic meters per minute to become a Group 2 continuous process
vent with a flow rate of 0.005 standard cubic meters per minute or greater, the owner or operator shall submit a report within 180 calendar days after the process change is made or the information regarding the process change is known, unless the organic HAP concentration is less than 50 ppmv. The report may be submitted as part of the next periodic report. The report shall include:

(i) A description of the process change;

(ii) The results of the calculation of the TRE index value required under §63.1428(h)(2), and recorded under paragraph (f)(3) of this section; and

(iii) A statement that the owner or operator will comply with the process vent monitoring requirements specified in §63.1429, as appropriate.

(3) Whenever a process change, as defined in §63.1420(g)(3), is made that causes a Group 2 continuous process vent with an organic HAP concentration less than 50 ppmv to become a Group 2 continuous process vent with an organic HAP concentration of 50 ppmv or greater and a TRE index value less than 4.0, the owner or operator shall submit a report within 180 calendar days after the process change is made or the information regarding the process change is known, unless the flow rate is less than 0.005 standard cubic meters per minute. The report may be submitted as part of the next periodic report. The report shall include:

(i) A description of the process change;

(ii) The results of the calculation of the TRE index value required under §63.1428(h)(2), and recorded under paragraph (f)(3) of this section; and

(iii) A statement that the owner or operator will comply with the process vent monitoring requirements specified in §63.1429, as appropriate.

(k) Alternative requests. If an owner or operator uses a combustion, recovery, or recapture device other than those specified in the process vent monitoring requirements in §63.1429(a)(1) through (7) and listed in Table 5 of this subpart; requests approval to monitor a parameter other than those listed in §63.1427(i)(1)(i) through (iii), as allowed under §63.1427(i)(1)(iv), the owner or operator shall submit a description of planned reporting and recordkeeping procedures, as specified in §63.1439(f)(3), as part of the Precompliance Report as required under §63.1439(e)(4), or to the Administrator as a separate submittal. The Administrator will specify appropriate reporting and recordkeeping requirements as part of the review of the Precompliance Report.

§63.1431 Process vent annual epoxides emission factor plan requirements.

(a) Applicability of emission factor plan requirements. An owner or operator electing to comply with an annual epoxide emission factor limitation in §63.1425(b)(1)(iii) or (b)(2)(iv) shall develop and implement an epoxide emission factor plan in accordance with the provisions of this section.

(b) Emission factor plan requirements. The owner or operator shall develop an epoxide emission factor plan.

(1) If epoxide emissions are maintained below the epoxide emission factor limitation through the use of a combustion, recovery, or recapture device (without extended cookout), the owner or operator shall develop and implement the plan in accordance with paragraph (c) of this section.

(2) If epoxide emissions are maintained below the epoxide emission factor limitation through the use of extended cookout (without a combustion, recovery, or recapture device), the owner or operator shall develop and implement the plan in accordance with paragraph (d) of this section.

(3) If epoxide emissions are maintained below the epoxide emission factor limitation through the use of extended cookout in conjunction with a combustion, recovery, or recapture device, the owner or operator shall develop and implement the plan in accordance with paragraph (e) of this section.

(c) Compliance with epoxide emission factor limitation using a combustion, recovery, or recapture device. (1) The owner or operator shall notify the Agency of the intent to use a combustion, recovery, or recapture device to...
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Comply with the epoxide emission factor limitation in §63.1425(b)(1)(iii) or (b)(2)(iv). The owner or operator shall prepare an estimate of the annual epoxide emissions and the actual production rate in accordance with paragraphs (c)(1)(i) through (iv) of this section. This notification and emission estimate shall be submitted in the Precompliance Report as specified in §63.1439(e)(4), or in the operating permit application, as allowed in §63.1439(e)(8).

(i) Annual uncontrolled epoxide emissions. These emission estimates shall be determined in accordance with the batch process vent group determination procedures in the NESHAP for Group I Polymers and Resins (40 CFR part 63, subpart U, §63.488(b)) and shall be based on anticipated production.

(ii) A description of the combustion, recovery, or recapture device, along with the expected percent efficiency.

(iii) Annual emissions after the combustion, recovery, or recapture device. The expected annual emissions after control shall be determined using Equation 15.

\[
AE_{\text{control}} = (AE_{\text{uncontrolled}}) \left(1 - \frac{R}{100}\right)\quad [\text{Equation 15}]
\]

Where:

- \(AE_{\text{control}}\) = Annual epoxide emissions after control, kg/yr.
- \(AE_{\text{uncontrolled}}\) = Annual uncontrolled epoxide emissions, determined in accordance with paragraph (c)(1)(i) of this section, kg/yr.
- \(R\) = Expected control efficiency of the combustion, recovery, or recapture device, percent, as determined in §63.1426(c).

(iv) The actual annual production rate means the annual mass of polyether polyol product produced from the applicable PMPU. This production rate shall be for the same annual time period as the annual emission estimate as calculated in accordance with paragraph (c)(1)(iii) of this section.

(2) The owner or operator shall conduct a performance test in accordance with §63.1426(c) to determine the epoxide control efficiency of the combustion, recovery, or recapture device. The owner or operator shall then recalculate the annual epoxide emissions after control using Equation 15, except that the control efficiency, \(R\), shall be the measured control efficiency. This information shall be submitted as part of the Notification of Compliance Status, as provided in §63.1439(e)(5).

(3) The owner or operator shall comply with the process vent monitoring provisions in §63.1429.

(e) Compliance with the epoxide emission factor limitation through the use of extended cookout in conjunction with one

(d) Compliance with epoxide emission factor limitation using extended cookout. (1) The owner or operator shall notify the Agency of the intent to use extended cookout to comply with the epoxide emission factor limitation in §63.1425(b)(1)(iii) or (b)(2)(iv). The owner or operator shall prepare an estimate of the annual epoxide emissions after the extended cookout. This notification and emission estimate shall be submitted in the Precompliance Report as specified in §63.1439(e)(4), or in the operating permit application, as allowed in §63.1439(e)(8).

(2) The owner or operator shall determine the annual epoxide emissions in accordance with §63.1427(d), based on anticipated production. This information shall be submitted as part of the Notification of Compliance Status, as provided in §63.1439(e)(5).

(3) The owner or operator shall comply with the ECO monitoring provisions in §63.1427(i).

(4) The owner or operator shall comply with the process vent record-keeping and reporting requirements in §63.1430.
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§ 63.1432 Storage vessel provisions.

(a) For each storage vessel located at an affected source, the owner or operator shall comply with the HON storage vessel requirements of §§ 63.119 through 63.123 and the HON leak inspection provisions in § 63.148, with the differences noted in paragraphs (b) through (p) of this section, for the purposes of this subpart.

(b) When the term “storage vessel” is used in the HON storage vessel requirements in §§ 63.119 through 63.123, the definition of this term in § 63.1423 shall apply for the purposes of this subpart.

(c) When the term “Group 1 storage vessel” is used in the HON storage vessel requirements in §§ 63.119 through 63.123, the definition of this term in § 63.1423 shall apply for the purposes of this subpart.

(d) When the term “Group 2 storage vessel” is used in the HON storage vessel requirements in §§ 63.119 through 63.123, the definition of this term in § 63.1423 shall apply for the purposes of this subpart.

(e) When the HON storage vessel requirements in § 63.119 refer to “December 31, 1992,” the phrase “September 4, 1997” shall apply instead, for the purposes of this subpart.

(f) When the HON storage vessel requirements in § 63.119 refer to “April 22, 1994,” the phrase “June 1, 1999,” shall apply instead, for the purposes of this subpart.

(g) The owner or operator of an affected source shall comply with this paragraph instead of § 63.120(d)(1)(ii) for the purposes of this subpart. If the combustion, recovery, or recapture device used to comply with § 63.119(e) is also used to comply with any of the requirements found in §§ 63.1425 through 63.1431 and/or § 63.1433, the performance test required in or accepted by §§ 63.1425 through 63.1431 and/or § 63.1433 is acceptable for demonstrating compliance with the HON storage vessel requirements in § 63.119(e), for the purposes of this subpart. The owner or operator will not be required to prepare a design evaluation for the combustion, recovery, or recapture device as described in § 63.120(d)(1)(i), if the performance test meets the criteria specified in paragraphs (g)(1) and (2) of this section.

1. The performance test demonstrates that the combustion, recovery, or recapture device achieves greater than or equal to the required control efficiency specified in the HON storage vessel requirements.
vessel requirements in §63.119(e)(1) or (2), as applicable; and

(2) The performance test is submitted as part of the Notification of Compliance Status required by §63.1439(e)(5).

(h) When the HON storage vessel requirements in §63.120(d)(3)(i) uses the term “operating range,” the term “level,” shall apply instead, for the purposes of this subpart.

(i) For purposes of this subpart, the monitoring plan required by the HON storage vessel requirements in §63.120(d)(2) shall specify for which combustion, recovery, or recapture device the owner or operator has selected to follow the procedures for continuous monitoring specified in §63.1438. For the combustion, recovery, or recapture device(s) for which the owner or operator has selected not to follow the procedures for continuous monitoring specified in §63.1438, the monitoring plan shall include a description of the parameter(s) to be monitored to ensure that the combustion, recovery, or recapture device is being properly operated and maintained, an explanation of the criteria used for selection of that parameter(s), and the frequency with which monitoring will be performed (e.g., when the liquid level in the storage vessel is being raised), as specified in §63.120(d)(2)(i).

(j) For purposes of this subpart, the monitoring plan required by §63.122(b) shall be included in the Notification of Compliance Status required by §63.1439(e)(5).

(k) When the HON Notification of Compliance Status requirements contained in §63.152(b) are referred to in §§63.120, 63.122, and 63.123, the Notification of Compliance Status requirements contained in §63.1439(e)(5) shall apply for the purposes of this subpart.

(l) When the HON Periodic Report requirements contained in §63.152(c) are referred to in §§63.120, 63.122, and 63.123, the Periodic Report requirements contained in §63.1439(e)(6) shall apply for the purposes of this subpart.

(m) When other reports as required in §63.152(d) are referred to in §63.122, the reporting requirements contained in §63.1439(e)(7) shall apply for the purposes of this subpart.

(n) When the HON Initial Notification requirements contained in §63.151(b) are referred to in §63.119 through §63.123, the owner or operator shall comply with the Initial Notification requirements contained in §63.1439(e)(3), for the purposes of this subpart.

(o) When the determination of equivalence criteria in §63.102(b) are referred to in the HON storage vessel requirements in §63.121(a), the General Provisions’ alternative nonopacity emission provisions in §63.6(g) shall apply for the purposes of this subpart.

(p) The compliance date for storage vessels at affected sources subject to the provisions of this section is specified in §63.1422.

(q) In addition to the records required by §63.122, the owner or operator shall maintain records of all times when the storage tank is being filled (i.e., when the liquid level in the storage vessel is being raised). These records shall consist of documentation of the time when each filling period begins and ends.

§63.1433 Wastewater provisions.

(a) Process wastewater. Except as specified in paragraph (c) of this section, the owner or operator of each affected source shall comply with the HON wastewater requirements in §§63.132 through 63.147 for each process wastewater stream originating at an affected source, with the HON leak inspection requirements in §63.148, and with the HON requirements in §63.149 for equipment that is subject to §63.149, with the differences noted in paragraphs (a)(1) through (20) of this section. Further, the owner or operator of each affected source shall comply with the requirements of §63.105(a) for maintenance wastewater, as specified in paragraph (b) of this section.

(1) Owners and operators of affected sources are not required to comply with the HON new source wastewater requirements in §63.132(b)(1) and §63.132(d), for the purposes of this subpart. Owners or operators of all new affected sources, as defined in this subpart, shall comply with the HON wastewater requirements for existing sources in §§63.132 through 63.149.

(2) When the HON requirements in §§63.132 through 63.149 refer to Table 9 or Table 36 of 40 CFR part 63, subpart
G, the owner or operator is only required to consider organic HAP listed in Table 9 or Table 36 of 40 CFR part 63, subpart G, that are also listed on Table 4 of this subpart, for the purposes of this subpart. Owners and operators are exempt from all requirements in §§63.132 through 63.149 that pertain solely and exclusively to organic HAP listed on Table 8 of 40 CFR part 63, subpart G. In addition, when §§63.132 through 63.149 refer to List 1 or List 2, as listed in Table 36 of 40 CFR part 63, subpart G, the owner or operator is only required to consider organic HAP contained in those lists that are also listed on Table 4 of this subpart, for the purposes of this subpart.

(3) When the determination of equivalence criteria in §63.102(b) is referred to in §§63.132, 63.133, and 63.137, the General Provisions’ alternative nonopacity emission standard provisions in §63.6(g) shall apply for the purposes of this subpart.

(4) When the HON storage vessel requirements contained in §§63.119 through 63.123 are referred to in §§63.132 through 63.149, the HON storage vessel requirements in §§63.119 through 63.123 are applicable, with the exception of the differences referred to in the storage vessel requirements in §63.1432, for the purposes of this subpart.

(5) When the HON process wastewater reporting requirements in §63.146(a) require the submission of a request for approval to monitor alternative parameters according to the procedures specified in §63.151(g) or §63.152(e), the owner or operator requesting to monitor alternative parameters shall follow the procedures specified in §63.1439(f), for the purposes of this subpart.

(6) When the HON process wastewater recordkeeping requirements in §63.147(d) require the owner or operator to keep records of the daily average value of each continuously monitored parameter for each operating day as specified in the HON recordkeeping provisions in §63.152(f), the owner or operator shall instead keep records of the daily average value of each continuously monitored parameter as specified in §63.1439(d), for the purposes of this subpart.

(7) When the HON requirements in §§63.132 through 63.149 refer to an “existing source,” the term “existing affected source,” as defined in §63.1420(a)(3) shall apply, for the purposes of this subpart.

(8) When the HON requirements in §§63.132 through 63.149 refer to a “new source,” the term “new affected source,” as defined in §63.1420(a)(4) shall apply, for the purposes of this subpart.

(9) When the HON process wastewater provisions in §63.132 refer to a Group 1 wastewater stream or a Group 2 wastewater stream, the definitions of these terms contained in §63.1423 shall apply, for the purposes of this subpart.

(10) Whenever the HON process wastewater provisions in §§63.132 through 63.147 refer to a Group 1 wastewater stream or a Group 2 wastewater stream, the definitions of these terms contained in §63.1423 shall apply, for the purposes of this subpart.

(11) When the HON control requirements for certain liquid streams in open systems, in §63.149(d), refer to “§ 63.100(f) of subpart F,” the terms defined in §63.1420(c), shall apply for the purposes of this subpart. In addition, where §63.149(d) states “and the item of equipment is not otherwise exempt from controls by the provisions of subparts A, F, G, H, or P, or PPP of this part,” the applicable compliance dates specified in §63.1422 shall apply, for the purposes of this subpart.

(12) When the HON control requirements for certain liquid streams in open systems, in §63.149(e)(1) and (2), refer to “a chemical manufacturing process unit subject to the new source requirements of 40 CFR 63.100(l)(1) or (2),” the phrase “a new affected source as described in §63.1420(a)(4),” shall apply for the purposes of this subpart.

(13) When the HON Notification of Compliance Status requirements contained in §63.152(b) are referred to in the HON process wastewater provisions in §§63.138 or §63.146, the Notification of Compliance Status requirements contained in §63.1439(e)(5) shall apply for the purposes of this subpart. In addition, when the HON process wastewater
provisions in §63.138 or §63.146 require that information be reported according to §63.152(b) in the HON Notification of Compliance Status, owners or operators of affected sources shall report the specified information in the Notification of Compliance Status required by §63.1439(e)(5), for the purposes of this subpart.

(14) When the HON Periodic Report requirements contained in §63.152(c) are referred to in the HON process wastewater provisions in §63.146, the Periodic Report requirements contained in §63.1439(e)(6) shall apply for the purposes of this subpart. In addition, when §63.146 requires that information be reported in the HON Periodic Reports required in §63.152(c), owners or operators of affected sources shall report the specified information in the Periodic Reports required in §63.1439(e)(6), for the purposes of this subpart.

(15) When the term “range” is used in the HON requirements in §§63.132 through 63.149, the term “level” shall be used instead, for the purposes of this subpart. This level shall be determined using the procedures specified in parameter monitoring procedures in §63.1438.

(16) When the HON process wastewater monitoring and inspection provisions in §63.143(f) specify that the owner or operator shall establish the range that indicates proper operation of the treatment process or control technique, the owner or operator shall instead comply with the requirements §63.1438 (c) or (d) for establishing parameter level maximums/minimums, for the purposes of this subpart.

(17) When the HON process wastewater provisions in §63.146(b) (7) and (8) require that “the information on parameter ranges specified in §63.152(b)(2)” be reported in the HON Notification of Compliance Status, owners and operators of affected sources are instead required to report the information on parameter levels in the Notification of Compliance Status as specified in §63.1439(e)(5)(ii), for the purposes of this subpart.

(18) For the purposes of this subpart, the owner or operator is not required to comply with the HON process wastewater emission reduction provisions in §63.138(g).

(19) When the provisions of HON process wastewater provisions in §63.139(c)(1)(ii), §63.145(d)(4), or §63.145(i)(2) specify that Method 18, 40 CFR part 60, appendix A shall be used, Method 18 or Method 25A, 40 CFR part 60, appendix A may be used for the purposes of this subpart. The use of Method 25A, 40 CFR part 60, appendix A shall comply with paragraphs (a)(19) (i) and (ii) of this section.

(i) The organic HAP used as the calibration gas for Method 25A, 40 CFR part 60, appendix A shall be the single organic HAP representing the largest percent by volume of the emissions.

(ii) The use of Method 25A, 40 CFR part 60, appendix A is acceptable if the response from the high-level calibration gas is at least 20 times the standard deviation of the response from the zero calibration gas when the instrument is zeroed on the most sensitive scale.

(20) The owner or operator of a facility which receives a Group 1 wastewater stream, or a residual removed from a Group 1 wastewater stream, for treatment pursuant to the HON provisions in §63.132(g) is subject to the requirements of §63.132(g), with the differences identified in this section, and is not subject to the NESHAP from offsite waste and recovery operations in 40 CFR part 63, subpart DD, with respect to the received material.

(b) Maintenance wastewater. The owner or operator of each affected source shall comply with the HON maintenance wastewater requirements in §63.105, with the exceptions noted in paragraphs (b) (1), (2), and (3) of this section.

(1) When the HON maintenance wastewater provisions in §63.105(a) refer to “organic HAPs,” the definition of “organic HAP” in §63.1423 shall apply, for the purposes of this subpart.

(2) When the term “maintenance wastewater” is used in the HON maintenance wastewater provisions in §63.105, the definition of “maintenance wastewater” in §63.1423 shall apply, for the purposes of this subpart.
(3) When the term "wastewater" is used in the HON maintenance wastewater provisions in §63.105, the definition of "wastewater" in §63.1423 shall apply, for the purposes of this subpart.

(c) Compliance date. The compliance date for the affected source subject to the provisions of this section is specified in §63.1422.

§ 63.1434 Equipment leak provisions.

(a) The owner or operator of each affected source shall comply with the HON equipment leak requirements in 40 CFR part 63, subpart H for all equipment in organic HAP service, except as specified in paragraphs (b) through (g) of this section.

(b) The compliance date for the equipment leak provisions in this section is provided in §63.1422(d).

(c) Affected sources subject to the HON equipment leak provisions in 40 CFR part 63, subpart H shall continue to comply with 40 CFR part 63, subpart H until the compliance date specified in §63.1422. After the compliance date in §63.1422, the source shall be subject to this subpart (40 CFR part 63, subpart PPP), and shall no longer be subject to 40 CFR part 63, subpart H. However, sources subject to 40 CFR part 63, subpart H that have elected to comply through a quality improvement program, as specified in the HON quality improvement plans for valves or pumps in §63.175 or §63.176 or both, may elect to continue these programs without interruption as a means of complying with this subpart. In other words, becoming subject to this subpart does not restart or reset the "compliance clock" as it relates to reduced burden earned through a quality improvement program.

(d) When the HON equipment leak Initial Notification requirements contained in §63.182(a)(1) and §63.182(b) are referred to in 40 CFR part 63, subpart H, the owner or operator shall comply with the Initial Notification requirements contained in §63.1439(e)(3), for the purposes of this subpart. The Initial Notification shall be submitted no later than June 1, 2000 for existing sources, as stated in §63.1439(e)(3)(ii)(A).

(e) The HON equipment leak Notification of Compliance Status required by §63.182(a)(2) and §63.182(c) shall be submitted within 150 days (rather than 90 days) of the applicable compliance date specified in §63.1422 for the equipment leak provisions. The notification may be submitted as part of the Notification of Compliance Status required by §63.1439(e)(5).

(f) The Periodic Reports required by §63.182(a)(3) and §63.182(d) may be submitted as part of the Periodic Reports required by §63.1439(e)(6).

(g) If specific items of equipment, comprising part of a process unit subject to this subpart, are managed by different administrative organizations (e.g., different companies, affiliates, departments, divisions, etc.), those items of equipment may be aggregated with any PMPU within the affected source for all purposes under subpart H, providing there is no delay in achieving the applicable compliance date.

(h) The phrase "the provisions of subparts F, I, or PPP of this part" shall apply instead of the phrase "the provisions of subparts F or I of this part," and instead of the phrase "the provisions of subpart F or I of this part" throughout §§63.163 and 63.168, for the purposes of this subpart. In addition, the phrase "subparts F, I, and PPP" shall apply instead of the phrase "subparts F and I" in §63.174(c)(2)(iii), for the purposes of this subpart.

§ 63.1435 Heat exchanger provisions.

(a) The owner or operator of each affected source shall comply with the requirements of §63.104 for heat exchange systems, with the exceptions noted in paragraphs (b) through (e) of this section.

(b) When the term "chemical manufacturing process unit" is used in §63.104, the term "polyether polyols manufacturing process unit" shall apply for the purposes of this subpart. Further, when the phrase "a chemical manufacturing process unit meeting the conditions of §63.100(b)(1) through (3) of this subpart, except for chemical manufacturing process units meeting the conditions specified in §63.100(c) of this subpart" is used in §63.104(a), the term "PMPU, except for PMPU meeting the conditions specified in
§ 63.1420(b)" shall apply for the purposes of this subpart.

(c) When the HON heat exchange system requirements in § 63.104(c)(3) and § 63.104(f)(1) specify that the monitoring plan and records required by § 63.104(f)(1)(i) through (iv) shall be kept as specified in the HON general compliance, reporting, and recordkeeping provisions in § 63.103(c), the provisions of the general recordkeeping and reporting requirements in § 63.1439(a) and the applicable provisions of the General Provisions in 40 CFR part 63, subpart A, as specified in Table 1 of this subpart, shall apply for the purposes of this subpart.

(d) When the HON heat exchange system requirements in § 63.104(f)(2) require information to be reported in the Periodic Reports required by the HON general reporting provisions in § 63.152(c), the owner or operator shall instead report the information specified in § 63.104(f)(2) in the Periodic Reports required by the general reporting requirements in § 63.1439(e)(6), for the purposes of this subpart.

(e) When the HON heat exchange system requirements in § 63.104 refer to Table 4 of 40 CFR part 63, subpart F or Table 9 of 40 CFR part 63, subpart G, the owner or operator is only required to consider organic HAP listed in Table 4 of 40 CFR part 63, Table 9 of subpart G that are also listed on Table 4 of this subpart, for the purposes of this subpart.

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§ 63.1437 Additional requirements for performance testing.

(a) Performance testing shall be conducted in accordance with § 63.7(a)(1), (a)(3), (d), (e)(1), (e)(2), (e)(4), (g), and (h), with the exceptions specified in paragraphs (a)(1) through (4) of this section and the additions specified in paragraph (b) of this section.

(b) Performance tests shall be conducted according to the General Provisions' performance testing requirements in § 63.7(e)(1) and (2), except that for all emission sources except process vents from batch unit operations, performance tests shall be conducted during maximum representative operating conditions for the process achievable during one of the time periods described in paragraph (a)(1)(i) of this section, without causing any of the situations described in paragraph (a)(1)(ii) or (iii) of this section to occur. For process vents from batch unit operations, performance tests shall be conducted at absolute worst-case conditions, as defined in § 63.1426(c)(3)(i)(B), that are achievable during one of the time periods described in paragraph (a)(1)(i) of this section, without causing any of the situations described in paragraph (a)(1)(ii) or (iii) of this section to occur.

(i) The 6-month period that ends 2 months before the Notification of Compliance Status is due, according to § 63.1439(e)(5); or the 6-month period that begins 3 months before the performance test and ends 3 months after the performance test.

(ii) Causing damage to equipment; necessitating that the owner or operator make a product that does not meet an existing specification for sale to a customer; or necessitating that the owner or operator make a product in excess of demand.

(iii) Causing plant or testing personnel to be subject to unsafe conditions. Owners or operators that limit testing based on this paragraph shall maintain documentation that demonstrates the nature of the unsafe conditions and explains measures considered by the owner or operator to overcome these conditions. If requested, this documentation shall be provided to the Administrator.

(2) When the General Provisions' data analysis, recordkeeping, and reporting requirements in § 63.7(g) refer to the Notification of Compliance Status requirements in § 63.9(h), the Notification of Compliance Status requirements in § 63.1439(e)(5) shall instead apply, for the purposes of this subpart.

(3) Because the General Provisions' site-specific test plan in § 63.7(c)(3) is not required, the General Provisions' requirement for the Administrator to approve or deny site-specific test plans, in § 63.7(h)(4)(ii), is not applicable for the purposes of this subpart.

(4) The owner or operator of an affected source shall provide the Administrator at least 30 days prior notice of
any performance test, except as specified under other subparts, to afford the Administrator the opportunity to have an observer present. If after 30 days notice for an initially scheduled performance test, there is a delay (due to operational problems, etc.) in conducting the scheduled performance test, the owner or operator of an affected source shall notify the Administrator (or delegated State or local agency) as soon as possible of any delay in the original test date, either by providing at least 7 days prior notice of the rescheduled test date of the performance test, or by arranging a rescheduled date with the Administrator (or delegated State or local agency) by mutual agreement.

(b) Data shall be reduced in accordance with the EPA approved methods specified in the applicable subpart or, if other test methods are used, the data and methods shall be validated according to the protocol in Method 301, 40 CFR part 63, appendix A.

(c) Notwithstanding any other provision of this subpart, if an owner or operator of an affected source uses a flare to comply with any of the requirements of this subpart, the owner or operator shall comply with paragraphs (c)(1) through (3) of this section. The owner or operator is not required to conduct a performance test to determine percent emission reduction or outlet organic HAP or TOC concentration. If a compliance demonstration has been conducted previously for a flare, using the techniques specified in paragraphs (c)(1) through (3) of this section, that compliance demonstration may be used to satisfy the requirements of this paragraph if either no deliberate process changes have been made since the compliance demonstration, or the results of the compliance demonstration reliably demonstrate compliance despite process changes.

(1) Conduct a visible emission test using the techniques specified in §63.11(b)(4) of the General Provisions;

(2) Determine the net heating value of the gas being combusted, using the techniques specified in §63.11(b)(6) of the General Provisions; and

(3) Determine the exit velocity using the techniques specified in either §63.11(b)(7)(ii) and §63.11(b)(7)(iii), where applicable) or §63.11(b)(8) of the General Provisions, as appropriate.

§63.1438 Parameter monitoring levels and excursions.

(a) Establishment of parameter monitoring levels. The owner or operator of a combustion, recovery, or recapture device that has one or more parameter monitoring level requirements specified under this subpart shall establish a maximum or minimum level for each measured parameter. If a performance test is required by this subpart for a combustion, recovery, or recapture device, the owner or operator shall use the procedures in either paragraph (b) or (c) of this section to establish the parameter monitoring level(s). If a performance test is not required by this subpart for a combustion, recovery, or recapture device, the owner or operator may use the procedures in paragraph (b), (c), or (d) of this section to establish the parameter monitoring levels. When using the procedures specified in paragraph (c) or (d) of this section, the owner or operator shall submit the information specified in §63.1439(e)(4)(viii) for review and approval, as part of the Precompliance Report.

(1) The owner or operator shall operate combustion, recovery, and recapture devices such that the daily average value of monitored parameters remains at or above the minimum established level, or remains at or below the maximum established level, except as otherwise provided in this subpart.

(2) As specified in §63.1439(e)(5)(ii), all established levels, along with their supporting documentation and the definition of an operating day, shall be submitted as part of the Notification of Compliance Status.

(3) Nothing in this section shall be construed to allow a monitoring parameter excursion caused by an activity that violates other applicable provisions of 40 CFR part 63, subparts A, F, G, or H.

(b) Establishment of parameter monitoring levels based exclusively on performance tests. In cases where a performance test is required by this subpart, or the owner or operator of the affected source elects to do a performance test in accordance with the provisions of
this subpart, and an owner or operator elects to establish a parameter monitoring level for a combustion, recovery, or recapture device based exclusively on parameter values measured during the performance test, the owner or operator of the affected source shall comply with the procedures in paragraph (b)(1) or (2) of this section, as applicable.

(1) Process vents from continuous unit operations. During initial compliance testing, the appropriate parameter shall be continuously monitored during the required 1-hour runs for process vents from continuous unit operations. The monitoring level(s) shall then be established as the average of the maximum (or minimum) point values from the three 1-hour test runs. The average of the maximum values shall be used when establishing a maximum level, and the average of the minimum values shall be used when establishing a minimum level.

(2) Process vents from batch unit operations. For process vents from batch unit operations, during initial compliance testing, the appropriate parameter shall be continuously monitored during the entire test period. The monitoring level(s) shall be those established during the compliance test.

(c) Establishment of parameter monitoring levels based on performance tests, supplemented by engineering assessments and/or manufacturer’s recommendations. Parameter monitoring levels established under this paragraph shall be based on the parameter values measured during the performance test supplemented by engineering assessments and/or manufacturer’s recommendations. Performance testing is not required to be conducted over the entire range of expected parameter values. The information specified in paragraphs (c)(1) and (2) of this section shall be provided in the Notification of Compliance Status.

(1) The specific level of the monitored parameter(s) for each emission point.

(2) The rationale for the specific level for each parameter for each emission point, including any data and calculations used to develop the level and a description of why the level indicates proper operation of the combustion, recovery, or recapture device.

(d) Establishment of parameter monitoring based on engineering assessments and/or manufacturer’s recommendations. If a performance test is not required by this subpart for a combustion, recovery, or recapture device, the maximum or minimum level may be based solely on engineering assessments and/or manufacturers’ recommendations. As required in paragraph (a)(2) of this section, the determined level and all supporting documentation shall be provided in the Notification of Compliance Status.

(e) Monitoring violations. (1) With the exception of excursions excused in accordance with paragraph (g) of this section, each excursion, as defined in paragraphs (f)(1)(i), (f)(2)(i)(A), (f)(2)(ii), (f)(3)(i), and (f)(4) of this section, constitutes a violation of the provisions of this subpart in accordance with paragraph (e)(1)(i), (ii), or (iii) of this section.

(i) For each condenser, each excursion constitutes a violation of the emission limit.

(ii) For each recovery or recapture device other than a condenser, where an organic monitoring device is used to monitor concentration, each excursion constitutes a violation of the emission limit.

(iii) For each combustion, recovery, or recapture device other than a condenser, each excursion constitutes a violation of the operating limit.

(2) With the exception of excursions excused in accordance with paragraph (g) of this section, each excursion, as defined in paragraphs (f)(1)(ii), (f)(1)(iii), (f)(2)(i)(B), and (f)(3)(ii) of this section constitutes a violation of the operating limit.

(f) Parameter monitoring excursion definitions. Parameter monitoring excursions are defined in paragraphs (f)(1) through (3) of this section.

(1) With respect to storage vessels (where the applicable monitoring plan specifies continuous monitoring), process vents from continuous unit operations using combustion, recovery, or recapture devices for purposes of compliance, and for process wastewater streams, an excursion means any of the
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three cases listed in paragraphs (f)(1)(i) through (iii) of this section.

(i) The daily average value of one or more monitored parameters is above the maximum level or below the minimum level established for the given parameters.

(ii) The period of combustion, recovery, or recapture device operation, with the exception noted in paragraph (f)(1)(v) of this section, is 4 hours or greater in an operating day and monitoring data are insufficient, as defined in paragraph (f)(1)(iv) of this section, to constitute a valid hour of data for at least 75 percent of the operating hours.

(iii) The period of combustion, recovery, or recapture device operation, with the exception noted in paragraph (f)(1)(v) of this section, is less than 4 hours in an operating day and more than 2 of the hours during the period of operation do not constitute a valid hour of data due to insufficient monitoring data, as defined in paragraph (f)(1)(iv) of this section.

(iv) Monitoring data are insufficient to constitute a valid hour of data, as used in paragraphs (f)(1)(ii) and (iii) of this section, if measured values are unavailable due to monitoring system breakdowns, repairs, calibrated checks, or zero (low-level) and high level adjustments, for any of the 15-minute periods within the hour. For data compression systems approved under §63.1439(g)(3), monitoring data are insufficient to calculate a valid hour of data if there are less than four data measurements made during the hour.

(v) The periods listed in paragraphs (f)(1)(v)(A) through (D) of this section are not considered to be part of the period of combustion, recovery, or recapture device operation, for the purposes of paragraphs (f)(1)(ii) and (iii) of this section.

(A) Start-ups;

(B) Shutdowns;

(C) Malfunctions; or

(D) Periods of non-operation of the affected source (or portion thereof), resulting in cessation of the emissions to which the monitoring applies.

(2) For storage vessels where the applicable monitoring plan does not specify continuous monitoring, an excursion is defined in paragraph (f)(2)(i) or (ii) of this section, as applicable.

(i) If the monitoring plan specifies monitoring a parameter and recording its value at specific intervals (such as every 15 minutes or every hour), either of the cases listed in paragraph (f)(2)(i)(A) or (B) of this section is considered a single excursion for the combustion device.

(A) When the average value of one or more parameters, averaged over the time during which the storage vessel is being filled (i.e., when the liquid level in the storage vessel is being raised), is above the maximum level or below the minimum level established for the given parameters.

(B) When monitoring data are insufficient. Monitoring data shall be considered insufficient when measured values are not available, due to monitoring system breakdowns, repairs, calibration checks, or zero (low-level) and high-level adjustments, for at least 75 percent of the specific intervals at which parameters are to be monitored and recorded, according to the storage vessel’s monitoring plan, during which the storage vessel is being filled.

(ii) If the monitoring plan does not specify monitoring a parameter and recording its value at specific intervals (for example, if the relevant operating requirement is to exchange a disposable carbon canister before expiration of its rated service life), the monitoring plan shall define an excursion in terms of the relevant operating requirement.

(3) With respect to process vents from batch unit operations, an excursion means one of the two cases listed in paragraphs (f)(3)(i) and (ii) of this section.

(i) When the daily average value of one or more monitored parameters is above the maximum or below the minimum established level for the given parameters.

(ii) When monitoring data are insufficient for an operating day. Monitoring data shall be considered insufficient when measured values are not available, due to monitoring system breakdowns, repairs, calibration checks, or zero (low-level) and high-level adjustments, for at least 75 percent of the 15-minute periods when batch emission episodes selected to be controlled are
being vented to the control device during the operating day, using the procedures specified in paragraphs (f)(3)(ii)(A) through (D) of this section.

(A) Determine the total amount of time during the operating day when batch emission episodes selected to be controlled are being vented to the control device.

(B) Subtract the time during the periods listed in paragraphs (f)(3)(ii)(B)(1) through (4) of this section from the total amount of time determined above in paragraph (f)(3)(ii)(A) of this section, to obtain the operating time used to determine if monitoring data are insufficient.

(1) Start-ups;
(2) Shutdowns;
(3) Malfunctions; or
(4) Periods of non-operation of the affected source (or portion thereof), resulting in cessation of the emissions to which the monitoring applies.

(C) Determine the total number of 15-minute periods in the operating time used to determine if monitoring data are insufficient, as was determined in accordance with paragraph (f)(3)(ii)(B) of this section.

(D) If measured values are not available for at least 75 percent of the total amount of 15-minute periods determined in paragraph (f)(3)(ii)(C) of this section, the monitoring data are insufficient for the operating day.

(4) With respect to process vents using ECO to reduce epoxide emissions, an excursion means any of the situations described in §63.1427(i)(3)(i) through (v). For each excursion, the owner or operator shall be deemed out of compliance with the provisions of this subpart, in accordance with paragraph (e) of this section, except as provided in paragraph (g) of this section.

(g) Excused excursions. A number of excused excursions shall be allowed for each combustion, recovery, or recapture device for each semiannual period. The number of excused excursions for each semiannual period is specified in paragraphs (g)(1) through (6) of this section. This paragraph applies to affected sources required to submit Periodic Reports semiannually or quarterly. The first semiannual period is the 6-month period starting the date the Notification of Compliance Status is due.

(1) For the first semiannual period—six excused excursions.
(2) For the second semiannual period—five excused excursions.
(3) For the third semiannual period—four excused excursions.
(4) For the fourth semiannual period—three excused excursions.
(5) For the fifth semiannual period—two excused excursions.
(6) For the sixth and all subsequent semiannual periods—one excused excursion.

§63.1439 General recordkeeping and reporting provisions.

(a) Data retention. Unless otherwise specified in this subpart, the owner or operator of an affected source shall keep copies of all applicable records and reports required by this subpart for at least 5 years. All applicable records shall be maintained in such a manner that they can be readily accessed. The most recent 6 months of records shall be retained on site or shall be accessible from a central location by computer or other means that provide access within 2 hours after a request. The remaining 4 and one-half years of records may be retained offsite. Records may be maintained in hard copy or computer-readable form including, but not limited to, on microfilm, computer, floppy disk, magnetic tape, or microfiche. If an owner or operator submits copies of reports to the applicable EPA Regional Office, the owner or operator is not required to maintain copies of reports. If the EPA Regional Office has waived the requirement of §63.10(a)(4)(ii) for submittal of copies of reports, the owner or operator is not required to maintain copies of reports.

(b) Subpart A requirements. The owner or operator of an affected source shall comply with the applicable recordkeeping and reporting requirements in 40 CFR part 63, subpart A (the General Provisions) as specified in Table 1 of this subpart. These requirements include, but are not limited to, the requirements specified in paragraphs (b)(1) and (2) of this section.

(1) Start-up, shutdown, and malfunction plan. The owner or operator of an
affected source shall develop and implement a written start-up, shutdown, and malfunction plan as specified in the General Provisions' requirements for a Startup, Shutdown, and Malfunction Plan in §63.6(e)(3). This plan shall describe, in detail, procedures for operating and maintaining the affected source during periods of start-up, shutdown, and malfunction and a program for corrective action for malfunctioning process and air pollution control equipment used to comply with this subpart. A provision for ceasing to collect, during a start-up, shutdown, or malfunction, monitoring data that would otherwise be required by the provisions of this subpart may be included in the start-up, shutdown, and malfunction plan only if the owner or operator has demonstrated to the Administrator, through the Precompliance Report or a supplement to the Precompliance Report, that the monitoring system would be damaged or destroyed if it were not shut down during the start-up, shutdown, or malfunction. The owner or operator of the affected source shall keep the start-up, shutdown, and malfunction plan on site. In addition, if the start-up, shutdown, and malfunction plan is revised, the owner or operator shall keep previous (i.e., superseded) versions of the start-up, shutdown, and malfunction plan for a period of 5 years after each revision to the plan. If the new version of the start-up, shutdown, and malfunction plan includes a provision for ceasing to collect, during a start-up, shutdown, or malfunction, monitoring data that would otherwise be required, the owner or operator shall submit a supplement to the Precompliance Report to the Administrator for the Administrator's approval, documenting that the monitoring system would be damaged or destroyed if it were not shut down during the start-up, shutdown, or malfunction. Records associated with the plan shall be kept as specified in paragraphs (b)(1)(i)(A) and (B) of this section. Reports related to the plan shall be submitted as specified in paragraph (b)(1)(ii) of this section.

(A) Records of the occurrence and duration of each start-up, shutdown, and malfunction of operation of process equipment or combustion, recovery, or recapture devices or continuous monitoring systems used to comply with this subpart during which excess emissions (as defined in §63.1420(h)(4)) occur.

(B) For each start-up, shutdown, or malfunction during which excess emissions (as defined in §63.1420(h)(4)) occur, records reflecting whether the procedures specified in the affected source's start-up, shutdown, and malfunction plan were followed, and documentation of actions taken that are not consistent with the plan. For example, if a start-up, shutdown, and malfunction plan includes procedures for routing a combustion, recovery, or recapture device to a backup combustion, recovery, or recapture device, records shall be kept of whether the plan was followed. These records may take the form of a "checklist," or other form of recordkeeping that confirms conformance with the start-up, shutdown, and malfunction plan for the event.

(ii) For the purposes of this subpart, the semiannual start-up, shutdown, and malfunction reports shall be submitted on the same schedule as the Periodic Reports required under paragraph (e)(6) of this section instead of according to the General Provisions' Periodic Reporting schedule specified in §63.10(d)(5)(i). The reports shall include the information specified in paragraphs (b)(1)(i)(A) and (B) of this section and shall contain the name, title, and signature of the owner or operator or other responsible official who is certifying its accuracy.

(2) Application for approval of construction or reconstruction. For new affected sources, the owner or operator shall comply with the General Provisions' requirements for the application for approval of construction or reconstruction, as specified in §63.5, excluding the provisions specified in §63.5(d)(1)(i)(H), (d)(1)(iii), (d)(2), and (d)(3)(ii).

(c) Subpart H requirements. The owner or operator of an affected source shall comply with the HON equipment leak
reporting and recordkeeping requirements in 40 CFR part 63, subpart H, except as specified in §63.1434(b) through (g).

(d) Recordkeeping and documentation. The owner or operator required to keep continuous records shall keep records as specified in paragraphs (d)(1) through (7) of this section, unless an alternative recordkeeping system has been requested and approved as specified in paragraph (g) of this section, and except as provided in paragraph (h) of this section. If a monitoring plan for storage vessels pursuant to §63.1432(i) requires continuous records, the monitoring plan shall specify which provisions, if any, of paragraphs (d)(1) through (7) of this section apply. As described in §63.1432(i), certain storage vessels are not required to keep continuous records as specified in this paragraph. The owner or operator of such storage vessels shall keep records as specified in the monitoring plan required by §63.1432(i).

(1) The monitoring system shall measure data values at least once during approximately equal 15-minute intervals.

(2) The owner or operator shall record either each measured data value or block average values for 1 hour or shorter periods calculated from all measured data values during each period. If values are measured more frequently than once per minute, a single value for each minute may be used to calculate the hourly (or shorter period) block average instead of all measured values. The owner or operator of process vents from batch unit operations shall record each measured data value.

(3) Daily average values of each continuously monitored parameter shall be calculated for each operating day as specified in paragraphs (d)(3)(i) through (ii) of this section, except as specified in paragraphs (d)(6) and (7) of this section.

(i) The daily average value shall be calculated as the average of all parameter values recorded during the operating day, except as specified in paragraph (d)(7) of this section. The calculated average shall cover a 24-hour period if operation is continuous. If intermittent emissions episodes occur resulting in emissions being vented to a combustion, recapture, or recovery device for a period of less than 24 hours in the operating day, the daily average shall be calculated based only on the period when emissions are being vented to the combustion, recapture, or recovery device. For example, if a batch unit operation operates such that emissions are vented to a combustion device for 6 hours, then the daily average is the average of the temperature measurements taken during those 6 hours.

(ii) The operating day shall be the 24-hour period that the owner or operator specifies in the operating permit or the Notification of Compliance Status, for purposes of determining daily average values.

(4)-(5) [Reserved]

(6) If all recorded values for a monitored parameter during an operating day are above the minimum level or below the maximum level established in the Notification of Compliance Status or operating permit, the owner or operator may record that all values were above the minimum level or below the maximum level rather than calculating and recording a daily average for that operating day.

(7) Monitoring data recorded during periods identified in paragraphs (d)(7)(i) through (v) of this section shall not be included in any average computed under this subpart. Records shall be kept of the times and durations of all such periods and any other periods during process or combustion, recapture, or recapture device operation when monitors are not operating.

(i) Monitoring system breakdowns, repairs, calibration checks, and zero (low-level) and high-level adjustments;

(ii) Start-ups;

(iii) Shutdowns;

(iv) Malfunctions; or

(v) Periods of non-operation of the affected source (or portion thereof), resulting in cessation of the emissions to which the monitoring applies.

(8) For continuous monitoring systems used to comply with this subpart, records documenting the completion of calibration checks, and records documenting the maintenance of continuous monitoring systems that are specified in the manufacturer's instructions or that are specified in other
written procedures that provide adequate assurance that the equipment would reasonably be expected to monitor accurately.

(9) The owner or operator of an affected source granted a waiver of recordkeeping or reporting requirements under the General Provisions’ recordkeeping and reporting requirements in §63.10(f) shall maintain the information, if any, specified by the Administrator as a condition of the waiver of recordkeeping or reporting requirements.

(e) Reporting and notification. In addition to the reports and notifications required by 40 CFR part 63, subpart A, as specified in this subpart, the owner or operator of an affected source shall prepare and submit the reports listed in paragraphs (e)(3) through (8) of this section, as applicable. All reports required by this subpart, and the schedule for their submittal, are listed in Table 8 of this subpart.

(1) Violation of reporting requirements. Owners and operators shall not be in violation of the reporting requirements of this paragraph (e) for failing to submit information required to be included in a specified report if the owner or operator meets the requirements in paragraphs (e)(i) through (iii) of this section. Examples of circumstances where this paragraph may apply include information related to newly-added equipment or emission points, changes in the process, changes in equipment required or utilized for compliance with the requirements of this subpart, or changes in methods or equipment for monitoring, recordkeeping, or reporting.

(i) The information was not known in time for inclusion in the report specified by this subpart.

(ii) The owner or operator has been diligent in obtaining the information.

(iii) The owner or operator submits a report according to the provisions of paragraphs (e)(3)(i) through (iii) of this section.

(A) If this subpart expressly provides for supplements to the report in which the information is required, the owner or operator shall submit the information as a supplement to that report. The information shall be submitted no later than 60 days after it is obtained, unless otherwise specified in this subpart.

(B) If this subpart does not expressly provide for supplements, but the owner or operator must submit a request for revision of an operating permit pursuant to the State operating permit programs in part 70 or the Federal operating permit programs in part 71, due to circumstances to which the information pertains, the owner or operator shall submit the information with the request for revision to the operating permit.

(C) In any case not addressed by paragraph (e)(1)(iii)(A) or (B) of this section, the owner or operator shall submit the information with the first Periodic Report, as required by this subpart, which has a submission deadline at least 60 days after the information is obtained.

(2) Submittal of reports. All reports required under this subpart shall be sent to the Administrator at the applicable address listed in the General Provisions’ list of addresses of State air pollution control agencies and EPA Regional Offices, in §63.13. If acceptable to both the Administrator and the owner or operator of a source, reports may be submitted on electronic media.

(3) Initial Notification. The owner or operator of an existing or new affected source shall submit a written Initial Notification to the Administrator, containing the information described in paragraph (e)(3)(i) of this section, according to the schedule in paragraph (e)(3)(ii) of this section. The General Provisions’ Initial Notification requirements in §63.9(b)(2), (3), and (6) shall not apply, for the purposes of this subpart.

(i) The Initial Notification shall include the following information:

(A) The name and address of the owner or operator;

(B) The address (physical location) of the affected source;

(C) An identification of the kinds of emission points within the affected source;

(D) An identification of the relevant standard, or other requirement, that is the basis of the notification and the source’s compliance date; and

(E) A statement of whether or not the affected source is a major source.
(ii) The Initial Notification shall be submitted according to the schedule in paragraph (e)(3)(ii)(A), (B), or (C) of this section, as applicable.

(A) For an existing source, the Initial Notification shall be submitted no later than June 1, 2000.

(B) For a new source that has an initial start-up on or after August 30, 1999, the application for approval of construction or reconstruction required by the General Provisions in §63.5(d) shall be submitted in lieu of the Initial Notification. The application shall be submitted as soon as practical before construction or reconstruction is planned to commence (but it need not be sooner than August 30, 1999).

(C) For a new source that has an initial start-up prior to August 30, 1999, the Initial Notification shall be submitted no later than August 30, 1999. The application for approval of construction or reconstruction described in the General Provisions' requirements in §63.5(d) is not required for these sources.

(4) Precompliance Report. The owner or operator of an affected source requesting an extension for compliance; requesting approval to use alternative monitoring parameters, alternative continuous monitoring and recordkeeping, or alternative controls; requesting approval to incorporate a provision for ceasing to collect monitoring data, during a start-up, shutdown, or malfunction, into the start-up, shutdown, and malfunction plan, when that monitoring equipment would be damaged if it did not cease to collect monitoring data, as permitted under §63.1420(h)(3); or requesting approval to establish parameter monitoring levels according to the procedures contained in §63.1438(c) or (d) shall submit a Precompliance Report according to the schedule described in paragraph (e)(4)(i) of this section. The Precompliance Report shall contain the information specified in paragraphs (e)(4)(ii) through (viii) of this section, as appropriate.

(i) The Precompliance Report shall be submitted to the Administrator no later than 12 months prior to the compliance date. Unless the Administrator objects to a request submitted in the Precompliance Report within 45 days after its receipt, the request shall be deemed approved. For new affected sources, the Precompliance Report shall be submitted to the Administrator with the application for approval of construction or reconstruction required in paragraph (b)(2) of this section. Supplements to the Precompliance Report may be submitted as specified in paragraph (e)(4)(vii) of this section.

(ii) A request for an extension for compliance, as specified in §63.1422(e), may be submitted in the Precompliance Report. The request for a compliance extension shall include the data outlined in the General Provisions' compliance requirements in §63.6(i)(6)(i)(A), (B), and (D), as required in §63.1422(e)(1).

(iii) The alternative monitoring parameter information required in paragraph (f) of this section shall be submitted in the Precompliance Report if, for any emission point, the owner or operator of an affected source seeks to comply through the use of a control technique other than those for which monitoring parameters are specified in this subpart or in 40 CFR part 63, subpart G, or seeks to comply by monitoring a different parameter than those specified in this subpart or in 40 CFR part 63, subpart G.

(iv) If the affected source seeks to comply using alternative continuous monitoring and recordkeeping as specified in paragraph (g) of this section, the owner or operator shall submit a request for approval in the Precompliance Report.

(v) The owner or operator shall report the intent to use alternative controls to comply with the provisions of this subpart in the Precompliance Report. The Administrator may deem alternative controls to be equivalent to the controls required by the standard, under the procedures outlined in the General Provisions' requirements for use of an alternative nonopacity emission standard, in §63.6(g).

(vi) If the owner or operator is requesting approval to incorporate a provision for ceasing to collect monitoring data, during a start-up, shutdown, or malfunction, into the start-up, shutdown, and malfunction plan, when that
monitoring equipment would be damaged if it did not cease to collect monitoring data, the information specified in paragraphs (e)(4)(vi)(A) and (B) of this section shall be supplied in the Precompliance Report or in a supplement to the Precompliance Report. The Administrator shall evaluate the supporting documentation and shall approve the request only if, in the Administrator’s judgment, the specific monitoring equipment would be damaged by the contemporaneous start-up, shutdown, or malfunction.

(A) Documentation supporting a claim that the monitoring equipment would be damaged by the contemporaneous start-up, shutdown, or malfunction; and

(B) A request to incorporate such a provision for ceasing to collect monitoring data during a start-up, shutdown, or malfunction into the start-up, shutdown, and malfunction plan.

(vii) Supplements to the Precompliance Report may be submitted as specified in paragraph (e)(4)(vii)(A) of this section, or as specified in paragraph (e)(4)(vii)(B) of this section. Unless the Administrator objects to a request submitted in a supplement to the Precompliance Report within 45 days after its receipt, the request shall be deemed approved.

(A) Supplements to the Precompliance Report may be submitted to clarify or modify information previously submitted.

(B) Supplements to the Precompliance Report may be submitted to request approval to use alternative monitoring parameters, as specified in paragraph (e)(4)(iii) of this section; to use alternative continuous monitoring and recordkeeping, as specified in paragraph (e)(4)(iv) of this section; to use alternative controls, as specified in paragraph (e)(4)(v) of this section; or to include a provision for ceasing to collect monitoring data during a start-up, shutdown, or malfunction, in the start-up, shutdown, and malfunction plan, when that monitoring equipment would be damaged if it did not cease to collect monitoring data, as specified in paragraph (e)(4)(vi) of this section.

(viii) If an owner or operator establishes parameter monitoring levels according to the procedures contained in the parameter monitoring provisions in §63.1438(c) or (d), the following information shall be submitted in the Precompliance Report:

(A) Identification of which procedures (i.e., §63.1438(c) or (d)) are to be used; and

(B) A description of how the parameter monitoring level is to be established. If the procedures in §63.1438(c) are to be used, a description of how performance test data will be used shall be included.

(5) Notification of Compliance Status. For existing and new affected sources, a Notification of Compliance Status shall be submitted within 150 days after the compliance dates specified in §63.1422. For equipment leaks subject to §63.1434, the owner or operator shall submit the information specified in the HON equipment leak Notification of Compliance Status requirements in §63.182(c), in the Notification of Compliance Status required by this paragraph. For all other emission points, including heat exchange systems, the Notification of Compliance Status shall list the information listed in paragraphs (e)(5)(i) through (vii) of this section.

(i) The results of any emission point group determinations, process section applicability determinations, performance tests, inspections, continuous monitoring system performance evaluations, any other information required by the test method to be in the test report used to demonstrate compliance, values of monitored parameters established during performance tests, and any other information required to be included in a Notification of Compliance Status under the requirements for overlapping regulations in §63.1422(j), the HON equipment leak reporting provisions in §63.122 and the storage vessel provisions in §63.1432, and the HON process wastewater reporting provisions in §63.146. In addition, the owner or operator shall comply with paragraphs (e)(5)(i)(A) and (B) of this section.

(A) For performance tests, group determinations, or determination that controls are needed, the Notification of Compliance Status shall include one complete test report, as described in
paragraph (e)(5)(i)(B) of this section, for each test method used for a particular kind of emission point. For additional tests performed for the same kind of emission point using the same method, the results and any other information required by the test method to be in the test report shall be submitted, but a complete test report is not required.

(B) A complete test report shall include a brief process description, sampling site description, description of sampling and analysis procedures and any modifications to standard procedures, quality assurance procedures, record of operating conditions during the test, record of preparation of standards (if the owner or operator prepares the standards), record of calibrations, raw data sheets for field sampling, raw data sheets for field and laboratory analyses, documentation of calculations, and any other information required by the test method to be in the test report.

(ii) For each monitored parameter for which a maximum or minimum level is required to be established under the HON process vent monitoring requirements in §63.114(e) and the process vent monitoring requirements in §63.1429(d), the HON process wastewater parameter monitoring requirements in §63.143(f), paragraph (e)(8) of this section, or paragraph (f) of this section, the information specified in paragraphs (e)(5)(ii)(A) through (C) of this section shall be submitted. Further, as described in the storage vessel provisions in §63.1432(k), for those storage vessels for which the parameter monitoring plan (required to be submitted under the HON Notification of Compliance Status requirements for storage vessels in §63.120(d)(3)) specifies compliance with the parameter monitoring provisions of §63.1438, the owner or operator shall provide the information specified in §63.120(d)(3) as part of the Notification of Compliance Status.

(A) The required information shall include the specific maximum or minimum level of the monitored parameter(s) for each emission point.

(B) The required information shall include the rationale for the specific maximum or minimum level for each parameter for each emission point, including any data and calculations used to develop the level and a description of why the level indicates that the combustion, recovery, or recapture device is operated in a manner to ensure compliance with the provisions of this subpart.

(C) The required information shall include a definition of the affected source’s operating day, as specified in paragraph (d)(3)(ii) of this section, for purposes of determining daily average values of monitored parameters.

(iii) The determination of applicability for flexible operation units as specified in §63.1420(e)(1)(iii).

(iv) The parameter monitoring levels for flexible operation units, and the basis on which these levels were selected, or a demonstration that these levels are appropriate at all times, as specified in §63.1420(e)(7).

(v) The results for each predominant use determination made under §63.1420(f)(1) through (7), for storage vessels assigned to an affected source subject to this subpart.

(vi) If any emission point is subject to this subpart and to other standards as specified in §63.1422(j), and if the provisions of §63.1422(j) allow the owner or operator to choose which testing, monitoring, reporting, and record-keeping provisions will be followed, then the Notification of Compliance Status shall indicate which rule’s requirements will be followed for testing, monitoring, reporting, and record-keeping.

(vii) An owner or operator who transfers a Group 1 wastewater stream or residual removed from a Group 1 wastewater stream for treatment pursuant to §63.132(g) shall include in the Notification of Compliance Status the name and location of the transferee and a description of the Group 1 wastewater
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stream or residual sent to the treatment facility.

(6) Periodic Reports. For existing and new affected sources, the owner or operator shall submit Periodic Reports as specified in paragraphs (e)(6)(i) through (vii) of this section. In addition, for equipment leaks subject to §63.1434, the owner or operator shall submit the information specified in the HON periodic reporting requirements in §63.182(d), and for heat exchange systems subject to §63.1434, the owner or operator shall submit the information specified in the HON heat exchange system reporting requirements in §63.104(f)(2), as part of the Periodic Report required by this paragraph (e)(6).

(i) Except as specified in paragraphs (e)(6)(vi) through (vii) of this section, a report containing the information in paragraph (e)(6)(ii) of this section or paragraphs (e)(6)(iii) through (vii) of this section, as appropriate, shall be submitted semiannually no later than 60 days after the end of each 180-day period. The first report shall be submitted no later than 240 days after the date the Notification of Compliance Status is due and shall cover the 6-month period beginning on the date the Notification of Compliance Status is due. Subsequent reports shall cover each preceding 6-month period.

(ii) If none of the compliance exceptions in paragraphs (e)(6)(iii) through (vii) of this section occurred during the 6-month period, the Periodic Report required by paragraph (e)(6)(i) of this section shall be a statement that there were no compliance exceptions, as described in this paragraph, for the 6-month period covered by that report and that none of the activities specified in paragraphs (e)(6)(iii) through (vii) of this section occurred during the period covered by that report.

(iii) For an owner or operator of an affected source complying with the provisions of §63.1432 through 63.1433 for any emission point, Periodic Reports shall include:

(A) All information specified in the HON periodic reporting requirements in §63.122(a)(4) for storage vessels and in §63.146(c) through §63.146(f) for process wastewater.

(B) The daily average values of monitored parameters for all excursions, as defined in §63.1438(f).

(C) The periods when monitoring data were not collected shall be specified;

(D) The information in paragraphs (e)(6)(iii)(D)(1) through (3) of this section, as applicable:

(1) Notification if a process change is made such that the group status of any emission point changes from Group 2 to Group 1. The owner or operator is not required to submit a notification of a process change if that process change caused the group status of an emission point to change from Group 1 to Group 2. However, until the owner or operator notifies the Administrator that the group status of an emission point has changed from Group 1 to Group 2, the owner or operator is required to continue to comply with the Group 1 requirements for that emission point. This notification may be submitted at any time.

(2) Notification if one or more emission points (other than equipment leak components subject to §63.1434), or one or more PMPU is added to an affected source. The owner or operator shall submit the information contained in paragraphs (e)(6)(iii)(D)(2)(i) and (ii) of this section.

(i) A description of the addition to the affected source.

(ii) Notification of the group status or control requirement for the additional emission point or all emission points in the PMPU.

(3) For process wastewater streams sent for treatment pursuant to §63.132(g), reports of changes in the identity of the treatment facility or transferee.

(E) The information in paragraph (b)(1)(iii) of this section for reports of start-up, shutdown, and malfunction.

(iv) If any performance tests are reported in a Periodic Report, the following information shall be included:

(A) One complete test report shall be submitted for each test method used for a particular kind of emission point tested. A complete test report shall contain the information specified in paragraph (e)(5)(i)(B) of this section.

(B) For additional tests performed for the same kind of emission point using
(v) The results for each change made to a primary product determination for a PMPU made under § 63.1420(e)(3) or (10).

(vi) The results for each reevaluation of the applicability of this subpart to a storage vessel that begins receiving material from (or sending material to) a process unit that was not included in the initial determination, or a storage vessel that ceases to receive material from (or send material to) a process unit that was included in the initial determination, in accordance with § 63.1420(f)(18).

(vii) The Periodic Report required by the equipment leak provisions in § 63.1434(f) shall be submitted as part of the Periodic Report required by paragraph (e)(6) of this section.

(viii) The owner or operator of an affected source shall submit quarterly reports for particular emission points and process sections as specified in paragraphs (e)(6)(viii)(A) through (D) of this section.

(A) The owner or operator of an affected source shall submit quarterly reports for a period of 1 year for an emission point or process section if the emission point or process section meets the conditions in paragraph (e)(6)(viii)(A)(1) or (2) of this section.

1. A combustion, recovery, or recapture device for a particular emission point or process section has more excursions, as defined in § 63.1438(f), than the number of excused excursions allowed under § 63.1438(g) for a semiannual reporting period; or

2. The Administrator requests the owner or operator to submit quarterly reports for that emission point or process section.

(B) The quarterly reports shall include all information specified in paragraphs (e)(6)(viii)(A) through (vii) of this section, as applicable to the emission point or process section for which quarterly reporting is required under paragraph (e)(6)(viii)(A) of this section. Information applicable to other emission points within the affected source shall be submitted in the semiannual reports required under paragraph (e)(6)(i) of this section.

(C) Quarterly reports shall be submitted no later than 60 days after the end of each quarter.

(D) After quarterly reports have been submitted for an emission point for 1 year without more excursions occurring (during that year) than the number of excused excursions allowed under § 63.1438(g), the owner or operator may return to semiannual reporting for the emission point or process section.

(7) Other reports. The notifications of inspections required by the storage vessel provisions in § 63.1432 shall be submitted, as specified in the HON storage vessel provisions in § 63.122(h)(1) and (2), and in paragraphs (e)(7)(i) and (ii) of this section.

(i) When the conditions in the HON storage vessel provisions in §§ 63.1420(e)(3)(i) or 63.1420(e)(4)(i) are met, reports of changes to the primary product for a PMPU or process unit, as required by § 63.1420(e)(3)(i) or § 63.1420(g)(3), respectively, shall be submitted.

(ii) Owners or operators of PMPUs or emission points (other than equipment leak components subject to § 63.1434) that are subject to provisions for changes or additions to plant sites in § 63.1420(g)(1) or (2) shall submit a report as specified in paragraphs (e)(7)(ii)(A) and (B) of this section.

(A) Reports shall include:

1. A description of the process change or addition, as appropriate;

2. The planned start-up date and the appropriate compliance date, according to § 63.1420(g)(1) or (2); and

3. Identification of the group status of emission points (except equipment leak components subject to the requirements in § 63.1434) specified in paragraphs (e)(7)(ii)(A)(3)(i) through (iii) of this section, as applicable.

(i) All the emission points in the added PMPU, as described in § 63.1420(g)(1).

(ii) All the emission points in an affected source designated as a new affected source under § 63.1420(g)(2)(i).

(iii) All the added or created emission points as described in § 63.1420(g)(2)(ii).

(B) The owner or operator of an affected source shall submit quarterly reports for that emission point or process section.

4. If the owner or operator wishes to request approval to use alternative
monitoring parameters, alternative continuous monitoring or record-keeping, alternative controls, or wishes to establish parameter monitoring levels according to the procedures contained in §63.1438(c) or (d), a Precompliance Report shall be submitted in accordance with paragraph (e)(7)(ii)(B) of this section.

(B) Reports shall be submitted as specified in paragraphs (e)(7)(ii)(B)(1) through (3) of this section, as appropriate.

(1) Owners or operators of an added PMPU subject to §63.1420(g)(1) shall submit a report no later than 180 days prior to the compliance date for the PMPU.

(2) Owners or operators of an affected source designated as a new affected source under §63.1420(g)(2)(i) shall submit a report no later than 180 days prior to the compliance date for the affected source.

(3) Owners and operators of any emission point (other than equipment leak components subject to §63.1434) subject to §63.1420(g)(2)(ii) shall submit a report no later than 180 days prior to the compliance date for those emission points.

(8) Operating permit application. An owner or operator who submits an operating permit application instead of a Precompliance Report shall submit the information specified in paragraph (e)(4) of this section, as applicable, with the operating permit application.

(f) Alternative monitoring parameters. The owner or operator who has been directed by any section of this subpart, or any section of another subpart referenced by this subpart, that specifically references this paragraph to set unique monitoring parameters, or who requests approval to monitor a different parameter than those listed in §63.1432 for storage vessels, §63.1427 for ECO, §63.1429 for process vents, or §63.143 for process wastewater shall submit the information specified in paragraphs (f)(1) through (3) of this section in the Precompliance Report, as required by paragraph (e)(4) of this section. The owner or operator shall retain for a period of 5 years each record required by paragraphs (f)(1) through (3) of this section.

(1) The required information shall include a description of the parameter(s) to be monitored to ensure the combustion, recovery, or recapture device; control technique; or pollution prevention measure is operated in conformance with its design and achieves the specified emission limit, percent reduction, or nominal efficiency, and an explanation of the criteria used to select the parameter(s).

(2) The required information shall include a description of the methods and procedures that will be used to demonstrate that the parameter indicates proper operation, the schedule for this demonstration, and a statement that the owner or operator will establish a level for the monitored parameter as part of the Notification of Compliance Status report required in paragraph (e)(5) of this section, unless this information has already been included in the operating permit application.

(3) The required information shall include a description of the proposed monitoring, recordkeeping, and reporting system, to include the frequency and content of monitoring, recordkeeping, and reporting. Further, the rationale for the proposed monitoring, recordkeeping, and reporting system shall be included if either condition in paragraph (f)(3)(i) or (ii) of this section is met:

(i) If monitoring and recordkeeping is not continuous; or

(ii) If reports of daily average values will not be included in Periodic Reports when the monitored parameter value is above the maximum level or below the minimum level as established in the operating permit or the Notification of Compliance Status.

(g) Alternative continuous monitoring and recordkeeping. An owner or operator choosing not to implement the continuous parameter operating and recordkeeping provisions listed in §63.1429 for process vents, and §63.1433 for wastewater, may instead request approval to use alternative continuous monitoring and recordkeeping provisions according to the procedures specified in paragraphs (g)(1) through (4) of this section. Requests shall be submitted in the Precompliance Report as specified in paragraph (e)(4)(iv) of this section.
§ 63.1439  

Reduced recordkeeping program.

For any parameter with respect to any item of equipment, the owner or operator may implement the recordkeeping requirements in paragraph (h)(1) or (2) of this section as alternatives to the continuous operating parameter monitoring and recordkeeping provisions that would otherwise apply under this subpart. The owner or operator shall retain for a period of 5 years each record required by paragraph (h)(1) or (2) of this section.

(A) Measure the operating parameter value at least once during approximately equal 15-minute intervals;

(B) Record at least four values each hour during periods of operation;

(C) Record the date and time when monitors are turned off or on;

(D) Recognize unchanging data that may indicate the monitor is not functioning properly, alert the operator, and record the incident;

(E) Calculate daily average values of the monitored operating parameter based on all measured data; and

(F) If the daily average is not an excursion, as defined in §63.1438(f), the data for that operating day may be converted to hourly average values and the four or more individual records for each hour in the operating day may be discarded.

(i) The request shall contain:

(A) A description of the monitoring system and data compression recording system, including the criteria used to determine which monitored values are recorded and retained;

(B) The method for calculating daily averages; and

(C) A demonstration that the system meets all criteria in paragraph (g)(3)(i) of this section.

(3) An owner or operator may request approval to use other alternative monitoring systems according to the procedures specified in the General Provisions' requirements for using an alternative monitoring method in §63.8(f)(4).

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or operator electing to comply with the requirements of paragraph (h)(1) of this section shall notify the Administrator in the Notification of Compliance Status or, if the Notification of Compliance Status has already been submitted, in the Periodic Report immediately preceding implementation of the requirements of paragraph (h)(1) of this section.

(i) The monitoring system is capable of detecting unrealistic or impossible data during periods of operation other than start-ups, shutdowns or malfunctions (e.g., a temperature reading of –200°C on a boiler), and will alert the operator by alarm or other means. The owner or operator shall record the occurrence. All instances of the alarm or other alert in an operating day constitute a single occurrence.

(ii) The monitoring system generates, updated at least hourly throughout each operating day, a running average of the monitoring values that have been obtained during that operating day, and the capability to observe this running average is readily available to the Administrator on-site during the operating day. The owner or operator shall record the occurrence of any period meeting the criteria in paragraphs (h)(1)(ii)(A) through (C) of this section. All instances in an operating day constitute a single occurrence.

(A) The running average is above the maximum or below the minimum established limits;

(B) The running average is based on at least six 1-hour average values; and

(C) The running average reflects a period of operation other than a start-up, shutdown, or malfunction.

(iii) The monitoring system is capable of detecting unchanging data during periods of operation other than start-ups, shutdowns or malfunctions, except in circumstances where the presence of unchanging data are the expected operating condition based on past experience (e.g., pH in some scrubbers), and will alert the operator by alarm or other means. The owner or operator shall record the occurrence. All instances of the alarm or other alert in an operating day constitute a single occurrence.

(iv) The monitoring system will alert the owner or operator by an alarm or other means, if the running average parameter value calculated under paragraph (h)(1)(ii) of this section reaches a set point that is appropriately related to the established limit for the parameter that is being monitored.

(v) The owner or operator shall verify the proper functioning of the monitoring system, including its ability to comply with the requirements of paragraph (h)(1) of this section, at the times specified in paragraphs (h)(1)(v)(A) through (C) of this section. The owner or operator shall document that the required verifications occurred.

(A) Upon initial installation.

(B) Annually after initial installation.

(C) After any change to the programming or equipment constituting the monitoring system, which might reasonably be expected to alter the monitoring system's ability to comply with the requirements of this section.

(vi) The owner or operator shall retain the records identified in paragraphs (h)(1)(vi)(A) through (D) of this section.

(A) Identification of each parameter, for each item of equipment, for which the owner or operator has elected to comply with the requirements of paragraph (h) of this section.

(B) A description of the applicable monitoring system(s), and how compliance will be achieved with each requirement of paragraphs (h)(1)(i) through (v) of this section. The description shall identify the location and format (e.g., on-line storage, log entries) for each required record. If the description changes, the owner or operator shall retain both the current and the most recent superseded description, as specified in paragraph (h)(1)(vi)(D) of this section.

(C) A description, and the date, of any change to the monitoring system condition that would reasonably be expected to affect its ability to comply with the requirements of paragraph (h)(1) of this section.

(D) The owner or operator subject to paragraph (h)(1)(vi)(B) of this section shall retain the current description of the monitoring system as long as the
description is current. The current description shall, at all times, be retained on-site or be accessible from a central location by computer or other means that provides access within 2 hours after a request. The owner or operator shall retain all superseded descriptions for at least 5 years after the date of their creation. Superseded descriptions shall be retained on-site (or accessible from a central location by computer or other means that provides access within 2 hours after a request) for at least 6 months after their creation. Thereafter, superseded descriptions may be stored off-site.

(2) If an owner or operator has elected to implement the requirements of paragraph (h)(1) of this section for a monitored parameter with respect to an item of equipment and a period of 6 consecutive months has passed without an excursion as defined in paragraph (h)(2)(iv) of this section, the owner or operator is no longer required to record the daily average value, for any operating day when the daily average is less than the maximum, or greater than the minimum established limit. With approval by the Administrator, monitoring data generated prior to the compliance date of this subpart shall be credited toward the period of 6 consecutive months, if the parameter limit and the monitoring accomplished during the period prior to the compliance date was required and/or approved by the Administrator.

(i) If the owner or operator elects not to retain the daily average values, the owner or operator shall notify the Administrator in the next Periodic Report. The notification shall identify the parameter and unit of equipment.

(ii) If, on any operating day after the owner or operator has ceased recording daily average values as provided in paragraph (h)(2) of this section, there is an excursion as defined in paragraph (h)(2)(iv) of this section, the owner or operator shall immediately resume retaining the daily average value for each operating day and shall notify the Administrator in the next Periodic Report. The owner or operator shall continue to retain each daily average value until another period of 6 consecutive months has passed without an excursion as defined in paragraph (h)(2)(iv) of this section.

(iii) The owner or operator shall retain the records specified in paragraph (h)(1) of this section, for the duration specified in paragraph (h) of this section. For any calendar week, if compliance with paragraphs (h)(1)(i) through (iv) of this section does not result in retention of a record of at least one occurrence or measured parameter value, the owner or operator shall record and retain at least one parameter value during a period of operation other than a start-up, shutdown, or malfunction.

(iv) For the purposes of paragraph (h) of this section, an excursion means that the daily average of monitoring data for a parameter is greater than the maximum, or less than the minimum established value, except as provided in paragraphs (h)(2)(iv)(A) and (B) of this section.

(A) The daily average value during any start-up, shutdown, or malfunction shall not be considered an excursion for purposes of paragraph (h)(2) of this section, if the owner or operator follows the applicable provisions of the start-up, shutdown, and malfunction plan required by the General Provisions in §63.6(e)(3).

(B) An excused excursion, as described in §63.1438(g), shall not be considered an excursion for the purposes of paragraph (h)(2) of this section.

Table 1 to Subpart PPP of Part 63—Applicability of General Provisions To Subpart PPP Affected Sources

<table>
<thead>
<tr>
<th>Reference</th>
<th>Applies to subpart PPP</th>
<th>Explanation</th>
</tr>
</thead>
<tbody>
<tr>
<td>63.1(a)(1)</td>
<td>Yes</td>
<td>§63.1423 specifies definitions in addition to or that apply instead of definitions in §63.2.</td>
</tr>
<tr>
<td>63.1(a)(2)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.1(a)(3)</td>
<td>Yes</td>
<td>§63.1422(f) through (k) of this subpart and §63.160(b) identify those standards which overlap with the requirements of subparts PPP and H and specify how compliance shall be achieved.</td>
</tr>
<tr>
<td>63.1(a)(4)</td>
<td>Yes</td>
<td>Subpart PPP (this table) specifies the applicability of each paragraph in subpart A to subpart PPP.</td>
</tr>
</tbody>
</table>
### TABLE 1 TO SUBPART PPP OF PART 63.—APPLICABILITY OF GENERAL PROVISIONS TO SUBPART PPP AFFECTED SOURCES—Continued

<table>
<thead>
<tr>
<th>Reference</th>
<th>Applies to subpart PPP</th>
<th>Explanation</th>
</tr>
</thead>
<tbody>
<tr>
<td>63.1(a)(5)</td>
<td>No</td>
<td>Reserved.</td>
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<tr>
<td>63.1(a)(6)–(8)</td>
<td>Yes</td>
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<tr>
<td>63.1(a)(9)</td>
<td>No</td>
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<td>63.1(a)(10)</td>
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<td>63.1(a)(11)</td>
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<td>63.1(a)(12)–(14)</td>
<td>Yes</td>
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<tr>
<td>63.1(b)(1)</td>
<td>No</td>
<td>§ 63.1420(a) contains specific applicability criteria.</td>
</tr>
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<td>63.1(b)(2)</td>
<td>Yes</td>
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<tr>
<td>63.1(b)(3)</td>
<td>Yes</td>
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<td>63.1(c)(1)</td>
<td>Yes</td>
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<tr>
<td>63.1(c)(2)</td>
<td>No</td>
<td>Subpart PPP (this table) specifies the applicability of each paragraph in subpart A to subpart PPP.</td>
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<td>63.1(c)(3)</td>
<td>No</td>
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<td>63.1(c)(4)</td>
<td>Yes</td>
<td>Except that affected sources are not required to submit notifications overridden by this table.</td>
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<td>63.1(d)(1)(i)</td>
<td>Yes</td>
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<tr>
<td>63.1(d)(1)(ii)</td>
<td>No</td>
<td>§ 63.1423 specifies those subpart A definitions that apply to subpart PPP.</td>
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<tr>
<td>63.1(d)(1)(iii)</td>
<td>No</td>
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<td>63.1(b)(1)</td>
<td>Yes</td>
<td>§ 63.1420 contains specific applicability criteria.</td>
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<td>63.1(b)(2)</td>
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<td>63.1(b)(3)</td>
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<td>63.1(b)(4)</td>
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<td>63.5(b)(2)</td>
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<td>Except § 63.1420(g) defines when construction or reconstruction is subject to new source standards.</td>
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<td>63.5(b)(3)</td>
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<td>63.5(b)(4)</td>
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<td>Except § 63.1420(g) defines when construction or reconstruction is subject to new source standards.</td>
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<td>63.5(b)(6)</td>
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<td>63.5(c)</td>
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<td>63.5(d)(1)(i)</td>
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<td>63.5(d)(1)(ii)</td>
<td>No</td>
<td>Except that § 63.5(d)(1)(ii) does not apply.</td>
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<tr>
<td>63.5(d)(1)(iii)</td>
<td>No</td>
<td>§ 63.1439(e)(5) and § 63.1434(e) specify Notification of Compliance Status requirements.</td>
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<td>63.5(d)(2)</td>
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<td>63.5(d)(3)</td>
<td>Yes</td>
<td>Except § 63.5(d)(3)(ii) does not apply, and equipment leaks subject to § 63.1434 are exempt.</td>
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<td>63.6(b)(6)</td>
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<td>§ 63.1422 specifies the compliance date.</td>
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<td>63.6(b)(7)</td>
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<td>63.6(c)(1)</td>
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<td>63.6(c)(3)</td>
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<td>63.6(e)(1)(i)</td>
<td>No</td>
<td>Except as otherwise specified for individual paragraphs (below), and § 63.6(e) does not apply to Group 2 emission points.†</td>
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<td>63.6(e)(1)(ii)</td>
<td>Yes</td>
<td>This is addressed by § 63.1420(h)(4).</td>
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<tr>
<td>Reference</td>
<td>Applies to subpart PPP</td>
<td>Explanation</td>
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<td>63.6(e)(2)</td>
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<tr>
<td>63.6(e)(3)(i)</td>
<td>Yes</td>
<td>For equipment leaks (subject to §63.1434), the start-up, shutdown, and malfunction plan requirement of §63.6(e)(3)(i) is limited to combustion, recovery, or recapture devices and is optional for other equipment. The start-up, shutdown, and malfunction plan may include written procedures that identify conditions that justify a delay of repair.</td>
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<tr>
<td>63.6(e)(3)(ii)</td>
<td>Yes</td>
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<td>63.6(e)(3)(iii)</td>
<td>Yes</td>
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<tr>
<td>63.6(e)(3)(iv)</td>
<td>No</td>
<td>This is also addressed by §63.1420(h)(4).</td>
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<tr>
<td>63.6(e)(3)(v)</td>
<td>Yes</td>
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<tr>
<td>63.6(e)(3)(vi)</td>
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<tr>
<td>63.6(e)(3)(vii)</td>
<td>Yes</td>
<td>Except the plan shall provide for operation in compliance with §63.1420((i)(4)).</td>
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<tr>
<td>63.6(e)(3)(viii)</td>
<td>Yes</td>
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<td>63.6(e)(4)(i)</td>
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<td>63.6(e)(4)(ii)</td>
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<tr>
<td>63.6(h)</td>
<td>No</td>
<td>Subpart PPP does not require opacity and visible emission standards.</td>
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<tr>
<td>63.6(i)</td>
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<td>63.6(i)(1)</td>
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<tr>
<td>63.6(i)(4)(i)</td>
<td>Yes</td>
<td>Dates are specified in §63.1422(e) and §63.1439(e)(4)(i) for all emission points except equipment leaks, which are covered under §63.1820(a)(6)(i).</td>
</tr>
<tr>
<td>63.6(i)(4)(ii)</td>
<td>No</td>
<td>Reserved.</td>
</tr>
<tr>
<td>63.6(i)(5)(1)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.6(i)(5)(2)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.6(i)(6)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.6(i)(7)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.7(a)(1)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.7(a)(2)</td>
<td>No</td>
<td>§63.1439(e)(5) and §63.1439(e)(6) specify the submittal dates of performance test results for all emission points except equipment leaks; for equipment leaks, compliance demonstration results are reported in the Periodic Reports.</td>
</tr>
<tr>
<td>63.7(a)(3)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.7(b)</td>
<td>No</td>
<td>§63.1437(a)(4) specifies notification requirements.</td>
</tr>
<tr>
<td>63.7(c)</td>
<td>No</td>
<td>Except if the owner or operator chooses to submit an alternative non-opacity emission standard for approval under §63.6(g).</td>
</tr>
<tr>
<td>63.7(d)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.7(e)(1)</td>
<td>Yes</td>
<td>Except that all performance tests shall be conducted during worst case operating conditions.</td>
</tr>
<tr>
<td>63.7(e)(2)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.7(e)(3)</td>
<td>No</td>
<td>Subpart PPP specifies requirements.</td>
</tr>
<tr>
<td>63.7(e)(4)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.7(f)</td>
<td>Yes</td>
<td>Since a site specific test plan is not required, the notification deadline in §63.7(f)(2)(i) shall be 60 days prior to the performance test, and in §63.7(f)(3) approval or disapproval of the alternative test method shall not be tied to the site specific test plan.</td>
</tr>
<tr>
<td>63.7(g)</td>
<td>Yes</td>
<td>Except that references to the Notification of Compliance Status report in §63.8(h) are replaced with the requirements in §63.1439(e)(5). In addition, equipment leaks subject to §63.1434 are not required to conduct performance tests.</td>
</tr>
<tr>
<td>63.7(h)</td>
<td>Yes</td>
<td>Except §63.7(h)(4)(ii) is not applicable, since the site-specific test plans in §63.7(c)(2) are not required.</td>
</tr>
<tr>
<td>63.8(a)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(a)(1)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(a)(2)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.8(a)(3)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.8(a)(4)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(b)(1)</td>
<td>Yes</td>
<td></td>
</tr>
</tbody>
</table>
### Table 1 to Subpart PPP of Part 63—Applicability of General Provisions to Subpart PPP Affected Sources—Continued

<table>
<thead>
<tr>
<th>Reference</th>
<th>Applies to subpart PPP</th>
<th>Explanation</th>
</tr>
</thead>
<tbody>
<tr>
<td>63.8(b)(2)</td>
<td>No</td>
<td>Support PPP specifies locations to conduct monitoring.</td>
</tr>
<tr>
<td>63.8(b)(3)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(c)(1)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(c)(1)(i)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(c)(1)(ii)</td>
<td>No</td>
<td>For all emission points except equipment leaks, comply with §63.1439(b)(1)(i)(B); for equipment leaks, comply with §63.1439(b)(2)(ii).</td>
</tr>
<tr>
<td>63.8(c)(1)(iii)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(c)(2)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(c)(3)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(c)(4)</td>
<td>No</td>
<td>§63.1438 specifies monitoring requirements; not applicable to equipment leaks, because §63.1434 does not require continuous monitoring systems.</td>
</tr>
<tr>
<td>63.8(c)(5)–(8)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.8(d)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.8(e)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.8(f)(1)–(3)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(f)(4)(i)</td>
<td>Yes</td>
<td>Except the timeframe for submitting request is specified in §63.1439(f) or (g); not applicable to equipment leaks, because §63.1434 (through subpart H) specifies acceptable alternative methods.</td>
</tr>
<tr>
<td>63.8(f)(4)(ii)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(f)(4)(iii)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(f)(5)(i)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(f)(5)(ii)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.8(f)(5)(iii)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.8(g)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.9(a)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.9(b)</td>
<td>No</td>
<td>The Initial Notification requirements are specified in §63.1439(e)(3).</td>
</tr>
<tr>
<td>63.9(c)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.9(d)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.9(e)</td>
<td>No</td>
<td>§63.1437(a)(4) specifies notification deadline.</td>
</tr>
<tr>
<td>63.9(f)</td>
<td>No</td>
<td>Subpart PPP does not require opacity and visible emission standards.</td>
</tr>
<tr>
<td>63.9(g)</td>
<td>No</td>
<td>§63.1439(e)(5) specifies Notification of Compliance Status requirements.</td>
</tr>
<tr>
<td>63.9(h)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.9(i)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.9(j)</td>
<td>No</td>
<td>§63.1439(a) specifies record retention requirements.</td>
</tr>
<tr>
<td>63.10(a)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.10(b)(1)</td>
<td>No</td>
<td>Subpart PPP specifies recordkeeping requirements.</td>
</tr>
<tr>
<td>63.10(b)(2)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.10(b)(3)</td>
<td>Yes</td>
<td>§63.1439 specifies recordkeeping requirements.</td>
</tr>
<tr>
<td>63.10(c)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.10(d)(1)</td>
<td>Yes</td>
<td>§63.1439(e)(5) and §63.1439(e)(6) specify performance test reporting requirements; not applicable to equipment leaks.</td>
</tr>
<tr>
<td>63.10(d)(2)</td>
<td>No</td>
<td>Subpart PPP does not require opacity and visible emission standards.</td>
</tr>
<tr>
<td>63.10(d)(3)</td>
<td>No</td>
<td></td>
</tr>
<tr>
<td>63.10(d)(4)</td>
<td>Yes</td>
<td>Except that reports required by §63.10(d)(5)(ii) shall be submitted at the same time as Periodic Reports specified in §63.1439(e)(6). The start-up, shutdown, and malfunction plan, and any records or reports of start-up, shutdown, and malfunction do not apply to Group 2 emission points.</td>
</tr>
<tr>
<td>63.10(d)(5)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.10(e)</td>
<td>No</td>
<td>§63.1439 specifies reporting requirements.</td>
</tr>
<tr>
<td>63.10(f)</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.11</td>
<td>Yes</td>
<td></td>
</tr>
<tr>
<td>63.12</td>
<td>Yes</td>
<td>Except that the authority of §63.177 (for equipment leaks) will not be delegated to States.</td>
</tr>
<tr>
<td>63.13–63.15</td>
<td>Yes</td>
<td></td>
</tr>
</tbody>
</table>

*The plan, and any records or reports of start-up, shutdown, and malfunction do not apply to Group 2 emission points.*
### Table 2: Applicability of Subparts F, G, H, and U to Subpart PPP Affected Sources

<table>
<thead>
<tr>
<th>Reference</th>
<th>Applies to subpart PPP</th>
<th>Explanation</th>
<th>Applicable section of subpart PPP</th>
</tr>
</thead>
<tbody>
<tr>
<td>Subpart F:</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

| 63.100    | No.                    | Several definitions from 63.101 are referenced at 63.1423. | 63.1423. |
| 63.101    | Yes .......................... |                                                                       |         |
| 63.102-63.103 | No.                  | With the differences noted in 63.1435(b) through (d).            | 63.1435. |
| 63.104    | Yes .......................... |                                                                       |         |
| 63.105    | Yes .......................... | With the differences noted in 63.1433(b)                        | 63.1433. |
| 63.106    | No.                    |                                                                       |         |

| Subpart G: |                        |             |                                   |

| 63.110    | No.                    | Several definitions from 63.111 are incorporated by reference into 63.1423. | 63.1423. |
| 63.111    | Yes .......................... |                                                                       |         |
| 63.112    | No.                    | For THF facilities, with the differences noted in 63.1435(f)(1) through (f)(10). | 63.1425. |
| 63.113-63.118 | No.                  | For epoxy facilities, except that 63.115(d) is used for TRE determinations. | 63.1428. |
| 63.119-63.123 | Yes .......................... | With the differences noted in 63.1432(b) through 63.1432(p). | 63.1432. |

| Subpart H: |                        |             |                                   |

| 63.124-63.125 | No.                  | Reserved. | 63.1425. |
| 63.126-63.130 | No.                  | Reserved. | 63.1425. |
| 63.131    | No.                    | With the differences noted in 63.1433(a)(1) through 63.1433(a)(19). | 63.1433. |
| 63.132-63.147 | Yes .......................... |                                                                       |         |
| 63.148-63.149 | Yes .......................... | With the differences noted in 63.1432(b) through 63.1432(p) and 63.1433(a)(1) through 63.1433(a)(19). | 63.1432 and 63.1433. |

| Subpart U: |                        |             |                                   |

| 63.160-63.182 | Yes .......................... | Subpart PPP affected sources shall comply with all requirements of subpart H, with the differences noted in 63.1422(d), 63.1422(h), and 63.1434(b) through (g). | 63.1434. |

| 63.480-63.487 | No.                    | Portions of 63.480(b) and (e) are cross-referenced in subpart PPP. |         |
| 63.488    | Yes .......................... |                                                                       |         |
| 63.489-63.506 | No.                    |                                                                       |         |

### Table 3: Group 1 Storage Vessels at Existing and New Affected Sources

<table>
<thead>
<tr>
<th>Vessel capacity (cubic meters)</th>
<th>Vapour Pressure ≥ (kilopascals)</th>
</tr>
</thead>
<tbody>
<tr>
<td>75 &lt; capacity &lt; 151</td>
<td>≥ 13.1</td>
</tr>
<tr>
<td>capacity ≥ 151</td>
<td>≥ 5.2</td>
</tr>
</tbody>
</table>

*Maximum true vapor pressure of total organic HAP at storage temperature.

### Table 4: Known Organic HAP from Polyether Polyol Products

<table>
<thead>
<tr>
<th>Organic HAP/Chemical Name (CAS No.)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1,3 Butadiene (106990)</td>
</tr>
<tr>
<td>Ethylene Oxide (75569)</td>
</tr>
<tr>
<td>n-Hexane (110543)</td>
</tr>
<tr>
<td>Methanol (67561)</td>
</tr>
<tr>
<td>Propylene Oxide (75569)</td>
</tr>
<tr>
<td>Toluene (108883)</td>
</tr>
</tbody>
</table>

CAS No. = Chemical Abstracts Service Registry Number
### Environmental Protection Agency

**Pl. 63, Subpt. PPP, Table 5**

**TABLE 5 TO SUBPART PPP OF PART 63.—PROCESS VENTS FROM BATCH UNIT OPERATIONS—MONITORING, RECORDKEEPING, AND REPORTING REQUIREMENTS**

<table>
<thead>
<tr>
<th>Control technique</th>
<th>Parameter to be monitored</th>
<th>Recordkeeping and reporting requirements for monitored parameters</th>
</tr>
</thead>
</table>
| Thermal Incinerator | Firebox temperature | 1. Continuous records as specified in §63.1429.  
2. Record and report the average firebox temperature measured during the performance test—NCS.  
3. Record the daily average firebox temperature measured during the performance test—NCS.  
4. Report all daily average temperatures that are below the minimum operating temperature established in the NCS or operating permit and all instances when monitoring data are not collected—PR.  
| | | 6. Report all instances when monitoring data are not collected. |
| Catalytic Incinerator | Temperature upstream and downstream of the catalyst bed. | 1. Continuous records as specified in §63.1429.  
2. Record and report the average upstream and downstream temperatures and the average temperature difference across the catalyst bed measured during the performance test—NCS.  
3. Record the daily average upstream temperature and temperature difference across catalyst bed as specified in §63.1429.  
4. Report all daily average temperature differences across the catalyst bed that are below the minimum difference established in the NCS or operating permit—PR.  
5. Report all daily average upstream temperature that are below the minimum temperature established in the NCS or operating permit—PR.  
6. Report all instances when monitoring data are not collected. |
| Boiler or Process Heater with a design heat input capacity less than 44 megawatts and where the process vents are not introduced with or used as the primary fuel. | Firebox temperature | 1. Continuous records as specified in §63.1429.  
2. Record and report the average firebox temperature measured during the performance test—NCS.  
3. Record the daily average firebox temperature as specified in §63.1429.  
4. Report all daily average temperatures that are below the minimum operating temperature established in the NCS or operating permit and all instances when monitoring data are not collected—PR.  
| | | 6. Report all instances when monitoring data are not collected. |
| Flare | Presence of a flame at the pilot light. | 1. Hourly records of whether the monitor was continuously operating during batch emission episodes selected for control and whether a flame was continuously present at the pilot light during each hour.  
2. Record and report the presence of a flame at the pilot light over the full period of the compliance determination—NCS.  
3. Record the times and durations of all periods during batch emission episodes when all flames at the pilot light of a flare are absent or the monitor is not operating.  
4. Report the times and durations of all periods during batch emission episodes selected for control when all flames at the pilot light of a flare are absent—Pr.  
| | | 6. Report all instances when monitoring data are not collected. |
| Absorber | Liquid flow rate into or out of the scrubber, or the pressure drop across the scrubber. | 1. Records every 15 minutes, as specified in §63.1429.  
2. Record and report the average liquid flow rate into or out of the scrubber, or the pressure drop across the scrubber, every 15 minutes, as specified in §63.1429.  
3. Record the liquid flow rate into or out of the scrubber, or the pressure drop across the scrubber, measured during the performance test—NCS.  
4. Report all scrubber flow rates or pressure drop values that are below the minimum operating value established in the NCS or operating permit and all instances when monitoring data are not collected—PR.  
| | | 6. Report all instances when monitoring data are not collected. |
| | pH of the scrubber | 1. Once daily records as specified in §63.1429.  
2. Record and report the average pH of the scrubber effluent measured during the performance test—NCS.  
3. Record at least once daily the pH of the scrubber effluent. |
### Table 5 to Subpart PPP of Part 63.—Process Vents From Batch Unit Operations—Monitoring, Recordkeeping, and Reporting Requirements—Continued

<table>
<thead>
<tr>
<th>Control technique</th>
<th>Parameter to be monitored</th>
<th>Recordkeeping and reporting requirements for monitored parameters</th>
</tr>
</thead>
</table>
| **Condenser**     | Exit (product side) temperature | 1. Continuous records as specified in §63.1429.  
2. Record and report the average exit temperature measured during the performance test—NCS.  
3. Record the daily average exit temperature as specified in §63.1429.  
4. Report all daily average exit temperatures that are above the maximum operating temperature established in the NCS or operating permit and all instances when monitoring data are not collected—PR.  
5. Condenser (as an alternative to the above).  
| **Carbon Adsorber** | Total regeneration stream mass or volumetric flow during carbon bed regeneration cycle(s), and.  
Temperature of the carbon bed after regeneration and within 15 minutes of completing any cooling cycle(s). | 1. Record of total regeneration stream mass or volumetric flow for each carbon bed regeneration cycle.  
2. Record and report the total regeneration stream mass or volumetric flow during each carbon bed regeneration cycle during the performance test—NCS.  
3. Report all carbon bed regeneration cycles when the total regeneration stream mass or volumetric flow is above the maximum flow rate established in the NCS or operating permit—PR.  
4. Carbon Adsorber (as an alternative to the above).  
| **Absorber, Condenser, and Carbon Adsorber** | Concentration level or reading indicated by an organic monitoring device at the outlet of the recovery device. | 1. Continuous records as specified in §63.1429.  
2. Record and report the average concentration level or reading measured during the performance test—NCS.  
3. Record the daily average concentration level or reading as specified in §63.1429.  
4. Report all daily average concentration levels or readings that are above the maximum concentration or reading established in the NCS or operating permit and all instances when monitoring data are not collected—PR.  
5. All Combustion, recovery, or recapture devices.  
| **Diversion to the atmosphere** | Diversion to the atmosphere from the combustion, recovery, or recapture device or.  
Monthly inspections of sealed valves. | 1. Hourly records of whether the flow indicator was operating during batch emission episodes selected for control and whether a diversion was detected at any time during the hour, as specified in §63.1429.  
2. Record and report the times of all periods during batch emission episodes selected for control when emissions are diverted through a bypass line, or the flow indicator is not operating—PR.  
4. All Combustion, recovery, or recapture devices.  
| **Diversion to the atmosphere** | Diversion to the atmosphere from the combustion, recovery, or recapture device or.  
Monthly inspections of sealed valves. | 1. Records that monthly inspections were performed as specified in §63.1429.  
2. Record and report all monthly inspections that show that valves are in the diverting position or that a seal has been broken—PR.  
3. All Combustion, recovery, or recapture devices.  

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4. Report all pH scrubber effluent readings out of the range established in the NCS or operating permit and all instances when monitoring data are not collected—PR. If a base absorbent is used, report all pH values that are below the minimum operating values. If an acid absorbent is used, report all pH values that are above the maximum operating values.
### TABLE 5 TO SUBPART PPP OF PART 63.—PROCESS VENTS FROM BATCH UNIT OPERATIONS—MONITORING, RECORDKEEPING, AND REPORTING REQUIREMENTS—Continued

<table>
<thead>
<tr>
<th>Control technique</th>
<th>Parameter to be monitored</th>
<th>Recordkeeping and reporting requirements for monitored parameters</th>
</tr>
</thead>
<tbody>
<tr>
<td>ECO</td>
<td>Time from the end of the epoxide feed, or the epoxide partial pressure in the reactor or direct measurement of epoxide concentration in the reactor liquid at the end of the ECO.</td>
<td>1. Records at the end of each batch, as specified in §63.1427(i). 2. Record and report the average parameter value of the parameters chosen, measured during the performance test. 3. Record the batch cycle ECO duration, epoxide partial pressure, or epoxide concentration in the liquid at the end of the ECO. 4. Report all batch cycle parameter values outside of the ranges established in accordance with §63.1427(i)(3) and all instances when monitoring data were not collected—PR.</td>
</tr>
</tbody>
</table>

- Monitor may be installed in the firebox or in the ductwork immediately downstream of the firebox before any substantial heat exchange is encountered.
- Continuous records is defined in §63.111.
- NCS = Notification of Compliance Status described in §63.1429.
- PR = Periodic Reports described in §63.1429.
- The periodic reports shall include the duration of periods when monitoring data are not collected as specified in §63.1439.
- Alternatively, these devices may comply with the organic monitoring device provisions listed at the end of this table.

### TABLE 6 TO SUBPART PPP OF PART 63.—PROCESS VENTS FROM CONTINUOUS UNIT OPERATIONS—MONITORING, RECORDKEEPING, AND REPORTING REQUIREMENTS

<table>
<thead>
<tr>
<th>Control technique</th>
<th>Parameter to be monitored</th>
<th>Recordkeeping and reporting requirements for monitored parameters</th>
</tr>
</thead>
<tbody>
<tr>
<td>Thermal Incinerator</td>
<td>Firebox temperature</td>
<td>1. Continuous records as specified in §63.1429. 2. Record and report the average firebox temperature measured during the performance test—NCS. 3. Record the daily average firebox temperature for each operating day. 4. Report all daily average temperatures that are below the minimum operating temperature established in the NCS or operating permit and all instances when sufficient monitoring data are not collected—PR.</td>
</tr>
<tr>
<td>Catalytic Incinerator</td>
<td>Temperature upstream and downstream of the catalyst bed.</td>
<td>1. Continuous records as specified in §63.1429. 2. Record and report the average upstream and downstream temperatures and the average temperature difference across the catalyst bed measured during the performance test—NCS. 3. Record the daily average upstream temperature and temperature difference across catalyst bed for each operating day. 4. Report all daily average upstream temperatures that are below the minimum upstream temperature established in the NCS or operating permit—PR. 5. Report all daily average temperature differences across the catalyst bed that are below the minimum difference established in the NCS or operating permit—PR. 6. Report all operating days when insufficient monitoring data are collected.</td>
</tr>
<tr>
<td>Boiler or Process Heater with a design heat input capacity less than 44 megawatts and where the process vents are not introduced with or used as the primary fuel.</td>
<td>Firebox temperature</td>
<td>1. Continuous records as specified in §63.1429. 2. Record and report the average firebox temperature measured during the performance test—NCS. 3. Record the daily average firebox temperature for each operating day. 4. Report all daily average temperatures that are below the minimum operating temperature established in the NCS or operating permit and all instances when insufficient monitoring data are collected—PR.</td>
</tr>
<tr>
<td>Flare</td>
<td>Presence of a flame at the pilot light.</td>
<td>1. Hourly records of whether the monitor was continuously operating and whether a flame was continuously present at the pilot light during each hour. 2. Record and report the presence of a flame at the pilot light over the full period of the compliance determination—NCS. 3. Record the times and durations of all periods when all flames at the pilot light of a flare are absent or the monitor is not operating.</td>
</tr>
<tr>
<td>Control technique</td>
<td>Parameter to be monitored</td>
<td>Recordkeeping and reporting requirements for monitored parameters</td>
</tr>
<tr>
<td>------------------</td>
<td>---------------------------</td>
<td>---------------------------------------------------------------</td>
</tr>
</tbody>
</table>
| Absorber         | Exit temperature of the absorbing liquid, and. | 4. Report the times and durations of all periods when all flames at the pilot light of a flare are absent—PR. 
1. Continuous records as specified in §63.1429. 
2. Record and report the exit temperature of the absorbing liquid averaged over the full period of the TRE determination—NCS. 
3. Record the daily average exit temperature of the absorbing liquid for each operating day. 
4. Report all the daily average exit temperatures of the absorbing liquid that are below the minimum operating value established in the NCS or operating permit—PR. |
|                  | Exit specific gravity for the absorbing liquid. | 1. Continuous records as specified in §63.1429. 
2. Record and report the exit specific gravity averaged over the full period of the TRE determination—NCS. 
3. Record the daily average exit specific gravity for each operating day. 
4. Report all daily average exit specific gravity values that are below the minimum operating value established in the NCS or operating permit—PR. |
| Condenser        | Exit (product side) temperature | 1. Continuous records as specified in §63.1429. 
2. Record and report the exit temperature averaged over the full period of the TRE determination—NCS. 
3. Record the daily average exit temperature for each operating day. 
4. Report all daily average exit temperatures that are above the maximum operating temperature established in the NCS or operating permit—PR. |
| Carbon Adsorber  | Total regeneration stream mass or volumetric flow during carbon bed regeneration cycle(s), and. | 1. Record of total regeneration stream mass or volumetric flow for each carbon bed regeneration cycle. 
2. Record and report the total regeneration stream mass or volumetric flow during each carbon bed regeneration cycle during the period of the TRE determination—NCS. 
3. Report all carbon bed regeneration cycles when the total regeneration stream mass or volumetric flow is above the maximum flow rate established in the NCS or operating permit—PR. |
|                  | Temperature of the carbon bed after regeneration and within 15 minutes of completing any cooling cycle(s). | 1. Record the temperature of the carbon bed after each regeneration and within 15 minutes of completing any cooling cycle(s). 
2. Record and report the temperature of the carbon bed after each regeneration during the period of the TRE determination—NCS. 
3. Report all carbon bed regeneration cycles when the temperature of the carbon bed after regeneration is above the maximum temperature established in the NCS or operating permit—PR. |
| Absorber, Condenser, and Carbon Adsorber (as an alternative to the above). | Concentration level or reading indicated by an organic monitoring device at the outlet of the recovery device. | 1. Continuous records as specified in §63.1429. 
2. Record and report the concentration level or reading averaged over the full period of the TRE determination—NCS. 
3. Record the daily average concentration level or reading for each operating day. 
4. Report all daily average concentration levels or readings that are above the maximum concentration or reading established in the NCS or operating permit—PR. |
| All Combustion, recovery, or recapture devices. | Diversion to the atmosphere from the combustion, recovery, or recapture device or. | 1. Hourly records of whether the flow indicator was operating and whether a diversion was detected at any time during each hour. 
2. Record and report the times of all periods when the vent stream is diverted through a bypass line, or the flow indicator is not operating—PR. 
3. Records that monthly inspections were performed as specified in §63.1429. 
4. Report and record all monthly inspections that show that valves are in the diverting position or that a seal has been broken—PR. |

*Monitor may be installed in the firebox or in the ductwork immediately downstream of the firebox before any substantial heat exchange is encountered.

**Continuous records** is defined in §63.111.

NCS = Notification of Compliance Status described in §63.1429.

PR = Periodic Reports described in §63.1429.
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The periodic reports shall include the duration of periods when monitoring data are not collected as specified in §63.1439.

Alternatively, these devices may comply with the organic monitoring device provisions listed at the end of this table.

**TABLE 7 TO SUBPART PPP OF PART 63—OPERATING PARAMETERS FOR WHICH MONITORING LEVELS ARE REQUIRED TO BE ESTABLISHED FOR PROCESS VENTS STREAMS**

<table>
<thead>
<tr>
<th>Control technique</th>
<th>Parameters to be monitored</th>
<th>Established operating parameter(s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Thermal incinerator</td>
<td>Firebox temperature</td>
<td>Minimum temperature.</td>
</tr>
<tr>
<td>Catalytic incinerator</td>
<td>Temperature upstream and downstream of the catalyst bed.</td>
<td>Minimum temperature; and minimum temperature difference across the catalyst bed.</td>
</tr>
<tr>
<td>Boiler or process heater</td>
<td>Firebox temperature</td>
<td>Minimum temperature.</td>
</tr>
<tr>
<td>Absorber</td>
<td>Liquid flow rate or pressure drop; and pH of scrubber effluent, if an acid or base absorbent is used.</td>
<td>Maximum flow rate or pressure drop; and maximum pH if an acid absorbent is used, or minimum pH if a base absorbent is used.</td>
</tr>
<tr>
<td>Condenser</td>
<td>Exit temperature</td>
<td>Maximum temperature.</td>
</tr>
<tr>
<td>Carbon adsorber</td>
<td>Total regeneration stream mass or volumetric flow during carbon bed regeneration cycle, and temperature of the carbon bed after regeneration (and within 15 minutes of completing any cooling cycle(s)).</td>
<td>Maximum mass or volumetric flow; and maximum temperature.</td>
</tr>
<tr>
<td>Extended Cookout (ECO)</td>
<td>Time from the end of the epoxide feed to the end of the ECO, or the reactor epoxide partial pressure at the end of the ECO, or the epoxide concentration in the reactor liquid at the end of the ECO.</td>
<td>Minimum duration, or maximum partial pressure at the end of ECO, or maximum epoxide concentration in the reactor liquid at the end of the ECO.</td>
</tr>
<tr>
<td>Other devices (or as an alternate to the above).</td>
<td>HAP concentration level or reading at outlet of device.</td>
<td>Maximum HAP concentration or reading.</td>
</tr>
</tbody>
</table>

**Concentration is measured instead of an operating parameter.**

**TABLE 8 TO SUBPART PPP OF PART 63—ROUTINE REPORTS REQUIRED BY THIS SUBPART**

<table>
<thead>
<tr>
<th>Reference</th>
<th>Description of Report</th>
<th>Due Date</th>
</tr>
</thead>
<tbody>
<tr>
<td>§63.1439(b) and Subpart A</td>
<td>Refer to §63.1439(b), Table 1 of this subpart, and to subpart A.</td>
<td>Refer to subpart A.</td>
</tr>
<tr>
<td>§63.1439(e)(3)</td>
<td>Initial notification</td>
<td>Existing affected sources: by 120 days after June 1, 1999. New affected sources w/initial start-up at least 90 days after June 1, 1999: submit the application for approval of construction or reconstruction in lieu of the Initial Notification. New affected sources w/initial start-up prior to 90 days after June 1, 1999: by 90 days after June 1, 1999.</td>
</tr>
<tr>
<td>§63.1439(e)(4)</td>
<td>Precompliance Report*</td>
<td>Existing affected sources: 12 months prior to compliance date. New affected sources: with the application for approval of construction or reconstruction. Within 150 days after the compliance date.</td>
</tr>
<tr>
<td>§63.1439(e)(5)</td>
<td>Notification of Compliance Status*</td>
<td>Semiannually, no later than 60 days after the end of each 6-month period. See §63.1439(e)(6)(i) for the due date for this report. No later than 60 days after the end of each quarter.</td>
</tr>
<tr>
<td>§63.1439(e)(6)</td>
<td>Periodic Reports</td>
<td>No later than 60 days after the end of each quarter.</td>
</tr>
<tr>
<td>§63.1439(e)(6)(v)(iii)</td>
<td>Quarterly reports for sources with excursions (upon request of the Administrator).</td>
<td>At least 30 days prior to the refilling of each storage vessel or the inspection of each storage vessel.</td>
</tr>
<tr>
<td>§6.506(e)(7)(i)</td>
<td>Storage Vessels Notification of Inspection.</td>
<td></td>
</tr>
</tbody>
</table>

*There may be two versions of this report due at different times; one for equipment subject to §63.1434 and one for other emission points subject to this subpart.

*There will be two versions of this report due at different times; one for equipment subject to §63.1434 and one for other emission points subject to this subpart.
§ 63.1541 Applicability.

(a) The provisions of this subpart apply to the following affected sources at primary lead smelters: sinter machine, blast furnace, dross furnace, process fugitive sources, and fugitive dust sources. The provisions of this subpart do not apply to secondary lead smelters, lead refiners, or lead remelters.

(b) Table 1 of this subpart specifies the provisions of subpart A that apply and those that do not apply to owners and operators of primary lead smelters. The following sections of part 63 apply to this subpart as stated in subpart A and Table 1: §63.1 (Applicability), §63.2 (Definitions), §63.3 (Units and abbreviations), §63.4 (Prohibited activities and circumvention), §63.5 (Construction and reconstruction), §63.7 (Performance testing requirements), §63.8 (Monitoring requirements), §63.12 (State authority and delegations), §63.13 (Addresses of State air pollution control agencies and EPA Regional Offices), §63.14 (Incorporations by reference), and §63.15 (Availability of information confidentiality). The following sections of part 63 apply to the extent specified in this subpart and Table 1: §63.6 (Compliance with standards and maintenance requirements), §63.9 (Notification requirements), and §63.10 (Recordkeeping and reporting requirements). Section §63.11 (Control device requirements) does not apply to this subpart.

§ 63.1542 Definitions.

Terms used in this subpart are defined in the Act, in subpart A of this part, or in this section as follows:

Bag leak detection system means a system that is capable of continuously monitoring relative particulate matter (dust) loadings in the exhaust of a baghouse in order to detect bag leaks and other upset conditions. A bag leak detection system includes, but is not limited to, an instrument that operates on triboelectric, light scattering, light transmittance, or other effect to continuously monitor relative particulate matter loadings.

Blast furnace means any reduction furnace to which sinter is charged and which forms separate layers of molten slag and lead bullion.

Building means a roofed and walled structure with limited openings to allow access and egress for people and vehicles.

Charging location means the physical opening through which raw materials are introduced into a sinter machine, blast furnace, or dross furnace.

Dross furnace means any smelting furnace to which drosses are charged and which chemically and physically separates lead from other impurities.

Drossing and refining kettle means an open-top vessel that is constructed of cast iron or steel and is indirectly heated from below and contains molten lead for the purpose of drossing, refining, or alloying lead. Included are pot furnaces, receiving kettles, and holding kettles.

Fugitive dust source means a stationary source of hazardous air pollutant emissions at a primary lead smelter resulting from the handling, storage, transfer, or other management of lead-bearing materials where the source is not associated with a specific process, process vent, or stack. Fugitive dust sources include roadways, storage piles, materials handling transfer points, and materials transport areas.

Furnace area means any area of a primary lead smelter in which a blast furnace or dross furnace is located.

Malfunction means any sudden, infrequent, and not reasonably preventable failure of air pollution control equipment, process equipment, or a process to operate in a normal or usual manner. Failures that are caused in part by poor maintenance or careless operation are not malfunctions.

Materials storage and handling area means any area of a primary lead smelter in which lead-bearing materials (including ore concentrate, sinter, granulated lead, dross, slag, and flue dust) are stored or handled between process steps, including areas in which...
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§ 63.1543 Standards for process and process fugitive sources.

(a) No owner or operator of any existing, new, or reconstructed primary lead smelter shall discharge or cause to be discharged into the atmosphere lead compounds in excess of 500 grams of lead per megagram of lead metal produced (1.0 pounds of lead per ton of lead metal produced) from the aggregation of emissions discharged from the air pollution control devices used to control emissions from the sources listed in paragraphs (a)(1) through (a)(9) of this section.

1. Sinter machine;
2. Blast furnace;
3. Dross furnace;
4. Dross furnace charging location;
5. Blast furnace and dross furnace tapping location;
6. Sinter machine charging location;
7. Sinter machine discharge end;
8. Sinter crushing and sizing equipment; and
9. Sinter machine area.

(b) The process fugitive sources listed in paragraphs (a)(4) through (a)(8) of this section shall be equipped with a hood and shall be ventilated to a baghouse or equivalent control device. The hood design and ventilation rate shall be consistent with American Conference of Governmental Industrial Hygienists recommended practices.

(c) The sinter machine area shall be enclosed in a building that is ventilated to a baghouse or equivalent control device at a rate that maintains a positive in-draft through any doorway opening.

(d) Except as provided in paragraph (e) of this section, following the initial test to demonstrate compliance with paragraph (a) of this section, the owner or operator of a primary lead smelter shall conduct a compliance test for lead compounds on an annual basis (no later than 12 calendar months following any previous compliance test).
§ 63.1544 Standards for fugitive dust sources.

(a) Each owner or operator of a primary lead smelter shall prepare, and at all times operate according to, a standard operating procedures manual that describes in detail the measures that will be put in place to control fugitive dust emissions from the sources listed in paragraphs (a)(1) through (a)(5) of this section:

(1) Plant roadways;
(2) Material storage and handling area(s);
(3) Sinter machine area(s);
(4) Furnace area(s); and
(5) Refining and casting area(s).

(b) Notwithstanding paragraph (c) of this section, the standard operating procedures manual shall be submitted to the Administrator or delegated authority for review and approval.

(c) Existing manuals that describe the measures in place to control fugitive dust sources required as part of a State implementation plan for lead shall satisfy the requirements of paragraph (a) of this section provided they address the sources listed in paragraphs (a)(1) through (a)(5) of this section.

§ 63.1545 Compliance dates.

(a) Each owner or operator of an existing primary lead smelter shall achieve compliance with the requirements of this subpart no later than May 4, 2001.

(b) Each owner or operator of a primary lead smelter that commences construction or reconstruction after April 17, 1998, shall achieve compliance with the requirements of this subpart by June 4, 1999 or upon startup of operations, whichever is later.

§ 63.1546 Test methods.

(a) The following procedure shall be used to determine compliance with the emissions standard for lead compounds under § 63.1543(a):

(1) The lead compound emission rate, in units of grams of lead per hour, for each source listed in § 63.1543(a)(1) through § 63.1543(a)(9) shall be determined according to the following test methods in appendix A of part 60 of this chapter:

(i) Method 1 shall be used to select the sampling port location and the number of traverse points.

(ii) Method 2 shall be used to measure volumetric flow rate.

(iii) Method 3 shall be used for gas analysis.

(iv) Method 4 shall be used to determine moisture content of the stack gas.

(v) Method 12 shall be used to measure the lead emission rate of the stack gas. The minimum sample volume shall be 0.85 dry standard cubic meters (30 dry standard cubic feet) and the minimum sampling time shall be 60 minutes for each run. Three runs shall be performed and the average of the three runs shall be used to determine compliance.

(2) The lead production rate, in units of megagrams per hour, shall be determined based on production data for the previous 12 calendar months according to the procedures detailed in paragraphs (a)(2)(i) through (a)(2)(v) of this section:

(i) Total lead products production multiplied by the fractional lead content shall be determined in units of megagrams.
(ii) Total copper matte production multiplied by the fractional lead content shall be determined in units of megargrams.

(iii) Total copper speiss production multiplied by the fractional lead content shall be determined in units of megargrams.

(iv) Total lead production shall be determined by summing the values obtained in paragraphs (a)(2)(i) through (a)(2)(iii) of this section.

(v) The lead production rate, in units of megargrams per hours, shall be calculated based on the total lead production, as determined in accordance with paragraph (a)(2)(iv) of this section, divided by the total plant operating time, in hours, for the previous 12 months.

(3) The sum of lead compound emission rates for the sources in §63.1543(a) through (a)(9), as determined in accordance with paragraph (a)(1) of this section, shall be divided by the lead production rate, as determined in accordance with paragraph (a)(2)(v) of this section, to obtain a production-based, lead compound emission rate in units of grams of lead per megagram of lead metal produced. The production-based, lead compound emission rate shall be used to determine compliance with the emissions standard for lead compounds under §63.1543.

(b) Owner and operators shall perform an initial compliance test to demonstrate compliance with the sinter building in-draft requirements of §63.1543(c) at each doorway opening in accordance with paragraphs (b)(1) through (b)(4) of this section.

(1) Use a propeller anemometer or equivalent device.

(2) Determine doorway in-draft by placing the anemometer in the plane of the doorway opening near its center.

(3) Determine doorway in-draft for each doorway that is open during normal operation with all remaining doorways in their customary position during normal operation.

(4) Do not determine doorway in-draft when ambient wind speed exceeds 2 meters per second.

§63.1547 Monitoring requirements.

(a) Owners and operators of primary lead smelters shall prepare, and at all times operate according to, a standard operating procedures manual that describes in detail the procedures for inspection, maintenance, and bag leak detection and corrective action for all baghouses that are used to control process, process fugitive, or fugitive dust emissions from any source subject to the lead emission standards in §§63.1543 and 63.1544, including those used to control emissions from general ventilation systems.

(b) The standard operating procedures manual for baghouses required by paragraph (a) of this section shall be submitted to the Administrator or delegated authority for review and approval.

(c) The procedures specified in the standard operating procedures manual for inspections and routine maintenance shall, at a minimum, include the requirements of paragraphs (c)(1) through (c)(9) of this section.

(1) Daily monitoring of pressure drop across each baghouse cell to ensure pressure drop is within the normal operating range identified in the standard operating procedures manual.

(2) Weekly confirmation that dust is being removed from hoppers through visual inspection or equivalent means of ensuring the proper functioning of removal mechanisms.

(3) Daily check of compressed air supply for pulse-jet baghouses.

(4) An appropriate methodology for monitoring cleaning cycles to ensure proper operation.

(5) Monthly check of bag cleaning mechanisms for proper functioning through visual inspection or equivalent means.

(6) Quarterly visual check of bag tension on reverse air and shaker-type baghouses to ensure that bags are not kinked (knead or bent) or laying on their sides. Such checks are not required for shaker-type baghouses using self-tensioning (spring loaded) devices.

(7) Quarterly confirmation of the physical integrity of the baghouse through visual inspection of the baghouse interior for air leaks.

(8) Quarterly inspection of fans for wear, material buildup, and corrosion.
through visual inspection, vibration detectors, or equivalent means.

(9) Except as provided in paragraph (h) of this section, continuous operation of a bag leak detection system.

(d) The procedures specified in the standard operating procedures manual for maintenance shall, at a minimum, include a preventative maintenance schedule that is consistent with the baghouse manufacturer's instructions for routine and long-term maintenance.

(e) The bag leak detection system required by paragraph (c)(9) of this section shall meet the specifications and requirements of (e)(1) through (e)(8) of this section.

(1) The bag leak detection system must be certified by the manufacturer to be capable of detecting particulate matter emissions at concentrations of 10 milligram per actual cubic meter (0.0044 grains per actual cubic foot) or less.

(2) The bag leak detection system sensor must provide output of relative particulate matter loadings, and the owner or operator shall continuously record the output from the bag leak detection system.

(3) The bag leak detection system must be equipped with an alarm system that will sound when an increase in relative particulate loading is detected over a preset level, and the alarm must be located such that it can be heard by the appropriate plant personnel.

(4) Each bag leak detection system that works based on the triboelectric effect shall be installed, calibrated, and maintained in a manner consistent with guidance provided in the U.S. Environmental Protection Agency guidance document “Fabric Filter Bag Leak Detection Guidance” (EPA-454/R-98-015). Other bag leak detection systems shall be installed, calibrated, and maintained in a manner consistent with the manufacturer's written specifications and recommendations.

(5) The initial adjustment of the system shall, at a minimum, consist of establishing the baseline output by adjusting the sensitivity (range) and the averaging period of the device, and establishing the alarm set points and the alarm delay time.

(6) Following initial adjustment, the owner or operator shall not adjust the sensitivity or range, averaging period, alarm set points, or alarm delay time, except as detailed in the approved SOP required under paragraph (a) of this section. In no event shall the sensitivity be increased by more than 100 percent or decreased more than 50 percent over a 365-day period unless a responsible official certifies that the baghouse has been inspected and found to be in good operating condition.

(7) For negative pressure, induced air baghouses, and positive pressure baghouses that are discharged to the atmosphere through a stack, the bag leak detector must be installed downstream of the baghouse and upstream of any wet acid gas scrubber.

(8) Where multiple detectors are required, the system's instrumentation and alarm may be shared among detectors.

(f) The standard operating procedures manual required by paragraph (a) of this section shall include a corrective action plan that specifies the procedures to be followed in the event of a bag leak detection system alarm. The corrective action plan shall include, at a minimum, procedures to be used to determine the cause of an alarm, as well as actions to be taken to minimize emissions, which may include, but are not limited to, the following.

(1) Inspecting the baghouse for air leaks, torn or broken bags or filter media, or any other condition that may cause an increase in emissions.

(2) Sealing off defective bags or filter media.

(3) Replacing defective bags or filter media, or otherwise repairing the control device.

(4) Sealing off a defective baghouse compartment.

(5) Cleaning the bag leak detection system probe, or otherwise repairing the bag leak detection system.

(6) Shutting down the process producing the particulate emissions.

(g) The percentage of total operating time the alarm on the bag leak detection system sounds in a 6-month reporting period shall be calculated in order to determine compliance with the five percent operating limit in §63.1543(f). The percentage of time the
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alarm on the bag leak detection system sounds shall be determined according to paragraphs (g)(1) through (g)(5) of this section.

(1) Alarms that occur due solely to a malfunction of the bag leak detection system shall not be included in the calculation.

(2) Alarms that occur during startup, shutdown, or malfunction shall not be included in the calculation if the condition is described in the startup, shutdown, and malfunction plan and the owner or operator follows all the procedures in the plan defined for this condition.

(3) For each alarm where the owner or operator initiates procedures to determine the cause of an alarm within 1 hour of the alarm, 1 hour of alarm time shall be counted.

(4) For each alarm where the owner or operator does not initiate procedures to determine the cause of the alarm within 1 hour of the alarm, alarm time will be counted as the actual amount of time taken by the owner or operator to initiate procedures to determine the cause of the alarm.

(5) The percentage of time the alarm on the bag leak detection system sounds shall be calculated as the ratio of the sum of alarm times to the total operating time multiplied by 100.

(h) Baghouses equipped with HEPA filters as a secondary filter used to control process or process fugitive sources subject to the lead emission standards in §63.1543 are exempt from the requirement in §63.1543(c)(9) to be equipped with a bag leak detector. The owner or operator of an affected source that uses a HEPA filter shall monitor and record the pressure drop across the HEPA filter system daily. If the pressure drop is outside the limit(s) specified by the filter manufacturer, the owner or operator must take appropriate corrective measures, which may include, but not be limited to, the following:

(1) Inspecting the filter and filter housing for air leaks and torn or broken filters.

(2) Replacing defective filter media, or otherwise repairing the control device.

(3) Sealing off a defective control device by routing air to other control devices.

(4) Shutting down the process producing the particulate emissions.

(i) Owners and operators shall monitor sinter machine building in-draft to demonstrate continued compliance with the operating standard specified in §63.1543(c) in accordance with either paragraph (i)(1), (i)(2), or (i)(3) of this section.

(1) Owners and operators shall check and record on a daily basis doorway in-draft at each doorway in accordance with the methodology specified in §63.1546(b).

(2) Owners and operators shall establish and maintain baseline ventilation parameters which result in a positive in-draft according to paragraphs (i)(2)(i) through (ii)(2)(iv) of this section.

(1) Owners and operators shall install, calibrate, maintain, and operate a monitoring device that continuously records the actual volumetric flow rate through each separately ducted hood; or install, calibrate, maintain, and operate a monitoring device that continuously records the volumetric flow rate at the control device inlet of each exhaust system ventilating the building. The flow rate monitoring device(s) can be installed in any location in the exhaust duct such that reproducible flow rate monitoring will result. The flow rate monitoring device(s) shall have an accuracy of plus or minus 10 percent over its normal operating range and shall be calibrated according to manufacturer’s instructions.

(ii) During the initial demonstration of sinter building in-draft, and at any time the owner or operator wishes to re-establish the baseline ventilation parameters, the owner or operator shall continuously record the volumetric flow rate through each separately ducted hood, or continuously record the volumetric flow rate at the control device inlet of each exhaust system ventilating the building and record exhaust system damper positions. The owner or operator shall determine the average volumetric flow rate(s) corresponding to the period of time the in-draft compliance determinations are being conducted.
§ 63.1548 Notification requirements.

(a) The owner or operator of a primary lead smelter shall comply with all of the notification requirements of §63.9 of subpart A, General Provisions.

(b) The owner or operator of a primary lead smelter shall submit the fugitive dust control standard operating procedures manual required under §63.1544(a) to the Administrator or delegated authority along with a notification that the smelter is seeking review and approval of these plans and procedures. Owners or operators of existing primary lead smelters shall submit this notification no later than November 6, 2000. The owner or operator of a primary lead smelter that commences construction or reconstruction after April 17, 1998, shall submit this notification no later than 180 days before startup of the constructed or reconstructed primary lead smelter, but no sooner than September 2, 1999.

§ 63.1549 Recordkeeping and reporting requirements.

(a) The owner or operator of a primary lead smelter shall comply with all of the recordkeeping requirements of §63.10 of subpart A, General Provisions.

(b) In addition to the general records required by paragraph (a) of this section, each owner or operator of a primary lead smelter shall maintain for a period of 5 years, records of the information listed in paragraphs (b)(1) through (b)(8) of this section.

1. Production records of the weight and lead content of lead products, copper matte, and copper speiss.

2. Records of the bag leak detection system output.

3. An identification of the date and time of all bag leak detection system alarms, the time that procedures to determine the cause of the alarm were initiated, the cause of the alarm, an explanation of the actions taken, and the date and time the cause of the alarm was corrected.

4. Any recordkeeping required as part of the practices described in the standard operating procedures manual required under §63.1544(a) for the control of fugitive dust emissions.

5. Any recordkeeping required as part of the practices described in the standard operating procedures manual for baghouses required under §63.1547(a).

6. If an owner or operator chooses to demonstrate continuous compliance with the sinter building in-draft requirement under §63.1543(c) by employing the method allowed in §63.1546(i)(1), the records of the daily doorway in-draft checks, an identification of the periods when there was not a positive in-draft, and an explanation of the corrective actions taken.

7. If an owner or operator chooses to demonstrate continuous compliance with the sinter building in-draft requirement under §63.1543(c) by employing the method allowed in §63.1546(i)(2), the continuous volumetric flow monitor(s), an identification of the periods when the 15-minute volumetric flow rate dropped below the minimum established during the most recent in-draft determination, and an explanation of the corrective actions taken.

8. If an owner or operator chooses to demonstrate continuous compliance with the sinter building in-draft requirement under §63.1543(c) by employing the method allowed in §63.1546(i)(2), and volumetric flow rate is monitored at the baghouse inlet, records of the daily checks of damper positions, an identification of the days that the
damper positions were not in the positions established during the most recent in-draft determination, and an explanation of the corrective actions taken.
(c) Records for the most recent 2 years of operation must be maintained on site. Records for the previous 3 years may be maintained off site.
(d) The owner or operator of a primary lead smelter shall comply with all of the reporting requirements of §63.10 of subpart A, General Provisions.
(e) In addition to the information required under §63.10 of the General Provisions, the owner or operator shall provide semi-annual reports containing the information specified in paragraphs (e)(1) through (e)(7) of this section to the Administrator or designated authority.
(1) The reports shall include records of all alarms from the bag leak detection system specified in §63.1547(e).
(2) The reports shall include a description of the actions taken following each bag leak detection system alarm pursuant to §63.1547(f).
(3) The reports shall include a calculation of the percentage of time the alarm on the bag leak detection system sounded during the reporting period pursuant to §63.1547(g).
(4) If an owner or operator chooses to demonstrate continuous compliance with the sinter building in-draft requirement under §63.1543(c) by employing the method allowed in §63.1546(i)(1), the reports shall contain an identification of the periods when there was not a positive in-draft, and an explanation of the corrective actions taken.
(5) If an owner or operator chooses to demonstrate continuous compliance with the sinter building in-draft requirement under §63.1543(c) by employing the method allowed in §63.1546(i)(2), the reports shall contain an identification of the periods when the 15-minute volumetric flow rate(s) dropped below the minimum established during the most recent in-draft determination, and an explanation of the corrective actions taken.
(6) If an owner or operator chooses to demonstrate continuous compliance with the sinter building in-draft requirement under §63.1543(c) by employing the method allowed in §63.1546(i)(2), and volumetric flow rate is monitored at the baghouse inlet, the reports shall contain an identification of the days that the damper positions were not in the positions established during the most recent in-draft determination, and an explanation of the corrective actions taken.
(7) The reports shall contain a summary of the records maintained as part of the practices described in the standard operating procedures manual for baghouses required under §63.1547(a), including an explanation of the periods when the procedures were not followed and the corrective actions taken.
(8) The reports shall contain a summary of the fugitive dust control measures performed during the required reporting period, including an explanation of any periods when the procedures outlined in the standard operating procedures manual required by §63.1544(a) were not followed and the corrective actions taken. The reports shall not contain copies of the daily records required to demonstrate compliance with the requirements of the standard operating procedures manuals required under §§63.1544(a) and §63.1547(a).

§63.1550 Delegation of authority

(a) In delegating implementation and enforcement authority to a State under section 112(1) of the act, the authorities contained in paragraph (b) of this section shall be retained by the Administrator and not transferred to a State.
(b) Authorities which will not be delegated to States; no restrictions.

<table>
<thead>
<tr>
<th>Reference</th>
<th>Applies to subpart TTT</th>
<th>Comment</th>
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<tbody>
<tr>
<td>§63.1</td>
<td></td>
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<td>§63.2</td>
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<td>§63.5</td>
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</table>
Subparts UUU—WWW [Reserved]

Subpart XXX—National Emission Standards for Hazardous Air Pollutants for Ferroalloys Production: Ferromanganese and Silicomanganese

SOURCE: 64 FR 27458, May 20, 1999, unless otherwise noted.

§§ 63.1620–63.1649 [Reserved]

§ 63.1650 Applicability and compliance dates.

(a) This subpart applies to all new and existing ferromanganese and silicomanganese production facilities that manufacture ferromanganese or silicomanganese and are major sources or are co-located at major sources of hazardous air pollutant emissions.

(b) The following sources at a ferromanganese and silicomanganese production facility are subject to this subpart:

(1) Submerged arc furnaces.
(2) Metal oxygen refining (MOR) process.
(3) Crushing and screening operations.
(4) Fugitive dust sources.

(c) A new affected source is one for which construction or reconstruction commenced after August 4, 1998.

(d) The following table specifies which provisions of subpart A of this part apply to owners and operators of ferromanganese and silicomanganese production facilities subject to this subpart:
### General Provisions Applicability to Subpart XXX

<table>
<thead>
<tr>
<th>Reference, Subpart A General Provisions</th>
<th>Applies to Subpart XXX, §§63.1620–63.1679</th>
<th>Comment</th>
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<td>63.1–63.5</td>
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<td>63.6(a)–(g), (i)–(j)</td>
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<td>63.7(h)(1)–(h)(6), (h)(8)–(h)(9)</td>
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<td>63.7(h)(7)</td>
<td>No</td>
<td>§ 63.6(h)(7), use of continuous opacity monitoring system, not applicable.</td>
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<td>63.8</td>
<td>Yes</td>
<td></td>
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<tr>
<td>63.9</td>
<td>Yes</td>
<td>Notification of performance test results changed to a 30-day notification period.</td>
</tr>
<tr>
<td>63.10</td>
<td>Yes</td>
<td>Allow changes in dates by which periodic reports are submitted by mutual agreement between the owner or operator and the State to occur any time after the source's compliance date.</td>
</tr>
<tr>
<td>63.11</td>
<td>No</td>
<td>Flares will not be used to comply with the emission limits.</td>
</tr>
<tr>
<td>63.12–63.15</td>
<td>Yes</td>
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</table>
(e) Compliance dates. (1) Each owner or operator of an existing affected source must comply with the requirements of this subpart no later than May 21, 2001.

(2) Each owner or operator of a new or reconstructed affected source that commences construction or reconstruction after August 4, 1998, must comply with the requirements of this subpart by May 20, 1999 or upon startup of operations, whichever is later.

§ 63.1651 Definitions.

Terms in this subpart are defined in the Clean Air Act (Act), in subpart A of this part, or in this section as follows:

Bag leak detection system means a system that is capable of continuously monitoring particulate matter (dust) loadings in the exhaust of a baghouse in order to detect bag leaks and other upset conditions. A bag leak detection system includes, but is not limited to, an instrument that operates on triboelectric, light scattering, light transmittance, or other effect to continuously monitor relative particulate matter loadings.

Capture system means the equipment (including hoods, ducts, fans, dampers, etc.) used to capture or transport particulate matter generated by an affected submerged arc furnace.

Casting means the period of time from when molten ferroalloy falls from the furnace tapping runner into the ladle until pouring into molds is completed. This includes the following operations: ladle filling, pouring alloy from one ladle to another, slag separation, slag removal, and ladle transfer by crane, truck, or other conveyance.

Crushing and screening equipment means the crushers, grinders, mills, screens and conveying systems used to crush, size, and prepare for packing manganese-containing materials, including raw materials, intermediate products, and final products.

Fugitive dust source means a stationary source from which manganese-bearing particles are discharged to the atmosphere due to wind or mechanical inducement such as vehicle traffic. Fugitive dust sources include plant roadways, yard areas, and outdoor material storage and transfer operations.

Furnace power input means the resistive electrical power consumption of a submerged arc furnace, expressed as megawatts (MW).

Malfunction means any sudden, infrequent, and not reasonably preventable failure of air pollution control equipment, process equipment, or a process to operate in a normal or usual manner. Failures caused in part by poor maintenance or careless operation are not malfunctions.

Metal oxygen refining (MOR) process means the reduction of the carbon content of ferromanganese through the use of oxygen.

Open submerged arc furnace means an electric submerged arc furnace that is equipped with a canopy hood above the furnace to collect primary emissions.

Operating time means the period of time in hours that the affected source is in operation beginning at a startup and ending at the next shutdown.

Plant roadway means any area at a ferromanganese and silicomanganese production facility that is subject to plant mobile equipment, such as fork lifts, front end loaders, or trucks, carrying manganese-bearing materials. Excluded from this definition are employee and visitor parking areas, provided they are not subject to traffic by plant mobile equipment.

Primary emissions means gases and emissions collected by hoods and ductwork located above an open furnace or under the cover of a semi-closed or sealed furnace.

Sealed submerged arc furnace means an electric submerged arc furnace equipped with a total enclosure or cover from which primary emissions are evacuated directly.

Semi-closed submerged arc furnace means an electric submerged arc furnace equipped with a partially sealed cover over the furnace. This cover is equipped with openings to allow penetration of the electrodes into the furnace. Mix is introduced into the furnace around the electrode holes forming a partial seal between the electrodes and the cover. Furnace emissions generated under the cover are ducted to an emission control device. Emissions that escape the cover are collected and vented through stacks directly to the atmosphere.
Shop means the building which houses one or more submerged arc furnaces.

Shutdown means the cessation of operation of an affected source for any purpose.

Startup means the setting in operation of an affected source for any purpose.

Submerged arc furnace means any furnace wherein electrical energy is converted to heat energy by transmission of current between electrodes partially submerged in the furnace charge. The furnace may be of an open, semi-sealed, or sealed design.

Tapping emissions means a source of air pollutant emissions that occur during the process of removing the molten product from the furnace.

Tapping period means the time from when a tap hole is opened until the time a tap hole is closed.

§ 63.1652 Emission standards.

(a) New and reconstructed submerged arc furnaces. No owner or operator shall cause to be discharged into the atmosphere from any new or reconstructed submerged arc furnace exhaust gases (including primary and tapping) containing particulate matter in excess of one of the following:

(1) 0.23 kilograms per hour per megawatt (kg/hr/MW) (0.51 pounds per hour per megawatt [lb/hr/MW]), or

(2) 35 milligrams per dry standard cubic meter (mg/dscm) (0.015 grains per dry standard cubic foot [gr/dscf]).

(b) Existing open submerged arc furnaces. No owner or operator shall cause to be discharged into the atmosphere from any existing open submerged arc furnace exhaust gases (including primary and tapping) containing particulate matter in excess of one of the following:

(1) 16.3 kilograms per hour (kg/hr) (35.9 pounds per hour [lb/hr]) when producing silicomanganese, or

(2) 6.4 kg/hr (14.0 lb/hr) when producing ferromanganese.

(c) Existing semi-sealed submerged arc furnaces. No owner or operator shall cause to be discharged into the atmosphere from any existing semi-sealed submerged arc furnace exhaust gases (including primary, tapping, and vent stacks) containing particulate matter in excess of 11.2 kg/hr (24.7 lb/hr) when producing ferromanganese.

(d) MOR process. No owner or operator shall cause to be discharged into the atmosphere from any new, reconstructed, or existing MOR process exhaust gases containing particulate matter in excess of 69 mg/dscm (0.03 gr/dscf).

(e) Crushing and screening equipment. (1) New and reconstructed equipment. No owner or operator shall cause to be discharged into the atmosphere from any new or reconstructed piece of equipment associated with crushing and screening exhaust gases containing particulate matter in excess of 50 mg/dscm (0.022 gr/dscf).

(2) Existing equipment. No owner or operator shall cause to be discharged into the atmosphere from any existing piece of equipment associated with crushing and screening exhaust gases containing particulate matter in excess of 69 mg/dscm (0.03 gr/dscf).

§ 63.1653 Opacity standards.

No owner or operator shall cause emissions exiting from a shop due solely to operations of any affected submerged arc furnace, to exceed 20 percent opacity for more than one 6-minute period during any performance test, with the following exceptions:

(a) Visible particulate emissions from a shop due solely to operation of a semi-closed submerged arc furnace, may exceed 20 percent opacity, measured as a 6-minute average, one time during any performance test, so long as the emissions never exceed 60 percent opacity, measured as a 6-minute average.

(b) Blowing taps, poling and oxygen lancing of the tap hole; burndowns associated with electrode measurements; and maintenance activities associated with submerged arc furnaces and casting operations are exempt from the opacity standards specified in this section.

§ 63.1654 Operational and work practice standards.

(a) Fugitive dust sources. (1) Each owner or operator of an affected ferromanganese and silicomanganese production facility must prepare, and
§ 63.1655  Maintenance requirements.

(a) The owner or operator of an affected source must comply with the requirements of §63.6(e) of subpart A.

(b)(1) The owner or operator must develop and implement a written maintenance plan for each air pollution control device associated with submerged arc furnaces, metal oxygen refining processes, and crushing and screening operations subject to the provisions of this part. The owner or operator must keep the maintenance plan on record and available for the Administrator's inspection for the life of the air pollution control device or until the affected source is no longer subject to the provisions of this part.

(2) To satisfy the requirement to develop maintenance plans, the owner or operator may use the affected source's standard operating procedures (SOP) manual or other plan, provided the alternative plan meets the requirements of this paragraph and is made available for inspection when requested by the Administrator.

(c) The procedures specified in the maintenance plan must include a preventive maintenance schedule that is consistent with good air pollution control practices for minimizing emissions and, for baghouses, ensure that the requirements specified in §63.1657(a) are met.

(d) The owner or operator must perform monthly inspections of the equipment that is important to the performance of the furnace capture system. This inspection must include an examination of the physical condition of the equipment, suitable for detecting holes in ductwork or hoods, flow restrictions in ductwork due to dents or accumulated dust, and operational status of flow rate controllers (pressure sensors, dampers, damper switches, etc.). Any deficiencies must be recorded and proper maintenance and repairs performed.

§ 63.1656 Performance testing, test methods, and compliance demonstrations.

(a) Performance testing. (1) All performance tests must be conducted according to the requirements in §63.7 of subpart A.

(2) Each performance test must consist of three separate and complete runs using the applicable test methods.

(3) Each run must be conducted under conditions that are representative of normal process operations.

(4) Performance tests conducted on air pollution control devices serving submerged arc furnaces must be conducted such that at least one tapping
period, or at least 20 minutes of a tapping period, whichever is less, is included in at least two of the three runs. The sampling time for each run must be at least as long as three times the average tapping period of the tested furnace, but no less than 60 minutes.

(5) The sample volume for each run must be at least 0.9 dscm (30 dscf).

(b) Test methods. The following test methods in Appendix A of part 60 of this chapter must be used to determine compliance with the emission standards.

(1) Method 1 to select the sampling port location and the number of traverse points.

(2) Method 2 to determine the volumetric flow rate of the stack gas.

(3) Method 3 to determine the dry molecular weight of the stack gas.

(4) Method 4 to determine the moisture content of the stack gas.

(5) Method 5 to determine the particulate matter concentration of the stack gas for negative pressure baghouses and positive pressure baghouses with stacks.

(6) Method 5D to determine particulate matter concentration and volumetric flow rate of the stack gas for positive pressure baghouses without stacks.

(7) Method 9 to determine opacity.

(8) The owner or operator may use equivalent alternative measurement methods approved by the Administrator following the procedures described in §63.1656(f) of subpart A.

(c) Compliance demonstration with the emission standards. (1) The owner or operator must conduct an initial performance test for air pollution control devices or vent stacks subject to §63.1652(a) through (e) to demonstrate compliance with the applicable emission standards.

(2) The owner or operator must conduct annual performance tests for the air pollution control devices and vent stacks associated with the submerged arc furnaces, with the exception of any air pollution control devices that serve tapping emissions combined with non-furnace emissions, such as the MOR process or equipment associated with crushing and screening. Also excluded are air pollution control devices that serve dedicated non-furnace emissions, such as the MOR process or equipment associated with crushing and screening. The results of these annual tests will be used to demonstrate compliance with the emission standards in §63.1652(a) through (e), as applicable.

(3) Following development, and approval, if required, of the site-specific test plan, the owner or operator must conduct a performance test for each air pollution control device or vent stack to measure particulate matter and determine compliance with the applicable standard.

(i) An owner or operator of sources subject to the particulate matter concentration standards in §63.1652(a)(2), (d), or (e), must determine compliance as follows:

(A) Determine the particulate matter concentration using Method 5 or 5D, as applicable.

(B) Compliance is demonstrated if the average concentration for the three runs comprising the performance test does not exceed the standard.

(ii) An owner or operator of sources subject to the particulate matter concentration and volumetric flow rate standards in §63.1652(b) or (c) must determine compliance as follows:

(A) Determine the particulate matter concentration and volumetric flow rate using Method 5 or 5D, as applicable.

(B) Compute the mass rate ($E_M$) of particulate matter for each run using the following equation:

$$E_M = \left( \frac{\sum C_{si} Q_{sdi}}{K} \right)$$

Where:

$E_M$ = mass rate of particulate matter, kg/hr (lb/hr).

$N$ = total number of exhaust streams at which emissions are quantified.

$C_{si}$ = concentration of particulate matter from exhaust stream “i”, mg/dscm (gr/dscf).

$Q_{sdi}$ = volumetric flow rate of effluent gas from exhaust stream “i”, dscm/hr (dscf/hr).

$K$ = conversion factor, $1 \times 10^4$ mg/kg (7,000 gr/lb).

(C) Compliance is demonstrated if the average of the mass rates for the three runs comprising the performance test does not exceed the standard.

(iii) An owner or operator of sources subject to the particulate matter process-weighted rate standard in
§ 63.1652(a)(1) must determine compliance as follows:
(A) Determine particulate matter concentration and volumetric flow rate using Method 5 or 5D, as applicable.
(B) Compute the process-weighted mass rate ($E_P$) of particulate matter for each run using the following equation:

$$E_P = \left[ \sum_{i=1}^{N} C_{si}Q_{sdi} \right] / PK$$

Where:
- $E_P$ = process-weighted mass rate of particulate matter, kg/hr/MW (lb/hr/MW).
- $N$ = total number of exhaust streams at which emissions are quantified.
- $C_{si}$ = concentration of particulate matter from exhaust stream “i”, mg/dscm (gr/dscf).
- $Q_{sdi}$ = volumetric flow rate of effluent gas from exhaust stream “i”, dscm/hr (dscf/hr).
- $P$ = average furnace power input, MW.
- $K$ = conversion factor, $1 \times 10^6$ mg/kg (7,000 gr/lb).
(C) Compliance is demonstrated if the average process-weighted mass rate for the three runs comprising the performance test does not exceed the standard.
(4) If a venturi scrubber is used to comply with the emission standards, the owner or operator must establish as a site-specific operating parameter the lowest average pressure drop on any individual complying run in the three runs constituting any compliant test. The pressure drop must be monitored at least every 5 minutes during the test and hourly averages recorded.
(i) [Reserved]
(ii) The owner or operator may augment the data obtained under paragraph (a)(4) of this section by conducting multiple performance tests to establish a range of compliant operating parameter values. The lowest value of this range would be selected as the operating parameter monitoring value. The use of historic compliance data may be used to establish the compliant operating parameter value if the previous values were recorded during performance tests using the same test methods specified in this subpart and established as required in paragraph (a)(4) of this section.
(d) Compliance demonstration with opacity standards.
(1)(i) The owner or operator subject to §63.1653 must conduct initial opacity observations of the shop building to demonstrate compliance with the applicable opacity standards according to §63.6(h)(5), which addresses the conduct of opacity or visible emission observations.
(ii) In conducting the opacity observations of the shop building, the observer must limit his or her field of view to the area of the shop building roof monitor that corresponds to the placement of the affected submerged arc furnaces.
(iii) The owner or operator must conduct the opacity observations according to EPA Method 9 of 40 CFR part 60, appendix A, for a minimum of 60 minutes.
(2)(i) When demonstrating initial compliance with the shop building opacity standard, as required by paragraph (d)(1) of this section, the owner or operator must simultaneously establish parameter values for one of the following: the control system fan motor amperes and all capture system damper positions, the total volumetric flow rate to the air pollution control device and all capture system damper positions, or volumetric flow rate through each separately ducted hood that comprises the capture system.
(ii) The owner or operator may petition the Administrator to reestablish these parameters whenever he or she can demonstrate to the Administrator’s satisfaction that the submerged arc furnace operating conditions upon which the parameters were previously established are no longer applicable. The values of these parameters determined during the most recent demonstration of compliance must be maintained at the appropriate level for each applicable period.
(3) The owner or operator must demonstrate continuing compliance with the opacity standards by following the monitoring requirements specified in §63.1657(c) and the reporting and recordkeeping requirements specified in §§63.1659(b)(4) and 63.1660(b).
(e) Compliance demonstration with the operational and work practice standards.
(1) Fugitive dust sources. Failure to have a fugitive dust control plan or failure to report deviations from the plan and take necessary corrective action would
be a violation of the general duty to ensure that fugitive dust sources are operated and maintained in a manner consistent with good air pollution control practices for minimizing emissions per §63.6(e)(1)(i) of subpart A.

(2) Baghouses equipped with bag leak detection systems. The owner or operator demonstrates compliance with the bag leak detection system requirements by submitting reports as required by §63.1659(b)(5) showing that the alarm on the system does not sound for more than 5 percent of the total operating time in a 6-month period. Calculate the percentage of total operating time the alarm on the bag leak detection system sounds as follows:

(i) Do not include alarms that occur due solely to a malfunction of the bag leak detection system in the calculation.

(ii) Do not include alarms that occur during startup, shutdown, and malfunction in the calculation if the condition is described in the startup, shutdown, and malfunction plan and the owner or operator follows all the procedures in the plan defined for this condition.

(iii) Count 1 hour of alarm time for each alarm where the owner or operator initiates procedures to determine the cause within 1 hour of the alarm.

(iv) Count the actual time it takes the owner or operator to initiate procedures to determine the cause of the alarm for each alarm where the owner or operator does not initiate procedures to determine the cause within 1 hour of the alarm.

(v) Calculate the percentage of time the alarm on the bag leak detection system sounds as the ratio of the sum of alarm times to the total operating time multiplied by 100.

§ 63.1657 Monitoring requirements.

(a) Baghouses. (1) For the baghouses serving the submerged arc furnaces, the metal oxygen refining process, and crushing and screening operations, the owner or operator must observe on a daily basis for the presence of any visible emissions.

(2) In addition to the daily visible emissions observation, the owner or operator must conduct the following activities:

(i) Daily monitoring of pressure drop across each baghouse cell, or across the baghouse if it is not possible to monitor each cell individually, to ensure the pressure drop is within the normal operating range identified in the baghouse maintenance plan.

(ii) Weekly confirmation that dust is being removed from hoppers through visual inspection, or equivalent means of ensuring the proper functioning of removal mechanisms.

(iii) Daily check of compressed air supply for pulse-jet baghouses.

(iv) An appropriate methodology for monitoring cleaning cycles to ensure proper operation.

(v) Monthly check of bag cleaning mechanisms for proper functioning through visual inspection or equivalent means.

(vi) Quarterly visual check of bag tension on reverse air and shaker-type baghouses to ensure that the bags are not kinked (kneed or bent) or laying on their sides. Such checks are not required for shaker-type baghouses using self-tensioning (spring loaded) devices.

(vii) Quarterly confirmation of the physical integrity of the baghouse structure through visual inspection of the baghouse interior for air leaks.

(viii) Semiannual inspection of fans for wear, material buildup, and corrosion through visual inspection, vibration detectors, or equivalent means.

(3) In addition to meeting the requirements of paragraphs (a)(1) and (a)(2) of this section, the owner or operator of a new or reconstructed submerged arc furnace must install and continuously operate a bag leak detection system if the furnace primary and/or tapping emissions are ducted to a negative pressure baghouse or to a positive pressure baghouse equipped with a stack. The bag leak detection system must meet the following requirements:

(i) The bag leak detection system must be certified by the manufacturer to be capable of detecting particulate matter emissions at concentrations of 10 milligrams per actual cubic meter (0.0044 grains per actual cubic foot) or less.

(ii) The bag leak detection system sensor must provide output of relative particulate matter loadings, and the...
owner or operator must continuously record the output from the bag leak detection system.

(iii) The bag leak detection system must be equipped with an alarm system that will sound when an increase in relative particulate loadings is detected over a preset level. The alarm must be located where it can be heard by the appropriate plant personnel.

(iv) Each bag leak detection system that works based on the triboelectric effect must be installed, calibrated, operated, and maintained consistent with the U.S. Environmental Protection Agency guidance document “Fabric Filter Bag Leak Detection Guidance” (EPA-454/R-98-015). Other bag leak detection systems must be installed, calibrated, and maintained consistent with the manufacturer’s written specifications and recommendations.

(v) The initial adjustment of the system must, at a minimum, consist of establishing the baseline output by adjusting the sensitivity (range) and the averaging period of the device, and establishing the alarm set points and the alarm delay time.

(vi) Following initial adjustment, the owner or operator must not adjust the sensitivity or range, averaging period, alarm set points, or alarm delay time, except as detailed in the maintenance plan required under §63.1655(b). In no event must the sensitivity be increased by more than 100 percent or decreased more than 50 percent over a 365-day period unless a responsible official certifies the baghouse has been inspected and found to be in good operating condition.

(vii) Where multiple detectors are required, the system’s instrumentation and alarm may be shared among detectors.

(4) As part of the maintenance plan required by §63.1655(b), the owner or operator must develop and implement corrective action procedures to be followed in the case of a bag leak detection system alarm (for baghouses equipped with such a system), the observation of visible emissions from the baghouse, or the indication through the periodic baghouse system inspections that the system is not operating properly. The owner or operator must initiate corrective action as soon as practicable after the occurrence of the observation or event indicating a problem.

(5) The corrective action plan must include procedures used to determine the cause of an alarm or other indications of problems as well as actions to minimize emissions. These actions may include the following:

(i) Inspecting the baghouse for air leaks, torn or broken bags or filter media, or any other condition that may cause an increase in emissions.

(ii) Sealing off defective bags or filter media.

(iii) Replacing defective bags or filter media, or otherwise repairing the control device.

(iv) Sealing off a defective baghouse compartment.

(v) Cleaning the bag leak detection system probe, or otherwise repairing the bag leak detection system.

(vi) Shutting down the process producing the particulate matter emissions.

(6) Failure to monitor or failure to take corrective action under the requirements of paragraph (a) of this section would be a violation of the general duty to operate in a manner consistent with good air pollution control practices that minimizes emissions per §63.6(e)(1)(i) of subpart A.

(b) Venturi scrubbers. (1) The owner or operator must monitor the pressure drop across the venturi at least every 5 minutes and record the average hourly pressure drop. Measurement of an average hourly pressure drop less than the pressure drop operating parameter limit established during a successful compliance demonstration would be a violation of the applicable emission standard, unless the excursion in the pressure drop is due to a malfunction.

(2) As part of the maintenance plan required by §63.1655(b), the owner or operator must develop and implement corrective action procedures to be followed in the case of a violation of the pressure drop requirement. The owner or operator must initiate corrective action as soon as practicable after the excursion.

(3) Failure to monitor or failure to take corrective action under the requirements of paragraph (b) of this section is a violation of the general duty
§ 63.1658 Notification requirements.

(a) As required by §63.9(b) of subpart A, unless otherwise specified in this subpart, the owner or operator must submit the following written notifications to the Administrator:

(1) The owner or operator of an area source that subsequently becomes subject to the requirements of the standard must provide notification to the applicable permitting authority as required by §63.9(b)(1).

(2) As required by §63.9(b)(2), the owner or operator of an affected source that has an initial startup before the effective date of the standard must notify the Administrator that the source is subject to the requirements of the standard. The notification must be submitted no later than 120 calendar days after May 20, 1999 (or within 120 calendar days after the source becomes subject to this standard) and must contain the information specified in §63.9(b)(2)(i) through (b)(2)(v).

(3) As required by §63.9(b)(3), the owner or operator of a new or reconstructed affected source, or a source that has been reconstructed such that it is an affected source, that has an initial startup after the effective date and for which an application for approval of construction or reconstruction is not required under §63.5(d), must notify the Administrator in writing that the source is subject to the standards no later than 120 days after initial startup. The notification must contain the information specified in §63.9(b)(2)(i) through (b)(2)(v), delivered or postmarked with the notification required in §63.9(b)(5).

(4) As required by §63.9(b)(4), the owner or operator of a new or reconstructed major affected source that has an initial startup after the effective date of this standard and for which an application for approval of construction or reconstruction is required under §63.5(d) must provide the information specified in §63.9(b)(4)(i) through (b)(4)(v).
(5) As required by §63.9(b)(5), the owner or operator who, after the effective date of this standard, intends to construct a new affected source or reconstruct an affected source subject to this standard, or reconstruct a source such that it becomes an affected source subject to this standard, must notify the Administrator, in writing, of the intended construction or reconstruction.

(b) Request for extension of compliance. As required by §63.9(c), if the owner or operator of an affected source cannot comply with this standard by the applicable compliance date for that source, or if the owner or operator has installed BACT or technology to meet LAER consistent with §63.6(i)(5), he or she may submit to the Administrator (or the State with an approved permit program) a request for an extension of compliance as specified in §63.6(i)(4) through (i)(6).

(c) Notification that source is subject to special compliance requirements. As required by §63.9(d), an owner or operator of a new source that is subject to special compliance requirements as specified in §63.6(b)(3) and (b)(4) must notify the Administrator of his or her compliance obligations no later than the notification dates established in §63.9(b) for new sources that are not subject to the special provisions.

(d) Notification of performance test. As required by §63.9(e), the owner or operator of an affected source must notify the Administrator in writing of his or her intention to conduct a performance test at least 30 calendar days before the performance test is scheduled to begin to allow the Administrator to review and approve the site-specific test plan required under §63.7(c) and to have an observer present during the test.

(e) Notification of opacity and visible emission observations. As required by §63.9(f), the owner or operator of an affected source must notify the Administrator in writing of the anticipated date for conducting the opacity or visible emission observations specified in §63.6(h)(5). The notification must be submitted with the notification of the performance test date, as specified in paragraph (d) of this section, or if visibility or other conditions prevent the opacity or visible emission observations from being conducted concurrently with the initial performance test required under §63.7, the owner or operator must deliver or postmark the notification not less than 30 days before the opacity or visible emission observations are scheduled to take place.

(f) Notification of compliance status. The owner or operator of an affected source must submit a notification of compliance status as required by §63.9(h). The notification must be sent before the close of business on the 60th day following completion of the relevant compliance demonstration.

§ 63.1659 Reporting requirements.

(a) General reporting requirements. The owner or operator of a ferromanganese and silicomanganese production facility must comply with all of the reporting requirements under §63.10 of subpart A, unless otherwise specified in this subpart.

(1) Frequency of reports. As provided by §63.10(a)(5), if the owner or operator is required to submit periodic reports to a State on an established time line, he or she may change the dates by which periodic reports submitted under this part may be submitted (without changing the frequency of reporting) to be consistent with the State's schedule by mutual agreement between the owner or operator and the State. This provision may be applied at any point after the source's compliance date.

(2) Reporting results of performance tests. As required by §63.10(d)(2), the owner or operator of an affected source must report the results of the initial performance test as part of the notification of the compliance status required in §63.1658(f).

(3) [Reserved]

(4) Periodic startup, shutdown, and malfunction reports. (i) As required by §63.10(d)(5)(i), if actions taken by an owner or operator during a startup, shutdown, or malfunction of an affected source (including actions taken to correct a malfunction) are consistent with the procedures specified in the startup, shutdown, and malfunction plan, the owner or operator must state such information in a semiannual report. The report, to be certified by
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the owner or operator or other responsible official, must be submitted semi-annually and delivered or postmarked by the 30th day following the end of each calendar half; and

(ii) Any time an action taken by an owner or operator during a startup, shutdown, or malfunction (including actions taken to correct a malfunction) is not consistent with the procedures in the startup, shutdown, and malfunction plan, the owner or operator must comply with all requirements of §63.10(d)(5)(ii).

(b) Specific reporting requirements. In addition to the information required under §63.10, reports required under paragraph (a) of this section must include the information specified in paragraphs (b)(1) through (b)(5) of this section. As allowed by §63.10(a)(3), if any State requires a report that contains all of the information required in a report listed in this section, an owner or operator may send the Administrator a copy of the report sent to the State to satisfy the requirements of this section for that report.

(1) Air pollution control devices. The owner or operator must submit reports that summarize the records maintained as part of the practices described in the maintenance plan for air pollution control devices required under §63.1655(b), including an explanation of the periods when the procedures were not followed and the corrective actions taken.

(2) Venturi scrubbers. In addition to the information required to be submitted in paragraph (b)(1) of this section, the owner or operator must submit reports that identify the periods when the average hourly pressure drop of venturi scrubbers used to control particulate emissions dropped below the levels established in §63.1656(c)(4), and an explanation of the corrective actions taken.

(3) Fugitive dust. The owner or operator must submit reports that explain the periods when the procedures outlined in the fugitive dust control plan pursuant to §63.1654(a) were not followed and the corrective actions taken.

(4) Capture system. The owner or operator must submit reports that summarize the monitoring parameter excursions measured pursuant to §63.1657(c) and the corrective actions taken.

(5) Bag leak detection system. The owner or operator must submit reports including the following information:

(i) Records of all alarms.

(ii) Description of the actions taken following each bag leak detection system alarm.

(iii) Calculation of the percent of time the alarm on the bag leak detection system sounded during the reporting period.

(6) Frequency of reports. (i) The owner or operator must submit reports pursuant to §63.10(e)(3) that are associated with excess emissions events such as the excursion of the scrubber pressure drop limit per paragraph (b)(2) of this section. These reports are to be submitted on a quarterly basis, unless the owner or operator can satisfy the requirements in §63.10(e)(3) to reduce the frequency to a semiannual basis.

(ii) All other reports specified in paragraphs (b)(1) through (b)(5) of this section must be submitted semiannually.

§ 63.1660 Recordkeeping requirements.

(a) General recordkeeping requirements. (1) The owner or operator of a ferromanganese and silicomanganese production facility must comply with all of the recordkeeping requirements under §63.10.

(2) As required by §63.10(b)(2), the owner or operator must maintain records for 5 years from the date of each record of:

(i) The occurrence and duration of each startup, shutdown, or malfunction of operation (i.e., process equipment and control devices);

(ii) The occurrence and duration of each malfunction of the source or air pollution control equipment;

(iii) All maintenance performed on the air pollution control equipment;

(iv) Actions taken during periods of startup, shutdown, and malfunction (including corrective actions to restore malfunctioning process and air pollution control equipment to its normal or usual manner of operation) when such actions are different from the procedures specified in the startup, shutdown, and malfunction plan;

(v) All information necessary to demonstrate conformance with the startup, shutdown, and malfunction plan when
all actions taken during periods of startup, shutdown, and malfunction (including corrective actions) are consistent with the procedures specified in such plan. This information can be recorded in a checklist or similar form (see §63.10(b)(2)(vi));

(vi) All required measurements needed to demonstrate compliance with the standard and to support data that the source is required to report, including, but not limited to, performance test measurements (including initial and any subsequent performance tests) and measurements as may be necessary to determine the conditions of the initial test or subsequent tests;

(vii) All results of initial or subsequent performance tests;

(viii) If the owner or operator has been granted a waiver from recordkeeping or reporting requirements under §63.10(f), any information demonstrating whether a source is meeting the requirements for a waiver of recordkeeping or reporting requirements;

(ix) If the owner or operator has been granted a waiver from the initial performance test under §63.7(h), a copy of the full request and the Administrator's approval or disapproval;

(x) All documentation supporting initial notifications and notifications of compliance status required by §63.9; and

(xi) As required by §63.10(b)(3), records of any applicability determination, including supporting analyses.

§63.1661 Delegation of authorities.

In delegating implementation and enforcement authority to a State under subpart E of this part, the Administrator retains no authorities.

§§63.1662–63.1679 [Reserved]

APPENDIX A TO PART 63—TEST METHODS

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<th>METHOD 301—FIELD VALIDATION OF POLLUTANT MEASUREMENT METHODS FROM VARIOUS WASTE MEDIA</th>
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1. Applicability and principle

1.1 Applicability. This method, as specified in the applicable subpart, is to be used whenever a source owner or operator (hereafter referred to as an “analyst”) proposes a test method to meet a U.S. Environmental Protection Agency (EPA) requirement in the absence of a validated method. This Method includes procedures for determining and documenting the quality, i.e., systematic error (bias) and random error (precision), of the measured concentrations from an affected source. This method is applicable to various waste media (i.e., exhaust gas, wastewater, sludge, etc.).

1.1.1 If EPA currently recognizes an appropriate test method or considers the analyst’s test method to be satisfactory for a particular source, the Administrator may waive the use of this protocol or may specify a less rigorous validation procedure. A list of validated methods may be obtained by contacting the Emission Measurement Technical Information Center (EMTIC), Mail Drop 19, U.S. Environmental Protection Agency, Research Triangle Park, NC 27711, (919) 541-0200. Procedures for obtaining a waiver are in Section 12.0.
1.2 This method includes optional procedures that may be used to expand the applicability of the proposed method. Section 7.0 involves ruggedness testing (Laboratory Evaluation), which demonstrates the sensitivity of the method to various parameters. Section 8.0 involves a procedure for including sample stability in bias and precision for assessing sample recovery and analysis times; Section 9.0 involves a procedure for the determination of the practical limit of quantitation for determining the lower limit of the method. These optional procedures are required for the waiver consideration outlined in Section 12.0.

1.2 Principle. The purpose of these procedures is to determine bias and precision of a test method at the level of the applicable standard. The procedures involve (a) introducing known concentrations of an analyte or comparing the test method against a validated test method to determine the method's bias and (b) collecting multiple or collocated simultaneous samples to determine the method's precision.

1.2.1 Bias. Bias is established by comparing the method's results against a reference value and may be eliminated by employing a correction factor established from the data obtained during the validation test. An offset bias may be handled accordingly. Methods that have bias correction factors outside 0.7 to 1.3 are unacceptable. Validated method to proposed method comparisons, section 6.2, requires a more restrictive test of central tendency and a lower correction factor allowance of 0.90 to 1.10.

1.2.2 Precision. At the minimum, paired sampling systems shall be used to establish precision. The precision of the method at the level of the standard shall not be greater than 50 percent relative standard deviation. For a validated method to proposed method equivalency comparisons, section 6.2, the analyst must demonstrate that the precision of the proposed test method is as precise as the validated method for acceptance.

2. Definitions

2.1 Negative bias. Bias resulting when the measured result is less than the "true" value.

2.2 Positive bias. Bias resulting when the measured result is greater than the "true" value.

2.3 Parallel sampling system. A sampling system capable of obtaining two replicate samples that were collected as closely as possible in sampling time and sampling location.

2.4 Proposed method. The sampling and analytical methodology selected for field validation using the method described herein.

2.5 Quadruplet sampling system. A sampling system capable of obtaining four replicate samples that were collected as closely as possible in sampling time and sampling location.

2.6 Surrogate compound. A compound that serves as a model for the types of compounds being analyzed (i.e., similar chemical structure, properties, behavior). The model can be distinguished by the method from the compounds being analyzed.

3. Reference Material

The reference materials shall be obtained or prepared at the level of the standard. Additional runs with higher and lower reference material concentrations may be made to expand the applicable range of the method, in accordance with the ruggedness test procedures.

3.1 Exhaust Gas Tests. The analyst shall obtain a known concentration of the reference material (i.e., analyte of concern) from an independent source such as a specialty gas manufacturer, specialty chemical company, or commercial laboratory. A list of vendors may be obtained from EMTIC (see Section 1.1.1). The analyst should obtain the manufacturer's stability data of the analyte concentration and recommendations for recertification.

3.2 Other Waste Media Tests. The analyst shall obtain pure liquid components of the reference materials (i.e., analytes of concern) from an independent manufacturer and dilute them in the same type matrix as the source waste. The pure reference materials shall be certified by the manufacturer as to purity and shelf life. The accuracy of all diluted reference material concentrations shall be verified by comparing their response to independently-prepared materials (independently prepared in this case means prepared from pure components by a different analyst).

3.3 Surrogate Reference Materials. The analyst may use surrogate compounds, e.g., for highly toxic or reactive organic compounds, provided the analyst can demonstrate to the Administrator's satisfaction that the surrogate compound behaves as the analyte. A surrogate may be an isotope or one that contains a unique element (e.g., chlorine) that is not present in the source or a derivation of the toxic or reactive compound, if the derivative formation is part of the method's procedure. Laboratory experiments or literature data may be used to show behavioral acceptability.

3.4 Isotopically Labeled Materials. Isotope mixtures may contain the isotope and the natural analyte. For best results, the isotope labeled analyte concentration should be more than five times the natural concentration of the analyte.

4. EPA Performance Audit Material

4.1 To assess the method bias independently, the analyst shall use (in addition to
the reference material) an EPA performance audit material, if it is available. The analyst may contact EMTIC (see section 1.1.1) to receive a list of currently available EPA audit materials. If the analyte is listed, the analyst should request the audit material at least 30 days before the validation test. If an EPA audit material is not available, request documentation from the validation report reviewing authority that the audit material is currently not available from EPA. Include this documentation with the field validation report.

4.2 The analyst shall sample and analyze the performance audit sample three times according to the instructions provided with the audit sample. The analyst shall submit the three results with the field validation report. Although no acceptance criteria are set for these performance audit results, the analyst and reviewing authority may use them to assess the relative error of sample recovery, sample preparation, and analytical procedures and then consider the relative error in evaluating the measured emissions.

5. Procedure for Determination of Bias and Precision in the Field

The analyst shall select one of the sampling approaches below to determine the bias and precision of the data. After analyzing the samples, the analyst shall calculate the bias and precision according to the procedure described in section 6.0. When sampling a stationary source, follow the probe placement procedures in section 5.4.

5.1 Isotopic Spiking. This approach shall be used only for methods that require mass spectrometry (MS) analysis. Bias and precision are calculated by procedures described in section 6.1.

5.1.1 Number of Samples and Sampling Runs. Collect a total of 12 replicate samples using the procedures described in section 6.2. This approach shall be used when a validated method is available and an alternative method is being proposed.

5.1.2 Spiking Procedure. Spike all 12 samples with the reference material according to the applicable waste medium.

5.1.2.1 Gaseous Reference Material with Sorbent or Impinger Trains. Sample the reference material (in the laboratory or in the field) at a concentration which is close to the allowable concentration standard for the time required by the method, and then sample the gas stream for an equal amount of time. The time for sampling both the reference material and gas stream should be equal; however, the time should be adjusted to avoid sorbent breakthrough.

5.1.2.2 Gaseous Reference Material with Sample Container (Bag or Canister). Spike the sample containers after completion of each test run with an amount equal to the allowable concentration standard of the emission point. The final concentration of the reference material shall approximate the level of the emission concentration in the stack. The volume amount of reference material shall be less than 10 percent of the sample volume.

5.2 Comparison Against a Validated Test Method. Bias and precision are calculated using the procedures described in section 6.3. This approach shall be used when a validated method is available and an alternative method is being proposed.

5.2.1 Number of Samples and Sampling Runs. Collect nine sets of replicate samples using a paired sampling system (a total of 18 samples) or four sets of replicate samples using a quadruplet sampling system (a total of 16 samples). In each sample set, the validated test method shall be used to collect and analyze half of the samples.

5.2.2 Performance Audit Exception. Conduct the performance audit as required in section 4.0 for the validated test method. Conducting a performance audit on the test method being evaluated is recommended.

5.3 Analyte Spiking. This approach shall be used when sections 5.1 and 5.2 are not applicable. Bias and precision are calculated using the procedures described in section 6.3.

5.3.1 Number of Samples and Sampling Runs. Collect a total of 24 samples using the quadruplet sampling system (a total of 6 sets of replicate samples). In each quadruplet set, spike half of the samples (two out of the four) with the reference material according to the applicable procedure in section 5.1.2.1 or 5.1.2.2.

5.4 Probe Placement and Arrangement for Stationary Source Stack or Duct Sampling. The probes shall be placed in the same horizontal plane. For paired sample probes the arrangement should be that the probe tip is 2.5 cm from the outside edge of the other with a pitot tube on the outside of each probe. Other paired arrangements for the pitot tube may be acceptable. For quadruplet sampling probes, the tips should be in a 6.0 cm × 6.0 cm square area measured from the center line of the opening of the probe tip with a single
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pitot tube in the center or two pitot tubes with their location on either side of the probe tip configuration. An alternative arrangement should be proposed whenever the cross-sectional area of the probe tip configuration is approximately 5 percent of the stack or duct cross-sectional area.

6. Calculations

Data resulting from the procedures specified in section 5.0 shall be treated as follows to determine bias, correction factors, relative standard deviations, precision, and data acceptance.

6.1 Isotopic Spiking. Analyze the data for isotopic spiking tests as outlined in sections 6.1.1 through 6.1.6.

6.1.1 Calculate the numerical value of the bias using the results from the analysis of the isotopically spiked field samples and the calculated value of the isotopically labeled spike:

\[ B = CS - S_m \]  
Eq. 301-1

where:

\( B \) = Bias at the spike level.
\( S_m \) = Mean of the measured values of the isotopically spiked samples.
\( CS \) = Calculated value of the isotopically labeled spike.

6.1.2 Calculate the standard deviation of the \( S_i \) values as follows:

\[ SD = \sqrt{\frac{\sum (S_i - S_m)^2}{n - 1}} \]  
Eq. 301-2

where:

\( S_i \) = Measured value of the isotopically labeled analyte in the \( i \)th field sample,
\( n \) = Number of isotopically spiked samples, 12.

6.1.3 Calculate the standard deviation of the mean (SDM) as follows:

\[ SDM = \frac{SD}{\sqrt{n}} \]  
Eq. 301-3

6.1.4 Test the bias for statistical significance by calculating the \( t \)-statistic,

\[ t = \frac{|B|}{SDM} \]  
Eq. 301-4

and compare it with the critical value of the two-sided \( t \)-distribution at the 95-percent confidence level and \( n - 1 \) degrees of freedom. This critical value is 2.201 for the eleven degrees of freedom when the procedure specified in section 5.1.2 is followed. If the calculated \( t \)-value is greater than the critical value the bias is statistically significant and the analyst should proceed to evaluate the correction factor.

6.1.5 Calculation of a Correction Factor. If the \( t \)-test does not show that the bias is statistically significant, use all analytical results without correction and proceed to the precision evaluation. If the method’s bias is statistically significant, calculate the correction factor, \( CF \), using the following equation:

\[ CF = \frac{1}{1 + \frac{B}{CS}} \]  
Eq. 301-5

If the \( CF \) is outside the range of 0.70 to 1.30, the data and method are considered unacceptable. For correction factors within the range, multiply all analytical results by the \( CF \) to obtain the final values.

6.1.6 Calculation of the Relative Standard Deviation (Precision). Calculate the relative standard deviation as follows:

\[ RSD = \frac{SD}{S_m} \times 100 \]  
Eq. 301-6

where \( S_m \) is the measured mean of the isotopically labeled spiked samples.

6.2 Comparison with Validated Method. Analyze the data for comparison with a validated method as outlined in sections 6.2.1 or 6.2.2, as appropriate. Conduct these procedures in order to determine if a proposed method produces results equivalent to a validated method. Make all necessary bias corrections for the validated method, as appropriate. If the proposed method fails either test, the method results are unacceptable, and conclude that the proposed method is not as precise or accurate as the validated method. For highly variable sources, additional precision checks may be necessary. The analyst should consult with the Administrator if a highly variable source is suspected.

6.2.1 Paired Sampling Systems.

6.2.1.1 Precision. Determine the acceptance of the proposed method’s variance with respect to the variability of the validated method results. If a significant difference is determined, the proposed method and the results are rejected. Proposed methods demonstrating \( F \)-values equal to or less than the critical value have acceptable precision.

6.2.1.2 Calculate the variance of the proposed method, \( S^2 \), and the variance of the validated method, \( S^2 \), using the following equation:

\[ S^2 = SD^2 \]  
Eq. 301-7

where:
6.2.1.4 Bias Analysis. Test the bias for statistical significance by calculating the t-statistic and determine if the mean of the differences between the proposed method and the validated method is significant at the 80 percent confidence level. This procedure requires the standard deviation of the validated method, $S_v$, to be known. Employ the value furnished with the method. If the standard deviation of the validated method is not available, the paired replicate sampling procedure may not be used. Determine the mean of the paired sample differences, $d$, and the standard deviation, $S_d$, of the differences, $d_i$’s, using Equation 301-2 where:

$$d = \frac{d}{S_v}$$

Eq. 301-8

Compare the experimental $F$ value with the critical value of $F$. The critical value is 1.0 when the procedure specified in section 5.2.1 for paired trains is followed. If the calculated $F$ is greater than the critical value, the difference in precision is significant and the data and proposed method are unacceptable.

6.2.1.5 Calculation of a Correction Factor. If the statistical test cited above does not show a significant bias with respect to the reference method, assume that the proposed method is unbiased and use all analytical results without correction. If the method’s bias is statistically significant, calculate the correction factor, $CF$, as follows:

$$CF = \frac{1}{1 + \frac{d}{V_m}}$$

Eq. 301-10

where $V_m$ is the mean of the validated method’s values.

Multiply all analytical results by $CF$ to obtain the final values. The method results, and the method, are unacceptable if the correction factor is outside the range of 0.9 to 1.10.

6.2.2 Quadruplet Replicate Sampling Systems.

6.2.2.1 Precision. Determine the acceptance of the proposed method’s variance with respect to the variability of the validated method results. If a significant difference is determined the proposed method and the results are rejected.

6.2.2.2 Calculate the variance of the proposed method, $S_{p^2}$, using the following equation:

$$S_p^2 = \frac{\sum d_i^2}{2n}$$

Eq. 301-11

where the $d_i$’s are the differences between the validated method values and the proposed method values.

6.2.2.3 The $F$-test. Determine if the variance of the proposed method is more variable than that of the validated method by calculating the $F$-value using Equation 301-8. Compare the experimental $F$ value with the critical value of $F$. The critical value is 1.0 when the procedure specified in section 5.2.2 for quadruplet trains is followed. If the calculated $F$ should be less than or equal to the critical value. If the difference in precision is significant the results and the proposed method are unacceptable.

6.2.2.4 Bias Analysis. Test the bias for statistical significance at the 80 percent confidence level by calculating the t-statistic. Determine the bias (mean of the differences between the proposed method and the validated method, $d_m$) and the standard deviation, $S_m$, of the differences. Calculate the standard deviation of the differences, $S_{d_m}$ using Equation 301-2 and substituting $d_i$ for $S_v$. The following equation is used to calculate $d_i$: 

$$F = \frac{d}{V_m}$$

Eq. 301-9

where $n$ is the total number of paired samples. For the procedure in section 5.2.1, n equals nine. Compare the calculated t-statistic with the corresponding value from the table of the t-statistic. When nine runs are conducted, as specified in section 5.2.1, the critical value of the t-statistic is 1.397 for eight degrees of freedom. If the calculated t-value is greater than the critical value the bias is statistically significant and the analyst should proceed to evaluate the correction factor.
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\[ d_i = \frac{(V_{i1} + V_{i2})(P_{i1} + P_{i2})}{2} \]

Eq. 301-12

and: \( V_{i} \) = first measured value of the validated method in the ith test sample.

\( P_{i} \) = first measured value of the proposed method in the ith test sample.

Calculate the t-statistic using Equation 301-9 where \( n \) is the total number of test sample differences (\( d_i \)). For the procedure in section 5.2.2, \( n \) equals four. Compare the calculated t-statistic with the corresponding value from the table of the t-statistic and determine if the mean is significant at the 95-percent confidence level. When four runs are conducted, as specified in section 5.2.2, the critical value of the t-statistic is 2.776 for three degrees of freedom. If the calculated t-value is greater than the critical value the bias is statistically significant and the analyst should proceed to evaluate the correction factor.

6.2.2.5 Correction Factor Calculation. If the method's bias is statistically significant, calculate the correction factor, \( CF \), using Equation 301-10. Multiply all analytical results by \( CF \) to obtain the final values. The method results, and the method, are unacceptable if the correction factor is outside the range of 0.9 to 1.1.

6.3 Analyte Spiking. Analyze the data for analyte spike testing as outlined in Sections 6.3.1 through 6.3.3.

6.3.1 Precision.

6.3.1.1 Spiked Samples. Calculate the difference, \( d_i \), between the pairs of the spiked proposed method measurements for each replicate sample set. Determine the standard deviation (\( SD_s \)) of the spiked values using the following equation:

\[ SD_s = \sqrt{\frac{\sum d_i^2}{2n}} \]

Eq. 301-13

where: \( n \) = Number of runs.

Calculate the relative standard deviation of the proposed spiked method using Equation 301-6 where \( S_u \) is the measured mean of the analyte spiked samples. The proposed method is unacceptable if the RSD is greater than 50 percent.

6.3.1.2 Unspiked Samples. Calculate the standard deviation of the unspiked values using Equation 301-13 and the relative standard deviation of the proposed unspiked method using Equation 301-6 where \( S_u \) is the measured mean of the analyte spiked samples. The RSD must be less than 50 percent.

6.3.2 Bias. Calculate the numerical value of the bias using the results from the analysis of the spiked field samples, the unspiked field samples, and the calculated value of the spike:

\[ B = S_u - M_u - CS \]

Eq. 301-14

where: \( B \) = Bias at the spike level.

\( S_u \) = Mean of the spiked samples.

\( M_u \) = Mean of the unspiked samples.

\( CS \) = Calculated value of the spiked level.

6.3.2.1 Calculate the standard deviation of the mean using the following equation where \( SD_u \) and \( SD_s \) are the standard deviations of the spiked and unspiked sample values respectively as calculated using Equation 301-13.

\[ SD = \sqrt{SD_u^2 + SD_s^2} \]

Eq. 301-15

6.3.2.2 Test the bias for statistical significance by calculating the t-statistic using Equation 301-4 and comparing it with the critical value of the two-sided t-distribution at the 95-percent confidence level and \( n-1 \) degrees of freedom. This critical value is 2.201 for the eleven degrees of freedom.

6.3.3 Calculation of a Correction Factor. If the t-test shows that the bias is not statistically significant, use all analytical results without correction. If the method's bias is statistically significant, calculate the correction factor using Equation 301-5. Multiply all analytical results by \( CF \) to obtain the final values.

7. Ruggedness Testing (Optional)

7.1 Laboratory Evaluation.

7.1.1 Ruggedness testing is a useful and cost-effective laboratory study to determine the sensitivity of a method to certain parameters such as sample collection rate, interefant concentration, collecting medium temperature, or sample recovery temperature. This Section generally discusses the principle of the ruggedness test. A more detailed description is presented in citation 10 of Section 13.0.

7.1.2 In a ruggedness test, several variables are changed simultaneously rather than one variable at a time. This reduces the number of experiments required to evaluate the effect of a variable. For example, the effect of seven variables can be determined in eight experiments rather than 128 (W.J. Youden, Statistical Manual of the Association of Official Analytical Chemists, Association of Official Analytical Chemists, Washington, DC, 1975, pp. 33-36).

7.1.3 Data from ruggedness tests are helpful in extending the applicability of a test method to different source concentrations or source categories.
8. Procedure for Including Sample Stability in Bias and Precision Evaluations

8.1 Sample Stability.
8.1.1 The test method being evaluated must include procedures for sample storage and the time within which the collected samples shall be analyzed.
8.1.2 This section identifies the procedures for including the effect of storage time in bias and precision evaluations. The evaluation may be deleted if the test method specifies a time for sample storage.
8.2 Stability Test Design. The following procedures shall be conducted to identify the effect of storage times on analyte samples. Store the samples according to the procedure specified in the test method. When using the analyte spiking procedures (section 5.3), the study should include equal numbers of spiked and unspiked samples.
8.2.1 Stack Emission Testing.
8.2.1.1 For sample container (bag or canister) and impinger sampling systems, sections 5.1 and 5.3, analyze six of the samples at the minimum storage time. Then analyze the same six samples at the maximum storage time.
8.2.1.2 For sorbent and impinger sampling systems, sections 5.1 and 5.3, that require extraction or digestion, extract or digest six of the samples at the minimum storage time and extract or digest six other samples at the maximum storage time. Analyze an aliquot of the first six extracts (digestates) at both the minimum and maximum storage times. This will provide some freedom to analyze extract storage impacts.
8.2.1.3 For sorbent sampling systems, sections 5.1 and 5.3, that require thermal desorption, analyze six samples at the minimum storage time. Analyze another set of six samples at the maximum storage time.
8.2.1.4 For systems set up in accordance with section 5.2, the number of samples analyzed at the minimum and maximum storage times shall be half those collected (8 or 9). The procedures for samples requiring extraction or digestion should parallel those in section 8.2.1.
8.2.2 Other Waste Media Testing. Analyze half of the replicate samples at the minimum storage time and the other half at the maximum storage time in order to identify the effect of storage times on analyte samples.

9. Procedure for Determination of Practical Limit of Quantitation (Optional)
9.1 Practical Limit of Quantitation.
9.1.1 The practical limit of quantitation (PLQ) is the lowest level above which quantitative results may be obtained with an acceptable degree of confidence. For this protocol, the PLQ is defined as 10 times the standard deviation, s, at the blank level. This PLQ corresponds to an uncertainty of ±30 percent at the 99-percent confidence level.
9.1.2 The PLQ will be used to establish the lower limit of the test method.
9.2 Procedure I for Estimating s. This procedure is acceptable if the estimated PLQ is no more than twice the calculated PLQ. If the PLQ is greater than twice the calculated PLQ use Procedure II.
9.2.1 Estimate the PLQ and prepare a test standard at this level. The test standard could consist of a dilution of the reference material described in section 3.0.
9.2.2 Using the normal sampling and analytical procedures for the method, sample and analyze this standard at least seven times in the laboratory.
9.2.3 Calculate the standard deviation, s, of the measured values.
9.2.4 Calculate the PLQ as 10 times s.
9.3 Procedure II for Estimating s. This procedure is to be used if the estimated PLQ is more than twice the calculated PLQ.
9.3.1 Prepare two additional standards at concentration levels lower than the standard used in Procedure I.
9.3.2 Sample and analyze each of these standards at least seven times.
9.3.3 Calculate the standard deviation for each concentration level.
9.3.4 Plot the standard deviations of the three test standards as a function of the standard concentrations.
9.3.5 Draw a best-fit straight line through the data points and extrapolate to zero concentration. The standard deviation at zero concentration is s∞.
9.3.6 Calculate the PLQ as 10 times s∞.

10. Field Validation Report Requirements
The field validation report shall include a discussion of the regulatory objectives for the testing which describe the reasons for the test, applicable emission limits, and a description of the source. In addition, validation results shall include:
10.1 Summary of the results and calculations shown in section 6.0.
10.2 Reference material certification and value(s).
10.3 Performance audit results or letter from the reviewing authority stating the audit material is currently not available.
10.4 Laboratory demonstration of the quality of the spiking system.
10.5 Discussion of laboratory evaluations.
10.6 Discussion of field sampling.
10.7 Discussion of sample preparations and analysis.
10.8 Storage times of samples (and extracts, if applicable).
10.9 Reasons for eliminating any results.

11. Followup Testing
The correction factor calculated in section 6.0 shall be used to adjust the sample concentrations in all followup tests conducted
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12.2.2 The method must in-
clude an applicability statement, concentra-

12.2.3 Results of testing conducted with-
12.2.2 Summaries (see section 10.0) of
12.2.1 A clearly written test method, pref-
12.2.1.3 Conditional Test Methods. When
12.2.1.2 Documented Methods. In some
12.2.1.1 Similar Sources. If the test method
12.2.1.2 Conditional Test Methods. When
12.2.1.3 Documented Test Methods. In some
cases, bias and precision may have been doc-
umented through laboratory tests or proto-
cols different from this method. If the ana-
lyst can demonstrate to the satisfaction of the
Administrator that the bias and precision
apply to a particular application, the Admin-
istrator may waive these procedures or parts of
the procedures.
12.2.2 Application for Waiver. In general, the
requester shall provide a thorough descrip-
tion of the test method, the intended appli-
cation, and results of any validation or other
Supporting documents. Because of the many
potential situations in which the Adminis-
trator may grant a waiver, it is neither pos-
sible nor desirable to prescribe the exact cri-
teria for a waiver. At a minimum, the re-
quester is responsible for providing the fol-
lowing.
12.2.2.1 A clearly written test method, pref-

11.3 Validated RSD ≤ ±50 Percent. Nine
replicate samples.
11.2 Validated RSD ≤ ±30 Percent. Six rep-
clicate samples.
11.1 Validated relative standard deviation
(RSD) ≤ ±15 Percent. Three replicate sam-
11.1.2 Documented Methods.
11.1.1 Similar Sources.

12. Procedure for Obtaining a Waiver
12.1 Waivers. These procedures may be
waived or a less rigorous protocol may be
granted for site-specific applications. The
following are three example situations for
which a waiver may be considered.
12.1.1 Similar Sources. If the test method
has been validated previously at a "similar"
source, the procedures may be waived pro-
vided the requester can demonstrate to the
satisfaction of the Administrator that the
sources are "similar." The methods' appli-
cability to the "similar" source may be dem-
onstrated by conducting a ruggedness test as
described in section 6.0.
12.1.2 Documented Methods. In some
cases, bias and precision may have been doc-
umented through laboratory tests or proto-
cols different from this method. If the ana-
lyst can demonstrate to the satisfaction of the
Administrator that the bias and precision
apply to a particular application, the Admin-
istrator may waive these procedures or parts of
the procedures.
12.1.3 Conditional Test Methods. When
the method has been demonstrated to be
valid at several sources, the analyst may seek a
"conditional" method designation from the
Administrator. "Conditional" method status
provides an automatic waiver from the pro-
cedures provided the test method
is used within the stated applicability.
12.2 Application for Waiver. In general, the
requester shall provide a thorough descrip-
tion of the test method, the intended appli-
cation, and results of any validation or other
supporting documents. Because of the many
potential situations in which the Adminis-
trator may grant a waiver, it is neither pos-
sible nor desirable to prescribe the exact cri-
teria for a waiver. At a minimum, the re-
quester is responsible for providing the fol-
lowing.
12.2.1 A clearly written test method, prefer-
ably in the format of 40 CFR part 60, ap-
pendix A Test Methods. The method must in-
clude an applicability statement, concentra-
tion range, precision, bias (accuracy), and
time in which samples must be analyzed.

at the same source. These tests shall consist
of at least three replicate samples, and the
average shall be used to determine the pol-
lutant concentration. The number of samples
to be collected and analyzed shall be as fol-
lows, depending on the validated method pre-
icision level:
11.2.2.2 Summaries (see section 10.0) of
previous validation tests or other support-
ing documents. If a different procedure from
that described in this method was used, the
requester shall provide appropriate docu-
ments substantiating (to the satisfaction of the
Administrator) the bias and precision
values.
12.2.2.3 Discussion of the applicability
statement and arguments for approval of the
waiver. This discussion should address as
applicable the following: Applicable regula-
tion, emission standards, effluent charac-
teristics, and process operations.
12.3 Requests for Waiver. Each request
shall be in writing and signed by the analyst.
Submit requests to the Director, OAQPS,
Technical Support Division, U.S. Environ-
mental Protection Agency, Research Tri-
gle Park, NC 27711.
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III. Stationary Source Specific Methods.
1.3.2 By-product Coke Oven Battery. A source consisting of a group of ovens connected by common walls, where coal undergoes destructive distillation under positive pressure to produce coke and coke oven gas, from which by-products are recovered.

1.3.3 Charging System. An apparatus used to charge coal to a coke oven (e.g., a larry car for wet coal charging systems).

1.3.4 Coke Oven Door. Each end enclosure on the pusher side and the coking side of an oven. The chuck, or leveler-bar, door is considered part of the pusher side door. The coke oven door area includes the entire area on the vertical face of a coke oven between the bench and the top of the battery between two adjacent buck stays.

1.3.6 Coke Side. The side of a battery from which the coke is discharged from ovens at the end of the coking cycle.

1.3.7 Collecting Main. Any apparatus that is connected to one or more offtake systems and that provides a passage for conveying gases under positive pressure from the by-product coke oven battery to the by-product recovery system.

1.3.8 Consecutive Charges. Charges observed successively, excluding any charge during which the observer’s view of the charging system or topside ports is obscured.

1.3.9 Damper-off. To close off the gas passage between the coke oven and the collecting main, with no flow of raw coke oven gas from the collecting main into the oven or into the oven’s offtake system(s).

1.3.10 Decarbonization Period. The period of time for combusting oven carbon that commences when the oven lids are removed from an empty oven or when standpipe caps of an oven are opened. The period ends with the initiation of the next charging period for that oven.

1.3.11 Larry Car. An apparatus used to charge coal to a coke oven with a wet coal charging system.

1.3.12 Log Average. Logarithmic average as calculated in section 3.8.

1.3.13 Offtake System. Any individual oven apparatus that is stationary and provides a passage for gases from an oven to a coke oven battery collecting main or to another oven. Offtake system components include the standpipe and standpipe caps, goosenecks, stationary jumper pipes, mini-standpipes, and standpipe and gooseneck connections.

1.3.14 Operating Oven. Any oven not out of operation for rebuild or maintenance work extensive enough to require the oven to be skipped in the charging sequence.

1.3.15 Oven. A chamber in the coke oven battery in which coal undergoes destructive distillation to produce coke.

1.3.16 Push Side. The side of the battery from which the cokes are pushed from ovens at the end of the coking cycle.

1.3.17 Run. The observation of visible emissions from topside port lids, offtake systems, coke oven doors, or the charging of a single oven in accordance with this method.

1.3.18 Shed. Structures for capturing coke oven emissions on the coke side or pusher side of the coke oven battery, which route the emissions to a control device or system.

1.3.19 Standpipe Cap. An apparatus used to cover the opening in the gooseneck of an offtake system.

1.3.20 Topside Port Lid. A cover, removed during charging or decarbonizing, that is placed over the opening through which coal
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2.1 Certification Procedures. This method requires only the determination of whether VE or other criteria require the determination of opacity levels; therefore, observer certification according to Method 9 in appendix A to part 60 of this chapter is not required to obtain certification under this method. However, in order to receive Method 303 observer certification, the first-time observer (trainee) shall have attended the lecture portion of the Method 9 certification course. In addition, the trainee shall successfully complete the Method 303 training course, satisfy the field observation requirement, and demonstrate adequate performance and sufficient knowledge of Method 303. The Method 303 training course shall be conducted by or under the sanction of the EPA and shall consist of classroom instruction and field observations, and a proficiency test.

2.1.1 The classroom instruction shall familiarize the trainees with Method 303 through lecture, written training materials, and a Method 303 demonstration video. A successful completion of the classroom portion of the Method 303 training course shall be demonstrated by a perfect score on a written test. If the trainee fails to answer all of the questions correctly, the trainee may review the appropriate portion of the training materials and retake the test.

2.1.2 The field observations shall be a minimum of 12 hours and shall be completed before attending the Method 303 certification course. Trainees shall observe the operation of a coke oven battery as it pertains to Method 303, including topside operations, and shall also practice conducting Method 303 or similar methods. During the field observations, trainees unfamiliar with coke oven batteries shall receive instruction from an experienced coke oven observer familiar with Method 303 or similar methods and the operation of coke battery. The trainee must verify completion of at least 12 hours of field observation prior to attending the Method 303 certification course.

2.1.3 All trainees must demonstrate proficiency in the application of Method 303 to a panel of three certified Method 303 observers, including an ability to differentiate coke oven emissions from condensing water vapor and smoldering coal. Each panel member shall have at least 120 days experience in reading visible emissions from coke ovens. The visible emissions inspections that will satisfy the experience requirement must be inspections of coke oven battery fugitive emissions from the emission points subject to emission standards under subpart L of this part (i.e., coke oven doors, topside port lids, offtake systems, and charging operations), using either Method 303 or predecessor State or local test methods. A "day's experience" for a particular inspection is a day on which one complete inspection was performed for that emission point under Method 303 or a predecessor State or local method. A "day's experience" does not mean 8 or 10 hours performing inspections, or any particular time expressed in minutes or hours that may have been spent performing them. Thus, it would be possible for an individual to qualify as a Method 303 panel member for some emission points, but not others (e.g., an individual might satisfy the experience requirement for coke oven doors, but not topside port lids). Until November 15, 1994, the EPA may waive the certification requirement (but not the experience requirement) for panel members. The composition of the panel shall be approved by the EPA. The panel shall observe the trainee in a series of training runs and a series of certification runs. There shall be a minimum of 1 training run for doors, topside port lids, and offtake systems, and a minimum of 5 training runs (i.e., 5 charges) for charging. During training runs, the panel can advise the trainee on proper procedures. There shall be a minimum of 3 certification runs for charging (i.e., 15 charges). The certifications runs shall be unassisted. Following the certification test runs, the panel shall approve or disapprove certification based on the trainee's performance during the certification runs. To obtain certification, the trainee shall demonstrate to the satisfaction of the panel a high degree of proficiency in performing Method 303. To aid in evaluating the trainee's performance, a checklist, provided by the EPA, will be used.

Caution: Because coke oven batteries have hazardous environments, the training materials and the field training shall cover the precautions required by the company to address health and safety hazards. Special emphasis shall be given to the Occupational Safety and Health Administration (OSHA) regulations pertaining to exposure of coke oven workers (see Citation 3 in the Bibliography). In general, the regulation requires that special fire-retardant clothing and respirators be worn in certain restricted areas of the coke oven battery. The OSHA regulation also prohibits certain activities, such as
chewing gum, smoking, and eating in these areas.

2.2 Observer Certification/Recertification. The coke oven observer certification is valid for 1 year from date of issue. The observer shall recertify annually by viewing the training video and answering all of the questions on the certification test correctly. Every 3 years, an observer shall be required to pass the proficiency test in section 2.1.3 in order to be certified.

2.3 The EPA (or applicable enforcement agency) shall maintain records reflecting a certified observer’s successful completion of the proficiency test, which shall include the completed proficiency test checklists for the certification runs.

2.4 An owner or operator of a coke oven battery subject to subpart L of this part may observe a training and certification program under this section.

3. Procedure for Determining VE From Charging Systems During Charging

3.1 Number of Oven Charges. Refer to §63.306(c)(1) of this part for the number of oven charges to observe. The observer shall observe consecutive charges. Charges that are nonconsecutive can only be observed when necessary to replace observations terminated prior to the completion of a charge because of visual interferences. (See section 3.5.)

3.2 Data Records. Record all the information requested at the top of the charging system inspection sheet (Figure 303-1). For each charge, record the identification number of the oven being charged, the approximate beginning time of the charge, and the identification of the larry car used for the charge.

3.3 Observer Position. Stand in an area or move to positions on the topside of the coke oven battery with an unobstructed view of the emission points of the charging system, including larry car hoppers, drop sleeves, and the topside ports of the oven being charged. Some charging systems are configured so that all emission points can only be seen from a distance of five ovens. For other batteries, distances of 8 to 12 ovens are adequate.

3.4 Observation. The charging period begins when coal begins to flow into the oven and ends when the last charging port is recapped. During the charging period, observe all of the potential sources of VE from the entire charging system. For wet coal charging systems or non-pipeline coal charging systems, sources of VE typically include the larry car hoppers, drop sleeves, slide gates, and topside ports on the oven being charged. Any VE from an open standpipe cap on the oven being charged is included as charging VE.

3.4.1 Using an accumulative-type stopwatch with unit divisions of at least 0.5 seconds, determine the total time VE are observed as follows. Upon observing any VE emerging from any part of the charging system, start the stopwatch. Stop the watch when VE are no longer observed emerging, and restart the watch when VE reemerges.

3.4.2 When VE occur simultaneously from several points during a charge, consider the sources as one. Time overlapping VE as continuous VE. Time single puffs of VE only for the time it takes for the puff to emerge from the charging system. Continue to time VE in this manner for the entire charging period. Record the accumulated time to the nearest 0.5 second under “Visible emissions, seconds” on Figure 303-1.

3.5 Visual Interference. If fugitive VE from other sources at the coke oven battery site (e.g., door leaks or condensing water vapor from the coke oven wharf) prevent a clear view of the charging system during a charge, stop the stopwatch and make an appropriate notation under “Comments” on Figure 303-1. Label the observation an observation of an incomplete charge, and observe another charge to fulfill the requirements of section 3.1.

3.6 VE Exemptions. Do not time the following VE:

3.6.1 The VE from burning or smoldering coal spilled on top of the oven, topside port lid, or larry car surfaces;

Note: The VE from smoldering coal are generally white or gray. These VE generally have a plume of less than 1 meter long. If the observer cannot safely and with reasonable confidence determine that VE are from charging, do not count them as charging emissions.

3.6.2 The VE from the coke oven doors or from the leveler bar; or

3.6.3 The VE that drift from the top of a larry car hopper if the emissions had already been timed as VE from the drop sleeve.

Note: When the slide gate on a larry car hopper closes after the coal has been added to the oven, the seal may not be airtight. On occasions, a puff of smoke observed at the drop sleeves is forced past the slide gate up into the larry car hopper and may drift from the top; time these VE as charging VE; or

3.7 Total Time Record. Record the total time that VE were observed for each charging operation in the appropriate column on the charging system inspection sheet.

3.8 Five charging observations (runs) obtained in accordance with this method shall
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be considered a valid set of observations for that day. No observation of an incomplete charge shall be included in a daily set of observations that is lower than the lowest reading for a complete charge. If both complete and incomplete charges have been observed, the daily set of observations shall include the five highest values observed. Four or three charging observations (runs) obtained in accordance with this method shall be considered a valid set of charging observations only where it is not possible to obtain five charging observations, because of visual interferences (see section 3.5) or inclement weather prevent a clear view of the charging system during charging. However, observations from the four area if they satisfy these requirements shall not be considered a valid set of charging observations if use of such set of observations in a calculation under section 3.9 would cause the value of A to be less than 145.

3.9 Log Average. For each day on which a valid daily set of observations is obtained, calculate the daily 30-day rolling log average of seconds of visible emissions from the charging operation for each battery using these data and the 29 previous valid daily sets of observations, in accordance with the following equation:

\[ \log_{10} \text{average} = e^y - 1 \quad (\text{Eq. 303-1}) \]

where

- \( e = 2.72 \)
- \( y = \frac{\ln(X_1 + 1) + \ln(X_2 + 1) + \ldots + \ln(X_A + 1)}{A} \)

\( \ln \) = Natural logarithm, and

\( X_i \) = Seconds of VE during the \( i \)th charge.

\( A = 150 \) or the number of valid observations (runs). The value of \( A \) shall not be less than 145, except for purposes of determinations under §63.306(c) (work practice plan implementation) or §63.306(d) (work practice plan revisions) of this part. No set of observations shall be considered valid for such a recalculation that otherwise would not be considered a valid set of observations for a calculation under this paragraph.

4. Procedure for Determining VE From Coke Oven Door Areas

The intent of this procedure is to determine VE from coke oven door areas by carefully observing the door area from a standard distance while walking at a normal pace.

4.1 Number of Runs. Refer to §63.309(c)(1) of this part for the appropriate number of runs.

4.2 Battery Traverse. To conduct a battery traverse, walk the length of the battery on the outside of the pusher machine and quench car tracks at a steady, normal walking pace, pausing to make appropriate entries on the door area inspection sheet (Figure 303-2). A single test run consists of two timed traverses, one for the coke side and one for the push side. The walking pace shall not exceed an average rate of 4 seconds per oven door, excluding time spent moving around stationary obstructions or waiting for other obstructions to move from positions blocking the view of a series of doors. Extra time is allowed for each leak for the observer to make the proper notation. A walking pace of 3 seconds per oven door has been found to be typical. Record the actual traverse time with a stopwatch.

4.2.1 Time only the time spent observing the doors and recording door leaks. To measure actual traverse time, use an accumulative-type stopwatch with unit divisions of 0.5 seconds or less. Exclude interruptions to the traverse and time required for the observer to move to positions where the view of the battery is unobstructed, or for obstructions, such as the door machine, to move from positions blocking the view of a series of doors.

4.2.2 Various situations may arise that will prevent the observer from viewing a door or a series of doors. Prior to the door inspection, the owner or operator may elect to temporarily suspend charging operations for the duration of the inspection, so that all of the doors can be viewed by the observer. The observer has two options for dealing with obstructions to view: (a) Stop the stopwatch and wait for the equipment to move or the fugitive emissions to dissipate before completing the traverse; or (b) stop the stopwatch, skip the affected ovens, and move to a position to continue the traverse. Restart the stopwatch and continue the traverse.

After the completion of the traverse, if the equipment has moved or the fugitive emissions have dissipated, inspect the affected doors. If the equipment is still preventing the observer from viewing the doors, then the affected doors may be counted as not observed. If option (b) is used because of doors blocked by machines during charging operations, then, of the affected doors, exclude the door from the most recently charged oven from the inspection. Record the oven numbers and make an appropriate notation under "Comments" on the door area inspection sheet (Figure 303-2).

4.2.3 When batteries have sheds to control emissions, conduct the inspection from outside the shed unless the doors cannot be adequately viewed. In this case, conduct the inspection from the bench. Be aware of special safety considerations pertinent to walking on the bench and follow the instructions of company personnel on the required equipment and operations procedures. If possible, conduct the bench traverse whenever the bench is clear of the door machine and hot coke guide.

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4.3 Observations. Record all the information requested at the top of the door area inspection sheet (Figure 303-2), including the number of inoperable ovens. Record the clock time at the start of the traverse on each side of the battery. Record which side is being inspected, i.e., coke side or push side. Other information may be recorded at the discretion of the observer, such as the location of the leak (i.e., top of the door, chuck door, etc.), the reason for any interruption of the traverse, or the position of the sun relative to the battery and sky conditions (i.e., overcast, partly sunny, etc.).

4.3.1 Begin the test run by starting the stopwatch and traversing either the coke side or the push side of the battery. After completing one side, stop the watch. Complete this procedure on the other side. If inspecting more than one battery, the observer may view the push sides and the coke sides sequentially.

4.3.2 During the traverse, look around the entire perimeter of each oven door. The door is considered leaking if VE are detected in the coke oven door area. The coke oven door area includes the entire area on the vertical face of a coke oven between the bench and the top of the battery between two adjacent buck stays (e.g., the oven door, chuck door, between the masonry brick, buck stay or jamb, or other sources). Record the oven number and make the appropriate notation on the door area inspection sheet (Figure 303-2).

NOTE: Multiple VE from the same door area (e.g., VE from both the chuck door and the push side door) are counted as only one emitting door, not as multiple emitting doors.

4.3.3 Do not record the following sources as door area VE:

4.3.3.1 VE from ovens with doors removed. Record the oven number and make an appropriate notation under “Comments.”

4.3.3.2 VE from ovens taken out of service. The owner or operator shall notify the observer as to which ovens are out of service. Record the oven number and make an appropriate notation under “Comments.”

4.3.3.3 VE from hot coke that has been spilled on the bench as a result of pushing.

4.4 Criteria for Acceptance. After completing the run, calculate the maximum time allowed to observe the ovens by the following equation:

\[ T = (4 \times D_o) + (10 \times L) \]  

(Eq. 303-2)

where

\[ T = \text{Total time allowed for traverse, seconds;} \]
\[ D_o = \text{Total number of oven doors on the battery;} \]
\[ L = \text{Number of doors with VE.} \]

4.4.1 If the total traverse time exceeds \( T \), void the run, and conduct another run to satisfy the requirements of §63.309(c)(1) of this part.

4.5 Calculations for Percent Leaking Doors (PLD). Determine the total number of doors for which observations were made on the coke oven battery as follows:

\[ D_{ob} = (2 \times N) - (D_i + D_{no}) \]  

(Eq. 303-3)

where

\[ D_{ob} = \text{Total number of doors observed on operating ovens;} \]
\[ D_i = \text{Number of doors on nonoperating ovens;} \]
\[ D_{no} = \text{Number of doors not observed;} \]
\[ N = \text{Total number of ovens in the battery.} \]

4.5.1 For each test run (one run includes both the coke side and the push side traverses), sum the number of doors with door area VE. For batteries subject to an approved alternative standard under §63.305 of this part, calculate the push side and the coke side PLD separately.

4.5.2 Calculate percent leaking doors by using the following equation:

\[ \text{PLD} = \frac{L_b}{D_{ob}} \times 100 \]  

(Eq. 303-4)

where

\[ \text{PLD} = \text{Percent leaking doors for the test run;} \]
\[ L_b = \text{Number of doors with VE observed from the yard;} \]
\[ D_{ob} = \text{Total number of doors observed on operating ovens.} \]

4.5.3 When traverses are conducted from the bench under sheds, calculate the coke side and the push side separately. Use the following equation to calculate a yard-equivalent reading:

\[ L_s = L_y - (N \times 0.06) \]  

(Eq. 303-5)

where

\[ L_b = L_s - (N \times 0.06) \]  

(Eq. 303-6)

4.5.3.1 Use the following equation to calculate PLD:

\[ \text{PLD} = \frac{L_b + L_y}{D_{ob}} \times 100 \]  

(Eq. 303-6)

where

\[ \text{PLD} = \text{Percent leaking coke oven doors for the run;} \]
\[ L_b = \text{Yard equivalent reading;} \]
\[ L_y = \text{Number of doors with VE observed from the yard on the push side;} \]
\[ D_{ob} = \text{Total number of doors observed on operating ovens.} \]
Round off PLD to the nearest hundredth of 1 percent and record as the percent leaking coke oven doors for the run.

4.5.3.2 30-day Rolling Average. For each day on which a valid observation is obtained, calculate the daily 30-day rolling average for each battery using these data and the 29 previous valid daily observations, in accordance with the following equation:

\[
\text{PLD}(30-\text{day}) = \frac{(\text{PLD}_1 + \text{PLD}_2 + \ldots + \text{PLD}_{30})}{30}
\]

(Eq. 303-7)

5. Procedure for Determining VE from Topside Port Lids and Offtake Systems

5.1 Number of Runs. Refer to §63.309(c)(1) of this part for the number of runs to be conducted. Simultaneous runs or separate runs for the topside port lids and offtake systems may be conducted.

5.2 Battery Traverse. To conduct a topside traverse of the battery, walk the length of the battery at a steady, normal walking pace, pausing only to make appropriate entries on the topside inspection sheet (Figure 303-3). The walking pace shall not exceed an average rate of 4 seconds per oven, excluding time spent moving around stationary obstructions or waiting for other obstructions to move from positions blocking the view. Extra time is allowed for each leak for the observer to make the proper notation. A walking pace of 3 seconds per oven is typical. Record the actual traverse time with a stopwatch.

5.3 Topside Port Lid Observations. To observe lids of the ovens involved in the charging operation, the observer shall wait to view the lids until approximately 5 minutes after the completion of the charge. Record all the information requested on the topside inspection sheet (Figure 303-3). Record the clock time when traverses begin and end. If the observer’s view is obstructed during the traverse (e.g., steam from the coke wharf, larry car, etc.), follow the guidelines given in section 4.2.2.

5.3.1 To perform a test run, conduct a single traverse on the topside of the battery. The observer shall walk near the center of the battery but may deviate from this path to avoid safety hazards (such as open or closed charging ports, luting buckets, lid removal bars, and topside port lids that have been removed) and any other obstacles. Upon noting VE from the topside port lids of an oven, record the oven number and port number, then resume the traverse. If any oven is dampered-off from the collecting main for decarbonization, note this under “Comments” for that particular oven.

NOTE: Count the number of topside ports, not the number of points, exhibiting VE, i.e., if a topside port has several points of VE, count this as one port exhibiting VE.

5.3.2 Do not count the following as topside port lid VE:

5.3.2.1 VE from between the brickwork and oven lid casing or VE from cracks in the oven brickwork. Note these VE under “Comments;”

5.3.2.2 VE from topside ports involved in a charging operation. Record the oven number, and make an appropriate notation (i.e., not observed because ports open for charging) under “Comments;”

5.3.2.3 Topside ports having maintenance work done. Record the oven number and make an appropriate notation under “Comments;” or

5.3.2.4 Condensing water from wet-sealing material. Ports with only visible condensing water from wet-sealing material are counted as observed but not as having VE.

5.3.2.5 Visible emissions from the flue inspection ports and caps.

5.4 Offtake Systems Observations. To perform a test run, traverse the battery as in section 5.3.1. Look ahead and back two to four ovens to get a clear view of the entire offtake system for each oven. Consider visible emissions from the following points as offtake system VE: (a) the flange between the gooseneck and collecting main (“saddle”), (b) the junction point of the standpipe and oven (“standpipe base”), (c) the other parts of the offtake system (e.g., the standpipe cap), and (d) the junction points with ovens and flanges of jumper pipes.

5.4.1 Do not stray from the traverse line in order to get a “closer look” at any part of the offtake system unless it is to distinguish leaks from interferences from other sources or to avoid obstacles.

5.4.2 If the centerline does not provide a clear view of the entire offtake system for each oven (e.g., when standpipes are longer than 15 feet), the observer may conduct the traverse farther from (rather than closer to) the offtake systems.

5.4.3 Upon noting a leak from an offtake system during a traverse, record the oven number. Resume the traverse. If the oven is dampered-off from the collecting main for decarbonization and VE are observed, note this under “Comments” for that particular oven.
5.4.4 If any part or parts of an offtake system have VE, count it as one emitting offtake system. Each stationary jumper pipe is considered a single offtake system.

5.4.5 Do not count standpipe caps open for a decarbonization period or standpipes of an oven being charged as source of offtake system VE. Record the oven number and write "Not observed" and the reason (i.e., decarb or charging) under "Comments."

NOTE: VE from open standpipes of an oven being charged count as charging emissions. All VE from closed standpipe caps count as offtake leaks.

5.5 Criteria for Acceptance. After completing the run (allow 2 traverses for batteries with double mains), calculate the maximum time allowed to observe the topside port lids and/or offtake systems by the following equation:

\[ T = (4 \text{ sec} \times N) + (10 \text{ sec} \times Z) \]  \hspace{1cm} (Eq. 303-8)

where
- \( T \) = Total time allowed for traverse, seconds;
- \( N \) = Total number of ovens in the battery; and
- \( Z \) = Number of topside port lids or offtake systems with VE.

5.5.1 If the total traverse time exceeds \( T \), void the run and conduct another run to satisfy the requirements of §63.309(c)(1) of this part.

5.6 In determining the percent leaking topside port lids and percent leaking offtake systems, do not include topside port lids or offtake systems with VE from the following ovens:

5.6.1 Empty ovens, including ovens undergoing maintenance, which are properly dampered off from the main.

5.6.2 Ovens being charged or being pushed.

5.6.3 Up to 3 full ovens that have been dampered off from the main prior to pushing.

5.6.4 Up to 3 additional full ovens in the pushing sequence that have been dampered off from the main for offtake system cleaning, for decarbonization, for safety reasons, or when a charging/pushing schedule involves widely separated ovens (e.g., a Marquard system); or that have been dampered off from the main for maintenance near the end of the coking cycle. Examples of reasons that ovens are dampered off for safety reasons are to avoid exposing workers in areas with insufficient clearance between standpipes and the larry car, or in areas where workers could be exposed to flames or hot gases from open standpipes, and to avoid the potential for removing a door on an oven that is not dampered off from the main.

5.6.5 Topside Port Lids. Determine the percent leaking topside port lids for each run as follows:

\[ PLL = \frac{P_{\text{VE}}}{P_{\text{ovn}} (N - N_i) - P_{\text{NO}}} \times 100 \]  \hspace{1cm} (Eq. 303-9)

where
- \( PLL \) = Percent leaking topside port lids for the run;
- \( P_{\text{VE}} \) = Number of topside port lids with VE;
- \( P_{\text{ovn}} \) = Number of ports per oven;
- \( N \) = Total number of ovens in the battery;
- \( N_i \) = Number of inoperable ovens; and
- \( P_{\text{NO}} \) = Number of ports not observed.

5.6.5.1 Round off this percentage to the nearest hundredth of 1 percent and record this percentage as the percent leaking topside port lids for the run.

5.6.5.2 30-day Rolling Average. For each day on which a valid daily observation is obtained, calculate the daily 30-day rolling average for each battery using these data and the 29 previous valid daily observations, in accordance with the following equation:

\[ PLL(30 \text{- day}) = \frac{(PLL_{1} + PLL_{2} + \ldots + PLL_{30})}{30} \]  \hspace{1cm} (Eq. 303-10)
5.6.6 Offtake Systems. Determine the percent leaking offtake systems for the run as follows:

\[
PLO = \frac{T_{VE}}{T_{ovn}(N-N_i)+J-T_{NO}} \times 100 \quad \text{(Eq. 303-11)}
\]

\(PLO\) = Percent leaking offtake systems; 
\(T_{VE}\) = Number of offtake systems with VE; 
\(T_{ovn}\) = Number of offtake systems (excluding jumper pipes) per oven; 
\(N\) = Total number of ovens in the battery; 
\(N_i\) = Total number of inoperable ovens; 
\(T_{NO}\) = Number of offtake systems not observed; and 
\(J\) = Number of stationary jumper pipes.

5.6.6.1 Round off this percentage to the nearest hundredth of 1 percent and record this percentage as the percent leaking offtake systems for the run.

5.6.6.2 30-day Rolling Average. For each day on which a valid daily observation is obtained, calculate the daily 30-day rolling average for each battery using these data and the 29 previous valid daily observations, in accordance with the following equation:

\[
PLO(30-\text{day}) = \frac{(PLO_1 + PLO_2 + \ldots + PLO_{30})}{30} \quad \text{(Eq. 303-12)}
\]

6. Procedure for Determining VE From Collecting Mains

6.1 Traverse. To perform a test run, traverse both the collecting main catwalk and the battery topside along the side closest to the collecting main. If the battery has a double main, conduct two sets of traverses for each run, i.e., one set for each main.

6.2 Data Recording. Upon noting VE from any portion of a collection main, identify the source and approximate location of the source of VE and record the time under “Collecting main” on Figure 303-3; then resume the traverse.

6.3 Collecting Main Pressure Check. After the completion of the door traverse, the topside port lids, and offtake systems, compare the collecting main pressure during the inspection to the collecting main pressure during the previous 8 to 24 hours. Record the following: (a) The pressure during inspection, (b) presence of pressure deviation from normal operations, and (c) the explanation for any pressure deviation from normal operations, if any, offered by the operators. The owner or operator of the coke battery shall maintain the pressure recording equipment and conduct the quality assurance/quality control (QA/QC) necessary to ensure reliable pressure readings and shall keep the QA/QC records for at least 6 months. The observer may periodically check the QA/QC records to determine their completeness. The owner or operator shall provide access to the records within 1 hour of an observer’s request.

7. Bibliography


Company name: ____________________________ Battery no.: __________ Date: __________ Run no.: __________
City, State: ________________________________
Observer name: ____________________________ Company representative(s): ____________________________

<table>
<thead>
<tr>
<th>Charge no.</th>
<th>Gear no.</th>
<th>Clamp type</th>
<th>Visible Delaminating damage</th>
<th>Comments</th>
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Figure 303-1. Charging system inspection.
Company name: ___________________________ Battery no.: __________ Date: __________

City, State: ___________________________ Total no. of ovens in battery: __________

Observer name: ___________________________ Certification expiration date: __________

Inoperable ovens: __________ Company representative(s): ___________________________

Traverse time CS: __________ Traverse time PS: __________ Valid run (Y or N): __________

<table>
<thead>
<tr>
<th>Time traverse started/ completed</th>
<th>PS/CS</th>
<th>Door Number</th>
<th>Comments (no. of blocked doors, interruptions to traverse, etc.)</th>
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**Figure 303-2. Door area inspection.**
METHOD 303A—DETERMINATION OF VISIBLE EMISSIONS FROM NONRECOVERY COKE OVEN BATTERIES

1. Applicability and Principle
   1.1 Applicability. This method determines percent leaking doors.
   1.2 Principle. A certified observer visually determines the VE from coke oven battery sources. This method does not require that opacity of emissions be determined or that magnitude be differentiated.
   1.3 Definitions.
   1.3.1 Bench. The platform structure in front of the oven doors.

1.3.2 Nonrecovery Coke Oven Battery. A source consisting of a group of ovens connected by common walls and operated as a unit, where coal undergoes destructive distillation under negative pressure to produce coke, and which is designed for the combustion of coke oven gas from which by-products are not recovered.
   1.3.3 Coke Oven Door. Each end enclosure on the pusher side and the coking side of an oven.
   1.3.4 Coke Side. The side of a battery from which the coke is discharged from ovens at the end of the coking cycle.

1.3.5 Operating Oven. Any oven not out of operation for rebuild or maintenance work.

<table>
<thead>
<tr>
<th>Time traverse started/ completed</th>
<th>Type of Inspection (lids, offtakes, collecting mains)</th>
<th>Location of VE (Oven #/Port #)</th>
<th>Comments</th>
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Figure 303-3. Topside inspection.
Environmental Protection Agency

extensive enough to require the oven to be skipped in the charging sequence.

1.3.6 Oven. A chamber in the coke oven battery in which coal undergoes destructive distillation to produce coke.

1.3.7 Push Side. The side of the battery from which the coke is pushed from ovens at the end of the coking cycle.

1.3.8 Run. The observation of visible emissions from coke oven doors in accordance with the procedures in this method.

1.3.9 Shed. An enclosure that covers the side of the coke oven battery, captures emissions from pushing operations and from leaking coke oven doors on the coke side or pusher side of the coke oven battery, and routes the emissions to a control device or system.

2. Training

2.1 Training. This method requires only the determination of whether VE occur and does not require the determination of opacity levels; therefore, observer certification according to Method 9 in appendix A to part 60 of this chapter is not required. However, the first-time observer (trainee) shall have attended the lecture portion of the Method 9 certification course. Furthermore, before conducting any VE observations, an observer shall become familiar with nonrecovery coke oven battery operations and with this test method by observing for a minimum of 4 hours the operation of a nonrecovery coke oven battery.

3. Procedure for Determining VE From Coke Oven Door Areas

The intent of this procedure is to determine VE from coke oven doors by carefully observing the door area while walking at a normal pace.

3.1 Number of Runs. Refer to §63.309(c)(1) of this part for the appropriate number of runs.

3.2 Battery Traverse. To conduct a battery traverse, walk the length of the battery on the outside of the pusher machine and quench car tracks at a steady, normal walking pace, pausing to make appropriate entries on the door area inspection sheet (Figure 303A–1). A single test run consists of two timed traverses, one for the coke side and one for the push side.

3.2.1 Various situations may arise that will prevent the observer from viewing a door or a series of doors. The observer has two options for dealing with obstructions to view: (a) Wait for the equipment to move or the fugitive emissions to dissipate before completing the traverse; or (b) skip the affected ovens and move to a position to continue the traverse. Continue the traverse. After the completion of the traverse, if the equipment has moved or the fugitive emissions have dissipated, complete the traverse by inspecting the affected doors. Record the oven numbers and make an appropriate notation under “Comments” on the door area inspection sheet (Figure 303A–1).

3.2.2 When batteries have sheds to control pushing emissions, conduct the inspection from outside the shed, if the shed allows such observations, or from the bench. Be aware of special safety considerations pertinent to walking on the bench and follow the instructions of company personnel on the required equipment and operations procedures. If possible, conduct the bench traverse whenever the bench is clear of the door machine and hot coke guide.

3.3 Observations. Record all the information requested at the top of the door area inspection sheet (Figure 303A–1), including the number of inoperable ovens. Record which side is being inspected, i.e., coke side or push side. Other information may be recorded at the discretion of the observer, such as the location of the leak (e.g., top of the door), the reason for any interruption of the traverse, or the position of the sun relative to the battery and sky conditions (i.e., overcast, partly sunny, etc.).

3.3.1 Begin the test run by traversing either the coke side or the push side of the battery. After completing one side, traverse the other side.

3.3.2 During the traverse, look around the entire perimeter of each oven door. The door is considered leaking if VE are detected in the coke oven door area. The coke oven door area includes the entire area on the vertical face of a coke oven between the bench and the top of the battery. Record the oven number and make the appropriate notation on the door area inspection sheet (Figure 303A–1).

3.3.3 Do not record the following sources as door area VE:

3.3.3.1 VE from ovens with doors removed. Record the oven number and make an appropriate notation under “Comments.”

3.3.3.2 VE from ovens where maintenance work is being conducted. Record the oven number and make an appropriate notation under “Comments.”

3.3.3.3 VE from hot coke that has been spilled on the bench as a result of pushing.

3.4 Calculations for percent leaking doors (PLD). Determine the total number of doors for which observations were made on the coke oven battery as follows:

\[ D_{oh} = (2 \times N) – (D_1 + D_{no}) \] (Eq. 303A–1)

where

- \( D_{oh} \) = Total number of doors observed on operating ovens;
- \( D_1 \) = Number of doors on nonoperating ovens;
- \( D_{no} \) = Number of doors not observed; and
- \( N \) = Total number of ovens in the battery.
3.4.1 For each test run (one run includes both the coke side and the push side traverses), sum the number of doors with door area VE.

NOTE: Multiple VE from the same door area are counted as only one emitting door, not as multiple emitting doors.

3.4.2 Calculate percent leaking doors by using the following equation:

\[ \text{PLD} = \frac{L_y}{D_{ob}} \times 100 \quad (\text{Eq. 303A-2}) \]

where

- PLD = Percent leaking doors for the test run;
- \( L_y \) = Number of doors with VE observed from the yard; and
- \( D_{ob} \) = Total number of doors observed on operating ovens.

3.4.3 When traverses are conducted from the bench under sheds, calculate the coke side and the push side reading separately. Use the following equation to calculate a yard-equivalent reading for the coke side:

\[ L_b = L_c - (N \times 0.06) \quad (\text{Eq. 303A-3}) \]

where

- \( N \) = Total number of ovens on the battery.

If \( L_b \) is less than zero, use zero for \( L_b \) in Equation 303A-4 in the calculation of PLD.

3.4.3.1 Use the following equation to calculate PLD:

\[ \text{PLD} = \frac{L_b + L_y}{D_{ob}} \times 100 \quad (\text{Eq. 303A-4}) \]

where

- PLD = Percent leaking coke oven doors for the run;
- \( L_b \) = Yard equivalent reading;
- \( L_y \) = Number of doors with VE observed from the yard on the push side; and
- \( D_{ob} \) = Total number of doors observed on operating ovens.

Round off PLD to the nearest hundredth of 1 percent and record as the percent leaking coke oven doors for the run.

3.4.3.2 30-day Rolling Average. For each day on which a valid observation is obtained, calculate the daily 30-day rolling average for each battery using these data and the 29 previous valid daily observations, in accordance with the following equation:

\[ \text{PLD}(30\text{-day}) = \frac{(\text{PLD}_1 + \text{PLD}_2 + \text{PLD}_3 + \ldots + \text{PLD}_{30})}{30} \quad (\text{Eq. 303-5}) \]

4. Bibliography


METHOD 304A: DETERMINATION OF BIO-DEGRADATION RATES OF ORGANIC COMPOUNDS (VENT OPTION)

1. Applicability and Principle

1.1 Applicability. This method is applicable for the determination of biodegradation rates of organic compounds in an activated sludge process. The test method is designed to evaluate the ability of an aerobic biological reaction system to degrade or destroy specific components in waste streams. The method may also be used to determine the effects of changes in wastewater composition on operation. The biodegradation rates determined by utilizing this method are not representative of a full-scale system. The rates measured by this method shall be used in conjunction with the procedures listed in appendix C of this part to calculate the fraction emitted to the air versus the fraction biodegraded.

1.2 Principle. A self-contained benchtop bioreactor system is assembled in the laboratory. A sample of mixed liquor is added and the waste stream is then fed continuously. The benchtop bioreactor is operated under conditions nearly identical to the target full-scale activated sludge process. Bioreactor temperature, dissolved oxygen concentration, average residence time in the reactor, waste composition, biomass concentration, and biomass composition of the full-scale process are the parameters which are duplicated in the benchtop bioreactor. Biomass shall be removed from the target full-scale activated sludge unit and held for no more than 4 hours prior to use in the benchtop bioreactor. If antifoaming agents are used in the full-scale system, they shall...
also be used in the benchtop bioreactor. The feed flowing into and the effluent exiting the benchtop bioreactor are analyzed to determine the biodegradation rates of the target compounds. The flow rate of the exit vent is used to calculate the concentration of target compounds (utilizing Henry’s law) in the exit gas stream. If Henry’s law constants for the compounds of interest are not known, this method cannot be used in the determination of the biodegradation rate and Method 304B is the suggested method. The choice of analytical methodology for measuring the compounds of interest at the inlet and outlet to the benchtop bioreactor are left to the discretion of the source, except where validated methods are available.

2. Apparatus

Figure 1 illustrates a typical laboratory apparatus used to measure biodegradation rates. While the following description refers to Figure 1, the EPA recognizes that alternative reactor configurations, such as alternative reactor shapes and locations of probes and the feed inlet, will also meet the intent of this method. Ensure that the benchtop bioreactor system is self-contained and isolated from the atmosphere (except for the exit vent stream) by leak-checking fittings, tubing, etc.

2.1 Laboratory apparatus.

2.1.1 Benchtop Bioreactor. The biological reaction is conducted in a biological oxidation reactor of at least 6 liters capacity. The benchtop bioreactor is sealed and equipped with internal probes for controlling and monitoring dissolved oxygen and internal temperature. The top of the reactor is equipped for aerators, gas flow ports, and instrumentation (while ensuring that no leaks to the atmosphere exist around the fittings).
2.1.2 Aeration gas. Aeration gas is added to the benchtop bioreactor through three diffusers, which are glass tubes that extend to the bottom fifth of the reactor depth. A pure oxygen pressurized cylinder is recommended in order to maintain the specified oxygen concentration. Install a blower (e.g., Diaphragm Type, 15 SCFH capacity) to blow the...
aeration gas into the reactor diffusers. Measure the aeration gas flow rate with a rotameter (e.g., 0-15 SCFH recommended). The aeration gas will rise through the benchtop bioreactor, dissolving oxygen into the mixture in the process. The aeration gas must provide sufficient agitation to keep the solids in suspension. Provide an exit for the aeration gas through the bioreactor closure. Alternatively, wastewater aeration may be provided by introducing the aeration gas into the bleed stream taken from the bioreactor through a water-cooled (e.g., Allihn-type) vertical condenser. Install the condenser through a gas-tight fitting in the bioreactor closure. Install a splitter which directs a portion of the gas to an exit vent and the rest of the gas through an air recycle pump back to the benchtop bioreactor. Monitor and record the flow rate through the exit vent at least 3 times per day throughout the day.

2.1.3 Wastewater Feed. Supply the wastewater to the bioreactor in collapsible low-density polyethylene container or collapsible liner in a container (e.g., 20 L) equipped with a spigot cap (collapsible containers or liners of other material may be required due to the permeability of some volatile compounds through polyethylene). Obtain the wastewater feed by sampling the wastewater feed in the target process. A representative sample of wastewater shall be obtained from the piping leading to the aeration tank. This sample may be obtained from existing sampling valves at the discharge of the wastewater feed pump, or collected from a pipe discharging to the aeration tank, or by pumping from a well-mixed equalization tank upstream from the aeration tank. Alternatively, wastewater can be pumped continuously to the laboratory apparatus from a bleed stream taken from the equalization tank of the full-scale treatment system.

2.1.3.1 Refrigeration System. Keep the wastewater cool by ice or by refrigeration to 4°C. If using a bleed stream from the equalization tank, refrigeration is not required if the residence time in the bleed stream is less than five minutes.

2.1.3.2 Wastewater Feed Pump. The wastewater is pumped from the refrigerated container using a variable-speed peristaltic pump drive equipped with a peristaltic pump head. Add the feed solution to the bioreactor through a fitting on the top flange. Determine the rate of feed addition to provide a retention time in the benchtop bioreactor that is numerically equivalent to the retention time in the full-scale system. The wastewater shall be fed at a rate sufficient to achieve 90 to 100 percent of the full-scale system residence time.

2.1.3.3 Treated Wastewater Feed. The benchtop bioreactor effluent exits at the bottom of the reactor through a tube and proceeds to the clarifier.

2.1.4 Clarifier. The effluent flows to a separate closed clarifier that allows separation of biomass and effluent (e.g., 2-liter pear-shaped glass separatory funnel, modified by removing the stopcock and adding a 25-mm OD glass tube at the bottom). Benchtop bioreactor effluent enters the clarifier through a tube inserted to a depth of 0.08 m (3 in.) through a stopper at the top of the clarifier. System effluent flows from a tube inserted through the stopper at the top of the clarifier to a drain (or sample bottle when sampling). The underflow from the clarifier leaves from the glass tube at the bottom of the clarifier. Flexible tubing connects this fitting to the sludge recycle pump. This pump is coupled to a variable speed pump drive. The discharge from this pump is returned through a tube inserted in a port on the side of the benchtop bioreactor. An additional port is provided near the bottom of the bioreactor for sampling the reactor contents. The mixed liquor from the bioreactor flows into the center of the clarifier. The clarified system effluent separates from the biomass and flows through an exit near the top of the clarifier. There shall be no headspace in the clarifier.

2.1.5 Temperature Control Apparatus. Capable of maintaining the system at a temperature equal to the temperature of the full-scale system. The average temperature should be maintained within ±2°C of the set point.

2.1.5.1 Temperature Monitoring Device. A resistance type temperature probe or a thermocouple connected to a temperature readout with a resolution of 0.1°C or better.

2.1.5.2 Benchtop Bioreactor Heater. The heater is connected to the temperature control device.

2.1.6 Oxygen Control System. Maintain the dissolved oxygen concentration at the levels present in the full-scale system. Target full-scale activated sludge systems with dissolved oxygen concentrations above 2 mg/L are required to maintain the dissolved oxygen concentration in the benchtop bioreactor within 0.5 mg/L of the target dissolved oxygen level. Target full-scale activated sludge systems with dissolved oxygen concentrations below 2 mg/L are required to maintain the dissolved oxygen concentration in the bioreactor within 1.5 mg/L of the target dissolved oxygen concentration. However, target full-scale activated sludge systems with dissolved oxygen concentrations above 2 mg/L, the dissolved oxygen concentration in the benchtop bioreactor may not drop below 1.5 mg/L. If the benchtop bioreactor is outside the control range, the dissolved oxygen is noted and the reactor operation is adjusted.

2.1.6.1 Dissolved Oxygen Monitor. Dissolved oxygen is monitored with a polarographic probe (gas permeable membrane) connected to a dissolved oxygen meter (e.g., 0 to 15 mg/L, 0 to 50°C).
2.1.6.2 Benchtop bioreactor Pressure Monitor. The benchtop bioreactor pressure is monitored through a port in the top flange of the reactor. This is connected to a gauge controlled by an adjustable (3 to 13-cm water vacuum to 13-cm water pressure) relay. A relay is activated when the vacuum exceeds an adjustable setting point which opens a solenoid valve (usually completely closed), admitting oxygen to the system. The vacuum setting controlling oxygen addition to the system shall be set at approximately 2.5 ± 0.5 cm water and maintained at this setting except during brief periods when the dissolved oxygen concentration is adjusted. (Note: Mention of trade names or products does not constitute endorsement by the U.S. Environmental Protection Agency)

2.1.7 Connecting Tubing. All connecting tubing shall be Teflon or equivalent in impermeability. The only exception to this specification is the tubing directly inside the pump head of the wastewater feed pump, which may be Viton, Silicone or another type of flexible tubing.

2.2 Analysis. If the identity of the compounds of interest in the wastewater is not known, a representative sample of the wastewater shall be analyzed in order to identify all of the compounds of interest present. A gas chromatography/mass spectrometry screening method is recommended.

2.2.1 After identifying the compounds of interest in the wastewater, develop and/or use one or more analytical techniques capable of measuring each of those compounds (more than one analytical technique may be required, depending on the characteristics of the wastewater). Test Method 18, found in Appendix A of 40 CFR Part 60, may be used as a guideline in developing the analytical technique. Purge and trap techniques may be used for analysis providing the target compounds are sufficiently volatile to make this technique appropriate. The limit of quantitation for each compound shall be determined. If the effluent concentration of any target compound is below the limit of quantitation determined for that compound, the operation of the Method 304 unit may be altered to attempt to increase the effluent concentration above the limit of quantitation. Modifications to the method shall be approved prior to the test. The request should be addressed to Method 304 contact, Emissions Measurement Center, Mail Drop 19, U.S. Environmental Protection Agency, Research Triangle Park, NC 27711.

2.2.2 Calibration Standards. Prepare calibration standards from pure certified standards in an aqueous medium. Prepare and analyze three concentrations of calibration standards for each target component (or for a mixture of components) in triplicate daily throughout the analyses of the test samples. At each concentration level, a single calibration shall be within 5 percent of the average of the three calibration results. The low and medium calibration standards shall bracket the expected concentration of the effluent (treated) wastewater. The medium and high standards shall bracket the expected influent concentration.

3. Reagents

3.1 Wastewater. Obtain a representative sample of wastewater at the inlet to the full-scale treatment plant if there is an existing full-scale treatment plant (see section 2.1.3). If there is no existing full-scale treatment plant, obtain the wastewater sample as close to the point of determination as possible. Collect the sample by pumping the wastewater into the 20-L collapsible container. The loss of volatiles shall be minimized from the wastewater by collapsing the container before filling, by minimizing the time of filling, and by avoiding a headspace in the container after filling. If the wastewater requires the addition of nutrients to support the biomass growth and maintain biomass characteristics, those nutrients are added and mixed with the container contents after the container is filled.

3.2 Biomass. Obtain the biomass or activated sludge used for rate constant determination in the bench-scale process from the existing full-scale process or from a representative biomass culture (e.g., biomass that has been developed for a future full-scale process). This biomass is preferentially obtained from a thickened acclimated mixed liquor sample. Collect the sample either by bailing from the mixed liquor in the aeration tank with a weighted container, or by collecting aeration tank effluent at the effluent overflow weir. Transport the sample to the laboratory within no more than 4 hours of collection. Maintain the biomass concentration in the benchtop bioreactor at the level of the full-scale system ±10 percent throughout the sampling period of the test method.

4. Procedure. Safety Note: If explosive gases are produced, be aware of the potential for exposure to the explosive gases and avoid breathing the gas. Avoid the risk of fire or explosion by using proper techniques and equipment and by avoiding the presence of an ignitable source. If an incendiary explosion occurs, use a fire extinguisher to control the fire. Use a fire extinguisher to control the fire. Do not use water as it will change the explosive properties of the gas. Use a fire extinguisher to control the fire. Use a fire extinguisher to control the fire.

4.1 Benchtop Bioreactor Operation. Charge the mixed liquor to the benchtop bioreactor, minimizing headspace over the liquid surface to minimize entrainment of mixed liquor in the circulating gas. Fasten the benchtop bioreactor headplate to the reactor over the liquid surface. Maintain the temperature of the contents of the benchtop bioreactor system at the temperature of the target full-scale system, +2°C. Throughout the testing period, Monitor and record the temperature of the benchtop bioreactor contents at least to the nearest 0.1°C. 
4.1 Wastewater Storage. Collect the wastewater sample in the 20-L collapsible container. Store the container at 4 °C throughout the testing period. Connect the container to the benchtop bioreactor feed pump.

4.1.2 Wastewater Flow Rate. The hydraulic residence time of the aeration tank is calculated as the ratio of the volume of the tank (L) to the flow rate (L/min). At the beginning of a test, the container shall be connected to the feed pump and solution shall be pumped continuously from the benchtop bioreactor at the required flow rate to achieve the calculated hydraulic residence time of wastewater in the aeration tank.

\[ Q_{\text{test}} = \frac{Q_{fs} \cdot L}{V_{fs}} \]

Where:
- \( Q_{\text{test}} \) = wastewater flow rate (L/min)
- \( Q_{fs} \) = average flow rate of full-scale process (L/min)
- \( V_{fs} \) = volume of full-scale aeration tank (L)

The target flow rate in the test apparatus is the same as the flow rate in the target full-scale process multiplied by the ratio of benchtop bioreactor volume (e.g., 6 L) to the volume of the full-scale aeration tank. The hydraulic residence time shall be maintained at 90 to 100 percent of the residence time maintained in the full-scale unit. A nominal flow rate is set on the pump based on a pump calibration. Changes in the elasticity of the tubing in the pump head and the accumulation of material in the tubing affect this calibration. The nominal pumping rate shall be changed as necessary based on volumetric flow measurements. Discharge the benchtop bioreactor influent to a wastewater storage, treatment, or disposal facility, except during sampling or flow measurement periods.

4.1.3 Sludge Recycle Rate. Set the sludge recycle rate at a rate sufficient to prevent accumulation in the bottom of the clarifier. Set the air circulation rate sufficient to maintain the biomass in suspension.

4.1.4 Benchtop Bioreactor Operation and Maintenance. Temperature, dissolved oxygen concentration, exit vent flow rate, benchtop bioreactor effluent flow rate, and air circulation rate shall be measured and recorded three times throughout each day of benchtop bioreactor operation. If other parameters (such as pH) are measured and maintained in the target full-scale unit, these parameters, where appropriate, shall be monitored and maintained to target full-scale specifications in the benchtop bioreactor. At the beginning of each sampling period (section 4.2), sample the benchtop bioreactor contents for suspended solids analysis. Take this sample by loosening a clamp on a length of tubing attached to the lower side port. Determine the suspended solids gravimetrically by the Gooch crucible/glass fiber filter method for total suspended solids, in accordance with Standard Methods or equivalent. When necessary, sludge shall be wasted from the lower side port of the benchtop bioreactor. The volume that is wasted shall be replaced with an equal volume of the reactor effluent. Add thickened activated sludge mixed liquor as necessary to the benchtop bioreactor to increase the suspended solids concentration to the desired level. Pump this mixed liquor to the benchtop bioreactor through the upper side port (Item 24 in Figure 3). Change the membrane on the dissolved oxygen probe before starting the test. Calibrate the oxygen probe immediately before the start of the test and each time the membrane is changed.

4.1.5 Inspection and Correction Procedures. If the feed line tubing becomes clogged, replace with new tubing. If the feed flow rate is not within 5 percent of target flow any time the flow rate is measured, reset pump or check the flow measuring device and measure flow rate again until target flow rate is achieved.

4.2 Test Sampling. At least two and one half hydraulic residence times after the system has reached the targeted specifications shall be permitted to elapse before the first sample is taken. Effluent samples of the clarifier discharge (Item 20 in Figure 3) and the influent wastewater feed are collected in 40-mL septum vials to which two drops of 1:10 hydrochloric acid (HCl) in water have been added. Sample the clarifier discharge directly from the drain line. These samples will be composed of the entire flow from the system for a period of several minutes. Feed samples shall be taken from the feed pump suction line after temporarily stopping the benchtop bioreactor feed, removing a connector, and squeezing the collapsible feed container. Store both influent and effluent samples at 4 °C immediately after collection and analyze within 8 hours of collection.

4.2.1 Frequency of Sampling. During the test, sample and analyze the wastewater feed and the clarifier effluent at least six times. The sampling intervals shall be separated by at least 8 hours. During any individual sampling interval, sample the wastewater feed and the clarifier effluent simultaneously with or immediately after the effluent sample. Calculate the relative standard deviation (RSD) of the amount removed (i.e., effluent concentration—wastewater feed concentration). The RSD values shall be < 15 percent. If an RSD value is > 15 percent, continue sampling and analyzing influent and effluent sets of samples until the RSD values are within specifications.

4.2.2 Sampling After Exposure of System to Atmosphere. If, after starting sampling procedures, the benchtop bioreactor system is exposed to the atmosphere (due to leaks, maintenance, etc.), allow at least one hydraulic residence time to elapse before resuming sampling.
5. Operational Checks and Calibration

5.1 Dissolved Oxygen. Fluctuation in dissolved oxygen concentration may occur for numerous reasons, including undetected gas leaks, increases and decreases in mixed liquor suspended solids resulting from cell growth and solids loss in the effluent stream, changes in diffuser performance, cycling of effluent flow rate, and overcorrection due to faulty or sluggish dissolved oxygen probe response. Control the dissolved oxygen concentration in the benchtop bioreactor by changing the proportion of oxygen in the circulating aeration gas. Should the dissolved oxygen concentration drift below the designated experimental condition, bleed a small amount of aeration gas from the system on the pressure side (i.e., immediately upstream of one of the diffusers). This will create a vacuum in the system, triggering the pressure sensitive relay to open the solenoid valve and admit oxygen to the system. Should the dissolved oxygen concentration drift above the designated experimental condition, slow or stop the oxygen input to the system until the dissolved oxygen concentration approaches the correct level.

5.2 Sludge Wasting. Determine the suspended solids concentration (section 4.1.4) at the beginning of a test, and once per day thereafter during the test. If the test is completed within a two day period, determine the suspended solids concentration after the final sample set is taken. If the suspended solids concentration exceeds the specified concentration, remove a fraction of the sludge from the benchtop bioreactor. The required volume of mixed liquor to remove is determined as follows:

\[ V_w = V_r \left( \frac{S_s - S_m}{S_s} \right) \]  
Eqn 304A-2

Where:
- \( V_w \) is the wasted volume (Liters),
- \( V_r \) is the volume of the benchtop bioreactor (Liters),
- \( S_s \) is the measured solids (g/L), and
- \( S_m \) is the specified solids (g/L).

Remove the mixed liquor from the benchtop bioreactor by loosening a clamp on the mixed liquor sampling tube and allowing the required volume to drain to a graduated flask. Clamp the tube when the correct volume has been wasted. Replace the volume of the liquid wasted by pouring the same volume of effluent back into the benchtop bioreactor. Dispose of the waste sludge properly.

5.3 Sludge Makeup. In the event that the suspended solids concentration is lower than the specifications, add makeup sludge back into the benchtop bioreactor. Determine the amount of sludge added by the following equation:

\[ V_w = V_r \left( \frac{S_s - S_m}{S_w} \right) \]  
Eqn 304A-3

Where:
- \( V_w \) is the volume of sludge to add (Liters),
- \( V_r \) is the volume of the benchtop bioreactor (Liters),
- \( S_w \) is the solids in the makeup sludge (g/L),
- \( S_m \) is the measured solids (g/L), and
- \( S_s \) is the specified solids (g/L).

5.4 Wastewater Pump Calibration. Determine the wastewater flow rate by collecting the system effluent for a time period of at least one hour, and measuring the volume with a graduated cylinder. Record the collection time period and volume collected. Determine flow rate. Adjust the pump speed to deliver the specified flow rate.

6. Calculations

6.1 Nomenclature. The following symbols are used in the calculations.

- \( C_i \): Average inlet feed concentration for a compound of interest, as analyzed (mg/L)
- \( C_o \): Average outlet (effluent) concentration for a compound of interest, as analyzed (mg/L)
- \( X \): Biomass concentration, mixed liquor suspended solids (g/L)
- \( t \): Hydraulic residence time in the benchtop bioreactor (hours)
- \( V \): Volume of the benchtop bioreactor (L)
- \( Q \): Flow rate of wastewater into the benchtop bioreactor, average (L/hour)

6.2 Residence Time. The hydraulic residence time of the benchtop bioreactor is equal to the ratio of the volume of the benchtop bioreactor \((L)\) to the flow rate \((L/h)\)

\[ t = \frac{V}{Q} \]  
Eqn 304A-4

6.3 Rate of Biodegradation. Calculate the rate of biodegradation for each component with the following equation:

\[ \text{Rate} = \frac{\left( \frac{\text{mg}}{L-h} \right)}{t} = \frac{C_i - C_o}{t} \]  
Eqn 304A-5
6.4 First-Order Biorate Constant. Calculate the first-order biorate constant ($K_1$) for each component with the following equation:

$$K_1 \left( \frac{L}{g-h} \right) = \frac{C_t - C_e}{t C_e X}$$

Eqn 304A-6

6.5 Relative Standard Deviation (RSD). Determine the standard deviation of both the influent and effluent sample concentrations ($S$) using the following equation:

$$RSD = \frac{100}{S} \left( \frac{\sum (S_i - \bar{S})^2}{(n-1)} \right)^{1/2}$$

Eqn 304A-7

6.6 Determination of Percent Air Emissions and Percent Biodegraded. Use the results from this test method and follow the applicable procedures in appendix C of 40 CFR part 63, entitled "Determination of the Fraction Biodegraded ($F_{bio}$) in a Biological Treatment Unit" to determine $F_{bio}$.

7. Bibliography

2. Test Method 18, 40 CFR part 60, appendix A.

METHOD 304B: DETERMINATION OF BIO-DEGRADATION RATES OF ORGANIC COMPOUNDS (SCRUBBER OPTION)

1. Applicability and Principle

1.1 Applicability. This method is applicable for the determination of biodegradation rates of organic compounds in an activated sludge process. The test method is designed to evaluate the ability of an aerobic biological reaction system to degrade or destroy specific components in waste streams. The method may also be used to determine the effects of changes in wastewater composition on operation. The biodegradation rates determined by utilizing this method are not representative of a full-scale system. Full-scale systems embody biodegradation and air emissions in competing reactions. This method measures biodegradation in absence of air emissions. The rates measured by this method shall be used in conjunction with the procedures listed in appendix C of this part to calculate the fraction emitted to the air versus the fraction biodegraded.

1.2 Principle. A self-contained benchtop bioreactor system is assembled in the laboratory. A sample of mixed liquor is added and the waste stream is then fed continuously. The benchtop bioreactor is operated under conditions nearly identical to the target full-scale activated sludge process, except that air emissions are not a factor. The benchtop bioreactor temperature, dissolved oxygen concentration, average residence time in the reactor, waste composition, biomass concentration, and biomass composition of the target full-scale process are the parameters which are duplicated in the laboratory system. Biomass shall be removed from the target full-scale activated sludge unit and held for no more than 4 hours prior to use in the benchtop bioreactor. If antifoaming agents are used in the full-scale system, they shall also be used in the benchtop bioreactor. If the feed flowing into and the effluent exiting the benchtop bioreactor are analyzed to determine the biodegradation rates of the target compounds. The choice of analytical methodology for measuring the compounds of interest at the inlet and outlet to the benchtop bioreactor are left to the discretion of the source, except where validated methods are available.

2. Apparatus

Figure 1 illustrates a typical laboratory apparatus used to measure biodegradation rates. While the following description refers to Figure 1, the EPA recognizes that alternative reactor configurations, such as alternative reactor shapes and locations of probes and the feed inlet, will also meet the intent of this method. Ensure that the benchtop
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A bioreactor system is self-contained and isolated from the atmosphere by leak-checking fittings, tubing, etc.
2.1 Laboratory apparatus.

2.1.1 Benchtop Bioreactor. The biological reaction is conducted in a biological oxidation reactor of at least 6 liters capacity. The reactor may be equipped with internal probes for controlling and monitoring dissolved oxygen and internal temperature. The top of the benchtop bioreactor is provided with aeration ports, a gas metering device, and instrumentation (while ensuring that no leaks to the atmosphere exist around the fittings).

2.1.2 Aeration gas. Aeration gas is added to the benchtop bioreactor through three diffusers, which are glass tubes that extend to the bottom fifth of the reactor depth. A pure oxygen pressurized cylinder is recommended in order to maintain the specified oxygen concentration. Install a blower (e.g., Diaphram Type, 15 SCFH capacity) to blow the aeration gas into the benchtop bioreactor diffusers. Measure the aeration gas flow rate with a rotameter (e.g., 0-15 SCFH recommended). The aeration gas will rise through the benchtop bioreactor, dissolving oxygen into the mixture in the process. The aeration gas must provide sufficient agitation to keep the solids in suspension. Provide an exit for the aeration gas from the top flange of the benchtop bioreactor through a water-cooled (e.g., Allihn-type) vertical condenser. Install the condenser through a gas-tight fitting in the benchtop bioreactor closure. Design the system so that at least 10 percent of the gas flows through an alkaline scrubber containing 175 mL of 45 percent by weight solution of potassium hydroxide (KOH) and 5 drops of 0.2 percent alizarin yellow dye. Route the balance of the gas through an adjustable scrubber bypass. Route all of the gas through a 1-L knock-out flask to remove entrained moisture and then through the condenser to the gas-to the benchtop bioreactor.

2.1.3 Wastewater Feed. Supply the wastewater feed to the benchtop bioreactor in a collapsible low-density polyethylene container or collapsible liner in a container (e.g., 20 L) equipped with a spigot cap (collapsible containers or liners of other material may be required due to the permeability of some volatile compounds through polyethylene). Obtain the wastewater feed by sampling the wastewater feed in the target process. A representative sample of wastewater shall be obtained from the piping leading to the aeration tank. This sample may be obtained from existing sampling valves at the discharge of the wastewater feed pump, or collected from a pipe discharging to the aeration tank, or by pumping from a well-mixed equalization tank upstream from the aeration tank. Alternatively, wastewater can be pumped continuously to the laboratory apparatus from a bleed stream taken from the equalization tank of the full-scale treatment system.

2.1.3.1 Refrigeration System. Keep the wastewater feed cool by ice or by refrigeration to 4°C. If using a bleed stream from the equalization tank, refrigeration is not required if the residence time in the bleed stream is less than five minutes.

2.1.3.2 Wastewater Feed Pump. The wastewater is pumped from the refrigerated container using a variable-speed peristaltic pump drive equipped with a peristaltic pump head. Add the feed solution to the benchtop bioreactor through a fitting on the top flange. Determine the rate of feed addition to provide a retention time in the benchtop bioreactor that is numerically equivalent to the retention time in the target full-scale system. The wastewater shall be fed at a rate sufficient to achieve 90 to 100 percent of the target full-scale system residence time.

2.1.3.3 Treated wastewater feed. The benchtop bioreactor effluent exits at the bottom of the reactor through a tube and proceeds to the clarifier.

2.1.4 Clarifier. The effluent flows to a separate closed clarifier that allows separation of biomass and effluent (e.g., 2-liter pear-shaped glass separatory funnel, modified by removing the stopcock and adding a 25-mm OD glass tube at the bottom). Benchtop bioreactor effluent enters the clarifier through a tube inserted to a depth of 0.08 m (3 in.) through a stopper at the top of the clarifier. System effluent flows from a tube inserted through the stopper at the top of the clarifier to a drain (or sample bottle when sampling). The underflow from the clarifier leaves from the glass tube at the bottom of the clarifier. Flexible tubing connects this fitting to the sludge recycle pump. This pump is coupled to a variable speed pump drive. The discharge from this pump is returned through a tube inserted in a port on the side of the benchtop bioreactor. An additional port is provided near the bottom of the benchtop bioreactor for sampling the reactor contents. The mixed liquor from the benchtop bioreactor flows into the center of the clarifier. The clarified system effluent separates from the biomass and flows through an exit near the top of the clarifier. There shall be no headspace in the clarifier.

2.1.5 Temperature Control Apparatus. Capable of maintaining the system at a temperature equal to the temperature of the full-scale system. The average temperature should be maintained within ±2°C of the set point.

2.1.5.1 Temperature Monitoring Device. A resistance type temperature probe or a thermocouple connected to a temperature read-out with a resolution of 0.1°C or better.

2.1.5.2 Benchtop Bioreactor Heater. The heater is connected to the temperature control device.

2.1.6 Oxygen Control System. Maintain the dissolved oxygen concentration at the levels present in the full-scale system. Target full-
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scale activated sludge systems with dissolved oxygen concentration below 2 mg/L are required to maintain the dissolved oxygen concentration in the benchtop bioreactor within 1.5 mg/L of the target dissolved oxygen concentration; however, for target full-scale activated sludge systems with dissolved oxygen concentrations above 2 mg/L, the dissolved oxygen concentration in the benchtop bioreactor may be set below 1.5 mg/L. If the benchtop bioreactor is outside the control range, the dissolved oxygen is noted and the reactor operation is adjusted.

2.1.6.1 Dissolved Oxygen Monitor. Dissolved oxygen is monitored with a polarographic probe (gas permeable membrane) connected to a dissolved oxygen meter (e.g., 0 to 15 mg/L, 0 to 50°C).

2.1.6.2 Benchtop Bioreactor Pressure Monitor. The benchtop bioreactor pressure is monitored through a port in the top flange of the reactor. This is connected to a gauge control with a span of 13-cm water vacuum to 13-cm water pressure or better. A relay is activated when the vacuum exceeds an adjustable setpoint which opens a solenoid valve (normally closed), admitting oxygen to the system. The vacuum setpoint controlling oxygen addition to the system shall be set at approximately 2.5 ± 0.5 cm water and maintained at this setting except during brief periods when the dissolved oxygen concentration is adjusted.

2.1.7 Connecting Tubing. All connecting tubing shall be Teflon or equivalent in impermeability. The only exception to this specification is the tubing directly inside the pump head of the wastewater feed pump, which may be Viton, Silicone or another type of flexible tubing. Note: Mention of trade names or products does not constitute endorsement by the U.S. Environmental Protection Agency.

2.2 Analysis. If the identity of the compounds of interest in the wastewater is not known, a representative sample of the wastewater shall be analyzed in order to identify all of the compounds of interest present. A gas chromatography/mass spectrometry screening method is recommended.

2.2.1 After identifying the compounds of interest in the wastewater, develop and/or use one or more analytical technique capable of measuring each of those compounds (more than one analytical method may be required, depending on the characteristics of the wastewater). Method 18, found in appendix A of 40 CFR part 60, may be used as a guideline in developing the analytical technique. Purge and trap techniques may be used for analysis providing the target components are sufficiently volatile to make this technique appropriate. The limit of quantitation for each compound shall be determined. If the effluent concentration of any target compound is below the limit of quantitation determined for that compound, the operation of the Method 304 unit may be altered to attempt to increase the effluent concentration above the limit of quantitation. Modifications to the method shall be approved prior to the test. The request should be addressed to Method 304 contact, Emissions Measurement Center, Mail Drop 19, U.S. Environmental Protection Agency, Research Triangle Park, NC 27711.

2.2.2 Calibration Standards. Prepare calibration standards from pure certified standards in an aqueous medium. Prepare and analyze three concentrations of calibration standards for each target component (or for a mixture of components) in triplicate daily throughout the analyses of the test samples. At each concentration level, a single calibration shall be within 5 percent of the average of the three calibration results. The low and medium calibration standards shall bracket the expected concentration of the effluent (treated) wastewater. The medium and high standards shall bracket the expected influent concentration.

3. Reagents

3.1 Wastewater. Obtain a representative sample of wastewater at the inlet to the full-scale treatment plant and/or wastewater from the benchtop bioreactor if there is an existing full-scale treatment plant (See Section 2.1.3). If there is no existing full-scale treatment plant, obtain the wastewater sample as close to the point of determination as possible.

Collect the sample by pumping the wastewater into the 20-L collapsible container. The loss of volatiles should be minimized from the wastewater by collapsing the container before filling, by minimizing the time of filling, and by avoiding a headspace in the container after filling. If the wastewater requires the addition of nutrients to support the biomass growth and maintain biomass characteristics, those nutrients are added and mixed with the container contents after the container is filled.

3.2 Biomass. Obtain the biomass or activated sludge used for rate constant determination in the bench-scale process from the existing full-scale process or from a representative biomass culture (e.g., biomass that has been developed for a future full-scale process). This biomass is preferentially obtained from a thickened acclimated mixed liquor sample. Collect the sample either by bailing from the mixed liquor in the aeration tank with a weighted container, or by collecting aeration tank effluent at the effluent overflow weir. Transport the sample to the laboratory within no more than 4 hours of
collection. Maintain the biomass concentration in the benchtop bioreactor at the level of the target full-scale system +10 percent throughout the sampling period of the test method.

4. Procedure

Safety Note: If explosive gases are produced as a byproduct of biodegradation and could realistically pose a hazard, closely monitor headspace concentration of these gases to ensure laboratory safety. Placement of the benchtop bioreactor system inside a laboratory hood is recommended regardless of byproducts produced.

4.1 Benchtop Bioreactor Operation. Charge the mixed liquor to the benchtop bioreactor, minimizing headspace over the liquid surface to minimize entrainment of mixed liquor in the circulating gas. Fasten the benchtop bioreactor headplate to the reactor over the liquid surface. Maintain the temperature of the contents of the benchtop bioreactor system at the temperature of the target full-scale system, +2 °C, throughout the testing period. Monitor and record the temperature of the reactor contents at least to the nearest 0.1 °C.

4.1.1 Wastewater Storage. Collect the wastewater sample in the 20-L collapsible container. Store the container at 4 °C throughout the testing period. Connect the container to the benchtop bioreactor feed pump.

4.1.2 Wastewater Flow Rate. The hydraulic residence time of the aeration tank is calculated as the ratio of the volume of the tank (L) to the flow rate (L/min). At the beginning of a test, the container shall be connected to the feed pump and solution shall be pumped to the benchtop bioreactor at the required flow rate to achieve the calculated hydraulic residence time of wastewater in the aeration tank.

\[ Q_{test} = \frac{Q_{fs}}{V_{fs}} \]  

Eqn 304B-1

Where:
- \( Q_{waste} \) = wastewater flow rate (L/min)
- \( Q_{fs} \) = average flow rate of full-scale process (L/min)
- \( V_{fs} \) = volume of full-scale aeration tank (L)

The target flow rate in the test apparatus is the same as the flow rate in the target full-scale process multiplied by the ratio of benchtop bioreactor volume (e.g., 6 L) to the volume of the full-scale aeration tank. The hydraulic residence time shall be maintained at 90 to 100 percent of the residence time maintained in the target full-scale unit. A nominal flow rate is set on the pump based on a pump calibration. Changes in the elasticity of the tubing in the pump head and the accumulation of material in the tubing affect this calibration. The nominal pumping rate shall be changed as necessary based on volumetric flow measurements. Discharge the benchtop bioreactor effluent to a wastewater storage, treatment, or disposal facility, except during sampling or flow measurement periods.

4.1.3 Sludge Recycle Rate. Set the sludge recycle rate at a rate sufficient to prevent accumulation in the bottom of the clarifier. Set the air circulation rate sufficient to maintain the biomass in suspension.

4.1.4 Benchtop Bioreactor Operation and Maintenance. Temperature, dissolved oxygen concentration, flow rate, and air circulation rate shall be measured and recorded three times throughout each day of testing. If other parameters (such as pH) are measured and maintained in the target full-scale unit, these parameters shall, where appropriate, be monitored and maintained to full-scale specifications in the benchtop bioreactor. At the beginning of each sampling period (section 4.2), sample the benchtop bioreactor contents for suspended solids analysis. Take this sample by loosening a clamp on a length of tubing attached to the lower side port. Determine the suspended solids gravimetrically by the Gooch crucible/glass fiber filter method for total suspended solids, in accordance with Standard Methods or equivalent. When necessary, sludge shall be wasted from the lower side port of the benchtop bioreactor, and the volume that is wasted shall be replaced with an equal volume of the benchtop bioreactor effluent. Add thickened activated sludge mixed liquor as necessary to the benchtop bioreactor to increase the suspended solids concentration to the desired level. Pump this mixed liquor to the benchtop bioreactor through the upper side port (Item 24 in Figure 1). Change the membrane on the dissolved oxygen probe before starting the test. Calibrate the oxygen probe immediately before the start of the test and each time the membrane is changed. The scrubber solution shall be replaced each weekday with 175 mL 45 percent W/W KOH solution to which five drops of 0.2 percent alizarin yellow indicator in water have been added. The potassium hydroxide solution in the alkaline scrubber shall be changed if the alizarin yellow dye color changes.

4.1.5 Inspection and Correction Procedures. If the fail line tubing becomes clogged, replace with new tubing. If the feed flow rate is not within 5 percent of target flow, the flow rate is measured, reset pump or check flow measuring device and measure flow rate again until target flow rate is achieved.

4.2 Test Sampling. At least two and one-half hydraulic residence times after the system has reached the targeted specifications shall be permitted to elapse before the first sample is taken. Effluent samples of the clarifier discharge (Item 20 in Figure 1) and the influent wastewater feed are collected in 40 mL
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Dissolved Oxygen

5.1 Dissolved Oxygen. Fluctuation in dissolved oxygen concentration may occur for numerous reasons, including undetected gas leaks, increases and decreases in mixed liquor suspended solids resulting from cell growth and solids loss in the effluent stream, changes in diffuser performance, cycling of effluent flow rate, and overcorrection due to faulty or sluggish dissolved oxygen probe response. Control the dissolved oxygen concentration in the benchtop bioreactor by changing the proportion of oxygen in the circulating aeration gas. Should the dissolved oxygen concentration drift below the designated experimental condition, bleed a small amount of aeration gas from the system on the pressure side (i.e., immediately upstream of one of the diffusers). This will create a vacuum in the system, triggering the pressure sensitive relay to open the solenoid valve and admit oxygen to the system. Should the dissolved oxygen concentration drift above the designated experimental condition, slow or stop the oxygen input to the system until the dissolved oxygen concentration approaches the correct level.

5.2 Sludge Wasting. Determine the suspended solids concentration (section 4.1.4) at the beginning of a test, and once per day thereafter during the test. If the test is completed within a two day period, determine the suspended solids concentration after the final sample set is taken. If the suspended solids concentration exceeds the specified concentration, remove a fraction of the sludge from the benchtop bioreactor. The required volume of mixed liquor to remove is determined as follows:

\[ V_w = V_r \left( \frac{S_m - S_s}{S_m} \right) \]  \hspace{1cm} Eqn 304B - 2

Where:
- \( V_w \) is the wasted volume (Liters),
- \( V_r \) is the volume of the benchtop bioreactor (Liters),
- \( S_m \) is the measured solids (g/L), and
- \( S_s \) is the specified solids (g/L).

Remove the mixed liquor from the benchtop bioreactor by loosening a clamp on the mixed liquor sampling tube and allowing the required volume to drain to a graduated flask. Clamp the tube when the correct volume has been wasted. Replace the volume of the liquid wasted by pouring the same volume of effluent back into the benchtop bioreactor. Dispose of the waste sludge properly.

5.3 Sludge Makeup. In the event that the suspended solids concentration is lower than the specifications, add makeup sludge back into the benchtop bioreactor. Determine the amount of sludge added by the following equation:

\[ V_w = V_r \left( \frac{S_s - S_m}{S_w} \right) \]  \hspace{1cm} Eqn 304B - 3

Where:
- \( V_w \) is the volume of sludge to add (Liters),
- \( V_r \) is the volume of the benchtop bioreactor (Liters),
- \( S_m \) is the solids in the makeup sludge (g/L),
- \( S_w \) is the measured solids (g/L), and
- \( S_s \) is the specified solids (g/L).

5.4 Wastewater Pump Calibration. Determine the wastewater flow rate by collecting the system effluent for a time period of at least one hour, and measuring the volume collected. Determine flow rate. Adjust the pump speed to deliver the specified flow rate.

6. Calculations

6.1 Nomenclature. The following symbols are used in the calculations.
- \( C_i \) = Average inlet feed concentration for a compound of interest, as analyzed (mg/L)
- \( C_o \) = Average outlet (effluent) concentration for a compound of interest, as analyzed (mg/L)

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Residence Time. The hydraulic residence time of the benchtop bioreactor is equal to the ratio of the volume of the benchtop bioreactor (L) to the flow rate (L/h):

\[ t = \frac{V}{Q} \quad \text{Eqn 304B-4} \]

Rate of Biodegradation. Calculate the rate of biodegradation for each component with the following equation:

\[ \text{Rate} = \frac{C_i - C_o}{t} \quad \text{Eqn 304B-5} \]

First-Order Biorate Constant. Calculate the first-order biorate constant \( K_1 \) for each component with the following equation:

\[ K_1 = \frac{C_i - C_o}{t C_o X} \quad \text{Eqn 304B-6} \]

Relative Standard Deviation (RSD). Determine the standard deviation of both the influent and effluent sample concentrations \( S \) using the following equation:

\[ \text{RSD} = \frac{100}{S} \left( \sum_{i=1}^{n} \left( \frac{S_i - S}{S} \right)^2 \right)^{1/2} \quad \text{Eqn 304B-7} \]

Determination of Percent Air Emissions and Percent Biodegraded. Use the results from this test method and follow the applicable procedures in appendix C of 40 CFR part 63, entitled “Determination of the Fraction Biodegraded (\( F_{bio} \)) in a Biological Treatment Unit” to determine \( F_{bio} \).

7. Bibliography

2. Test Method 18, 40 CFR part 60, Appendix A.

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2.1.1 Purge Chamber. The purge chamber shall accommodate the 10-g sample of waste suspended in a matrix of 50 mL of PEG and 50 mL of deionized, hydrocarbon-free water. Three fittings are used on the glass chamber top. Two #7 Ace-threads are used for the purge gas inlet and outlet connections. A #50 Ace-thread is used to connect the top of the chamber to the base (see Figure 1). The base of the chamber has a side-arm equipped with a #22 Sovirel fitting to allow for easy sample introductions into the chamber. The dimensions of the chamber are shown in Figure 1.

2.1.2 Flow Distribution Device (FDD). The FDD enhances the gas-to-liquid contact for improved purging efficiency. The FDD is a 6 mm OD by 30 cm long glass tube equipped with four arm bubblers as shown in Figure 1. Each arm shall have an opening of 1 mm in diameter.

2.1.3 Coalescing Filter. The coalescing filter serves to discourage aerosol formation of sample gas once it leaves the purge chamber. The glass filter has a fritted disc mounted 10 cm from the bottom. Two #7 Ace-threads are used for the inlet and outlet connections. The dimensions of the chamber are shown in Figure 2.

2.1.4 Oven. A forced convection airflow oven capable of maintaining the purge chamber and coalescing filter at 75 ± 2°C.

2.1.5 Toggle Valve. An on/off valve constructed from brass or stainless steel rated to 100 psig. This valve is placed in line between the purge nitrogen source and the flow controller.
Figure 1. Schematic of Purge Chamber
2.1.6 Flow Controller. High-quality stainless steel flow controller capable of restricting a flow of nitrogen to 6.00.06 L/min at 40 psig.

2.1.7 Polyethylene Glycol Cleaning System.
2.1.7.1 Round-Bottom Flask. One liter, three-neck glass round-bottom flask for cleaning PEG. Standard taper 24/40 joints are mounted on each neck.
2.1.7.2 Heating Mantle. Capable of heating contents of the 1-L flask to 120°C.
2.1.7.3 Nitrogen Bubbler. Teflon or glass tube, 0.25 in. OD.
2.1.7.4 Thermometer. Partial immersion glass thermometer.

2.1.8 Reagents.
2.1.8.1 Polyethylene Glycol. Ninety-eight percent pure organic polymer with an average molecular weight of 400. Volatile organics are removed from the PEG prior to use by heating to 120±5°C and purging with pure nitrogen at 1 L/min for 2 hours. The PEG is stored at room temperature under a nitrogen purge maintained at 1 L/min until used. A typical apparatus used to clean the PEG is shown in Figure 3.
2.1.8.2 Water. Organic-free deionized water is required.

Figure 2. Schematic of Coalescing Filter
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2.1.8.3 Nitrogen. High-purity nitrogen (less than 0.5 ppm total hydrocarbons) is used to remove test compounds from the purge matrix. The source of nitrogen shall be regulated continuously to 40 psig before the on/off toggle valve.

2.2 Volatile Organic Recovery System.

2.2.1 Splitter Valve (Optional). Stainless steel cross-pattern valve capable of splitting nominal flow rates from the purge flow of 6 L/min. The valve shall be maintained at 75±2°C in the heated zone and shall be placed downstream of the coalescing filter. It is recommended that 0.125 in. OD tubing be used to direct the split vent flow from the heated zone. The back pressure caused by the 0.125 in. OD tubing is critical for maintaining proper split valve operation. Note: The splitter valve design is optional; it may be used in cases where the concentration of a pollutant would saturate the adsorbents.

2.2.2 Injection Port. Stainless steel 1/4 in. OD compression fitting tee with a 6-mm septum fixed on the top port. The injection port is the point of entry for the recovery study solution. If using a gaseous standard to determine recovery efficiency, connect the gaseous standard to the injection port of the tee.

2.2.3 Knockout Trap (Optional but Recommended). A 25-mL capacity glass reservoir body with a full-stem impinger (to avoid leaks, a modified midget glass impinger with a screw cap and ball/socket clamps on the inlet and outlet is recommended). The empty impinger is placed in an ice water bath between the injection port and the sorbent cartridge. Its purpose is to reduce the water content of the purge gas (saturated at 75°C) before the sorbent cartridge.
2.2.4 Insulated Ice Bath. A 350-mL dewar or other type of insulated bath is used to maintain ice water around the knockout trap.

2.2.5 Sorbent Cartridges. Commercially available glass or stainless steel cartridge packed with one or more appropriate sorbents. The amount of adsorbent packed in the cartridge depends on the breakthrough volume of the test compound but is limited by back pressure caused by the packing (not to exceed 7 psig). More than one sorbent cartridge placed in series may be necessary depending upon the mixture of the measured components.

2.2.6 Volumetric Glassware. Type A glass 10-mL volumetric flasks for measuring a final volume from the water catch in the knockout trap.

2.2.7 Thermal Desorption Unit. A clamshell type oven, used for the desorption of direct thermal desorption sorbent tubes. The oven shall be capable of increasing the temperature of the desorption tubes rapidly to recommended desorption temperature.

2.2.8 Ultrasonic Bath. Small bath used to agitate sorbent material and desorption solvent. Ice water shall be used in the bath because of heat transfer caused by operation of the bath.

2.2.9 Desorption Vials. Four-dram (15-mL) capacity borosilicate glass vials with Teflon-lined caps.

2.2.10 Reagents.
2.2.10.1 Water. Same as specified in Section 2.1.8.2.
2.2.10.2 Desorption Solvent (when used). Appropriate high-purity (99.99 percent) solvent for desorption shall be used. Analysis shall be performed (utilizing the same analytical technique as that used in the analysis of the waste samples) on each lot to determine purity.

2.3 Analytical System. A gas chromatograph (GC) is commonly used to separate and quantify compounds from the sample collection and recovery procedure. Method 18 (40 CFR part 60, appendix A) may be used as a guideline for determining the appropriate GC column and GC detector based on the test compounds to be determined. Other types of analytical instrumentation may be used (i.e., HPLC) in lieu of GC systems as long as the recovery efficiency criteria of this method are met.

2.3.1 Gas Chromatograph. The GC shall be equipped with a constant-temperature liquid injection port or a heated sampling loop/valve system, as appropriate. The GC oven shall be temperature-programmable over the useful range of the GC column. The choice of detectors is based on the test compounds to be determined.

2.3.2 GC Column. Select the appropriate GC column based on (1) literature review or previous experience, (2) polarity of the analytes, (3) capacity of the column, or (4) resolving power (i.e., length, diameter, film thickness) required.

2.3.3 Data System. A programmable electronic integrator for recording, analyzing, and storing the signal generated by the detector.

2.3.4 Reagents. The gases required for GC operation shall be of the highest obtainable purity (hydrocarbon free). Consult the operating manual for recommended settings.

3. Procedure

Assemble the glassware and associated fittings (see Figures 4 or 5, as appropriate) and leak-check the system (approximately 7 psig is the target pressure). After an initial leak check, mark the pressure gauge and use the initial checkpoint to monitor for leaks throughout subsequent analyses. If the pressure in the system drops below the target pressure at any time during analysis, that analysis shall be considered invalid.

3.1 Recovery Efficiency Determination. Determine the individual recovery efficiency (RE) for each of the target compounds in duplicate before the waste samples are analyzed. To determine the RE, generate a water blank (Section 3.2.4) and use the injection port to introduce a known volume of spike solution (or certified gaseous standard).
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containing all of the target compounds at the levels expected in the waste sample. Introduce the spike solution immediately after the nitrogen purge has been started (Section 3.2.2). Follow the procedures outlined in Section 3.2.3. Analyze the recovery efficiency criteria in these cases would be difficult without adding the amount captured in the knockout trap.

3.2.4 Water Blank. A water blank shall be analyzed daily to determine the cleanliness of the purge and recovery system. A water blank is generated by adding 60 mL of organic-free deionized water to 50 mL of PEG in the purge chamber. Treat the blank as described in Section 3.2.2 and 3.2.3. The purpose of the water blank is to insure that no contaminants exist in the sampling and analytical apparatus which would interfere with the quantitation of the target compounds. If contaminants are present, locate the source of contamination, remove it, and repeat the water blank analysis.

3.3 Sample Analysis. Sample analysis in the context of this method refers to techniques to remove the target compounds from the sorbent tubes, separate them using a chromatography technique, and quantify them with an appropriate detector. Two types of sample extraction techniques typically used for sorbents include solvent desorption or direct thermal desorption of test compounds to a secondary focusing unit (either sorbent or cryogen based). The test compounds are then typically transferred to a GC system for analysis. Other analytical systems may be used (i.e., HPLC) in lieu of GC systems as long as the recovery efficiency criteria of this method are met.

3.3.1 Recover the test compounds from the sorbent tubes that require solvent desorption by transferring the adsorbent material to a sample vial containing the desorption solvent. The desorption solvent shall be the same as the solvent used to prepare calibration standards. The volume of solvent depends on the amount of adsorbed material to be desorbed (1.0 mL per 100 mg of adsorbent material) and also on the amount of test compounds present. Final volume adjustment and/or dilution can be made so that the concentration of test compounds in the desorption solvent is bracketed by the concentration of the calibration solutions.

Ultrasonicate the desorption solvent for 15 min in an ice bath. Allow the sample to sit for a period of time so that the adsorbent material can settle to the bottom of the vial. Transfer the solvent with a pasteur pipet (minimizing the amount of adsorbent material taken) to another vial and store at 4°C.

3.3.2 The analytical instrument shall be calibrated with a minimum of three levels of standards for each compound whose concentrations bracket the concentration of test compounds from the sorbent tubes. Liquid calibration standards shall be used for calibration in the analysis of the solvent extracts. The liquid calibration standards shall be prepared in the desorption solvent matrix. The calibration standards may be prepared...
and injected individually or as a mixture. If thermal desorption and focusing (onto another sorbent or cryogen focusing) are used, a certified gaseous mixture or a series of gaseous standards shall be used for calibration of the instrument. The gaseous standards shall be focused and analyzed in the same manner as the samples.

3.3.3 The analytical system shall be certified free from contaminants before a calibration is performed (see Section 3.2.4). The calibration standards are used to determine the linearity of the analytical system. Perform an initial calibration and linearity check by analyzing the three calibration standards for each target compound in triplicate starting with the lowest level and continuing to the highest level. If the triplicate analyses do not agree within 5 percent of their average, additional analyses will be needed until the 5 percent criteria is met. Calculate the response factor (Equation 3, Section 4.4) from the average area counts of the injections for each concentration level. Average the response factors of the standards for each compound. The linearity of the detector is acceptable if the response factor of each compound at a particular concentration is within 10 percent of the overall mean response factor for that compound. Analyze daily a mid-level calibration standard in duplicate and calculate a new response factor. Compare the daily response factor average to the average response factor calculated for the mid-level calibration during the initial linearity check; repeat the three-level calibration procedure if the daily average response factor differs from the initial linearity check mid-level response factor by more than 10 percent. Otherwise, proceed with the sample analysis.

3.3.4 Analyze the desorption solvent or direct thermal desorption tubes from each sample using the same analytical parameters used for the calibration standard. Calculate the total weight detected for each compound (Equation 4, Section 4.5). The slope (area/amount) and y-intercept are calculated from the line bracketed between the two closest calibration standards that bracket the concentration of the sample.

4. Calculations

4.1 Definitions and Variables

\[ A_s = \text{Mean area counts of test compound in standard.} \]

\[ A_w = \text{Mean area counts of test compound in sample desorption solvent.} \]

\[ b = \text{y-intercept of the line formed between the two closest calibration standards that bracket the concentration of the sample.} \]

\[ C_T = \text{Amount of test compound (µg) in calibration standard.} \]

\[ CF = \text{Correction for adjusting final amount of sample detected for losses during individual sample runs.} \]

\[ F_T = \text{Nitrogen flow through the purge chamber (6 L/min).} \]

\[ F_s = \text{Nitrogen split flow directed to the sample recovery system (use 6 L/min if split flow design was not used).} \]

\[ PPM = \text{Final concentration of test compound in waste sample (µg/g).} \]

\[ RE = \text{Response factor for adjusting final amount of sample detected for losses due to inefficient trapping and desorption techniques.} \]

\[ R.F. = \text{Response factor for test compound, calculated from a calibration standard.} \]

\[ S = \text{Slope of the line (area counts/C}_T\text{) formed between two closest calibration points that bracket the concentration of the sample.} \]

\[ W_c = \text{Weight of test compound expected to be recovered in spike solution based on theoretical amount.} \]

\[ W_v = \text{Weight of vial and PEG (g).} \]

\[ W_i = \text{Weight of vial, PEG and clean waste sample (g).} \]

\[ W_n = \text{Weight of original waste sample (g).} \]

\[ W_{s} = \text{Corrected weight of test compound measured (µg) in sample.} \]

\[ W_{c} = \text{Weight of test compound measured during analysis of recovery efficiency spike samples (µg).} \]

4.2 Recovery efficiency for determining trapping/desorption efficiency of individual test compounds in the spike solution, decimal value.

\[ \text{RE} = \frac{W_s}{W_c} \quad (1) \]

4.3 Weight of waste sample (g).

\[ W_w = W_i - W_n \quad (2) \]

4.4 Response Factor for individual test compounds.

\[ RF = \frac{C_T}{A_s} \quad (3) \]

4.5 Corrected weight of a test compound in the sample, in µg.
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METHOD 306—DETERMINATION OF CHROMIUM EMISSIONS FROM DECORATIVE AND HARD CHROMIUM ELECTROPLATING AND ANODIZING OPERATIONS

1. Applicability and Principle

1.1 Applicability. This method applies to the determination of chromium (Cr) in emissions from decorative and hard chrome electroplating facilities and anodizing operations.

1.2 Principle. (a) A sample is extracted isokinetically from the source using an unheated Method 5 sampling train (40 CFR part 60, appendix A), with a glass nozzle and probe liner, but with the filter omitted. The sample time has to be at least 2 hours. The Cr emissions are collected in an alkaline solution: 0.1 N sodium hydroxide (NaOH) or 0.1 N sodium bicarbonate (NaHCO₃). The collected samples remain in the alkaline solution until analysis. Samples with high Cr concentrations may be analyzed using inductively coupled plasma emission spectrometry (ICP) at 267.72 nm. Alternatively, if improved detection limits are required, a portion of the alkaline impinger solution is digested with nitric acid and analyzed by graphite furnace atomic absorption spectroscopy (GFAAS) at 357.9 nm.

(b) If it is desirable to determine hexavalent chromium (Cr+6) emissions, the samples may be analyzed using an ion chromatograph equipped with a post-column reactor (IC/PCR) and a visible wavelength detector. To increase sensitivity for trace levels of Cr+6, a preconcentration system can be used in conjunction with the IC/PCR.

2. Range, Sensitivity, Precision, and Interferences

2.1 Range. The recommended analytical range for each of the three analytical techniques is given below. The upper limit of all three techniques can be extended indefinitely by appropriate dilution.

2.1.1 GFAAS Range. As reported in Method 7191 of SW-846 (Citation 5 in Bibliography), the optimum concentration range for GFAAS is 5 to 100 µg Cr/l of concentrated analyte.

2.1.2 ICP Range. A linear response curve for ICP can be obtained in the range of 10 to at least 500 µg Cr/l of absorbing solution.

2.1.3 IC/PCR Range. In 40 CFR part 266, appendix IX, the lower limit of the detection range for IC/PCR when employing a preconcentration procedure is reported to be about 0.1 µg Cr+6/l of absorbing solution.

2.2 Sensitivity.

2.2.1 Analytical Sensitivity. The minimum detection limit for ICP, as reported in Method 6010A of SW-846, is 7 µg Cr/l.

2.2.2 In-stack Sensitivity. The in-stack sensitivity depends upon the analytical detection limit, the volume of stack gas sampled, and the total volume of the impinger absorbing solution plus the rinses. Using the analytical detection limits given in sections 2.2.1.1, 2.2.1.2, and 2.2.1.3; a stack gas sample volume of 1.7 dscm; and a total liquid sample volume of 500 ml; the corresponding in-stack detection limits are 0.0021 mg Cr/dscm for ICP, 0.00074 mg Cr/dscm for GFAAS, and 0.000015 mg Cr+6/dscm for IC/PCR with preconcentration. However, it is recommended that the concentration of Cr in the analytical solutions be at least five times the analytical detection limit to optimize sensitivity in the analyses. Using this guideline and the same assumptions for impinger sample volume and stack gas sample volume (500 ml and 1.7 dscm, respectively), the recommended minimum stack concentrations for optimum sensitivity are 0.0003 mg Cr/dscm for ICP, 0.000074 mg Cr/dscm for GFAAS, and 0.0000074 mg Cr+6/dscm for IC/PCR.
PCR with preconcentration. If required, the in-stack detection limits can be improved by either increasing the stack gas sample volume, reducing the volume of the digested sample relative to the GFAAS detection limits, or any combination of the three.

2.3 Precision. The following precision data have been reported for the three analytical methods. In the case of the GFAAS there is also bias data. In all cases, when sampling precision is combined with analytical precision, the resulting overall precision may be lower.

2.3.1 GFAAS Precision. As reported in Method 7009 of SW-846, in a single laboratory (EMSL), using Cincinnati, Ohio tap water spiked at concentrations of 19, 48, and 77 μg Cr/l, the standard deviations were ±0.1, ±0.2, and ±0.8, respectively. Recoveries at these levels were 97 percent, 101 percent, and 102 percent, respectively.

2.3.2 ICP Precision. As reported in Method 600A of SW-846, in an EPA round-robin Phase 1 study, seven laboratories applied the ICP technique to acid/distilled water matrices that had been spiked with various metal concentrates. For true values of 10, 50, and 150 μg Cr/l; the mean reported values were 10, 50, and 149 μg Cr/l; and the mean percent relative standard deviations were 18, 3.3, and 3.8 percent, respectively.

2.3.3 IC/PCR Precision. As reported in 40 CFR part 266, appendix IX, the precision of the IC/PCR with sample preconcentration is 5 to 10 percent; the overall precision for sewage sludge incinerators emitting 120 ng/dscm of Cr is 25 percent and 9 percent for Cr⁶⁺ and total Cr, respectively; and for hazardous waste incinerators emitting 300 ng/dscm of Cr⁶⁺ the precision is 20 percent.

2.4 Interferences.

2.4.1 GFAAS Interferences. Low concentrations of calcium and/or phosphate may cause interferences; at concentrations above 200 μg/l, calcium's effect is constant and eliminates the effect of phosphate. Calcium nitrate is therefore added to the concentrated analyte to ensure a known constant effect. Other matrix modifiers recommended by the instrument manufacturer may also be suitable. Nitrogen should not be used as the purge gas due to cyanide band interference. Background correction may be required because of possible significant levels of nonspecific absorption and scattering at the 373.9 nm analytical wavelength. Zeeman or Smith-Hieftje background correction is recommended to correct for interferences due to high levels of dissolved solids in the alkaline impinger solutions.

2.4.2 ICP Interferences.

2.4.2.1 ICP Spectral Interferences. (a) Spectral interferences are caused by:

(1) Overlap of a spectral line from another element;

(2) Unresolved overlap of a spectral line from another element;

(3) Background contribution from continuous or recombination phenomena; and

(4) Stray light from the line emission of high-concentration elements.
(b) Spectral overlap may be compensated for by computer correcting the raw data after monitoring and measuring the interfering element. At the 267.72-nm Cr analytical wavelength, iron, manganese, and uranium are potential interfering elements. Background and stray light interferences can usually be compensated for by a background correction adjacent to the analytical line. Unresolved overlap requires the selection of an alternative Cr wavelength. Consult the instrument manufacturer's operation manual for interference correction procedures.

2.4.2.2 ICP Physical Interferences. High levels of dissolved solids in the samples may cause significant inaccuracies due to salt buildup at the nebulizer and torch tips. This problem can be controlled by diluting the sample or providing for extended rinse times between sample analyses. Standards are prepared in the same matrix as the samples (i.e., 0.1 N NaOH or 0.1 N NaHCO₃).

2.4.2.3 ICP Chemical Interferences. These include molecular compound formation, ionization effects and solute vaporization effects, and are usually not significant in ICP, especially if the standards and samples are matrix matched.

2.4.3 IC/PCR Interferences. Components in the sample matrix may cause Cr⁶⁺ to convert to trivalent chromium (Cr⁳⁺) or cause Cr⁴⁺ to convert to Cr⁶⁺. The chromatographic separation of Cr⁶⁺ using ion chromatography reduces the potential for other metals to interfere with the post-column reaction. For the IC/PCR analysis, only compounds that coelute with Cr⁶⁺ and affect the diphenylcarbazide reaction will cause interference. Periodic analyses of reagent water blanks are used to demonstrate that the analytical system is essentially free of contamination. Sample cross-contamination that can occur when high-level and low-level samples or standards are analyzed alternately is eliminated by thorough purging of the sample loop. Purging can easily be achieved by increasing the injection volume of the samples to ten times the size of the sample loop.

3. Apparatus

3.1 Sampling Train. A schematic of the sampling train used in this method is shown in Figure 306-1. The train is the same as Method 5, section 21(40 CFR part 60, appendix A), except that the filter is omitted, and quartz or borosilicate glass must be used for the probe nozzle and liner in place of stainless steel. It is not necessary to heat the probe liner. Probe fittings of plastic such as...
Teflon, polypropylene, etc. are recommended over metal fittings to prevent contamination. If desired, a single combined probe nozzle and liner may be used, but such a single glass piece is not a requirement of this methodology. Use 0.1 N NaOH or 0.1 N NaHCO₃ in the impingers in place of water.

3.2 Sample Recovery. Same as Method 5, section 2.2 (40 CFR part 60, appendix A), with the following exceptions:

3.2.1 Probe-Liner and Probe-Nozzle Brushes. Brushes are not necessary for sample recovery. If a probe brush is used, it must be nonmetallic.

3.2.2 Sample Recovery Solution. Use 0.1 N NaOH or 0.1 N NaHCO₃, whichever was used as the impinger absorbing solution, in place of acetone to recover the sample.

3.2.3 Sample Storage Containers. Polyethylene, with leak-free screw cap, 500 ml or 1,000 ml.

3.2.4 Filtration Apparatus for IC/PCR. Teflon, or equivalent, filter holder and 0.45 µm acetate, or equivalent, filter.

3.3 Analysis. For analysis, the following equipment is needed.

3.3.1 General.

3.3.1.1 Phillips Beakers. (Phillips beakers are preferred, but regular beakers can also be used.)

3.3.1.2 Hot Plate.

3.3.1.3 Volumetric Flasks. Class A, various sizes as appropriate.

3.3.1.4 Assorted Pipettes.

3.3.2 Graphite Furnace Atomic Absorption Spectrophotometer.

3.3.3 Analysis by ICP.

3.3.3.1 ICP Spectrometer. Computer-controlled emission spectrometer with background correction and radio frequency generator.

3.3.3.2 Argon Gas Supply. Welding grade or better.

3.3.4 Analysis by IC/PCR.

3.3.4.1 IC/PCR System. High performance liquid chromatograph pump, sample injection valve, post-column reagent delivery and mixing system, and a visible detector, capable of operating at 520 nm, all with a nonmetallic (or inert) flow path. An electronic peak area mode is recommended, but other recording devices and integration techniques are acceptable provided the repeatability criteria and the linearity criteria for the calibration curve described in section 6.4.1 can be satisfied. A sample loading system will be required if preconcentration is employed.

3.3.4.2 Analytical Column. A high performance ion chromatograph (HPIC) nonmetallic column with anion separation characteristics and a high loading capacity designed for separation of metal chelating compounds to prevent metal interference. Resolution described in section 5.5 must be obtained. A nonmetallic guard column with the same ion-exchange material is recommended.

3.3.4.3 Preconcentration Column. An HPIC nonmetallic column with acceptable anion retention characteristics and sample loading rates as described in section 5.5.
3.3.4.4 0.45-µm Filter Cartridge. For the removal of insoluble material. To be used just prior to sample injection/analysis.

4. Reagents

Unless otherwise indicated, all reagents shall conform to the specifications established by the Committee on Analytical Reagents of the American Chemical Society.
(ACS reagent grade). Where such specifications are not available, use the best available grade.

4.1.1 Water. Reagent water that conforms to ASTM Specification D1193-77, Type II (incorporated by reference—see §63.14). It is recommended that water blanks be checked prior to preparing sampling reagents to ensure that the Cr content is less than the analytical detection limit.

4.1.2 Sodium Hydroxide (NaOH) Absorbing Solution. Prepare a 0.1 N or Sodium Bicarbonate (NaHCO₃) Absorbing Solution, 0.1 N. Dissolve 4.0 g of sodium hydroxide in 1 l of water, or dissolve 8.5 g of sodium bicarbonate in 1 l of water.

4.2 Sample Recovery.

4.2.1 0.1 N NaOH or 0.1 N NaHCO₃. See section 4.1.2. Use the same solution for recovery as was used in the impingers.

4.2.2 pH Indicator Strip, for IC/PCR. pH indicator capable of determining the pH of solutions between the pH range of 7 and 12, at 0.5 pH intervals.

4.3 Sample Preparation and Analysis.

4.3.1 Nitric Acid (HNO₃). See section 4.3.5. The zero standard shall be 1.0 percent (v/v) HNO₃. The zero standard shall be prepared daily by diluting the Cr standard stock solution (section 4.3.7) with 1.0 percent HNO₃. Use at least four standards to make the calibration curve. Suggested levels are 0, 5, 50, and 100 µg Cr/l.

4.3.2 HNO₃, 1.0 percent (v/v), for GFAAS. Add with stirring, 10 ml of concentrated HNO₃, to 800 ml of water. Dilute to 1,000 ml with this reagent. This reagent shall contain less than 0.002 mg Cr/l.

4.3.3 Calcium Nitrate Ca(NO₃)₂ Solution (10 µg Ca/ml) for GFAAS. Prepare the solution by weighing 36 mg of Ca(NO₃)₂ into a 1 l volumetric flask. Dilute with water to 1 l.

4.3.4 Matrix Modifier, for GFAAS. See instrument manufacturer's manual for suggested matrix modifier.

4.3.5 Chromatographic Eluent, for IC/PCR. The eluant used in the analytical system is ammonium sulfate based. Prepare by adding 6.5 ml of 29 percent ammonium hydroxide (NH₃, OH) and 33 g of ammonium sulfate ((NH₄)₂ SO₄) to 500 ml of reagent water. Dilute to 1 l with ammonium hydroxide and mix well. Other combinations of eluents and columns may be employed provided peak resolution, as described in section 6.4.1, and analytical sensitivity are acceptable.

4.3.6 Post-Column Reagent, for IC/PCR. An effective post-column reagent for use with the chromatographic eluent described in section 4.3.5 is a diphenylcarbazide (DPC) based system. Dissolve 0.5 g of 1,5-diphenylcarbazide in 10 ml of ACS grade methanol. Add 500 ml of reagent water containing 50 ml of 96 percent spectrophotometric grade sulfuric acid. Dilute to 1 l with reagent water.

4.3.7 Chromium Standard Stock Solution (1.000 mg/l). Procure a certified aqueous standard or dissolve 2.829 g of potassium dichromate (K₂ Cr₂ O₇) in water and dilute to 1 l.

4.3.8 Calibration Standards for GFAAS. Chromium solutions for GFAAS calibration shall be prepared to contain 1.0 percent (v/v) HNO₃. The zero standard shall be 1.0 percent (v/v) HNO₃. Calibration standards should be prepared daily by diluting the Cr standard stock solution (section 4.3.7) with 1.0 percent HNO₃. Use at least four standards to make the calibration curve. Suggested levels are 0, 5, 50, and 100 µg Cr/l.

4.3.9 Calibration Standards for ICP or IC/PCR. Prepare calibration standards for ICP or IC/PCR by diluting the Cr standard stock solution (section 4.3.7) with 0.1 N NaOH or 0.1 N NaHCO₃, whichever was used as the impinger absorbing solution, to achieve a matrix similar to the actual field samples. Suggested levels are 0, 25, 50, and 100 µg Cr/l for ICP, and 0, 0.5, 5, and 10 µg Cr/l for IC/PCR.

4.4 Glassware Cleaning Reagents.

4.4.1 HNO₃. Concentrated. The ACS reagent grade or equivalent.

4.4.2 Water. Reagent water that conforms to ASTM Specification D1193-77, Type II, (incorporated by reference—see §63.14).

4.4.3 HNO₃, 1.0 percent (v/v), for GFAAS. Add with stirring 500 ml of concentrated HNO₃, to a flask containing approximately 4,000 ml of water. Dilute to 5,000 ml with water. Mix well. The reagent shall contain less than 2 µg Cr/l.

5. Procedure

5.1 Sampling. (a) Same as Method 5, section 4.1 (40 CFR part 60, appendix A), except omit the filter and filter holder from the sampling train, use a glass nozzle and probe liner, do not heat the probe, place 100 ml of 0.1 N NaOH or 0.1 N NaHCO₃ in each of the first two impingers, and record the data for each run on a data sheet such as the one shown in Figure 306-2.

(b) Clean all glassware prior to sampling in hot soapy water designed for laboratory cleaning of glassware. Next, rinse the glassware three times with tap water, followed by three additional rinses with reagent water. Then soak all glassware in 10 percent (v/v) HNO₃ solution for a minimum of 4 hours, rinse three times with reagent water, and allowed to air dry. Cover all glassware openings where contamination can occur with Parafilm, or equivalent, until the sampling train is assembled for sampling.

(c) If the sample is going to be analyzed for Cr⁺⁺ using IC/PCR, determine the pH of the solution in the first impinger at the end of the sampling run using a pH indicator strip. The pH of the solution should be greater than 8.5. If not, the concentration of the NaOH or NaHCO₃ impinger absorbing solution should be increased to 0.5 N and the sample should be rerun.
5.2 Sample Recovery. Follow the basic procedures of Method 5, section 4.2, with the exceptions noted below; a filter is not recovered from this train.

5.2.1 Container No. 1. Measure the volume of the liquid in the first, second, and third impingers and quantitatively transfer into a labeled sample container. Use approximately 200 to 300 ml of 0.1 N NaOH or 0.1 N NaHCO\(_3\) to rinse the probe nozzle, probe liner, three impingers, and connecting glassware; add this rinse to the same container.

5.2.2 Container No. 2 (Reagent Blank). Place approximately 500 ml of 0.1 N NaOH or 0.1 N NaHCO\(_3\) absorbing solution in a labeled sample container.

5.2.3 Sample Filtration for IC/PCR. If the sample is to be analyzed for Cr\(^{6+}\) by IC/PCR, it must be filtered immediately following recovery to remove any insoluble matter. Nitrogen gas may be used as a pressure assist to the filtration process. Filter the entire contents of Container No. 1 through a 0.45-µm acetate filter (or equivalent), and collect the filtrate in a 1,000 ml graduated cylinder. Rinse the sample container with reagent water three separate times, pass these rinses through the filter, and add the rinses to the sample filtrate. Determine the final volume of the filtrate and rinses and return them to the rinsed polyethylene sample container.

5.2.4 Sample Preservation. Refrigerate samples upon receipt. (Containers Nos. 1 and 2).

5.3 Sample Preparation and Analysis for GFAAS. For analysis by GFAAS, an acid digestion of the alkaline impinger solution is required. Two types of blanks are required for the analysis. The calibration blank is used in establishing the analytical curve, and the reagent blank is used to assess possible contamination resulting from the sample processing. The 1.0 percent HNO\(_3\) is the calibration blank. The 0.1 N NaOH solution or the 0.1 N NaHCO\(_3\) from section 5.2.2 is the reagent blank. The reagent blank must be carried through the complete analytical procedure, including the acid digestion, and must contain the same acid concentration in the final solution as the sample solutions.

5.3.1 Acid Digestion for GFAAS. (a) In a beaker, add 10 ml of concentrated HNO\(_3\) to a sample aliquot of 100 ml taken for analysis. Cover the beaker with a watch glass. Place the beaker on a hot plate and reflux the sample down to near dryness. Add another 5 ml of concentrated HNO\(_3\) to complete the digestion. Carefully reflux the sample volume down to near dryness. Wash down the beaker walls and watch glass with reagent water. The final concentration of HNO\(_3\) in the solution should be 1 percent (v/v). Transfer the digested sample to a 50 ml volumetric flask. Add 0.5 ml of concentrated HNO\(_3\), and 1 ml of the 10 µg/ml of Ca(NO\(_3\)_2). (b) Dilute to 50 ml with reagent water. A different final volume may be used, based on the expected Cr concentration, but the HNO\(_3\) concentration must be maintained at 1 percent (v/v).
5.3.2 Sample Analysis by GFAAS. (a) The 357.9-nm wavelength line shall be used. Follow the manufacturer's operating instructions for all other spectrophotometer parameters.
(b) Furnace parameters suggested by the manufacturer should be employed as guidelines. Since temperature-sensing mechanisms and temperature controllers can vary between instruments and/or with time, the validity of the furnace parameters must be periodically confirmed by systematically altering the furnace parameters while analyzing a standard. In this manner, losses of analyte due to higher-than-necessary temperature settings or losses in sensitivity due to less than optimum settings can be minimized. Similar verification of furnace parameters may be required for complex sample matrices. Calibrate the GFAAS system following the procedures specified in section 6.

(c) Inject a measured aliquot of digested sample into the furnace and atomize. If the concentration found exceeds the calibration range, the sample should be diluted with the calibration blank solution (1.0 percent HNO₃) and reanalyzed. Consult the operator’s manual for suggested injection volumes. The use of multiple injections can improve accuracy and help detect furnace pipetting errors.

(d) Analyze a minimum of one matrix-matched reagent blank per sample batch to determine if contamination or any memory effects are occurring. Analyze a calibration blank and a midpoint calibration check standard after approximately every 10 sample injections.

(e) Calculate the Cr concentrations:

1. By the method of standard additions (see operator’s manual).
2. From the calibration curve, or
3. Directly from the instrument’s concentration readout. All dilution or concentration factors must be taken into account. All results should be reported in µg Cr/ml with up to three significant figures.

(f) If dilutions are performed, the appropriate factors must be applied to sample values. All results should be reported in µg Cr/ml with up to three significant figures.

5.5 Sample Analyses by IC/PCR. (a) The Cr⁺⁺⁺ content of the sample filtrate is determined by IC/PCR. To increase sensitivity for trace levels of chromium, a preconcentration system is also used in conjunction with the IC/PCR (if necessary).

(b) Prior to preconcentration and/or analysis, filter all field samples through a 0.45-µm filter. This filtration should be conducted just prior to sample injection/analysis.

(c) The preconcentration is accomplished by selectively retaining the analyte on a solid absorbent (as described in section 3.4.3.3), followed by removal of the analyte from the absorbent. Inject the sample into a sample loop of the desired size (use repeated loadings or a larger size loop for greater sensitivity). The Cr⁺⁺⁺ is collected on the resin bed of the column. Switch the injection valve so that the eluent displaces the concentrated Cr⁺⁺⁺ sample, moving it off the preconcentration column and onto the IC anion separation column. After separation from other sample components, the Cr⁺⁺⁺ forms a specific complex in the post-column reactor with the DPC reaction solution, and
the complex is detected by visible absorbance at a wavelength of 520 nm. The amount of absorbance measured is proportional to the concentration of the Cr⁶⁺ complex for concentrations below the instrument drift. Measure areas or heights of the calibration standards to assess the field samples. Finally, repeat the injection for the calibration blank (section 5.2.2), followed by the reagent blank (section 5.2.2), and the field samples. Next, repeat the injection of the calibration standards prepared fresh daily as described in section 4.3.9.

(e) Prior to sample analysis, establish a stable baseline with the detector set at the required attenuation by setting the eluent flow rate at approximately 0.5 ml/min and the post-column reagent flow rate at approximately 0.5 ml/min. Note: As long as the ratio of eluent flow rate to PCR flow rate remains constant, the standard curve should remain linear. Inject a sample of reagent water to ensure that no Cr⁶⁺ appears in the water blank.

(f) First, inject the calibration standards prepared, as described in section 4.3.9 to cover the appropriate concentration range, starting with the lowest standard first. Next, inject, in duplicate, the calibration reference standard (as described in section 7.3.1), followed by the reagent blank (section 5.2.2), and the field samples. Finally, repeat the injection of the calibration standards to assess instrument drift. Measure areas or heights of the Cr⁶⁺/DPC complex chromatogram peaks. The response for replicate, consecutive injections of samples must be within 5 percent of the average response, or the injection should be repeated until the 5 percent criterion can be met. Use the average response (peak areas or heights) from the duplicate injections of calibration standards to generate a linear calibration curve. From the calibration curve, determine the concentrations of the field samples employing the average response from the duplicate injections.

6. Calibration

6.1 Sampling Train Calibration. Perform all of the calibrations described in Method 5, section 5 (40 CFR part 60, appendix A). The alternate calibration procedures described in section 7 of Method 5 (40 CFR part 60, appendix A) may also be used.

6.2 GFAAS Calibration. Either run a series of chromium standards and a calibration blank and construct a calibration curve by plotting the concentrations of the standards against the absorbencies, or by using the method of standard additions, plot added concentration versus absorbance. For instruments that read directly in concentration, set the curve corrector to read out the proper concentration, if applicable. This is customarily performed automatically with most instrument computer-based data systems.

6.2.1 GFAAS Calibration Curve. If a calibration curve is used, it should be prepared daily with a minimum of a calibration blank and three standards. Calibration standards for total chromium should start with 1 percent NH₄HNO₃ with no chromium for the calibration blank, with appropriate increases in total chromium concentration for the other calibration standards (see section 4.3.9).

6.3 ICP Calibration. Calibrate the instrument according to the instrument manufacturer’s recommended procedures, using a calibration blank and three standards for the initial calibration. Calibration standards should be prepared fresh daily, as described in section 4.3.9. Be sure that samples and calibration standards are matrix matched. Flush the system with the calibration blank between each standard. Use the average intensity of multiple exposures for both standardization and sample analysis to reduce random error.

6.4 IC/PCR Calibration. Prepare a calibration curve using the calibration blank and three calibration standards prepared fresh daily as described in section 4.3.9. Run the standards with the field samples as described in section 5.5.

7. Quality Control

7.1 GFAAS Quality Control

7.1.1 GFAAS Calibration Reference Standards. If a calibration curve is used, it must be verified by use of at least one calibration reference standard (made from a reference material or other independent standard material) at or near the mid-range of the calibration curve. The calibration reference standard must be measured within 10 percent of its true value for the curve to be considered valid. The curve must be validated before sample analyses are performed.

7.1.2 GFAAS Check Standards. (a) Run a check standard and a calibration blank after approximately every 10 sample injections, and at the end of the analytical run. These standards are run, in part, to monitor the life and performance of the graphite tube. Lack of reproducibility or a significant change in the signal for the check standard indicates that the graphite tube should be replaced. Check standards can be the midrange calibration standard or the reference standard. The results of the check standard shall agree within 10 percent of the expected.
value. If not, terminate the analyses, correct the problem, recalibrate the instrument, and reanalyze all samples analyzed subsequent to the last acceptable check standard analysis.

(b) The results of the calibration blank are to agree within three standard deviations of the mean blank value. If not, repeat the analysis two more times and average the results. If the average is not within three standard deviations of the background mean, terminate the analyses, correct the problem, recalibrate, and reanalyze all samples analyzed subsequent to the last acceptable calibration blank analysis.

7.1.3 GFAAS Duplicate Samples. Run one duplicate sample for every 20 samples, (or one per source test, whichever is more frequent). Duplicate samples are brought through the whole sample preparation and analytical process separately. Duplicate samples shall agree within 10 percent.

7.1.4 GFAAS Matrix Spiking. Spiked samples shall be prepared and analyzed daily to ensure that correct procedures are being followed and that all equipment is operating properly. Spiked sample recovery analyses should indicate a recovery for the Cr spike of between 75 and 125 percent. Spikes are added prior to any sample preparation. Cr levels in the spiked sample should provide final solution concentrations that fall within the linear portion of the calibration curve.

7.1.5 GFAAS Method of Standard Additions. Whenever sample matrix problems are suspected and standard/sample matrix matching is not possible or whenever a new sample matrix is being analyzed, the method of standard additions shall be used for the analysis of all extracts. Section 5.4.2 of Method 12 (40 CFR part 60, appendix A) specifies a performance test to determine if the method of standard additions is necessary.

7.1.6 GFAAS Reagent Blank Samples. Analyze a minimum of one matrix-matched reagent blank (section 5.2.2) per sample batch to determine if contamination or memory effects are occurring. The results should agree within three standard deviations of the mean blank value.

7.2 ICP Quality Control.

7.2.1 ICP Interference Check. Prepare an interference check solution to contain known concentrations of interfering elements that will provide an adequate test of the correction factors in the event of potential spectral interferences. Two potential interferences, iron and manganese, may be prepared in 2, 50, and 200 µg/ml solutions, respectively. The solutions should be prepared in dilute HNO₃, (1-5 percent). Particular care must be taken to ensure that the solutions and/or salts used to prepare the solutions are of ICP grade purity (i.e., that no measurable Cr contamination exists in the salts/solutions). Commercially prepared interfering element check standards are available. Verify the interelement correction factors every three months by analyzing the interference check solution. The correction factors are calculated according to the instrument manufacturer’s directions. If interelement correction factors are used properly, no false Cr should be detected.

7.2.2 ICP Calibration Reference Standards. Prepare a calibration reference standard in the same alkaline matrix as the calibration standards; it should be at least 10 times the instrumental detection limit. This reference standard should be prepared from a different Cr stock solution source than that used for preparation of the calibration curve standards and is used to verify the accuracy of the calibration curve. Prior to sample analysis, analyze at least one reference standard. The calibration reference standard must be measured within 10 percent of it’s true value for the curve to be considered valid. The curve must be validated before sample analyses are performed.

7.2.3 ICP Check Standards. Run a check standard and a calibration blank after every 10 samples, and at the end of the analytical run. Check standards can be the mid-range calibration standard or the reference standard. The results of the check standard shall agree within 10 percent of the expected value; if not, terminate the analyses, correct the problem, recalibrate the instrument, and rerun all samples analyzed subsequent to the last acceptable check standard analysis. The results of the calibration blank are to agree within three standard deviations of the mean blank value. If not, repeat the analysis two more times and average the results. If the average is not within three standard deviations of the background mean, terminate the analyses, correct the problem, recalibrate, and reanalyze all samples analyzed subsequent to the last acceptable calibration blank analysis.

7.2.4 ICP Duplicate Samples. Analyze one duplicate sample for every 20 samples, (or one per source test, whichever is more frequent). Duplicate samples are brought through the whole sample preparation and analytical process. Duplicate samples shall agree within 10 percent.

7.2.5 ICP Reagent Blank Samples. Analyze a minimum of one matrix-matched reagent blank (section 5.2.2) per sample batch to determine if contamination or memory effects are occurring. The results should agree within three standard deviations of the mean blank value.

7.3 IC/PCR Quality Control.

7.3.1 IC/PCR Calibration Reference Standards. Prepare a calibration reference standard in the same alkaline matrix as the calibration standards at a concentration that is at or near the mid-point of the calibration curve. This reference standard should be prepared from a different Cr stock solution source than used for preparing the calibration curve standards. The reference
standard is used to verify the accuracy of the calibration curve. Prior to sample analysis, analyze at least one reference standard. The results of this analysis of the reference standard must be within 10 percent of the true value of the reference standard for the calibration curve to be considered valid. The curve must be validated before sample analyses are performed.

7.3.2 IC/PCR Check Standards. (a) Run the calibration blank and calibration standards with the field samples as described in section 5.5. For each standard, determine the peak areas (recommended) or the peak heights, calculate the average response from the duplicate injections, and plot the average response against the Cr+6 concentration in μg/ml. The individual responses for each calibration standard determined before and after field sample analysis must be within 5 percent of the average response for the analysis to be valid. If the 5 percent criteria is exceeded, excessive drift and/or instrument degradation may have occurred, and must be corrected before further analyses are performed.

(b) Employing linear regression, calculate a predicted value for each calibration standard using the average response for the duplicate injections. Each predicted value must be within 7 percent of the actual value for the calibration curve to be considered acceptable. If not acceptable, remake and/or rerun the calibration standards. If the calibration curve is still unacceptable, reduce the range of the curve.

7.3.3 IC/PCR Duplicate Samples. Analyze one duplicate sample for every 20 samples, (or one per source test, whichever is more frequent). Duplicate samples are brought through the whole sample preparation and analytical process. Duplicate samples shall agree within 10 percent.

7.3.4 IC/PCR Reagent Blank Samples. Analyze a minimum of one matrix-matched reagent blank (section 5.2.2) per sample batch to determine if contamination or memory effects are occurring. The results should agree within three standard deviations of the mean blank value.

8. Emission Calculations

Carry out the calculations, retaining one extra decimal figure beyond that of the acquired data. Round off figures after final calculations.

8.1 Total Cr in Sample. Calculate Mcv, the total μg Cr in each sample, as follows:

\[ M_{cv} = (V_{mi})(C_s)(F)(D) \]

where:

\[ V_{mi} = \text{Volume of impinger contents plus rinses, ml} \]

\[ C_s = \text{Concentration of Cr in sample solution, μg Cr/ml} \]

\[ F = \text{Dilution factor} \]

8.2 Average Dry Gas Meter Temperature and Average Orifice Pressure Drop. Same as Method 5, section 6.2.

8.3 Dry Gas Volume, Volume of Water Vapor, Moisture Content. Same as Method 5, sections 6.3, 6.4, and 6.5, respectively.

8.4 Cr Emission Concentration. Calculate Cc, the Cr concentration in the stack gas, in mg/dscm on a dry basis, corrected to standard conditions, as follows:

\[ C_c = (10^{-3} \text{mg/μg}) (M_{cv}/V_{meas}) \]

where:

\[ V_{meas} = \text{Gas sample volume measured by the dry gas meter, corrected to dry standard conditions, dscm} \]

8.5 Isokinetic Variation, Acceptable Results. Same as Method 5, sections 6.11 and 6.12, respectively.

9. Bibliography


3. Same as Bibliography of Method 5, Citations 2 to 5 and 7.


METHOD 306A—DETERMINATION OF CHROMIUM EMISSIONS FROM DECORATIVE AND HARD CHROMIUM ELECTROPLATING AND ANODIZING OPERATIONS

1. Applicability and Principle

11. Applicability. This method applies to the determination of chromium (Cr) in emissions from decorative and hard chromium electroplating facilities and anodizing operations. The method is less expensive and less complex to conduct than Method 306 of this appendix. Correctly applied, the precision and bias of the sample results will be comparable to those obtained with the isokinetic Method 306 of this appendix. This method is applicable under ambient moisture, air, and temperature conditions.
1.2 Principle. A sample is extracted from the source at a constant sampling rate determined by a critical orifice and collected in a probe and impingers. The sampling time at the sampling traverse points is varied according to the stack gas velocity at each point to obtain a proportional sample. The concentration is determined by the same analytical procedures used in Method 306 of this appendix: inductively-coupled plasma emission spectrometry (ICP), graphite furnace atomic absorption spectrometry (GFAAS), or ion chromatography with a post-column reactor (IC/PCR).

2. Range, Sensitivity, Precision, and Interferences
   Same as Method 306, section 2 of this appendix.

3. Apparatus
   Note: Mention of trade names or specific products does not constitute endorsement by the Environmental Protection Agency.

3.1 Sampling Train. A schematic of the sampling train is shown in Figure 306A-1. The components of the train are available commercially, but some fabrication and assembly are required. If Method 306 equipment is available, the sampling train may be assembled as specified in Method 306 of this appendix and the sampling rate of the meter box set at the delta H specified for the calibrated orifice; this train is then operated as specified in this method.

3.1.1 Probe Nozzle/Tubing and Sheath. Use approximately 1/4 in. inside diameter (ID) glass or rigid plastic tubing about 8 in. long with a short 90° bend at one end to form the nozzle. Grind a slight taper on the nozzle end before making the bend. Attach the nozzle to flexible tubing of sufficient length to collect a sample from the stack. Use a straight piece of larger diameter rigid tubing (such as metal conduit or plastic water pipe) to form a sheath that begins about 1 in. from the 90° bend on the nozzle and encases the flexible tubing.
3.1.2 S-Type Pitot. Same as Method 2, section 3 (40 CFR part 60, appendix A).

3.1.3 Sample Line. Use thick wall flexible plastic tubing (e.g., polyethylene, polypropylene, or polyvinylchloride) about ¼ in. to ½ in. ID to connect the train components. A combination of rigid plastic tubing and thin wall flexible tubing may be used as long as neither tubing collapses when leak-checking the train. Metal tubing cannot be used.

3.1.4 Impingers. One quart capacity "Mason" glass canning jars with vacuum seal lids are used. Three impingers are required: the first is for collecting the pollutant in the absorbing solution, the second is empty and is used to collect any absorbing solution carried over from the first impinger, and the third contains the drying agent. Install leak-tight inlet and outlet tubes in the lids of each impinger for assembly with the train. The tubes may be made of approximately ¼ in. ID glass or rigid plastic tubing. For the inlet tube of the first impinger, heat the glass or plastic tubing and
draw until the tubing separates. Cut the tip off until the tip orifice is \(\frac{3}{32}\) in. in diameter. When fabricating the first impinger, place the tip orifice \(\frac{3}{16}\) in. above the bottom of the jar when assembled. For the second impinger, the inlet tube need not be drawn and sized, but the tip should be approximately 2 in. above the bottom of the jar. The inlet tube of the third impinger should extend to about \(\frac{1}{2}\) in. above the bottom of the jar. Locate the outlet tube end of all impingers about \(\frac{1}{2}\) in. beneath the bottom of the lid.

3.1.5 Manometer. Inclined/vertical type, or equivalent device, as described in section 2.2 of Method 2 (40 CFR part 60, appendix A).

3.1.6 Critical Orifice. The critical orifice is a small restriction in the sample line (approximately \(\frac{1}{16}\) in. in diameter) that is located upstream of the vacuum pump and sets the sample rate at about 0.75 cfm. An orifice can be made of \(\frac{3}{32}\) in. brass tubing approximately \(\frac{3}{16}\) in. long sealed inside larger diameter, approximately \(\frac{1}{8}\) in., brass tubing to serve as a critical orifice giving a constant sample flow. Materials other than brass can be used to construct the critical orifice as long as the flow through the sampling train is approximately 0.75 cfm.

3.1.7 Connecting Hardware. Standard pipe and fittings, \(\frac{1}{4}\) in. or \(\frac{3}{8}\) in., are used to install the vacuum pump and dry gas meter in the sampling train.

3.1.8 Pump Oiler. A glass oil reservoir with a wick mounted at the vacuum pump inlet lubricates the pump vanes. The oiler should be an inline type and not vented to the atmosphere.

3.1.9 Vacuum Pump. Gast Model 0522-V103-G18DX, or equivalent, capable of delivering at least 1.5 cfm at 15 in. Hg vacuum.

3.1.10 Oil Trap. An empty glass oil reservoir without wick is mounted at pump outlet to prevent oil from reaching the dry gas meter.

3.1.11 Dry Gas Meter. A Rockwell model 175-s test meter, or equivalent, with a thermometer installed to monitor meter temperature. The dry gas meter must be capable of measuring volume to within 2 percent.

3.2 Sample Recovery.

3.2.1 Wash Bottles. These are glass or inert plastic, 500 or 1000 ml, with spray tube.

4. Reagents

4.1 Sampling. Same as Method 306, section 4.1 of this appendix.

4.2 Sample Recovery. Same as Method 306, section 4.2 of this appendix.

5. Procedure

5.1 Sampling.

5.1.1 Pretest Preparation.

5.1.1.1 Port Location. Locate the sampling ports as specified in section 2.1 of Method 1 (40 CFR part 60, appendix A). Use a total of 24 sampling points for round ducts and 25 points for rectangular ducts. Locate the sampling points as specified in section 2.3 of Method 1 (40 CFR part 60, Appendix A). Mark the pitot and sampling probe with thin strips of tape to permit velocity pressure and sample traversing. For ducts less than 12 in. in diameter, use a total of 16 points.

5.1.1.2 Velocity Pressure Traverse. (a) Perform a velocity pressure traverse before the first sample run. Figure 306A-2 may be used to record velocity pressure data. If testing occurs over several days, perform the traverse at the beginning of each day. Perform velocity pressure traverses as specified in section 3 of Method 2 (40 CFR part 60, appendix A), but record only the \(\Delta p\) (velocity head) values for each sampling point.

(b) Check for cyclonic flow during the first traverse to verify that it does not exist; if cyclonic flow does exist, make sure that the absolute average angle of misalignment does not exceed 20°. If the average angle of misalignment exceeds 20° at an outlet location, install straightening vanes to eliminate the cyclonic flow. If it is necessary to test an inlet location where cyclonic flow exists, it may not be possible to install straightening vanes. In this case, a variation of the alignment method must be used. This must be approved by the Administrator.
5.1.1.3 Point Sampling Times. Since the sampling rate of the train is held constant by the critical orifice, it is necessary to calculate specific sampling times for each point in order to obtain a proportional sample. If all sampling can be completed in a single day, it is necessary to calculate the point sampling times only once. If sampling occurs over several days, recalculate the point sampling times each day. Determine the average of

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<th>Traverse Point Number</th>
<th>Cyclonic Flow Angle (Degrees)</th>
<th>Δp</th>
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<th>$\frac{\sqrt{\Delta p} \times 5 \text{ min}}{(\Delta p)_{\text{avg}}} = \text{Numerical Minutes}$</th>
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Figure 306A-2. Velocity Traverse and Point Sample Time Calculation Sheet.
Calculate the sampling times for each point using Equation 306A-1. Convert the decimal parts of minutes to seconds. If the stack diameter is less than 12 in., use 7.5 minutes in place of 5 minutes in the equation and 16 sampling points.

\[
\text{Minutes at point } n = \left( \frac{\text{Point } n \Delta p}{\Delta p_{\text{avg}}} \right) \times 5 \text{ minutes} \quad \text{Eq. 306A-1}
\]

Where:
- \( n \) = Sampling point number,
- \( \Delta p \) = Velocity head measured by Type-S pitot tube, in. H\text{2}O

5.1.4 Preparation of Sampling Train. Assemble the sampling train as shown in Figure 306A-1. Secure the nozzle-liner assembly to the sheath to prevent slipping when sampling. Before charging, rinse the first mason jar impinger with either 0.1 N sodium hydroxide (NaOH) or 0.1 N sodium bicarbonate (NaHCO\(_3\)); discard the solution. Put 250 ml of 0.1 N NaOH or 0.1 N NaHCO\(_3\) absorbing solution into the first mason jar impinger. Similarly, rinse the second mason jar impinger and leave empty. Put silica gel into the third mason jar impinger until the impinger is half full. Place the impingers into an ice bath and check to ensure that the lids are tight.

5.1.5 Train Leak Check Procedure. Wait until the ice has cooled the impingers. Next, seal the nozzle with a finger covered by a piece of clear plastic wrap and turn on the pump. The vacuum in the line between the pump and the critical orifice must be at least 15 in. Hg. Observe any leak rate on the dry gas meter. The leak rate should not exceed 0.02 cfm.

5.1.2 Sampling Train Operation.
- 5.1.2.1 Record all pertinent process and sampling data on the data sheet (see Figure 306A-3). Ensure that the process operation is suitable for sample collection.
Place the probe nozzle into the duct at the first sampling point and seal the port. Turn on the pump. A minimum vacuum of 15 in. Hg or 0.47 atmosphere between the critical orifice and pump is required to maintain critical flow. Sample for the time interval previously determined for that point. Move to the second point and sample for the time interval determined for that point; sample all points on the traverse in this manner.
Keep ice around the impingers during the run. Complete the traverse and turn off the pump. Move to the next sampling port and repeat. Record the final dry gas meter reading. (NOTE: If an approximate mass emission rate is desired, record the stack temperature before and after the run.)

5.1.2.3 Post Test Leak Check. Remove the probe assembly and flexible tubing from the first impinger. Do not cover the nozzle. Seal the inlet tube of the first impinger with a finger covered by clear plastic wrap and turn on the pump. The vacuum in the line between the pump and the critical orifice must be at least 15 in. Hg. Observe any leak rate on the dry gas meter. If the leak rate exceeds 0.02 cfm, reject the run. If the leak rate is acceptable, take the probe assembly and impinger assembly to the sample recovery area.

5.2 Sample Recovery

5.2.1 Container No. 1. (a) After the train has been moved to the sample recovery area, disconnect the tubing that joins the first impinger with the second. (b) The first impinger jar is also used as the sample container jar. Unscrew the lid from the first impinger jar. Lift the inlet/outlet tube assembly almost out of the jar, and using the wash bottle, rinse the outside of the impinger tip that was immersed in the impinger jar with extra absorbing solution; rinse the inside of the tip as well. (c) Recover the second impinger by removing the lid and pouring any contents from the second impinger into the first impinger. Rinse the second impinger including the inside and outside of the impinger stem as well as any connecting plastic tubing with extra absorbing solution and place the rinse into the first impinger. (d) Hold the nozzle and connecting plastic tubing in a vertical position so that the tubing forms a “U.” Using the wash bottle, partially fill the tubing with sampling reagent. Raise and lower the end of the plastic tubing several times to cause the reagent to contact the major portion of the internal parts of the assembly thoroughly. Do not raise the solution level too high or part of the sample will be lost. Place the nozzle end of the assembly over the mouth of the first impinger jar (sample container) and elevate the plastic tubing so that the solution flows rapidly out of the nozzle. Perform this procedure three times. Next, repeat the recovery procedure but allow the solution to flow rapidly out the open end of the plastic tubing into the first impinger jar. (e) Place a piece of clear plastic wrap over the mouth of the first impinger jar. Use a standard lid and band assembly to seal the jar. Label the jar with the sample number and mark the liquid level to gauge any losses during handling.

5.2.2 Container No. 2 (Reagent Blank). Place approximately 500 ml of the 0.1 N NaOH or 0.1 N NaHCO₃, absorbing solution in a labeled sample container.

5.2.3 Sample Filtration for IC/PCR. If the sample is to be analyzed for Cr⁶⁺ by IC/PCR, it must be filtered immediately following recovery as described in section 5.2.3 of Method 306 of this appendix.

5.3 Analysis. Sample preparation and analysis procedures are identical to Method 306, section 5.3 of this appendix.

6. Calibration

6.1 Dry Gas Meter. (a) Dry gas meter calibrations may be performed by either the manufacturer, a firm who provides calibration services, or the tester. The dry gas meter calibration coefficient (Yₘ) must be determined prior to initial use of the meter, and must be checked following each field use. If the dry gas meter is new, the manufacturer will have specified the Yₘ for the meter. The manufacturer may also have included a calibration orifice and a data sheet with the meter that may be used for calibration purposes. The sheet will specify a standard cubic foot volume and a sample time, and these values were determined when the orifice was used to set the initial Yₘ for the meter. The Yₘ may be checked by disconnecting the critical orifice in the sampling train and replacing it with the calibration orifice. The inlet side of the calibration orifice is open to the atmosphere and is not reconnected to the sample train. Record the initial dry gas meter volume and meter temperature. Turn on the pump and operate it for the number of minutes specified by the manufacturer’s data sheet. Stop the pump and record the final dry gas meter volume and temperature. Subtract the start volume from the stop volume and average the temperatures. Check the Yₘ for the dry gas meter after the test by using the following equation:

\[ Y = \frac{Ft_3}{17.647 (Ft_3 m + 460)} \]

Where:
- Ft₃₃ = Cubic feet given by meter manufacturer
- Tₘ = Temperature of meter in degrees Fahrenheit
- Ft₃₃ = Cubic feet from dry gas meter, post test
- Pₐₚₗ = Barometric pressure in inches of mercury

Compare the Yₘ just calculated with the Yₘ given by the manufacturer:

\[ \frac{Yₘ (manufacturer)}{Yₘ (calculated after test)} \]
If this value is between 0.95 and 1.05, the $Y_m$ of the meter is acceptable. If the value lies outside the specified range, the test series shall either be voided, or calculations for the test series shall be performed using whichever meter coefficient value (i.e., before and after) that gives the lower value of total sample volume. Return the dry gas meter to the manufacturer for recalibration. The calibration may also be conducted as specified in section 5.3.1 or section 7 of Method 5 (40 CFR part 60, appendix A), except that it is only necessary to check the calibration at an approximate flow rate of 0.75 cfm. The calibration of the dry gas meter must be checked after each field use in the same manner. If the values of $Y_m$ obtained before and after a test series differ by more than 5%, the test series shall either be voided, or calculations for the test series shall be performed using whichever meter coefficient value (i.e., before or after) that gives the lower value of total sample volume.

6.2 GFAA Spectrometer. Same as Method 306, section 6.2 of this appendix.

6.3 ICP Spectrometer. Same as Method 306, section 6.3 of this appendix.

7. Quality Control
Same as Method 306, section 7 of this appendix.

8. Calculations

8.1 Pollutant Concentration. Calculate $C_{Cr}$, the Cr concentration in the stack gas, in mg/dscm on a dry basis as follows:

$$C_{Cr} = \frac{(M_{Cr})(T_m + 460)}{(499.8)(Y_m)(V_m)(P_{bar})}$$  
Eq. 306A-2

where:

- $M_{Cr}$=Amount of Cr in sample from Method 306 of this appendix, Eq. 306-1, µg.
- $T_m$=Dry gas meter temperature, °F.
- $Y_m$=Dry gas meter correction factor, dimensionless.
- $V_m$=Dry gas meter volume, ft$^3$.
- $P_{bar}$=Barometric pressure, in. Hg.

8.2 Approximate Mass Emission Rate (Optional). Calculate an approximate mass emission rate of Cr in kg/hr using the following equation:

$$\text{kg/hr} = 0.0001597 \left( C_{Cr} \right) \left( r^2 \right) \left( \sqrt{\Delta p} \right) \frac{\left( T_m + 460 \right)}{\left( P_{bar} \right) (28.73)}$$  
Eq. 306A-3

where:

- $r$=Radius of stack, in.
- $\Delta p$=Average of $\Delta p$ values.
- $T_m$=Stack temperature, °F.
- $P_{bar}$=Barometric pressure, in. Hg.
- $C_{Cr}$=Concentration of Cr, mg/dscm.

NOTE: The emission rate calculated using Equation 306A-3 is based on an assumed moisture content of 2%.

9. Bibliography

3.1 The surface tension of the tank bath may be measured by using a tensiometer, a stalagmometer or any other device suitable for measuring surface tension in dynes per centimeter. If the tensiometer is used, the instructions given in ASTM Method D 1331-89, Standard Test Methods for Surface and Interfacial Tension of Solutions of Surface Active Agents (incorporated by reference—see §63.14) must be followed. If a stalagmometer or other device is used to measure surface tension, the instructions that came with the measuring device must be followed.

3.2 (a) Measurements of the bath surface tension are done using a progressive system which minimizes the number of surface tension measurements required when the proper surface tension is maintained. Initially, measurements must be made every 4 hours of tank operation for the first 40 hours of tank operation after the compliance date. Once there are no exceedances during 40 hours of tank operation, measurements may be conducted once every 8 hours of tank operation. Once there are no exceedances during 40 hours of tank operation, measurements may be conducted once every 40 hours of tank operation on an on-going basis, until an exceedance occurs. The maximum time interval for measurements is once every 40 hours of tank operation.

(b) If a measurement of the surface tension of the solution is above the 45 dynes per centimeter limit, the time interval reverts back to the original monitoring schedule of once every 4 hours. A subsequent decrease in frequency would then be allowed according to the previous paragraph.

4. Recordkeeping

4.1 Log book of surface tension measurements and fume suppressant additions. The surface tension of the plating or anodizing tank bath must be measured as specified in section 3.2. The measurements must be recorded in the log book. In addition to the record of surface tension measurements, the frequency of fume suppressant maintenance additions and the amount of fume suppressant added during each maintenance addition will be recorded in the log book. The log book will be readily available for inspection by regulatory personnel.

4.2 Instructions for apparatus used in measuring surface tension. Also included with the log book must be a copy of the instructions for the apparatus used for measuring the surface tension of the plating or anodizing bath. If a tensiometer is used, a copy of ASTM Method D 1331-89, Standard Test Methods for Surface and Interfacial Tension of Solutions of Surface Active Agents (incorporated by reference—see §63.14) must be included with the log book.
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being used. A 6-inch by 1-inch slope is recommended; however the slope may vary depending on the size and design of the solvent cleaning machine.

**Note:** It is important that the inclined liquid level indicators be constructed with ease of reading in mind. The inclined liquid level indicators should also be mounted so that they can be raised or lowered if necessary to suit the solvent cleaning machine size.

![Diagram of inclined liquid level indicators](image)

**Figure 307-1. Inclined Liquid Level Indicator Apparatus.**

2.2 Horizontal Indicator. Device to check the inclined liquid level indicators orientation relative to horizontal.

2.3 Velocity Meter. Hotwire and vane anemometers, or other devices capable of measuring the flow rates ranging from 0 to 15.2 meters per minute across the solvent cleaning machine.

![Diagram of solvent cleaner test setup](image)

**Figure 307-2. Solvent Cleaner Test Setup.**

3. Procedure

3.1 Connection of the Inclined Liquid Level Indicator. Connect one of the inclined liquid level indicators to the boiling sump drain and the other inclined liquid level indicator to the immersion sump drain using Teflon tubing and the appropriate fittings. A schematic diagram is shown in figure 307-2.

<table>
<thead>
<tr>
<th>Date</th>
<th>Run</th>
<th>Solvent type</th>
<th>Solvent density, g/m³ (lb/ft³)</th>
<th>Length of boiling sump (Sₘ), m (ft)</th>
<th>Width of boiling sump (Wₘ), m (ft)</th>
<th>Length of immersion sump (Sᵢ), m (ft)</th>
<th>Width of immersion sump (Wᵢ), m (ft)</th>
<th>Length of solvent vapor/air interface (Sᵥ), m (ft)</th>
<th>Width of solvent vapor/air interface (Wᵥ), m (ft)</th>
</tr>
</thead>
</table>

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4. Calculations

4.1 Nomenclature.

\[ A_B = \text{area of boiling sump interface, m}^2 \text{ (ft}^2) \]

\[ A_I = \text{area of immersion sump interface, m}^2 \text{ (ft}^2) \]

\[ A_V = \text{area of solvent/air interface, m}^2 \text{ (ft}^2) \]

\[ E = \text{emission rate, kg/m}^2\text{-hr (lb/ft}^2\text{-hr)} \]

\[ K = 100,000 \text{ cm . g/m . kg for metric units.} \]

\[ K = 12 \text{ in./ft for English units.} \]

\[ L_{fi} = \text{final boiling sump inclined liquid level indicators reading, cm (in.).} \]

\[ L_{ii} = \text{initial boiling sump inclined liquid level indicators reading, cm (in.).} \]

\[ L_{si} = \text{initial immersion sump inclined liquid level indicators reading, cm (in.).} \]

\[ L_{fii} = \text{final immersion sump inclined liquid level indicators reading, cm (in.).} \]

\[ S_B = \text{length of the boiling sump, m (ft).} \]

\[ S_I = \text{length of the immersion sump, m (ft).} \]

\[ S_V = \text{length of the solvent vapor/air interface, m (ft).} \]

\[ W_B = \text{width of the boiling sump, m (ft).} \]

\[ W_I = \text{width of the immersion sump, m (ft).} \]

\[ W_V = \text{width of the solvent vapor/air interface, m (ft).} \]

\[ \rho = \text{density of solvent, g/m}^3 \text{ (lb/ft}^3\text{).} \]

\[ \theta = \text{test time, hr.} \]

4.2 Area of Sump Interfaces. Calculate the areas of the boiling and immersion sump interfaces as follows:

\[ A_B = S_B W_B \quad \text{Eq. 307-1} \]

\[ A_I = S_I W_I \quad \text{Eq. 307-2} \]

4.3 Area of Solvent/Air Interface. Calculate the area of the solvent vapor/air interface as follows:

\[ A_V = S_V W_V \quad \text{Eq. 307-3} \]

4.4 Emission Rate. Calculate the emission rate as follows:

\[ E = \frac{(L_{fi} - L_{ii})\rho A_B + (L_{fii} - L_{ii})\rho A_I}{K A_V \theta} \]

\[ \text{Eq. 307-4} \]

METHOD 308—PROCEDURE FOR DETERMINATION OF METHANOL EMISSION FROM STATIONARY SOURCES

1. Scope and Application


1.1 Applicability. This method applies to the measurement of methanol emissions from specified stationary sources.

2. Summary of Method

A gas sample is extracted from the sampling point in the stack. The methanol is collected in deionized distilled water and adsorbed on silica gel. The sample is returned to the laboratory where the methanol in the water fraction is separated from other organic compounds with a gas chromatograph.
Environmental Protection Agency

5.0 Safety

5.1 Disclaimer. This method may involve hazardous materials, operations, and equipment. This test method does not purport to address all of the safety problems associated with its use. It is the responsibility of the user of this test method to establish appropriate safety and health practices and to determine the applicability of regulatory limitations before performing this test method.

5.2 Methanol Characteristics. Methanol is flammable and a dangerous fire and explosion risk. It is moderately toxic by ingestion and inhalation.

6.0 Equipment and Supplies

6.1 Sample Collection. The following items are required for sample collection:

6.1.1 Sampling Train. The sampling train is shown in Figure 308±1 and component parts are discussed below.

6.1.1.1 Probe. Teflon®, approximately 6-millimeter (mm) (0.24 inch) outside diameter.

6.1.1.2 Impinger. A 30-milliliter (ml) midgert impinger. The impinger must be connected with leak-free glass connectors. Silicone grease may not be used to lubricate the connectors.

6.1.1.3 Adsorbent Tube. Glass tubes packed with the required amount of the specified adsorbent.

6.1.1.4 Valve. Needle valve, to regulate sample gas flow rate.

6.1.1.5 Pump. Leak-free diaphragm pump, or equivalent, to pull gas through the sampling train. Install a small surge tank between the pump and rate meter to eliminate the pulsation effect of the diaphragm pump on the rotameter.

6.1.1.6 Rate Meter. Rotameter, or equivalent, capable of measuring flow rate to within 2 percent of the selected flow rate of up to 1000 milliliter per minute (ml/min). Alternatively, the tester may use a critical orifice to set the flow rate.

6.1.1.7 Volume Meter. Dry gas meter (DGM), sufficiently accurate to measure the sample volume to within 2 percent, calibrated at the selected flow rate and conditions actually encountered during sampling, and equipped with a temperature sensor (dial thermometer, or equivalent) capable of measuring temperature accurately to within 3°C (54°F).

6.1.1.8 Barometer. Mercury (Hg) aneroid, or other barometer capable of measuring atmospheric pressure to within 2.5 mm (0.1 inch) Hg. See the NOTE in Method 5 (40 CFR part 60, appendix A), section 6.1.2.

6.1.1.9 Vacuum Gauge and Rotameter. At least 700-mm (30-inch) Hg gauge and 0 to 40-ml/min rotameter, to be used for leak-check of the sampling train.

6.2 Sample Recovery. The following items are required for sample recovery:

6.2.1 Wash Bottles. Polyethylene or glass, 500-ml, two.

6.2.2 Sample Vials. Glass, 40-ml, with Teflon®-lined septa, to store impinger samples (one per sample).

6.2.3 Graduated Cylinder. 100-ml size.

6.3 Analysis. The following are required for analysis:

6.3.1 Gas Chromatograph. GC with an FID, programmable temperature control, and heated liquid injection port.

6.3.2 Pump. Capable of pumping 100 ml/min. For flushing sample loop.

6.3.3 Flow Meter. To monitor accurately sample loop flow rate of 100 ml/min.

6.3.4 Regulators. Two-stage regulators used on gas cylinders for GC and for cylinder standards.

6.3.5 Recorder. To record, integrate, and store chromatograms.

6.3.6 Syringes. 1.0- and 10-microliter (l) size, calibrated, for injecting samples.

6.3.7 Tubing Fittings. Stainless steel, to plumb GC and gas cylinders.

6.3.8 Vials. Two 5.0-ml glass vials with screw caps fitted with Teflon®-lined septa for each sample.

6.3.9 Pipettes. Volumetric type, assorted sizes for preparing calibration standards.

6.3.10 Volumetric Flasks. Assorted sizes for preparing calibration standards.

6.3.11 Vials. Glass 40-ml with Teflon®-lined septa, to store calibration standards (one per standard).

7.0 Reagents and Standards

NOTE: Unless otherwise indicated, all reagents must conform to the specifications established by the Committee on Analytical Reagents of the American Chemical Society. Where such specifications are not available, use the best available grade.

7.1 Sampling. The following are required for sampling:

7.1.1 Water. Deionized distilled to conform to the American Society for Testing and Materials (ASTM) Specification D 1193±77, Type 3. At the option of the analyst, the potassium permanganate (KMnO4) test for oxidizable organic matter may be omitted when high concentrations of organic material are not expected to be present.

7.1.2 Silica Gel. Deactivated chromatographic grade 20/40 mesh silica gel packed in glass adsorbent tubes. The silica
gel is packed in two sections. The front section contains 520 milligrams (mg) of silica gel, and the back section contains 260 mg.

7.2 Analysis. The following are required for analysis:

7.2.1 Water. Same as specified in section 7.1.1.

7.2.2 n-Propanol, 3 Percent. Mix 3 ml of n-propanol with 97 ml of water.

7.2.3 Methanol Stock Standard. Prepare a methanol stock standard by weighing 1 gram of methanol into a 100-ml volumetric flask. Dilute to 100 ml with water.

7.2.3.1 Methanol Working Standard. Prepare a methanol working standard by pipetting 1 ml of the methanol stock standard into a 100-ml volumetric flask. Dilute the solution to 100 ml with water.

7.2.3.2 Methanol Standards For Impinger Samples. Prepare a series of methanol standards by pipetting 1, 2, 5, 10, and 25 ml of methanol working standard solution respectively into five 50-ml volumetric flasks. Dilute the solutions to 50 ml with water. These standards will have 2, 4, 10, 20, and 50 µg/ml of methanol, respectively. After preparation, transfer the solutions to 40-ml glass vials capped with Teflon®-lined septa and store the vials under refrigeration. Discard any excess solution.

7.2.3.3 Methanol Standards for Adsorbent Tube Samples. Prepare a series of methanol standards by first pipetting 10 ml of the methanol working standard into a 100-ml volumetric flask and diluting the contents to exactly 100 ml with 3 percent n-propanol solution. This standard will contain 10 µg/ml of methanol. Pipette 5, 15, and 25 ml of this standard, respectively, into four 50-ml volumetric flasks. Dilute each solution to 50 ml with 3 percent n-propanol solution. These standards will have 1, 3, and 5 µg/ml of methanol, respectively. Transfer all four standards into 40-ml glass vials capped with Teflon®-lined septa and store under refrigeration. Discard any excess solution.

7.2.4 GC Column. Capillary column, 30 meters (100 feet) long with an inside diameter (ID) of 0.53 mm (0.02 inch), coated with DB-624 to a film thickness of 3.0 micrometers, (µm) or an equivalent column. Alternatively, a 30-meter capillary column coated with polyethylene glycol to a film thickness of 1 µm such as AT-WAX or its equivalent.

7.2.5 Helium. Ultra high purity.

7.2.6 Hydrogen. Zero grade.

7.2.7 Oxygen. Zero grade.

8.0 Procedure

8.1 Sampling. The following items are required for sampling:

8.1.1 Preparation of Collection Train. Measure 20 ml of water into the midget impinger. The adsorbent tube must contain 520 mg of silica gel in the front section and 260 mg of silica gel in the backup section. Assemble the train as shown in Figure 308-1. An optional, second impinger that is left empty may be placed in front of the water-containing impinger to act as a condensate trap. Place crushed ice and water around the impinger.
8.1.2 Leak Check. A leak check prior to the sampling run is optional; however, a leak check after the sampling run is mandatory. The leak-check procedure is as follows:

Temporarily attach a suitable (e.g., 0 to 400 ml/min) rotameter to the outlet of the DGM, and place a vacuum gauge at or near the probe inlet. Plug the probe inlet, pull a vacuum of at least 250 mm (10 inch) Hg, and note the flow rate as indicated by the rotameter. A leakage rate not in excess of 2 percent of the average sampling rate is acceptable.

Note: Carefully release the probe inlet plug before turning off the pump.

8.1.3 Sample Collection. Record the initial DGM reading and barometric pressure. To begin sampling, position the tip of the Teflon tubing at the sampling point, connect the tubing to the impinger, and start the pump. Adjust the sample flow to a constant rate between 200 and 1000 ml/min as indicated by the rotameter. Maintain this constant rate (±10 percent) during the entire sampling run. Take readings (DGM, temperatures at DGM and at impinger outlet, and rate meter) at least every 5 minutes. Add more ice during the run to keep the temperature of the gases leaving the last impinger at 20 °C (68 °F) or less. At the conclusion of each run,
turn off the pump, remove the Teflon® tubing from the stack, and record the final readings. Conduct a leak check as in section 8.1.2. (This leak check is mandatory.) If a leak is found, void the test run or use procedures acceptable to the Administrator to adjust the sample volume for the leakage.

8.2 Sample Recovery. The following items are required for sample recovery:

8.2.1 Impinger. Disconnect the impinger. Pour the contents of the midget impinger into a graduated cylinder. Rinse the midget impinger and the connecting tubes with water, and add the rinses to the graduated cylinder. Record the sample volume. Transfer the sample to a glass vial and cap with a Teflon® septum. Discard any excess sample. Place the samples in an ice chest for shipment to the laboratory.

8.2.2 Adsorbent Tubes. Seal the silica gel adsorbent tubes and place them in an ice chest for shipment to the laboratory.

9.0 Quality Control

9.1 Miscellaneous Quality Control Measures. The following quality control measures are required:

<table>
<thead>
<tr>
<th>Section</th>
<th>Quality control measure</th>
<th>Effect</th>
</tr>
</thead>
<tbody>
<tr>
<td>8.1.2, 8.1.3, 10.1.3</td>
<td>Sampling equipment leak check and calibration</td>
<td>Ensures accurate measurement of sample volume.</td>
</tr>
<tr>
<td>10.2</td>
<td>GC calibration</td>
<td>Ensures precision of GC analysis.</td>
</tr>
</tbody>
</table>

9.2 Applicability. When the method is used to analyze samples to demonstrate compliance with a source emission regulation, an audit sample must be analyzed, subject to availability.

9.3 Audit Procedure. Analyze an audit sample with each set of compliance samples. Concurrently analyze the audit sample and a set of compliance samples in the same manner to evaluate the technique of the analyst and the standards preparation. The same analyst, analytical reagents, and analytical system shall be used both for the compliance samples and the EPA audit sample.

9.4 Audit Sample Availability. Audit samples will be supplied only to enforcement agencies for compliance tests. Audit samples may be obtained by writing: Source Test Audit Coordinator (MD-77B), Air Measurement Research Division, National Exposure Research Laboratory, U.S. Environmental Protection Agency, Research Triangle Park, NC 27711 or by calling the Source Test Audit Coordinator (STAC) at (919) 541-7834. The audit sample request must be made at least 30 days prior to the scheduled compliance sample analysis.

9.5 Audit Results. Calculate the audit sample concentration according to the calculation procedure provided in the audit instructions included with the audit sample.

Fill in the audit sample concentration and the analyst’s name on the audit response form included with the audit instructions. Send one copy to the EPA Regional Office or the appropriate enforcement agency and a second copy to the STAC. The EPA Regional office or the appropriate enforcement agency will report the results of the audit to the laboratory being audited. Include this response with the results of the compliance samples in relevant reports to the EPA Regional Office or the appropriate enforcement agency.

10.0 Calibration and Standardization

10.1 Metering System. The following items are required for the metering system:

10.1.1 Initial Calibration.

10.1.1.1 Before its initial use in the field, first leak-check the metering system (drying tube, needle valve, pump, rotameter, and DGM) as follows: Place a vacuum gauge at the inlet to the drying tube, and pull a vacuum of 250 mm (10 inch) Hg; plug or pinch off the outlet of the flow meter, and then turn off the pump. The vacuum shall remain stable for at least 30 seconds. Carefully release the vacuum gauge before releasing the flow meter end.

10.1.1.2 Next, remove the drying tube, and calibrate the metering system (at the sampling flow rate specified by the method) as follows: Connect an appropriately sized wet test meter (e.g., 1 liter per revolution (0.035 cubic feet per revolution)) to the inlet of the drying tube. Make three independent calibrations runs, using at least five revolutions of the DGM per run. Calculate the calibration factor, Y (wet test meter calibration volume divided by the DGM volume, both volumes adjusted to the same reference temperature and pressure), for each run, and average the results. If any Y-value deviates by more than 2 percent from the average, the metering system is unacceptable for use. Otherwise, use the average as the calibration factor for subsequent test runs.

10.1.2 Posttest Calibration Check. After each field test series, conduct a calibration check as in section 10.1.1 above, except for the following variations: (a) The leak check is not to be conducted, (b) three, or more revolutions of the DGM may be used, and (c) only two independent runs need be made. If the calibration factor does not deviate by more than 5 percent from the initial calibration factor (determined in section 10.1.1), then the DGM volumes obtained during the test series are acceptable. If the calibration factor deviates by more than 5 percent, recalibrate the metering system as in section 10.1.1, and for the calculations, use the calibration factor (initial or recalibration) that yields the lower gas volume for each test run.

10.1.3 Temperature Sensors. Calibrate against mercury-in-glass thermometers.
10.1.4 Rotameter. The rotameter need not be calibrated, but should be cleaned and maintained according to the manufacturer’s instruction.

10.2 Gas Chromatograph. The following procedures are required for the gas chromatograph:

10.2.1 Initial Calibration. Inject 1 µl of each of the standards prepared in sections 7.2.3.3 and 7.2.3.4 into the GC and record the response. Repeat the injections for each standard until two successive injections agree within 5 percent. Using the mean response for each calibration standard, prepare a linear least squares equation relating the response to the mass of methanol in the sample. Perform the calibration before analyzing each set of samples.

10.2.2 Continuing Calibration. At the beginning of each day, analyze the mid level calibration standard as described in section 10.5.1. The response from the daily analysis must agree with the response from the initial calibration within 10 percent. If it does not, the initial calibration must be repeated.

11.0 Analytical Procedure

11.1 Gas Chromatograph Operating Conditions. The following operating conditions are required for the GC:

11.1.1 Injector. Configured for capillary column, splitless, 200 °C (392 °F).

11.1.2 Carrier. Helium at 10 ml/min.

11.1.3 Oven. Initially at 45 °C for 3 minutes; then raise by 10 °C to 70 °C; then raise by 70 °C/min to 200 °C.

11.2 Impinger Sample. Inject 1 µl of the stored sample into the GC. Repeat the injection and average the results. If the sample response is above that of the highest calibration standard, either dilute the sample until it is in the measurement range of the calibration line or prepare additional calibration standards. If the sample response is below that of the lowest calibration standard, prepare additional calibration standards. If additional calibration standards are prepared, there shall be at least two that bracket the response of the sample. These standards should produce approximately 50 percent and 150 percent of the response of the sample.

11.3 Silica Gel Adsorbent Sample. The following items are required for the silica gel adsorbent samples:

11.3.1 Preparation of Samples. Extract the front and backup sections of the adsorbent tube separately. With a file, score the glass adsorbent tube in front of the first section of silica gel. Break the tube open. Remove and discard the glass wool. Transfer the first section of the silica gel to a 5-ml glass vial and stopper the vial. Remove the spacer between the first and second section of the adsorbent tube and discard it. Transfer the second section of silica gel to a separate 5-ml glass vial and stopper the vial.

11.3.2 Desorption of Samples. Add 3 ml of the 10 percent n-propanol solution to each of the stoppered vials and shake or vibrate the vials for 30 minutes.

11.3.3 Inject a 1-µl aliquot of the diluted sample from each vial into the GC. Repeat the injection and average the results. If the sample response is above that of the highest calibration standard, either dilute the sample until it is in the measurement range of the calibration line or prepare additional calibration standards. If the sample response is below that of the lowest calibration standard, prepare additional calibration standards. If additional calibration standards are prepared, there shall be at least two that bracket the response of the sample. These standards should produce approximately 50 percent and 150 percent of the response of the sample.

12.0 Data Analysis and Calculations

12.1 Nomenclature.

\[ V_i = \text{Volume of back half adsorbent sample, ml} \]

\[ V_b = \text{Volume of front half adsorbent sample, ml} \]

\[ V_{imp} = \text{Volume of impinger sample, ml} \]

\[ V_{dcm} = \text{Dry gas volume measured by the DGM, dry cubic meters (dcm)} \]

\[ V_{dcf} = \text{Dry gas volume measured by the DGM, corrected to standard conditions, dry cubic feet (dcf)} \]

12.2 Mass of Methanol. Calculate the total mass of methanol collected in the sampling train using Equation 308-1.
12.3 Dry Sample Gas Volume, Corrected to Standard Conditions. Calculate the volume of gas sampled at standard conditions using Equation 308-2.

\[ V_{m\text{ (std)}} = \frac{V_{m} Y T_{std} P_{bar}}{T_{m} P_{std}} \]  

Equation 308 - 2

12.4 Mass Emission Rate of Methanol. Calculate the mass emission rate of methanol using Equation 308-3.

\[ E = \frac{M_{tot} Q_{sd}}{V_{m\text{ (std)}}} \]  

Equation 308 - 3

13.0 Method Performance [Reserved]

14.0 Pollution Prevention [Reserved]

15.0 Waste Management [Reserved]

16.0 Bibliography


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equipped with a capillary column 30 meters long.

6.2 Chromatograph conditions for Sigma 1:
   6.2.1 Helium pressure: 50 l/min at inlet A, 14 psi aux
   6.2.2 Carrier flow: 25 cc/min
   6.2.3 Range switch: 100x
   6.2.4 DB: 1 capillary column

6.3 Chromatograph conditions for Hewlett-Packard GC:
   6.3.1 Initial temperature: 40 °C
   6.3.2 Initial time: 8 min
   6.3.3 Rate: 0
   6.3.4 Range: 2
   6.3.5 DB: 1705 capillary column
   6.4 Septum bottles and stoppers
   6.5 Gas Syringe—0.5 cc

7.0 Reagents and Standards

7.1 Chloroform, 99.9+%, A.S.C. HPLC grade

8.0 Sample Collection, Preservation, and Storage

8.1 A representative sample should be caught in a clean 8 oz. container with a secure lid.
8.2 The container should be labeled with sample identification, date and time.

9.0 Quality Control

9.1 The instrument is calibrated by injecting calibration solution (Section 10.2 of this method) five times.
9.2 The retention time for components of interest and relative response of monomer to the internal standard is determined. Recovery efficiency must be determined once for each sample type and whenever modifications are made to the method.
9.3 Determine the percent hexane in three separate dried rubber crumb samples.
9.4 Weigh a portion of each crumb sample into separate sample bottles and add a known amount of hexane (10 microliters) by microliter syringe and 20 microliters of internal standard. Analyze each by the described procedure and calculate the percent recovery of the known added hexane.
9.4.1 Repeat the previous step using twice the hexane level (20 microliters), analyze and calculate the percent recovery of the known added hexane.
9.4.2 Set up two additional sets of samples using 10 microliters and 20 microliters of hexane as before, but add an amount of water equal to the dry crumb used. Analyze and calculate percent recovery to show the effect of free water on the results obtained.
9.5 A value of R between 0.70 and 1.30 is acceptable.
9.6 R shall be used to correct all reported results for each compound by dividing the measured results of each compound by the R for that compound for the same sample type.

10.0 Calibration and Instrument Settings

10.1 Calibrate the chromatograph using a standard made by injecting 10 µl of fresh hexane and 20 µl of chloroform into a sealed septum bottle. This standard will be 0.6 wt.% total hexane based on 1 gram of dry rubber.
10.2 Analyze the hexane used and calculate the percentage of each hexane isomer (2-methylpentane, 3-methylpentane, n-hexane, and methylcyclo-pentane). Enter these percentages into the method calibration table.
10.3 Heat the standard bottle for 30 minutes in a 105 °C oven.
10.4 Inject about 0.25 cc of vapor into the gas chromatograph and after the analysis is finished, calibrate according to the procedures described by the instrument manufacturer.

11.0 Procedure

11.1 Using a cold mill set at a wide roller gap (125-150 mm), mill about 250 grams of crumb two times to homogenize the sample.
11.2 Weigh about 2 grams of wet crumb into a septum bottle and cap with a septum ring. Add 20 µl of chloroform with a syringe and place in a 105 °C oven for 45 minutes.
11.3 Run the moisture content on a separate portion of the sample and calculate the grams of dry rubber put into the septum bottle.
11.4 Set up the data station on the required method and enter the dry rubber weight in the sample weight field.
11.5 Inject a 0.25 cc vapor sample into the chromatograph and push the start button.
11.6 At the end of the analysis, the data station will print a report listing the concentration of each identified component.
11.7 To analyze water samples, pipet 5 ml of sample into the septum bottle, cap and add 20 µl of chloroform. Place in a 105 °C oven for 30 minutes.
11.8 Enter 5 grams into the sample weight field.
11.9 Inject a 0.25 cc vapor sample into the chromatograph and push the start button.
11.10 At the end of the analysis, the data station will print a report listing the concentration of each identified component.

12.0 Data Analysis and Calculation

12.1 For samples that are prepared as in section 11 of this method, ppm n-hexane is read directly from the computer.
12.2 The formulas for calculation of the results are as follows:

\[ ppm_{\text{n-hexane}} = \frac{(A_{\text{hexane}} \times R_{\text{hexane}})}{(A_{\text{int}} \times R_{\text{int}})} \]

Where:
- \( A_{\text{hexane}} \) = area of hexane
- \( R_{\text{hexane}} \) = response of hexane
- \( A_{\text{int}} \) = area of the internal standard
- \( R_{\text{int}} \) = response of the internal standard
% hexane in crumb = \frac{\text{ppm}_{\text{hexane}}}{\text{sample amount}} \times 100

12.3 Correct the results by the value of R (as determined in sections 9.3.4, 9.3.5, and 9.3.6 of this method).

13.0 Method Performance

13.1 The test has a standard deviation of 0.14 wt% at 0.66 wt% hexane. Spike recovery of 12 samples at two levels of hexane averaged 102.3%. Note: Recovery must be determined for each type of sample. The values given here are meant to be examples of method performance.

14.0 Pollution Prevention

14.1 Waste generation should be minimized where possible. Sample size should be an amount necessary to adequately run the analysis.

15.0 Waste Management

15.1 All waste shall be handled in accordance with federal and state environmental regulations.

16.0 References and Publications

16.1 DSM Copolymer Test Method T-3380.

METHOD 310B—DETERMINATION OF RESIDUAL HEXANE THROUGH GAS CHROMATOGRAPHY

1.0 Scope and Application

1.1 Data Quality Objectives:

In the production of ethylene-propylene terpolymer crumb rubber, the polymer is recovered from solution by flashing off the solvent with steam and hot water. The resulting water-crumble slurry is then pumped to the finishing units. Certain amounts of solvent (hexane being the most commonly used solvent) and diene monomer remain in the crumb. The analyst uses the following procedure to determine those amounts.

2.0 Summary of Method

2.1 The crumb rubber sample is dissolved in toluene to which heptane has been added as an internal standard. Acetone is then added to this solution to precipitate the crumb, and the supernatant is analyzed for hexane and diene by a gas chromatograph equipped with a flame ionization detector (FID).

3.0 Definitions

3.1 Included in text as needed.

4.0 Interferences

4.1 Benzene, introduced as a contaminant in the toluene solvent, elutes between methylicyclopentane and cyclohexane. However, the benzene peak is completely resolved.

4.2 2,2-dimethyl pentane, a minor component of the hexane used in our process, elutes just prior to methyl cyclopentane. It is included as “hexane” in the analysis whether it is integrated separately or included in the methyl cyclopentane peak.

5.0 Safety

5.1 This procedure does not purport to address all of the safety concerns associated with its use. It is the responsibility of the user of this procedure to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

5.2 Chemicals used in this analysis are flammable and hazardous (see specific toxicity information below). Avoid contact with sources of ignition during sample prep. All handling should be done beneath a hood. Playtex or nitrile gloves recommended.

5.3 Hexane is toxic by ingestion and inhalation. Vapor inhalation causes irritation of nasal and respiratory passages, headache, dizziness, nausea, central nervous system depression. Chronic overexposure can cause severe nerve damage. May cause irritation on contact with skin or eyes. May cause damage to kidneys.

5.3 ENB may be harmful by inhalation, ingestion, or skin absorption. Vapor or mist is irritating to the eyes, mucous membranes, and upper respiratory tract. Causes skin irritation.

5.4 Toluene is harmful or fatal if swallowed. Vapor harmful if inhaled. Symptoms: headache, dizziness, hallucinations, distorted perceptions, changes in motor activity, nausea, diarrhea, respiratory irritation, central nervous system depression, unconsciousness, liver, kidney and lung damage. Contact can cause severe eye irritation. May cause skin irritation. Causes irritation of eyes, nose, and throat.
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5.5 Acetone, at high concentrations or prolonged overexposure, may cause headache, dizziness, irritation of eyes and respiratory tract, loss of strength, and narcosis. Eye contact causes severe irritation; skin contact may cause mild irritation. Concentrations of 20,000 ppm are immediately dangerous to life and health.

5.6 Heptane is harmful if inhaled or swallowed. May be harmful if absorbed through the skin. Vapor or mist is irritating to the eyes, mucous membranes, and upper respiratory tract. Prolonged or repeated exposure to skin causes defatting and dermatitis.

5.7 The steam oven used to dry the polymer in this procedure is set at 110 °C. Wear leather gloves when removing bottles from the oven.

6.0 Equipment and Supplies

6.1 4000-ml volumetric flask
6.2 100-ml volumetric pipette
6.3 1000-ml volumetric flask
6.4 8-oz. French Square sample bottles with plastic-lined caps
6.5 Top-loading balance
6.6 Laboratory shaker
6.7 Laboratory oven set at 110 °C (steam oven)
6.8 Gas chromatograph, Hewlett-Packard 5890A, or equivalent, interfaced with HP 7673A (or equivalent) autosampler (equipped with nanoliter adapter and robotic arm), and HP 3396 series II or 3392A (or equivalent) integrator/controller.
6.9 GC column, capillary type, 50m x 0.53mm, methyl silicone, 5 micron film thickness, Quadrex, or equivalent.
6.10 Computerized data acquisition system, such as CISCALS

6.11 Crimp-top sample vials and HP p/n 5881-1211 crimp caps.
6.12 Glass syringes, 5-ml, with "Luer-lock" fitting
6.13 Filters, PTFE, 45um pore size, Gelman Acrodisc or equivalent, to fit on Luer-lock syringes (in 6.12, above).

7.0 Reagents and Standards

7.1 Reagent toluene, EM Science Omnisolv
Purity Check: Prior to using any bottle of reagent toluene, analyze it according to section 11.2 of this method. Use the bottle only if hexane, heptane, and ENB peak areas are less than 15 each (note that an area of 15 is equivalent to less than 0.01 wt% in a 10g sample).

7.2 Reagent acetone, EM Science Omnisolv HR±GC
Purity Check: Prior to using any bottle of reagent acetone, analyze it according to section 11.2 of this method. Use the bottle only if hexane, heptane, and ENB peak areas are less than 15 each.

7.3 Reagent heptane, Aldrich Chemical Gold Label, Cat #15,487±3
Purity Check: Prior to using any bottle of reagent heptane, analyze it according to section 11.2 of this method. Use the bottle only if hexane and ENB peak areas are less than 5 each.

7.4 Internal standard solution—used as a concentrate for preparation of the more dilute Polymer Dissolving Solution. It contains 12.0g heptane/100ml of solution which is 120.0g per liter.

Preparation of internal standard solution (polymer dissolving stock solution):

7.4.1 Tare a clean, dry 1-liter volumetric flask on the balance. Record the weight to three places.

7.4.2 Weigh 120.00 g of n-heptane into the flask. Record the total weight of the flask and heptane as well as the weight of heptane added.

7.4.3 Fill the flask close to the mark with toluene, about 1 to 2″ below the mark.

7.4.4 Shake the flask vigorously to mix the contents ............... Allow any bubbles to clear before proceeding to the next step.

7.4.5 Top off the flask to the mark with toluene. Shake vigorously, as in section 5.4.4 of this method, to mix well.

7.4.6 Weigh the flask containing the solution on the three place balance record the weight.

7.4.7 Transfer the contents of the flask to a 1 qt Boston round bottle.

7.4.8 Label the bottle with the identity of the contents, the weights of heptane and toluene used, the date of preparation and the preparer’s name.

7.4.9 Refrigerate the completed blend for the use of the routine Technicians.

7.5 Polymer Dissolving Solution ("PDS")—Heptane (as internal standard) in toluene. This solution contains 0.3g of
heptane internal standard per 100 ml of solution.

7.5.1 Fill a 4000ml volumetric flask about
¾ full with toluene.

7.5.2 Add 100 ml of the internal standard
solution (section 7.4 of this method) to the
flask using the 100ml pipette.

7.5.3 Fill the flask to the mark with toluene. Discard any excess.

7.5.4 Add a large magnetic stirring bar to
the flask and mix by stirring.

7.5.5 Transfer the polymer solvent solution
to the one-gallon labeled container with
50ml volumetric dispenser attached.

7.5.6 Purity Check: Analyze according to
section 11.2. NOTE: You must ‘precipitate’
the sample with an equal part of acetone
(thus duplicating actual test conditions—see
section 11.1 of this method, sample prep) be-
fore analyzing. Analyze the reagent 3 times
in order to find the percentage of each
isomer. The results must agree among the three runs (within 10%).

7.5.7 Tag the bottle with the following in-
formation:

POLYMER DISSOLVING SOLUTION
FOR C6 IN CRUMB ANALYSIS
PREPARER’S NAME
DATE
CALS FILE ID’S OF THE THREE
ANALYSES FOR PURITY (from section
7.5.6 of this method)

7.6 Quality Control Solution: The quality
control solution is prepared by adding spe-
cific amounts of mixed hexanes (barge
hexane), n-nonane and ENB to some
polymer dissolving solution. Nonane elutes in the
same approximate time region as ENB and is
used to quantify in that region because it
has a longer shelf life. ENB, having a high
tendency to polymerize, is used in the QC so-
lution only to ensure that both ENB isomers
elute at the proper time.

First, a concentrated stock solution is pre-
pared; the final QC solution can then be pre-
pared by diluting the stock solution.

7.6.1 In preparation of stock solution, fill
a 1-liter volumetric flask partially with
diluent stock solution (PDS)—see sec-
tion 7.5 of this method. Add 20.0 ml barge
hexane, 5.0 ml n-nonane, and 3 ml ENB. Fin-
ish filling the volumetric to the mark with
PDS.

7.6.2 In preparation of quality control so-
lution, dilute the quality control stock solu-
tion (above) precisely 1:10 with PDS, i.e. 10
ml of stock solution made up to 100 ml (volu-
metric flask) with PDS. Pour the solution
into a 4 oz. Boston round bottle and store in
the refrigerator.

8.0 Sample Collection, Preservation and
Storage

8.1 Line up facility to catch crumb sam-

8.2.1 Simultaneously close the cock valves
upstream and downstream of facility.

8.2.2 Close the cock valve beneath
the slurry line in service.

8.2.3 Line up the cooling tower water
through the sample bomb water jacket to
the sewer for a minimum of 30 minutes.

8.2.4 Place the sample catching basket be-
neath facility and open the cock valve under-
neath the bomb to retrieve the rubber
crumb.

8.2.5 If no rubber falls by gravity into the
basket, line up nitrogen to the bleeder up-
stream of the sample bomb and force the
rubber into the basket.

8.2.6 Close the cock valve underneath
the sample bomb.

8.3 Fill a plastic “Whirl-pak” sample bag
with slurry crumb and send it to the lab im-
mediately.

8.4 Once the sample reaches the lab, it
should be prepped as soon as possible to
avoid hexane loss through evaporation. Sam-
ples which have lain untouched for more
than 30 minutes should be discarded.

9.0 Quality Control

Quality control is monitored via a com-
puter program that tracks analyses of a pre-
pared QC sample (from section 7.6.2 of this
method). The QC sample result is entered
daily into the program, which plots the re-
sult as a data point on a statistical chart. If
the data point does not satisfy the “in-con-
trol” criteria (as defined by the lab quality
facilitator), an “out-of-control” flag appears,
mandating corrective action.

In addition, the area of the n-heptane peak
is monitored so that any errors in making up
the polymer dissolving solution will be
catched and corrected. Refer to section 12.4 of
this method.

9.1 Fill an autosampler vial with the qual-
ity control solution (from section 7.6.2 of
this method) and analyze on the GC as nor-
mal (per section 11 of this method).

9.2 Add the concentrations of the 5 hexane
isomers as they appear on the CALS print-
out. Also include the 2,2-dimethyl-pentane
peak just ahead of the methyl cyclopentane
(the fourth major isomer) peak in the event
that the peak integration split this peak out.
Do not include the benzene peak in the sum.

Note the nonane concentration. Record both
results (total hexane and nonane) in the QC
computer program. If out of control, and GC
appears to be functioning within normal pa-
rameters, reanalyze a fresh control sample.
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If the fresh QC is not in control, check stock solution for contaminants or make up a new QC sample with the toluene currently in use. If instrument remains out-of-control, more thorough GC troubleshooting may be needed.

Also, verify that the instrument has detected both isomers of ENB (quantification not necessary—see section 7.0 of this method).

9.3 Recovery efficiency must be determined for each sample type and whenever modifications are made to the method. Recovery shall be between 70 and 130 percent. All test results must be corrected by the recovery efficiency value (R).

9.3.1 Approximately 10 grams of wet EPDM crumb (equivalent to about 5 grams of dry rubber) shall be added to six sample bottles containing 100 ml of hexane in crumb polymer dissolving solution (toluene containing 0.3 gram n-heptane/100 ml solution). The polymer shall be dissolved by agitating the bottles on a shaker for 4 hours. The polymer shall be precipitated using 100 ml acetone.

9.3.2 The supernatant liquid shall be decanted from the polymer. Care shall be taken to remove as much of the liquid phase from the sample as possible to minimize the effect of retained liquid phase upon the next cycle of the analysis. The supernatant liquid shall be analyzed by gas chromatography using an internal standard quantitation method with heptane as the internal standard.

9.3.3 The precipitated polymer from the steps described above shall be re-dissolved using toluene as the solvent. The toluene solvent and acetone precipitant shall be determined to be free of interfering compounds.

9.3.4 The rubber which was dissolved in the toluene shall be precipitated with acetone as before, and the supernatant liquid decanted from the precipitated polymer. The liquid shall be analyzed by gas chromatography and the rubber phase dried in a steam-oven to determine the final polymer weight.

9.3.5 The ratios of the areas of the hexane peaks and of the heptane internal standard peak shall be calculated for each of the six samples in the two analysis cycles outlined above. The area ratios of the total hexane to heptane (R1) shall be determined for the two analysis cycles of the sample set. The ratio of the values of R1 from the second analysis cycle to the first cycle shall be determined to give a second ratio (R2).

10.0 Calibration and Standardization

The procedure for preparing a Quality Control sample with the internal standard in it is outlined in section 7.6 of this method.

10.1 The relative FID response factors for n-heptane, the internal standard, versus the various hexane isomers and ENB are relatively constant and should seldom need to be altered. However Baseline construction is a most critical factor in the production of good data. For this reason, close attention should be paid to peak integration. Procedures for handling peak integration will depend upon the data system used.

10.2 If recalibration of the analysis is needed, make up a calibration blend of the internal standard and the analytes as detailed below and analyze it using the analytical method used for the samples.

10.2.1 Weigh 5 g n-heptane into a tared scintillation vial to five places.

10.2.2 Add 0.2 ml ENB to the vial and reweigh.

10.2.3 Add 0.5 ml hexane to the vial and reweigh.

10.2.4 Cap, and shake vigorously to mix.

10.2.5 Calculate the weights of ENB and of hexane added and divide their weights by the weight of the n-heptane added. The result is the known of given value for the calibration.

10.2.6 Add 0.4 ml of this mixture to a mixture of 100 ml toluene and 100 ml of acetone. Cap and shake vigorously to mix.

10.2.7 Analyze the sample.

10.2.8 Divide the ENB area and the total areas of the hexane peaks by the n-heptane area. This result is the "found" value for the calibration.

10.2.9 Divide the appropriate "known" value from 10.2.5 by the found value from 10.2.8. The result is the response factor for the analyte in question. Previous work has shown that the standard deviation of the calibration method is about 1% relative.

11.0 Procedure

11.1 SAMPLE PREPARATION

11.1.1 Tare an 8 oz sample bottle—Tag attached, cap off; record weight and sample ID on tag in pencil.

11.1.2 Place crumb sample in bottle: RLA–1: 20g; RLA–2: 10g—(gives a dry wt of ~10g); (gives a dry wt of ~5.5g).

11.1.3 Dispense 100 ml of PDS into each bottle. SAMPLE SHOULD BE PLACED INTO SOLUTION ASAP TO AVOID HEXANE LOSS—Using "Dispensette" pipettor. Before dispensing, "purge" the dispensette (25% of its volume) into a waste bottle to eliminate any voids.

11.1.4 Tightly cap bottles and load samples into shaker.

11.1.5 Insure that "ON-OFF" switch on the shaker itself is "ON."

11.1.6 Locate shaker timer. Insure that toggle switch atop timer control box is in the middle ("off") position. If display reads "04:00" (4 hours), move toggle switch to the left position. Shaker should begin operating.

11.1.7 After shaker stops, add 100 ml acetone to each sample to precipitate polymer. Shake minimum of 5 minutes on shaker—
Vistalon sample may not have fully dissolved; nevertheless, for purposes of consistency, 4 hours is the agreed-upon dissolving time.

11.1.8 Using a 5-ml glass Luer-lock syringe and Acrodisc filter, filter some of the supernatant liquid into an autosampler vial; crimp the vial and load it into the GC autosampler for analysis (section 11.2 of this method)—The samples are filtered to prevent polymer buildup in the GC. Clean the syringes in toluene.

11.1.9 Decant remaining supernatant into a hydrocarbon waste sink, being careful not to discard any of the polymer. Place bottle of precipitate into the steam oven and dry for six hours—Some grades of Vistalon produce very small particles in the precipitate, thus making complete decanting impossible without discarding some polymer. In this case, decant as much as possible and put into the oven as is, allowing the oven to drive off remaining supernatant (this practice is avoided for environmental reasons). WARNING: OVEN IS HOT—110°C (230°F).

11.1.10 Cool, weigh and record final weight of bottle.

11.2 GC ANALYSIS

11.2.1 Initiate the CALS computer channel.

11.2.2 Enter the correct instrument method into the GC’s integrator.

11.2.3 Load sample vial(s) into autosampler.

11.2.4 Start the integrator.

11.2.5 When analysis is complete, plot CALS run to check baseline skim.

12.0 Data Analysis and Calculations

12.1 Add the concentrations of the hexane peaks as they appear on the CALS printout. Do not include the benzene peak in the sum.

12.2 Subtract any hexane interferences found in the PDS (see section 7.5.6 of this method); record the result.

12.3 Note the ENB concentration on the CALS printout. Subtract any ENB interference found in the PDS and record this result in a “% ENB by GC” column in a logbook.

12.4 Record the area (from CALS printout) of the heptane internal standard peak in a “C7 area” column in the logbook. This helps track instrument performance over the long term.

12.5 After obtaining the final dry weight of polymer used (section 11.1.10 of this method), record that result in a “dry wt.” column of the logbook.

12.6 Divide the %C6 by the dry weight to obtain the total PHR hexane in crumb. Similarly, divide the %ENB by the dry weight to obtain the total PHR ENB in crumb. Note that PHR is an abbreviation for “parts per hundred”. Record both the hexane and ENB results in the logbook.

12.7 Correct all results by the recovery efficiency value (R).

13.0 Method Performance

13.1 The method has been shown to provide 100% recovery of the hexane analyte. The method was found to give a 6% relative standard deviation when the same six portions of the same sample were carried through the procedure. Note: These values are examples; each sample type must be tested for sample recovery.

14.0 Pollution Prevention

14.1 Dispose of all hydrocarbon liquids in the appropriate disposal sink system; never pour hydrocarbons down a water sink.

14.2 As discussed in section 11.1.9 of this method, the analyst can minimize venting hydrocarbon vapor to the atmosphere by decanting as much hydrocarbon liquid as possible before oven drying.

15.0 Waste Management

15.1 The Technician conducting the analysis should follow the proper waste management practices for their laboratory location.

16.0 References

16.1 Baton Rouge Chemical Plant Analytical Procedure no. BRCP 1302

16.2 Material Safety Data Sheets (from chemical vendors) for hexane, ENB, toluene, acetone, and heptane

METHOD 310C—DETERMINATION OF RESIDUAL N-HExANE IN EPDM RUBBER THROUGH GAS CHROMATOGRAPHY

1.0 Scope and Application

1.1 This method describes a procedure for the determination of residual hexane in EPDM wet crumb rubber in the 0.01—2% range by solvent extraction of the hexane followed by gas chromatographic analysis where the hexane is detected by flame ionization and quantified via an internal standard.

1.2 This method may involve hazardous materials operations and equipment. This method does not purport to address all the safety problems associated with its use, if any. It is the responsibility of the user to consult and establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

2.0 Summary

2.1 Residual hexane contained in wet pieces of EPDM polymer is extracted with MIBK. A known amount of an internal standard (IS) is added to the extract which is subsequently analyzed via gas chromatography where the hexane and IS are separated and detected utilizing a megabore column and flame ionization detection (FID). From the
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response to the hexane and the IS, the amount of hexane in the EPDM polymer is calculated.

3. Definitions

3.1 Hexane—refers to n-hexane
3.2 Heptane—refers to n-heptane
3.3 MIBK—methyl isobutyl ketone (4 methyl 2–Pentanone)

4. Interferences

4.1 Material eluting at or near the hexane and/or the IS will cause erroneous results. Prior to extraction, solvent blanks must be analyzed to confirm the absence of interfering peaks.

5. Safety

5.1 Review Material Safety Data Sheets of the chemicals used in this method.

6. Equipment and Supplies

6.1 4 oz round glass jar with a wide mouth screw cap lid.
6.2 Vacuum oven.
6.3 50 ml pipettes.
6.4 A gas chromatograph with an auto sampler and a 50 meter, 0.53 ID, methyl silicone column with 5 micron phase thickness.
6.5 Shaker, large enough to hold 10, 4 oz. jars.
6.6 1000 and 4000 ml volumetric flasks.
6.7 Electronic integrator or equivalent data system.
6.8 GC autosampler vials.
6.9 50 uL syringe.

7. Reagents and Standards

7.1 Reagent grade Methyl-Iso-Butyl-Ketone (MIBK)
7.2 n-heptane, 99% + purity
7.3 n-hexane, 99% + purity

8. Sample Collection

8.1 Trap a sample of the EPDM crumb slurry in the sampling apparatus. Allow the crumb slurry to circulate through the sampling apparatus for 5 minutes; then close off the values at the bottom and top of the sampling apparatus, trapping the crumb slurry. Run cooling water through the water jacket for a minimum of 30 minutes. Expel the cooled crumb slurry into a sample catching basket. If the crumb does not fall by gravity, force it out with demineralized water or nitrogen. Send the crumb slurry to the lab for analysis.

9. Quality Control

9.1 The Royalene crumb sample is extracted three times with MIBK containing an internal standard. The hexane from each extraction is added together to obtain a total hexane content. The percent hexane in the first extraction is then calculated and used as the recovery factor for the analysis.

9.2 Follow this test method through section 11.4 of the method. After removing the sample of the first extraction to be run on the gas chromatograph, drain off the remainder of the extraction solvent, retaining the crumb sample in the sample jar. Rinse the crumb with demineralized water to remove any MIBK left on the surface of the crumb. Repeat the extraction procedure with fresh MIBK with internal standard two more times.

9.3 After the third extraction, proceed to section 11.5 of this method and obtain the percent hexane in each extraction. Use the sample weight obtained in section 12.1 of this method to calculate the percent hexane in each of the extracts.

9.4 Add the percent hexane obtained from the three extractions for a total percent hexane in the sample.

9.5 Use the following equations to determine the recovery factor (R):

\[
\text{% Recovery of the first extraction} = \left( \frac{\text{% hexane in the first extract}}{\text{total % hexane}} \right) \times 100
\]

\[
\text{Recovery Factor (R)} = \left( \frac{\text{% Hexane Recovered in the first extract}}{100} \right)
\]

10. Calibration

10.1 Preparation of Internal Standard (IS) solution:
Accuracy weigh 30 grams of n-heptane into a 1000 ml volumetric flask. Dilute to the mark with reagent grade MIBK. Label this Solution “A”. Pipette 100 mls. of Solution A into a 4 liter volumetric flask. Fill the flask to the mark with reagent MIBK. Label this Solution “B”. Solution “B” will have a concentration of 0.75 mg/ml of heptane.

10.2 Preparation of Hexane Standard Solution (HS):
Using a 50 uL syringe, weigh by difference, 20 mg of n-hexane into a 50 ml volumetric flask containing approximately 40 ml of Solution B. Fill the flask to the mark with Solution B and mix well.

10.3 Conditions for GC analysis of standards and samples:
Temperature:
Initial=80 °C
Final=150 °C
Injector=160 °C
Detector=250 °C
Program Rate=5.0 °C/min
Initial Time=5 minutes Final Time=6 minutes
Flow Rate=5.0 ml/min
Sensitivity=detector response must be adjusted to keep the hexane and IS on scale.

10.4 Fill an autosampler vial with the HS, analyze it three times and calculate a Hexane Relative Response Factor (RF) as follows:

\[
\text{RF} = \frac{A_{\text{HS}} \times C_{\text{HS}} \times P_{\text{HS}}}{A_{\text{IS}} \times C_{\text{IS}} \times P_{\text{IS}}} \quad (1)
\]
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Where:

\[ A_{IS} = \text{Area of IS peak (Heptane)} \]
\[ A_{HS} = \text{Area of peak (Hexane Standard)} \]
\[ C_{IS} = \text{Mg of Heptane/50 ml IS Solution B} \]
\[ P_{IS} = \text{Purity of the IS n-heptane} \]
\[ P_{HS} = \text{Purity of the HS n-hexane} \]

11.0 Procedure

11.1 Weight 10 grams of wet crumb into a tared (W1), wide mouth 4 oz. jar.
11.2 Pipette 50 ml of Solution B into the jar with the wet crumb rubber.
11.3 Screw the cap on tightly and place it on a shaker for 4 hours.
11.4 Remove the sample from the shaker and fill an autosampler vial with the MIBK extract.
11.5 Analyze the sample two times.
11.6 Analyze the HS twice, followed by the samples. Inject the HS twice at the end of each 10 samples or at the end of the run.

12.0 Calculations

12.1 Drain off the remainder of the MIBK extract from the polymer in the 4 oz. jar. Retain all the polymer in the jar. Place the uncovered jar and polymer in a heated vacuum oven until the polymer is dry. Reweigh the jar and polymer (W2) and calculate the dried sample weight of the polymer as follows:

\[ \text{Dried SW} = W_2 - W_1 (2) \]

12.2 Should the polymer be oil extended, pipette 10 ml of the MIBK extract into a tared evaporating dish (W1) and evaporate to dryness on a steam plate. Reweigh the evaporating dish containing the extracted oil (W2). Calculate the oil content of the polymer as follows:

\[ \text{Gram of oil extracted} = 5(W_2 - W_1) (3) \]

\[ \% \text{Hexane in polymer} = \frac{(A_{\text{IS}} X RF X C_{IS} X P_{IS})}{(A_{\text{IS}} X SW)} (4) \]

Where:

\[ A_{\text{IS}} = \text{Area of sample hexane sample peak} \]
\[ A_{\text{IS}} = \text{Area of IS peak} \]
\[ P_{IS} = \text{Purity of IS} \]
\[ SW = \text{Weight of dried rubber after extraction} \]

\[ \% \text{Corrected Hexane} = \% \text{Hexane in Polymer} / R (5) \]

\[ R = \text{Recovery factor determined in section 9 of this method.} \]

13.0 Method Performance

13.1 Performance must be determined for each sample type by following the procedures in section 9 of this method.

14.0 Waste Generation

14.1 Waste generation should be minimized wherever possible.

15.0 Waste Management

15.1 All waste shall be handled in accordance with Federal and State environmental regulations.

16.0 References

[Reserved]

METHOD 311—ANALYSIS OF HAZARDOUS AIR POLLUTANT COMPOUNDS IN PAINTS AND COATINGS BY DIRECT INJECTION INTO A GAS CHROMATOGRAPH

1. Scope and Application

1.1 Applicability. This method is applicable for determination of most compounds designated by the U.S. Environmental Protection Agency as volatile hazardous air pollutants (HAP’s) (See Reference 1) that are contained in paints and coatings. Styrene, ethyl acrylate, and methyl methacrylate can be measured by ASTM D 4827-93 or ASTM D 4747-87. Formaldehyde can be measured by ASTM PS 9-94 or ASTM D 1979-91. Toluene diisocyanate can be measured in urethane prepolymers by ASTM D 3432-89. Method 311 applies only to those volatile HAP’s which are added to the coating when it is manufactured, not to those which may form as the coating cures (reaction products or cure volatiles). A separate or modified test procedure must be used to measure these reaction products or cure volatiles in order to determine the total volatile HAP emissions from a coating. Cure volatiles are a significant component of the total HAP content of some coatings. The term “coating” used in this method shall be understood to mean paints and coatings.

1.2 Principle. The method uses the principle of gas chromatographic separation and quantification using a detector that responds to concentration differences. Because there are many potential analytical systems or sets of operating conditions that may represent useable methods for determining the concentrations of the compounds cited in Section 1.1 in the applicable matrices, all systems that employ this principle, but differ only in details of equipment and operation, may be used as alternative methods, provided that the prescribed quality control, calibration, and method performance requirements are met. Certified product data sheets (CPDS) may also include information relevant to the analysis of the coating sample including, but not limited to, separation column, oven temperature, carrier gas, injection port temperature, extraction solvent, and internal standard.

2. Summary of Method

Whole coating is added to dimethylformamide and a suitable internal standard compound is added. An aliquot of the sample mixture is injected onto a
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chromatographic column containing a stationary phase that separates the analytes from each other and from other volatile compounds contained in the sample. The concentrations of the analytes are determined by comparing the detector responses for the sample to the responses obtained using known concentrations of the analytes.

3. Definitions [Reserved]

4. Interferences

4.1 Coating samples of unknown composition may contain the compound used as the internal standard. Whether or not this is the case may be determined by following the procedures of Section II and deleting the addition of the internal standard specified in Section II.3. If necessary, a different internal standard may be used.

4.2 The GC column and operating conditions developed for one coating formulation may not ensure adequate resolution of target analytes for other coating formulations. Some formulations may contain nontarget analytes that coelute with target analytes. If there is any doubt about the identification of the internal standard, it may be necessary to analyze the sample using a different GC column or different GC operating conditions.

4.3 Cross-contamination may occur whenever high-level and low-level samples are analyzed sequentially. The order of sample analyses specified in Section II.7 is designed to minimize this problem.

4.4 Cross-contamination may also occur if the devices used to transfer coating during the sample preparation process or for injecting the sample into the GC are not adequately cleaned between uses. All such devices should be cleaned with acetone or other suitable solvent and checked for plugs or cracks before and after each use.

5. Safety

5.1 Many solvents used in coatings are hazardous. Precautions should be taken to avoid unnecessary inhalation and skin or eye contact. This method may involve hazardous materials, operations, and equipment. This test method does not purport to address all of the safety problems associated with its use. It is the responsibility of the user of this test method to establish appropriate safety and health practices and to determine the applicability of regulatory limitations in regards to the performance of this test method.

5.2 Dimethylformamide is harmful if inhaled or absorbed through the skin. The user should obtain relevant health and safety information from the manufacturer. Dimethylformamide should be used only with adequate ventilation. Avoid contact with skin, eyes, and clothing. In case of contact, immediately flush skin or eyes with plenty of water for at least 15 minutes. If eyes are affected, consult a physician. Remove and wash contaminated clothing before reuse.

5.3 User’s manuals for the gas chromatograph and other related equipment should be consulted for specific precautions to be taken related to their use.

6. Equipment and Supplies

NOTE: Certified product data sheets (CPDS) may also include information relevant to the analysis of the coating sample including, but not limited to, separation column, oven temperature, carrier gas, injection port temperature, extraction solvent, and internal standard.

6.1 Sample Collection.

6.1.1 Sampling Containers. Dual-seal sampling containers, four to eight fluid ounce capacity, should be used to collect the samples. Glass sample bottles or plastic containers with volatile organic compound (VOC) impermeable walls must be used for corrosive substances (e.g., etch primers and certain coating catalysts such as methyl ethyl ketone (MEK) peroxide). Sample containers, caps, and inner seal liners must be inert to the compounds in the sample and must be selected on a case-by-case basis.

6.1.1.1 Other routine sampling supplies needed include waterproof marking pens, tubing, scrapers/spatulas, clean rags, paper towels, cooler, long handle tongs, and mixing/stirring paddles.

6.1.1.2: Personal safety equipment needed includes eye protection, respiratory protection, a hard hat, gloves, steel toe shoes, etc.

6.1.3 Shipping supplies needed include shipping boxes, packing material, shipping labels, strapping tape, etc.

6.1.4 Data recording forms and labels needed include coating data sheets and sample can labels.

NOTE: The actual requirements will depend upon the conditions existing at the source sampled.

6.2 Laboratory Equipment and Supplies

6.2.1 Gas Chromatograph (GC). Any instrument equipped with a flame ionization detector and capable of being temperature programmed may be used. Optionally, other types of detectors (e.g., a mass spectrometer) may be used provided that the detector system yields an appropriate and reproducible response to the analytes in the injected sample. Autosampler injection may be used, if available.

6.2.2 Recorder. If available, an electronic data station or integrator may be used to record the gas chromatogram and associated data. If a strip chart recorder is used, it must
meet the following criteria: A 1 to 10 millivolt (mV) linear response with a full scale response time of 2 seconds or less and a maximum noise level of ±0.03 percent of full scale. Other types of recorders may be used as appropriate to the specific detector installed provided that the recorder has a full scale response time of 2 seconds or less and a maximum noise level of ±0.03 percent of full scale.

6.2.3 Column. The column must be constructed of materials that do not react with components of the sample (e.g., fused silica, stainless steel, glass). The column should be of appropriate physical dimensions (e.g., length, internal diameter) and contain sufficient suitable stationary phase to allow separation of the analytes. DB-5, DB-Wax, and FFAP columns are commonly used for paint analysis; however, it is the responsibility of each analyst to select appropriate columns and stationary phases.

6.2.4 Tube and Tube Fittings. Supplies to connect the GC and gas cylinders.

6.2.5 Pressure Regulators. Devices used to regulate the pressure between gas cylinders and the GC.

6.2.6 Flow Meter. A device used to determine the carrier gas flow rate through the GC. Either a digital flow meter or a soap film bubble meter may be used to measure gas flow rates.

6.2.7 Septa. Seals on the GC injection port through which liquid or gas samples can be injected using a syringe.

6.2.8 Liquid Charging Devices. Devices used to inject samples into the GC such as clean and graduated 1, 5, and 10 microliter (µl) capacity syringes.

6.2.9 Vials. Containers that can be sealed with a septum in which samples may be prepared or stored. The recommended size is 25 ml capacity. Mininert® valves have been found satisfactory and are available from Pierce Chemical Company, Rockford, Illinois.

6.2.10 Balance. Device used to determine the weights of standards and samples. An analytical balance capable of accurately weighing to 0.0001 g is required.

7. Reagents and Standards

7.1 Purity of Reagents. Reagent grade chemicals shall be used in all tests. Unless otherwise specified, all reagents shall conform to the specifications of the Committee on Analytical Reagents of the American Chemical Society, where such specifications are available. Other grades may be used provided it is first ascertained that the reagent is of sufficient purity to permit its use without lessening the accuracy of determination.

7.2 Carrier Gas. Helium carrier gas shall have a purity of 99.995 percent or higher. High purity nitrogen may also be used. Other carrier gases that are appropriate for the column system and analyte may also be used. Ultra-high purity grade hydrogen gas and zero-grade air shall be used for the flame ionization detector.

7.3 Dimethylformamide (DMF). Solvent for all standards and samples. Some other suitable solvent may be used if DMF is not compatible with the sample or coelutes with a target analyte.

NOTE: DMF may coelute with ethylbenzene or p-xylene under the conditions described in the note under Section 6.2.3.

7.4 Internal Standard Materials. The internal standard material is used in the quantitation of the analytes for this method. It shall be gas chromatography spectrophotometric quality or, if this grade is not available, the highest quality available. Obtain the assay for the internal standard material and maintain at that purity during use. The recommended internal standard material is 1-propanol; however, selection of an appropriate internal standard material for the particular coating and GC conditions used is the responsibility of each analyst.

7.5 Reference Standard Materials. The reference standard materials are the chemicals cited in Section 11 which are of known identity and purity and which are used to assist in the identification and quantification of the analytes of this method. They shall be the highest quality available. Obtain the assays for the reference standard materials and maintain at those purities during use.

7.6 Stock Reference Standards. Stock reference standards are dilutions of the reference standard materials that may be used on a daily basis to prepare calibration standards, calibration check standards, and quality control check standards. Stock reference standards may be prepared from the reference standard materials or purchased as certified solutions.

7.6.1 Stock reference standards should be prepared in dimethylformamide for each analyte expected in the coating samples to be analyzed. The concentrations of analytes in the stock reference standards are not specified but must be adequate to prepare the calibration standards required in the method. A stock reference standard may contain more than one analyte provided all analytes are chemically compatible and no analytes coelute. The actual concentrations prepared must be known to within 0.1 percent (e.g., ±0.001 g/g solution). The following procedure is suggested. Place about 25 ml of dimethylformamide into a tared ground-glass stoppered 50 ml volumetric flask. Weigh the flask to the nearest 0.1 mg. Add 12.5 g of the reference standard material and reweigh the flask. Dilute to volume with dimethylformamide and reweigh. Stopper the flask and mix the contents by inverting the flask several times. Calculate the concentration in grams per
7.6.2 Transfer the stock reference standard solution into one or more Teflon-sealed screw-cap bottles. Store, with minimal headspace, at –10°C to 0°C and protect from light.

7.6.3 Prepare fresh stock reference standards every six months, or sooner if analysis results from daily calibration check standards indicate a problem. Fresh stock reference standards for very volatile HAP’s may have to be prepared more frequently.

7.7 Calibration Standards. Calibration standards are used to determine the response of the detector to known amounts of reference material. Calibration standards must be prepared at a minimum of three concentration levels from the stock reference standards (see Section 7.6). Prepare the calibration standards in dimethylformamide (see Section 7.3). The lowest concentration standard should contain a concentration of analyte equivalent to a concentration of no more than 0.001% of the analyte in the coating, whichever concentration is higher. The highest concentration standard should contain a concentration of analyte equivalent to a concentration of no more than 0.01% of the analyte in a coating or to a concentration that is lower than the actual concentration of the analyte in the coating, whichever concentration is higher. The highest concentration standard should contain a concentration of analyte equivalent to slightly more than the highest concentration expected for the analyte in a coating. The remaining calibration standard should contain a concentration of analyte roughly at the midpoint of the range defined by the lowest and highest concentration calibration standards. The concentration range of the standards should thus correspond to the expected range of analyte concentrations in the prepared coating samples (see Section 11.3). Each calibration standard should contain each analyte for detection by this method expected in the actual coating samples (e.g., some or all of the compounds listed in Section 11.1 may be included). Each calibration standard should also contain an appropriate amount of internal standard material (response for the internal standard material is within 25 to 75 percent of full scale on the attenuation setting for the particular reference standard concentration level). Calibration Standards should be stored for 1 week only in sealed vials with minimal headspace. If the stock reference standards were prepared as specified in Section 7.6, the calibration standards may be prepared by either weighing each addition of the stock reference standard or by adding known volumes of the stock reference standard and calculating the mass of the standard reference material added. Alternative 1 (Section 7.7.1) specifies the procedure to be followed when the stock reference standard is added by volume. Alternative 2 (Section 7.7.2) specifies the procedure to be followed when the stock reference standard is added by weight.

NOTE: To assist with determining the appropriate amount of internal standard to add, as required here and in other sections of this method, the analyst may find it advantageous to prepare a curve showing the area response versus the amount of internal standard injected into the GC.

7.7.1 Preparation Alternative 1 Determine the amount of each stock reference standard and dimethylformamide solvent needed to prepare approximately 25 ml of the specific calibration concentration level desired. To a tared 25 ml vial that can be sealed with a crimp-on or Mininert valve, add the total amount of dimethylformamide calculated to be needed. As quickly as practical, add the calculated amount of each stock reference standard using new pipets (or pipet tips) for each stock reference standard. Weigh the vial and seal it. Using the known weights of the standard reference materials per ml in the stock reference standards, the volumes added, and the total weight of all reagents added to the vial, calculate the weight percent of each standard reference material in the calibration standard prepared. Repeat this process for each calibration standard to be prepared.

7.7.2 Preparation Alternative 2 Determine the amount of each stock reference standard and dimethylformamide solvent needed to prepare approximately 25 ml of the specific calibration concentration level desired. To a tared 25 ml vial that can be sealed with a crimp-on or Mininert valve, add the total amount of dimethylformamide calculated to be needed. As quickly as practical, add the calculated amount of a stock reference standard using a new pipet (or pipet tip) and reweigh the vial. Repeat this process for each stock reference standard to be added. Seal the vial after obtaining the final weight. Using the known weight percents of the standard reference materials in the stock reference standards, the weights of the stock reference standards added, and the total weight of all reagents added to the vial, calculate the weight percent of each standard reference material in the calibration standard prepared. Repeat this process for each calibration standard to be prepared.

8. Sample Collection, Preservation, Transport, and Storage

8.1 Copies of material safety data sheets (MSDS’s) for each sample should be obtained prior to sampling. The MSDS’s contain information on the ingredients, and physical and chemical properties data. The MSDS’s also
contain recommendations for proper handling or required safety precautions. Certified product data sheets (CPDS) may also include information relevant to the analysis of the coating sample including, but not limited to, separation column, oven temperature, carrier gas, injection port temperature, extraction solvent, and internal standard.

8.2 A copy of the blender's worksheet can be requested to obtain data on the exact coating being sampled. A blank coating data sheet form (see Section 18) may also be used. The manufacturer's formulation information from the product data sheet should also be obtained.

8.3 Prior to sample collection, thoroughly mix the coating to ensure that a representative, homogeneous sample is obtained. It is preferred that this be accomplished using a coating can shaker or similar device; however, when necessary, this may be accomplished using mechanical agitation or circulation systems.

8.3.1 Water-thinned coatings tend to incorporate or entrain air bubbles if stirred too vigorously; mix these types of coatings slowly and only as long as necessary to homogenize.

8.3.2 Each component of multicomponent coatings that harden when mixed must be sampled separately. The component mix ratios must be obtained at the facility at the time of sampling and submitted to the analytical laboratory.

8.4 Sample Collection. Samples must be collected in a manner that prevents or minimizes loss of volatile components and that does not contaminate the coating reservoir. A suggested procedure is as follows. Select a sample collection container which has a capacity at least 25 percent greater than the container in which the sample is to be transported. Make sure both sample containers are clean and dry. Using clean, long-handled tongs, turn the sample collection container upside down and lower it into the coating reservoir. The mouth of the sample collection container should be at approximately the midpoint of the reservoir (do not take the sample from the top surface). Turn the sample collection container over and slowly bring it to the top of the coating reservoir. Rapidly pour the collected coating into the sample container, filling it completely. It is important to fill the sample container completely to avoid any loss of volatiles due to volatilization into the headspace. Return any unused coating to the reservoir or dispose as appropriate.

NOTE: If a company requests a set of samples for its own analysis, a separate set of samples, using new sample containers, should be taken at the same time.

8.5 Once the sample is collected, place the sample container on a firm surface and insert the inner seal in the container by placing the seal inside the rim of the container, inverting a screw cap, and pressing down on the screw cap which will evenly force the inner seal into the container for a tight fit. Using clean towels or rags, remove any residual coating material from the outside of the sample container after inserting the inner seal. Screw the cap onto the container.

8.5.1 Affix a sample label (see Section 18) clearly identifying the sample, date collected, and person collecting the sample.

8.5.2 Prepare the sample for transportation to the laboratory. The sample should be maintained at the coating's recommended storage temperature specified on the Material Safety Data Sheet, or, if no temperature is specified, the sample should be maintained within the range of 5°C to 38°C.

8.9 The shipping container should adhere to U.S. Department of Transportation specification DOT 12-B. Coating samples are considered hazardous materials; appropriate shipping procedures should be followed.

9. Quality Control

9.1 Laboratories using this method should operate a formal quality control program. The minimum requirements of the program should consist of an initial demonstration of laboratory capability and an ongoing analysis of blanks and quality control samples to evaluate and document quality data. The laboratory must maintain records to document the quality of the data generated. When results indicate atypical method performance, a quality control check standard (see Section 9.4) must be analyzed to confirm that the measurements were performed in an in-control mode of operation.

9.2 Before processing any samples, the analyst must demonstrate, through analysis of a reagent blank, that there are no interferences from the analytical system, glassware, and reagents that would bias the sample analysis results. Each time a set of analytical samples is processed or there is a change in reagents, a reagent blank should be processed as a safeguard against chronic laboratory contamination. The blank samples should be carried through all stages of the sample preparation and measurement steps.

9.3 Required instrument quality control parameters are found in the following sections:

9.3.1 Baseline stability must be demonstrated to be ±5 percent of full scale using the procedures given in Section 10.1.

9.3.2 The GC calibration is not valid unless the retention time (RT) for each analyte at each concentration is within ±0.05 min of the retention time measured for that analyte in the stock standard.

9.3.3 The retention time (RT) of any sample analyte must be within ±0.05 min of the average RT of the analyte in the calibration
standards for the analyte to be considered tentatively identified.

9.3.4 The GC system must be calibrated as specified in Section 10.2.

9.4 A one-point daily calibration check must be performed as specified in Section 10.3.

9.4.4 To establish the ability to generate results having acceptable accuracy and precision, the analyst must perform the following operations.

9.4.1 Prepare a quality control check standard (QCCS) containing each analyte expected in the coating samples at a concentration expected to result in a response between 0.05 and 0.75 percent of the limits of the calibration curve when the sample is prepared as described in Section 11.5. The QCCS may be prepared from reference standard materials or purchased as certified solutions. If prepared in the laboratory, the QCCS must be prepared independently from the calibration standards.

9.4.2 Analyze three aliquots of the QCCS according to the method beginning in Section 11.5.3 and calculate the weight percent of each analyte using Equation 1, Section 12.

9.4.3 Calculate the mean weight percent (X) for each analyte from the three results obtained in Section 9.4.2.

9.4.4 Calculate the percent accuracy for each analyte using the known concentrations (Ti) in the QCCS using Equation 3, Section 12.

9.4.5 Calculate the percent relative standard deviation (percent RSD) for each analyte using Equation 7, Section 12, substituting the appropriate values for the relative response factors (RRF's) in said equation.

9.4.6 If the percent accuracy (Section 9.4.4) for all analytes is within the range 90 percent to 110 percent and the percent RSD (Section 9.4.5) for each analyte is ≤20 percent, system performance is acceptable and sample analysis may begin. If these criteria are not met for any analyte, then system performance is not acceptable for that analyte and the test must be repeated for those analytes only. Repeated failures indicate a general problem with the measurement system that must be located and corrected. In this case, the entire test, beginning at Section 9.4.1, must be repeated after the problem is corrected.

9.5 Great care must be exercised to maintain the integrity of all standards. It is recommended that all standards be stored at −10 °C to 0 °C in screw-cap amber glass bottles with Teflon liners.

9.6 Unless otherwise specified, all weights are to be recorded within 0.1 mg.

10. Calibration and Standardization.

10.1 Column Baseline Drift. Before each calibration and series of determinations and before the daily calibration check, condition the column using procedures developed by the laboratory or as specified by the column supplier. Operate the GC at initial (i.e., before sample injection) conditions on the lowest attenuation to be used during sample analysis. Adjust the recorder pen to zero on the chart and obtain a baseline for at least one minute. Initiate the GC operating cycle that would be used for sample analysis. On the recorder chart, mark the pen position at the end of the simulated sample analysis cycle. Baseline drift is defined as the absolute difference in the pen positions at the beginning and end of the cycle in the direction perpendicular to the chart movement. Calculate the percent baseline drift by dividing the baseline drift by the chart width representing full-scale deflection and multiply the result by 100.

10.2 Calibration of GC. Bring all stock standards and calibration standards to room temperature while establishing the GC at the determined operating conditions.

10.2.1 Retention Times (RT's) for Individual Compounds.

NOTE: The procedures of this subsection are required only for the initial calibration. However, it is good laboratory practice to follow these procedures for some or all analytes before each calibration. The procedures were written for chromatograms output to a strip chart recorder. More modern instruments (e.g., integrators and electronic data stations) determine and print out or display retention times automatically.

The RT for each analyte should be determined before calibration. This provides a positive identification for each peak observed from the calibration standards. Inject an appropriate volume (see NOTE in Section 11.5.2) of one of the stock reference standards into the gas chromatograph and record on the chart the pen position at the time of the injection (see Section 7.6.1). Dilute an aliquot of the stock reference standard as required in dimethylformamide to achieve a concentration that will result in an on-scale response. Operate the gas chromatograph according to the determined procedures. Select the peak(s) that correspond to the analyte(s) [and internal standard, if used] and measure the retention time(s). If a chart recorder is used, measure the distance(s) on the chart from the injection point to the peak maximum. These distances, divided by the chart speed, are defined as the RT's of the analytes in question. Repeat this process for each of the stock reference standard solutions.

NOTE: If gas chromatography with mass spectrometer detection (GC-MS) is used, a stock reference standard may contain a group of analytes, provided all analytes are adequately separated during the analysis. Mass spectral library matching can be used to identify the analyte associated with each peak in the gas chromatogram. The retention time for the analyte then becomes the
retention time of its peak in the chromatogram.

10.2.2 Calibration. The GC must be calibrated using a minimum of three concentration levels of each potential analyte. (See Section 7.7 for instructions on preparation of the calibration standards.) Beginning with the lowest concentration level calibration standard, carry out the analysis procedure as described beginning in Section 11.7. Repeat the procedure for each progressively higher concentration level until all calibration standards have been analyzed.

10.2.2.1 Calculate the RT's for the internal standard and for each analyte in the calibration standards at each concentration level as described in Section 10.2.1. The RT's for the internal standard must not vary by more than 0.10 minutes. Identify each analyte by comparison of the RT's for peak maxima to the RT's determined in Section 10.2.1.

10.2.2.2 Compare the retention times (RT's) for each potential analyte in the calibration standards for each concentration level to the retention times determined in Section 10.2.1. The calibration is not valid unless all RT's for all analytes meet the criteria given in Section 9.3.2.

10.2.2.3 Tabulate the area responses and the concentrations for the internal standard and each analyte in the calibration standards. Calculate the response factor for the internal standard (RF) and the response factor for each compound relative to the internal standard (RRF) for each concentration level using Equations 5 and 6, Section 12.

10.2.2.4 Using the RRF's from the calibration, calculate the percent relative standard deviation (percent RSD) for each analyte in the calibration standard using Equation 7, Section 12. The percent RSD for each individual calibration analyte must be less than 15 percent. This criterion must be met in order for the calibration to be valid. If the criterion is met, the mean RRF's determined above are to be used until the next calibration.

10.3 Daily Calibration Checks. The calibration curve (Section 10.2.2) must be checked and verified at least once each day that samples are analyzed. This is accomplished by analyzing a calibration standard that is at a concentration near the midpoint of the working range and performing the checks in Sections 10.3.1, 10.3.2, and 10.3.3.

10.3.1 For each analyte in the calibration standard, calculate the percent difference in the RRF from the last calibration using Equation 8, Section 12. If the percent difference for each calibration analyte is less than 10 percent, the last calibration curve is assumed to be valid. If the percent difference for any analyte is greater than 5 percent, the analyst should consider this a warning limit. If the percent difference for any one calibration analyte exceeds 10 percent, corrective action must be taken. If no source of the problem can be determined after corrective action has been taken, a new three-point (minimum) calibration must be generated. This criterion must be met before quantitative analysis begins.

10.3.2 If the RRF for the internal standard changes by more than ±20 percent from the last daily calibration check, the system must be inspected for malfunctions and corrections made as appropriate.

10.3.3 The retention times for the internal standard and all calibration check analytes must be evaluated. If the retention time for the internal standard or for any calibration check analyte changes by more than 0.10 min from the last calibration, the system must be inspected for malfunctions and corrections made as required.

11. Procedure

11.1 All samples and standards must be allowed to warm to room temperature before analysis. Observe the given order of ingredient addition to minimize loss of volatiles.

11.2 Bring the GC system to the determined operating conditions and condition the column as described in Section 10.1.

NOTE: The temperature of the injection port may be an especially critical parameter. Information about the proper temperature may be found on the CPDS.

11.3 Perform the daily calibration checks as described in Section 10.3. Samples are not to be analyzed until the criteria in Section 10.3 are met.

11.4 Place the as-received coating sample on a paint shaker, or similar device, and shake the sample for a minimum of 5 minutes to achieve homogenization.

11.5 NOTE: The steps in this section must be performed rapidly and without interruption to avoid loss of volatile organics. These steps must be performed in a laboratory hood free from solvent vapors. All weights must be recorded to the nearest 0.1 mg.

11.5.1 Add 16 g of dimethylformamide to each of two tared vials (A and B) capable of being septum sealed.

11.5.2 To each vial add a weight of coating that will result in the response for the major constituent being in the upper half of the linear range of the calibration curve.

NOTE: The magnitude of the response obviously depends on the amount of sample injected into the GC as specified in Section 11.8. This volume must be the same as used for preparation of the calibration curve, otherwise shifts in compound retention times may occur. If a sample is prepared that results in a response outside the limits of the calibration curve, new samples must be prepared; changing the volume injected to bring the response within the calibration curve limits is not permitted.
11.5.3 Add a weight of internal standard to each vial (A and B) that will result in the response for the internal standard being between 25 percent and 75 percent of the linear range of the calibration curve.

11.5.4 Seal the vials with crimp-on or Mininert® septum seals.

11.6 Shake the vials containing the prepared coating samples for 60 seconds. Allow the vials to stand undisturbed for ten minutes. If solids have not settled out on the bottom after 10 minutes, then centrifuge at 1,000 rpm for 5 minutes. The analyst also has the option of injecting the sample without allowing the solids to settle.

11.7 Analyses should be conducted in the following order: daily calibration check sample, method blank, up to 10 injections from sample vials (i.e., one injection each from up to five pairs of vials, which corresponds to analysis of 5 coating samples).

11.8 Inject the prescribed volume of supernatant from the calibration check sample, the method blank, and the sample vials onto the chromatographic column and record the chromatograms while operating the system under the specified operating conditions.

**NOTE:** The analyst has the option of injecting the unseparated sample.

12. Data Analysis and Calculations

12.1 Qualitative Analysis. An analyte (e.g., those cited in Section 1.1) is considered tentatively identified if two criteria are satisfied: (1) elution of the sample analyte within ±0.05 min of the average GC retention time of the same analyte in the calibration standard; and (2) either (a) confirmation of the identity of the compound by spectral matching on a gas chromatograph equipped with a mass selective detector or (b) elution of the sample analyte within ±0.05 min of the average GC retention time of the same analyte in the calibration standard analyzed on a dissimilar GC column.

12.1.1 The RT of the sample analyte must meet the criteria specified in Section 9.3.3.

12.1.2 When doubt exists as to the identification of a peak or the resolution of two or more components possibly comprising one peak, additional confirmatory techniques (listed in Section 12.1) must be used.

12.2 Quantitative Analysis. When an analyte has been identified, the quantification of that compound will be based on the internal standard technique.

12.2.1 A single analysis consists of one injection from each of two sample vials (A and B) prepared using the same coating. Calculate the concentration of each identified analyte in the sample as follows:

\[
\text{HAP}_{\text{wt} \%} = 100 \times \frac{(A_x)(W_i)}{(A_{i\text{int}})(\text{RRF}_x)(W_x)} \quad \text{Eq. (1)}
\]

where:

- \( \text{HAP}_{\text{wt} \%} \) = weight percent of the analyte in coating.
- \( A_x \) = Area response of the analyte in the sample.
- \( W_i \) = Weight of internal standard added to sample, g.
- \( A_{i\text{int}} \) = Area response of the internal standard in the sample.
- \( \text{RRF}_x \) = Mean relative response factor for the analyte in the calibration standards.
- \( W_x \) = Weight of coating added to the sample solution, g.

12.2.2 Report results for duplicate analysis (sample vials A and B) without correction.

12.3 Precision Data. Calculate the percent difference between the measured concentrations of each analyte in vials A and B as follows.

12.3.1 Calculate the weight percent of the analyte in each of the two sample vials as described in Section 12.2.1.

12.3.2 Calculate the percent difference for each analyte as:

\[
\% \text{Dif}_i = 100 \times \frac{|A_i - B_i|}{(A_i + B_i)/2} \quad \text{Eq. (2)}
\]

where \( A_i \) and \( B_i \) are the measured concentrations of the analyte in vials A and B.

12.4 Calculate the percent accuracy for analytes in the QCCS (See Section 9.4) as follows:
% Accuracy $x = 100 \times \frac{X_x}{T_x}$ \hspace{1cm} Eq. (3)

where $X_x$ is the mean measured value and $T_x$ is the known true value of the analyte in the QCCS.

12.5 Obtain retention times (RT's) from data station or integrator or, for chromatograms from a chart recorder, calculate the RT's for analytes in the calibration standards (See Section 10.2.2.2) as follows:

\[
RT = \frac{\text{Distance from injection to peak maximum}}{\text{Recorder chart speed}}
\] \hspace{1cm} Eq. (4)

12.6 Calculate the response factor for the internal standard (See Section 10.2.2.3) as follows:

\[
RF_{is} = \frac{A_{is}}{C_{is}}
\] \hspace{1cm} Eq. (5)

where:

- $A_{is}$ = Area response of the internal standard.
- $C_{is}$ = Weight percent of the internal standard.

12.7 Calculate the relative response factors for analytes in the calibration standards (See Section 10.2.2.3) as follows:

\[
\left( \frac{\sum_{i=1}^{n} (RF_x - \overline{RF_x})^2}{n-1} \right)^{\frac{1}{2}}
\] \hspace{1cm} Eq. (7)

where:

- $n = $ Number of calibration concentration levels used for an analyte.
- $RF_x = $ Individual RRF for an analyte.
- $\overline{RF_x} = $ Mean of all $RF$'s for an analyte.

12.8 Calculate the percent relative standard deviation of the relative response factors for analytes in the calibration standards (See Section 10.2.2.4) as follows:

\[
% \text{RSD} = 100 \times \frac{n-1}{\overline{RF_x}}
\] \hspace{1cm} Eq. (7)
Environmental Protection Agency

\[
\text{% Difference} = \left| \frac{RRF_x - RRF_c}{RRF_x} \right| \times 100 \quad \text{Eq. (8)}
\]

where:

\( RRF = \text{mean relative response factor from last calibration.} \)
\( RRF_c = \text{relative response factor from calibration check standard.} \)

13. Measurement of Reaction Byproducts That are HAP. [Reserved]
14. Method Performance. [Reserved]
15. Pollution Prevention. [Reserved]
16. Waste Management
16.1 The coating samples and laboratory standards and reagents may contain compounds which require management as hazardous waste. It is the laboratory's responsibility to ensure all wastes are managed in accordance with all applicable laws and regulations.
16.2 To avoid excessive laboratory waste, obtain only enough sample for laboratory analysis.
16.3 It is recommended that discarded waste coating solids, used rags, used paper towels, and other nonglass or nonsharp waste materials be placed in a plastic bag before disposal. A separate container, designated "For Sharp Objects Only," is recommended for collection of discarded glassware and other sharp-edge items used in the laboratory. It is recommended that unused or excess samples and reagents be placed in a solvent-resistant plastic or metal container with a lid or cover designed for flammable liquids. This container should not be stored in the area where analytical work is performed. It is recommended that a record be kept of all compounds placed in the container for identification of the contents upon disposal.

17. References
18. Tables, Diagrams, Flowcharts, and Validation Data

Agency: 
Inspector: 
Date/Time: 
Sample ID #: 
Source ID: 
Coating Name/Type: 
Plant Witness: 
Type Analysis Required: 
Special Handling: 
Sample Container Label: 
Coating Data

Date: 
Source: 

<table>
<thead>
<tr>
<th>Data</th>
<th>Sample ID No.</th>
<th>Sample ID No.</th>
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<tbody>
<tr>
<td>Coating:</td>
<td>Supplier Name</td>
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<tr>
<td></td>
<td>Name and Color of Coating</td>
<td></td>
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<tr>
<td></td>
<td>Type of Coating (primer, clearcoat, etc.)</td>
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<td></td>
<td>Identification Number for Coating</td>
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<td></td>
<td>Coating Density (lbs/gal)</td>
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### Stock Reference Standard

<table>
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<tr>
<th>Name of Reference Material:</th>
<th>Supplier Name:</th>
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<tr>
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<tr>
<td>Lot Number:</td>
<td></td>
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<tr>
<td>Purity:</td>
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</tbody>
</table>

<table>
<thead>
<tr>
<th>Name of Solvent Material:</th>
<th>Supplier Name:</th>
</tr>
</thead>
<tbody>
<tr>
<td>Dimethylformamide</td>
<td></td>
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<tr>
<td>Lot Number:</td>
<td></td>
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<tr>
<td>Purity:</td>
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**Preparation Information—Continued**


10. Weight Reference Material per ml of Solution (Line 7 ÷ Line 9).

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<th>Laboratory ID No. for this Standard.</th>
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<table>
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<tr>
<th>Expiration Date for this Standard.</th>
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<tbody>
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</table>

**Calibration Standard**

**Preparation Information**

Date Prepared: _______________

Date Expires: _______________

Prepared By: _______________

Notebook/page:

**Calibration Standard Identification No.**

<table>
<thead>
<tr>
<th>Analyte name*</th>
<th>Stock reference standard ID No.</th>
<th>Volume added, ml</th>
<th>Amount in standard, g/ml</th>
<th>Weight added, g</th>
<th>Amount in standard, g/ml</th>
<th>Calculated weight analyte added, g</th>
<th>Weight percent analyte in calibration standard†</th>
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* Include internal standard(s).

† Weight percent = weight analyte added ÷ total weight of reagents.
### Environmental Protection Agency

#### Quality Control Check Standard

<table>
<thead>
<tr>
<th>Analyte name¹</th>
<th>Stock reference standard ID No.</th>
<th>Amount of stock reference standard added (by volume or by weight)</th>
<th>Calculated weight analyte added, g</th>
<th>Weight percent analyte in OCCS standard²</th>
</tr>
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<tbody>
<tr>
<td></td>
<td></td>
<td>Volume added, ml</td>
<td>Amount in standard, g/ml</td>
<td>Weight added, g</td>
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</table>

¹ Include internal Standard(s).
² Weight percent=weight analyte added ÷ total weight of reagents.

#### Quality Control Check Standard Analysis

<table>
<thead>
<tr>
<th>Date OCCS Analyzed:</th>
<th>Analyst:</th>
<th>OCCS Identification No.:</th>
<th>QCC Expiration Date:</th>
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#### ANALYSIS RESULTS

<table>
<thead>
<tr>
<th>Analyte</th>
<th>Weight percent determined</th>
<th>Mean % weight</th>
<th>Percent accuracy</th>
<th>Percent RSD</th>
<th>Meets criteria in Section 9.4.6</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
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<td>Run 1</td>
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<td>Run 3</td>
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#### Calibration of Gas Chromatograph

<table>
<thead>
<tr>
<th>Calibrated By:</th>
<th>Calibration Date:</th>
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</thead>
</table>

#### PART 1.—RETENTION TIMES FOR INDIVIDUAL ANALYTES

<table>
<thead>
<tr>
<th>Analyte</th>
<th>Stock standard ID No.</th>
<th>Recorder chart speed</th>
<th>Distance from injection point to peak maximum</th>
<th>Retention time, minutes³</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>Inches/min.</td>
<td>cm/min.</td>
<td>Inches</td>
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</table>

³ Retention time is determined by the time from injection point to peak maximum.
### Part 1.—Retention Times for Individual Analytes—Continued

<table>
<thead>
<tr>
<th>Analyte</th>
<th>Stock standard ID No.</th>
<th>Recorder chart speed</th>
<th>Distance from injection point to peak maximum</th>
<th>Retention time, minutes</th>
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</thead>
<tbody>
<tr>
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<td>Inches/min.</td>
<td>cm/min.</td>
<td>Inches</td>
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* Retention time = distance to peak maxima / chart speed.

**Calibration of Gas Chromatograph**

Calibrated By: ___________________________

Calibration Date: _______________________

### Part 2.—Analysis of Calibration Standards

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**Calibration of Gas Chromatograph**

Calibrated By: ___________________________

Calibration Date: _______________________

### Part 3.—Data Analysis for Calibration Standards

<table>
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<tr>
<th>Analyte</th>
<th>Calib. STD ID</th>
<th>Calib. STD ID</th>
<th>Calib. STD ID</th>
<th>Mean</th>
<th>Mean</th>
<th>Is RT within ±0.02 min of RT for stock? (Y/N)</th>
<th>Is percent RSD of RF &lt;30% (Y/N)</th>
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</thead>
<tbody>
<tr>
<td>Name:</td>
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### Environmental Protection Agency

**PART 3.—DATA ANALYSIS FOR CALIBRATION STANDARDS—Continued**

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<tr>
<th>Analyte</th>
<th>Calib. STD ID</th>
<th>Calib. STD ID</th>
<th>Calib. STD ID</th>
<th>Mean</th>
<th>percent RSD of RF</th>
<th>Is RT within ±0.05 min of RT for stock? (Y/N)</th>
<th>Is percent RSD &lt;20% (Y/N)</th>
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<tbody>
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</table>

Retention time (RT) change (difference) must be less than ±0.10 minutes.

<table>
<thead>
<tr>
<th>Analyte</th>
<th>Retention Time (RT)</th>
<th>Response Factor (RF)</th>
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<td>Last</td>
<td>This</td>
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*Retention time (RT) change (difference) must be less than ±0.10 minutes.

**Sample Analysis**

<table>
<thead>
<tr>
<th>Vial A ID No.:</th>
<th>Analyzed By:</th>
<th>Date:</th>
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<tbody>
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</table>

Sample preparation information:

- wt empty vial
- wt plus DMF
- wt plus sample
- wt plus internal standard

Calculated:

- wt DMF
- wt sample
- wt internal standard

### ANALYSIS RESULTS: DUPLICATE SAMPLES

<table>
<thead>
<tr>
<th>Analyte</th>
<th>Area response</th>
<th>RF</th>
<th>Vial</th>
<th>Vial</th>
<th>Vial</th>
<th>Average</th>
</tr>
</thead>
</table>

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### METHOD 312A—DETERMINATION OF STYRENE IN LATEX STYRENE-BUTADIENE RUBBER, THROUGH GAS CHROMATOGRAPHY

1. **Scope and Application**

   1.1 This method describes a procedure for determining parts per million (ppm) styrene monomer (CAS No. 100-42-5) in aqueous samples, including latex samples and styrene stripper water.

   1.2 The sample is separated in a gas chromatograph equipped with a packed column and a flame ionization detector.

2. **Summary of Method**

   2.1 This method utilizes a packed column gas chromatograph with a flame ionization detector to determine the concentration of residual styrene in styrene butadiene rubber (SBR) latex samples.

3. **Definitions**

   3.1 The definitions are included in the text as needed.

4. **Interferences**

   4.1 In order to reduce matrix effects and emulsify the styrene, similar styrene free latex is added to the internal standard. There are no known interferences.

   4.2 The operating parameters are selected to obtain resolution necessary to determine styrene monomer concentrations in latex.

5. **Safety**

   5.1 It is the responsibility of the user of this procedure to establish appropriate safety and health practices.

6. **Equipment and Supplies**

   6.1 Adjustable bottle-top dispenser, set to deliver 3 ml. (for internal standard), Brinkmann Dispensette, or equivalent.

   6.2 Pipettor, set to 10 ml., Oxford Macrosset, or equivalent.

   6.3 Volumetric flask, 100-ml, with stopper.

   6.4 Hewlett Packard Model 5710A dual channel gas chromatograph equipped with flame ionization detector.

   6.4.1 11 ft. x ¼ in. stainless steel column packed with 10% TCEP on 100/120 mesh Chromosorb P, or equivalent.

   6.4.2 Perkin Elmer Model 023 strip chart recorder, or equivalent.

   6.5 Helium carrier gas, zero grade.

   6.6 Liquid syringe, 25-µl.

   6.7 Digital MicroVAX 3100 computer with VG Multichrom software, or equivalent data handling system.

   6.8 Wire Screens, circular, 70-mm, 80-mesh diamond weave.

   6.7 DEHA—(N,N-Diethyl hydroxylamine), 97+% purity, CAS No. 3710-84-7

   6.8 p-Dioxane, CAS No. 123-91-1

7. **Reagents and Standards**

   7.1 Internal standard preparation.

   7.1.1 Pipette 5 ml p-dioxane into a 1000-ml volumetric flask and fill to the mark with distilled water and mix thoroughly.

   7.2 Calibration solution preparation.

   7.2.1 Pipette 10 ml styrene-free latex (eg: NBR latex) into a 100-ml volumetric flask.

   7.2.2 Add 3 ml internal standard (section 7.1.1 of this method).

   7.2.3 Weigh exactly 10 µl fresh styrene and record the weight.

   7.2.4 Inject the styrene into the flask and mix well.

   7.2.5 Add 2 drops of DEHA, fill to the mark with water and mix well again.

   7.2.6 Calculate concentration of the calibration solution as follows:

   \[ \text{mg/l styrene} = \frac{\text{mg styrene added}}{0.1 \text{ L}} \]

8. **Sample Collection, Preservation, and Storage**

   8.1 A representative SBR emulsion sample should be caught in a clean, dry 6-oz. teflon lined glass container. Close it properly to assure no sample leakage.

   8.2 The container should be labeled with sample identification, date and time.
9.0 Quality Control

9.1 The instrument is calibrated by injecting calibration solution (Section 7.2 of this method) five times.

9.2 The retention time for components of interest and relative response of monomer to the internal standard is determined.

9.3 Recovery efficiency must be determined once for each sample type and whenever modifications are made to the method.

9.3.1 A set of six latex samples shall be collected. Two samples shall be prepared for analysis from each sample. Each sample shall be analyzed in duplicate.

9.3.2 The second set of six latex samples shall be analyzed in duplicate before spiking each sample with approximately 1000 ppm styrene. The spiked samples shall be analyzed in duplicate.

9.3.3 For each hydrocarbon, calculate the average recovery efficiency (R) using the following equations:

\[ R = \frac{\sum (R_n)}{6} \]

where:

\[ R_n = \frac{c_{ns} \cdot c_{nu}}{S_n} \]

\[ n = \text{sample number} \]

\[ c_{ns} = \text{concentration of compound measured in spiked sample number} \ n. \]

\[ c_{nu} = \text{concentration of compound measured in unspiked sample number} \ n. \]

\[ S_n = \text{theoretical concentration of compound spiked into sample} \ n. \]

9.3.4 A value of R between 0.70 and 1.30 is acceptable.

9.3.5 R is used to correct all reported results for each compound by dividing the measured results of each compound by the R for that compound for the same sample type.

10.0 Calibration and Instrument Settings

10.1 Injection port temperature, 250°C.

10.2 Oven temperature, 110°C, isothermal.

10.3 Carrier gas flow, 25 cc/min.

10.4 Detector temperature, 250°C.

10.5 Range, 1×.

11.0 Procedure

11.1 Turn on recorder and adjust baseline to zero.

11.2 Prepare sample.

11.2.1 For latex samples, add 3 ml Internal Standard (section 7.1 of this method) to a 100-ml volumetric flask. Pipet 10 ml sample into the flask using the Oxford pipettor, dilute to the 100-ml mark with water, and shake well.

11.2.2 For water samples, add 3 ml Internal Standard (section 7.1 of this method) to a 100-ml volumetric flask and fill to the mark with sample. Shake well.

11.3 Flush syringe with sample.

11.4 Carefully inject 2 µl of sample into the gas chromatograph column injection port and press the start button.

11.5 When the run is complete the computer will print a report of the analysis.

12.0 Data Analysis and Calculation

12.1 For samples that are prepared as in section 11.2.1 of this method:

\[ \text{ppm styrene} = A \times D \]

Where:

\[ A = \text{"ppm" readout from computer} \]

\[ D = \text{dilution factor (10 for latex samples)} \]

12.2 For samples that are prepared as in section 11.2.2 of this method, ppm styrene is read directly from the computer.

13.0 Method Performance

13.1 This test has a standard deviation (1) of 3.3 ppm at 100 ppm styrene. The average Spike Recovery from six samples at 1000 ppm Styrene was 96.7 percent. The test method was validated using 926 ppm styrene standard. Six analysis of the same standard provided average 97.7 percent recovery. Note: These are example recoveries and do not replace quality assurance procedures in this method.

14.0 Pollution Prevention

14.1 Waste generation should be minimized where possible. Sample size should be an amount necessary to adequately run the analysis.

15.0 Waste Management

15.1 All waste shall be handled in accordance with Federal and State environmental regulations.

16.0 References and Publications

16.1 40 CFR 63 Appendix A—Method 301 Test Methods Field Validation of Pollutant Measurement


METHOD 312B—DETERMINATION OF RESIDUAL STYRENE IN STYRENE-BUTADIENE (SBR) RUBBER LATEX BY CAPILLARY GAS CHROMATOGRAPHY

1.0 Scope

1.1 This method is applicable to SBR latex solutions.

1.2 This method quantitatively determines residual styrene concentrations in SBR latex solutions at levels from 80 to 1200 ppm.

2.0 Principle of Method

2.1 A weighed sample of a latex solution is coagulated with an ethyl alcohol (EtOH) solution containing a specific amount of alpha-methyl styrene (AMS) as the internal standard. The extract of this coagulation is then
injected into a gas chromatograph and separated into individual components. Quantification is achieved by the method of internal standardization.

3.0 Definitions

3.1 The definitions are included in the text as needed.

4.0 Interferences

[Reserved]

5.0 Safety

5.1 This method may involve hazardous materials, operations, and equipment. This method does not purport to address all of the safety problems associated with its use. It is the responsibility of the user of this method to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

6.0 Equipment and Supplies

6.1 Analytical balance, 160 g capacity, and 0.1 mg resolution
6.2 Bottles, 2-oz capacity, with poly-cap screw lids
6.3 Mechanical shaker
6.4 Syringe, 10-ul capacity
6.5 Gas chromatograph, Hewlett Packard model 5890A, or equivalent, configured with FID with a megabore jet, splitless injector packed with silanized glass wool.
   6.5.1 Establish the following gas chromatographic conditions, and allow the system to thoroughly equilibrate before use.
   Injection technique = Splitless
   Injector temperature = 225 deg C
   Oven temperature = 70 deg C (isothermal)
   Detector: temperature = 300 deg C
   range = 5
   attenuation = 0
   Carrier gas: helium = 47 ml/min
   Detector gases: hydrogen = 30 ml/min
   air = 270 ml/min
   make-up = 0 ml/min
   Analysis time: = 3.2 min at the specified carrier gas flow rate and column temperature.
6.6 Gas chromatographic column, DB-1, 30 M X 0.531D, or equivalent, with a 1.5 micron film thickness.
6.7 Data collection system, Perkin-Elmer/ Nelson Series Turbochrom 4 Series 900 Interface, or equivalent.
6.8 Pipet, automatic dispensing, 50-ml capacity, and 2-liter reservoir.
6.9 Flasks, volumetric, class A, 100-ml and 1000-ml capacity.
6.10 Pipet, volumetric delivery, 10-ml capacity, class A.

7.0 Chemicals and Reagents

CHEMICALS:
7.1 Styrene, C8H8, 99+%., CAS 100-42-5
7.2 Alpha methyl styrene, C9H10, 99%, CAS 98-83-9
7.3 Ethyl alcohol, C2H5OH, denatured formula 2B, CAS 64-17-5

REAGENTS:
7.4 Internal Standard Stock Solution: 5.0 mg/ml AMS in ethyl alcohol.
   7.4.1 Into a 100-ml volumetric flask, weigh 0.50 g of AMS to the nearest 0.1 mg.
   7.4.2 Dilute to the mark with ethyl alcohol. This solution will contain 5.0 mg/ml AMS in ethyl alcohol and will be labeled the AMS STOCK SOLUTION.
7.5 Internal Standard Working Solution: 2500 ug/50 ml of AMS in ethyl alcohol.
   7.5.1 Using a 10 ml volumetric pipet, quantitatively transfer 10.0 ml of the AMS STOCK SOLUTION into a 1000-ml volumetric flask.
   7.5.2 Dilute to the mark with ethyl alcohol. This solution will contain 5.0 mg/ml AMS in ethyl alcohol and will be labeled the AMS STOCK SOLUTION.
7.6 Styrene Stock Solution: 5.0 mg/ml styrene in ethyl alcohol.
   7.6.1 Into a 100-ml volumetric flask, weigh 0.50 g of styrene to the nearest 0.1 mg.
   7.6.2 Dilute to the mark with ethyl alcohol. This solution will contain 5.0 mg/ml styrene in ethyl alcohol and will be labeled the STYRENE STOCK SOLUTION.
7.7 Styrene Working Solution: 5000 ug/10 ml of styrene in ethyl alcohol.
   7.7.1 Using a 10-ml volumetric pipet, quantitatively transfer 10.0 ml of the STYRENE STOCK SOLUTION into a 100-ml volumetric flask.
   7.7.2 Dilute to the mark with ethyl alcohol. This solution will contain 5000 ug/10 ml of styrene in ethyl alcohol and will be labeled the STYRENE WORKING SOLUTION.

8.0 Sample Collection, Preservation and Storage

8.1 Label a 2-oz sample poly-cap lid with the identity, date and time of the sample to be obtained.
8.2 At the sample location, open sample valve for at least 15 seconds to ensure that the sampling pipe has been properly flushed with fresh sample.
8.3 Fill the sample jar to the top (no headspace) with sample, then cap it tightly.
8.4 Deliver sample to the Laboratory for testing within one hour of sampling.
8.5 Laboratory testing will be done within two hours of the sampling time.
8.6 No special storage conditions are required unless the storage time exceeds 2 hours in which case refrigeration of the sample is recommended.
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9.0 Quality Control

9.1 For each sample type, 12 samples of SBR latex shall be obtained from the process for the recovery study. Half the vials and caps shall be tared, labeled “spiked”, and numbered 1 through 6. The other vials are labeled “unspiked” and need not be tared, but are also numbered 1 through 6.

9.2 The six vials labeled “spiked” shall be spiked with an amount of styrene to approximate 50% of the solution’s expected residual styrene level.

9.3 The spiked samples shall be shaken for several hours and allowed to cool to room temperature before analysis.

9.4 The six samples of unspiked solution shall be coagulated and a mean styrene value shall be determined, along with the standard deviation, and the percent relative standard deviation.

9.5 The six samples of the spiked solution shall be coagulated and the results of the analyses shall be determined using the following equations:

\[ M_s \] - Mean value of styrene in the unspiked sample

\[ M_u \] - Measured amount of styrene in the spiked sample

\[ S \] - Amount of styrene added to the spiked sample

\[ R = \frac{M_u}{S} \]

where:

\[ R = \text{Fraction of spiked styrene recovered} \]

9.6 A value of R between 0.70 and 1.30 is acceptable.

9.7 R is used to correct all reported results for each compound by dividing the measured results of each compound by the R for that compound for the same sample type.

10.0 Calibration

10.1 Using a 10-ml volumetric pipet, quantitatively transfer 10.0 ml of the AMS WORKING SOLUTION (section 7.7.2 of this method) into a 2-oz bottle.

10.2 Using the AMS WORKING SOLUTION equipped with the automatic dispensing pipet (section 7.5.3 of this method), transfer 50.0 ml of the internal standard solution into the 2-oz bottle.

10.3 Cap the 2-oz bottle and swirl. This is the calibration standard, which contains 5000 g of styrene and 2500 g of AMS.

10.4 Using the conditions prescribed (section 6.5 of this method), chromatograph 1 ul of the calibration standard.

10.5 Obtain the peak areas and calculate the relative response factor as described in the calculations section (section 12.1 of this method).

11.0 Procedure

11.1 Into a tared 2-oz bottle, weigh 10.0 g of latex to the nearest 0.1 g.

11.2 Using the AMS WORKING SOLUTION equipped with the automatic dispensing pipet (section 7.5.3 of this method), transfer 50.0 ml of the internal standard solution into the 2-oz bottle.

11.3 Cap the bottle. Using a mechanical shaker, shake the bottle for at least one minute or until coagulation of the latex is complete as indicated by a clear solvent.

11.4 Using the conditions prescribed (section 6.5 of this method), chromatograph 1 ul of the latex.

11.5 Obtain the peak areas and calculate the concentration of styrene in the latex as described in the calculations section (section 12.2 of this method).

12.0 Calculations

12.1 Calibration:

\[ RF = \frac{(W_s \times A_s)}{(W_x \times A_x)} \]

where:

\[ W_s \] - the weight (ug) of AMS

\[ W_x \] - the weight (ug) of styrene

\[ A_s \] - the area of AMS

\[ A_x \] - the area of styrene

12.2 Procedure:

\[ \text{ppm}_{\text{styrene}} = \frac{(A_s \times RF \times W_s)}{(A_x \times W_x)} \]

12.3 Correct for recovery (R) as determined by section 9.0 of this method.

13.0 Precision

13.1 Precision for the method was determined at the 80, 144, 590, and 1160 ppm levels. The standard deviations were 0.8, 1.5, 5 and 9 ppm respectively. The percent relative standard deviations (%RSD) were 1% or less at all levels. Five degrees of freedom were used for all precision data except at the 80 ppm level, where nine degrees of freedom were used. Note: These are example results and do not replace quality assurance procedures in this method.

14.0 Pollution Prevention

14.1 Waste generation should be minimized where possible. Sample size should be an amount necessary to adequately run the analysis.

15.0 Waste Management

15.1 Discard liquid chemical waste into the chemical waste drum.
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15.2 Discard latex sample waste into the latex waste drum.
15.3 Discard polymer waste into the polymer waste container.

16.0 References
16.1 This method is based on Goodyear Chemical Division Test Method E-889.

METHOD 312C—DETERMINATION OF RESIDUAL STYRENE IN SBR LATEX PRODUCED BY EMLUSION POLYMERIZATION

1.0 Scope
1.1 This method is applicable for determining the amount of residual styrene in SBR latex as produced in the emulsion polymerization process.

2.0 Principle of Method
2.1 A weighed sample of latex is coagulated in 2-propanol which contains alpha-methyl styrene as an Internal Standard. The extract from the coagulation will contain the alpha-methyl styrene as the Internal Standard and the residual styrene from the latex. The extract is analyzed by a Gas Chromatograph. Percent styrene is calculated by relating the area of the styrene peak to the area of the Internal Standard peak of known concentration.

3.0 Definitions
3.1 The definitions are included in the text as needed.

4.0 Interferences
[Reserved]

5.0 Safety
5.1 When using solvents, avoid contact with skin and eyes. Wear hand and eye protection. Wash thoroughly after use.
5.2 Avoid overexposure to solvent vapors. Handle only in well ventilated areas.

6.0 Equipment and Supplies
6.1 Gas Chromatograph—Hewlett Packard 5990, Series II with flame ionization detector, or equivalent.
   Column—HP 19095F-123, 30m x 0.53mm, or equivalent. Substrate HP FFAP (cross-linked) film thickness 1 micrometer. Glass injector port liners with silanized glass wool plug.
   Integrator—HP 3396, Series II, or equivalent.
6.2 Wrist action shaker
6.3 Automatic dispenser
6.4 Automatic pipet, calibrated to deliver 5.0±0.01 grams of latex
6.5 Four-ounce wide-mouth bottles with foil lined lids
6.6 Crimp cap vials, 2ml, teflon lined septa
6.7 Disposable pipets

6.8 Qualitative filter paper
6.9 Cap crimper
6.10 Analytical balance
6.11 10ml pipette
6.12 Two-inch funnel

7.0 Reagents and Standards
7.1 2-Propanol (HP2C grade)
7.2 Alpha methyl styrene (99+% purity)
7.3 Styrene (99+% purity)
7.4 Zero air
7.5 Hydrogen (chromatographic grade)
7.6 Helium
7.7 Internal Standard preparation
7.7.1 Weigh 5.000-5.005 grams of alpha-methyl styrene into a 100ml volumetric flask and bring to mark with 2-propanol to make Stock “A” Solution.

7.7.2 Pipette 10ml of Stock “A” Solution into a 100ml volumetric flask and bring to mark with 2-propanol to prepare Stock “B” Solution.
7.7.3 Pipette 10ml of the Stock “B” solution to a 1000ml volumetric flask and bring to the mark with 2-propanol. This will be the Internal Standard Solution (0.00005 grams/ml).

7.8 Certification of Internal Standard—Each batch of Stock “B” Solution will be certified to confirm concentration.
7.8.1 Prepare a Standard Styrene Control Solution in 2-propanol by the following method:
7.8.1.1 Weigh 5.000±0.005g of styrene to a 100ml volumetric flask and fill to mark with 2-propanol to make Styrene Stock “A” Solution.
7.8.1.2 Pipette 10ml of Styrene Stock “A” Solution to a 100ml volumetric flask and fill to mark with 2-propanol to make Styrene Stock “B” Solution.
7.8.1.3 Pipette 10ml of Styrene Stock “B” solution to a 250ml volumetric flask and fill to mark with 2-propanol to make the Certification Solution.
7.8.2 Certify Alpha-Methyl Styrene Stock “B” Solution.
7.8.2.1 Pipette 5ml of the Certification Solution and 25ml of the Alpha Methyl Styrene Internal Standard Solution to a 4-oz. bottle, cap and shake well.
7.8.2.2 Analyze the resulting mixture by GC using the residual styrene method. (11.4-11.6 of this method)
7.8.2.3 Calculate the weight of alpha methyl styrene present in the 25ml aliquot of the new Alpha Methyl Styrene Standard by the following equation:

\[ W_x = F_x \times W_x (A_x / A_{xy}) \]

Where
\[ A_x = \text{Peak area of alpha methyl styrene} \]
\[ A_{xy} = \text{Peak area of styrene} \]
\[ W_x = \text{Weight of alpha methyl styrene} \]
\[ W_{xy} = \text{Weight of styrene (0.0010)} \]
\[ F_x = \text{Analyzed response factor = 1} \]
The Alpha Methyl Styrene Stock Solution used to prepare the Internal Standard Solution may be considered certified if the weight of alpha methyl styrene analyzed by this method is within the range of .00097 to .00103 g.

8.0 Sampling

8.1 Collect a latex sample in a capped container. Cap the bottle and identify the sample as to location and time.

8.2 Deliver sample to laboratory for testing within one hour.

8.3 Laboratory will test within two hours.

8.4 No special storage conditions are required.

9.0 Quality Control

9.1 The laboratory is required to operate a formal quality control program. This consists of an initial demonstration of the capability of the method as well as ongoing analysis of standards, blanks, and spiked samples to demonstrate continued performance.

9.1.1 When the method is first set up, a calibration is run and the recovery efficiency for each type of sample must be determined. New type includes any change, such as polymer type, physical form or a significant change in the composition of the matrix.

9.1.2 If new types of samples are being analyzed, then recovery efficiency for each new type of sample must be determined. New type includes any change, such as polymer type, physical form or a significant change in the composition of the matrix.

9.2 Recovery efficiency must be determined once for each type of sample and whenever modifications are made to the method.

9.2.1 In determining the recovery efficiency, the quadruplet sampling system shall be used. Six sets of samples (for a total of 24) shall be taken. In each quadruplet set, half of the samples (two out of the four) shall be spiked with styrene.

9.2.2 Prepare the samples as described in section 8 of this method. To the vials labeled “spiked”, add a known amount of styrene that is expected to be present in the latex.

9.2.3 Run the spiked and unspiked samples in the normal manner. Record the concentrations of styrene reported for each pair of spiked and unspiked samples with the same vial number.

9.2.4 For each hydrocarbon, calculate the average recovery efficiency (R) using the following equation:

\[ R = \frac{C}{C_0} \]

Where: \( n = \) sample number

\( R = \frac{M - M_s}{S} \)

\( M = \) total mass of compound (styrene) measured in spiked sample (µg)

\( M_s = \) total mass of compound (styrene) measured in unspiked sample (µg)

\( S = \) theoretical mass of compound (styrene) spiked into sample (µg)

\( R = \) fraction of spiked compound (styrene) recovered

9.2.5 A different R value should be obtained for each sample type. A value of R between 0.70 and 1.30 is acceptable.

9.2.6 R is used to correct all reported results for each compound by dividing the measured results of each compound by the R for that compound for the same sample type.

10.0 Calibration

A styrene control sample will be tested weekly to confirm the FID response and calibration.

10.1 Using the Styrene Certification Solution prepared in 7.8.1, perform test analysis as described in 7.8.2 using the equation in 7.8.2.3 to calculate results.

10.2 Calculate the weight of styrene in the styrene control sample using the following equation:

\[ W_s = \frac{(F \times A_{uv} \times W_l)A_s}{A_{uv}} \]

The instrument can be considered calibrated if the weight of the styrene analyzed is within range of 0.00097–0.00103 gms.

11.0 Procedure

11.1 Using an auto pipet, add 25 ml of Internal Standard Solution to a 4 oz. wide-mouth bottle.

11.2 Using a calibrated auto pipet, add 5.0 ± 0.01 g of latex to the bottle containing the 25 ml of Internal Standard Solution.

11.3 Cap the bottle and place on the wrist action shaker. Shake the sample for a minimum of five minutes using the timer on the shaker. Remove from shaker.

11.4 Using a disposable pipet, fill the 2 ml sample vial with the clear alcohol extract. (if the extract is not clear, it should be filtered using a funnel and filter paper.) Cap and seal the vial.

11.5 Place the sample in the autosampler tray and start the GC and Integrator. The sample will be injected into the GC by the auto-injector, and the Integrator will print the results.

11.6 Gas Chromatograph Conditions

Oven Temp—70 °C

Column Temp—225 °C

Detector Temp—275 °C

Heater Pressure—500 KPA

Column Head Pressure—70 KPA

Makeup Gas—30 ml/min.

Column—HP 1909F—123, 30 m x 0.53 mm

Substrate: HP—FFAP (cross-linked) 1 micrometer film thickness

12.0 Calculations

12.1 The integrator is programmed to do the following calculation at the end of the analysis:

\[ \% R_{\text{ResidualStyrene}} = \frac{(A_s \times X W_s)(A_{uv} \times W_l)X F_s}{X 100} \]

Where:

\( A_s = \) peak area of styrene

\( A_{uv} = \) peak area of internal standard
METHOD 313A—DETERMINATION OF RESIDUAL HYDROCARBONS IN RUBBER CRUMB

1.0 Scope and Application

1.1 This method determines residual toluene and styrene in stripper crumb of the following types of rubber: polybutadiene (PBR) and styrene-butadiene rubber (SBR), both derived from solution polymerization processes that utilize toluene as the polymerization solvent.

1.2 The method is applicable to a wide range of concentrations of toluene and styrene provided that calibration standards cover the desired range. It is applicable at least over the range of 0.01 to 100 % residual toluene and from 0.1 to 30 % residual styrene. It is probably applicable over a wider range, but this must be verified prior to use.

1.3 The method may also be applicable to other process samples as long as they are of similar composition to stripper crumb. See section 3.1 of this method for a description of stripper crumb.

2.0 Summary of Method

2.1 The wet crumb is placed in a sealed vial and run on a headspace sampler which heats the vial to a specified temperature for a specific time and then injects a known volume of vapor into a capillary GC. The concentration of each component in the vapor is proportional to the level of that component in the crumb sample and does not depend on water content of the crumb.

2.2 Identification of each component is performed by comparing the retention times to those of known standards.

2.3 Results are calculated by the external standard method since injections are all performed in an identical manner. The response for each component is compared with that obtained from dosed samples of crumb.

2.4 Measured results of each compound are corrected by dividing each by the average recovery efficiency determined for the same compound in the same sample type.

3.0 Definitions

3.1 Stripper crumb refers to pieces of rubber resulting from the steam stripping of a toluene solution of the same polymer in a water slurry. The primary component of this will be polymer with lesser amounts of entrained water and residual toluene and other hydrocarbons. The amounts of hydrocarbons present must be such that the crumb is a solid material, generally less than 10 % of the dry rubber weight.

4.0 Interferences

4.1 Contamination is not normally a problem since samples are sealed into vials immediately on sampling.

4.2 Cross contamination in the headspace sampler should not be a problem if the correct sampler settings are used. This should be verified by running a blank sample immediately following a normal or high sample. Settings may be modified if necessary if this proves to be a problem, or a blank sample may be inserted between samples.

4.3 Interferences may occur if volatile hydrocarbons are present which have retention times close to that of the components of interest. Since the solvent makeup of the processes involved are normally fairly well defined this should not be a problem. If it is found to be the case, switching to a different chromatographic column will probably resolve the situation.

5.0 Safety

5.1 The chemicals specified in this method should all be handled according to standard laboratory practices as well as any special precautions that may be listed in the MSDSs for that compound.

5.2 Sampling of strippers or other process streams may involve high pressures and temperatures or may have the potential for exposure to chemical fumes. Only personnel who have been trained in the specific sampling procedures required for that process should perform this operation. An understanding of the process involved is necessary. Proper personal protective equipment should be worn. Any sampling devices should be inspected prior to use. A detailed sampling
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procedure which specifies exactly how to obtain the sample must be written and followed.

6.0 Equipment and Supplies

6.1 Hewlett Packard (HP) 7694 Headspace sampler, or equivalent, with the following conditions:

- Times (min.): GC cycle time 6.0, vial equilibration 30.0, pressurization 0.25, loop fill 0.25, loop equilibration 0.05, inject 0.25
- Temperatures (deg C): oven 70, loop 80, transfer line 90
- Pressurization gas: He @ 16 psi
- HP 5890 Series II capillary gas chromatograph, or equivalent, with the following conditions:
  - Column: Supelco SPB-1, or equivalent, 15m × 0.25mm × 0.25µ film
  - Carrier: He @ 6 psi
  - Run time: 4 minutes
  - Oven: 70 deg C isothermal
  - Injector: 200 deg C split ratio 50:1
  - Detector: FID @ 220 deg C
- HP Chemstation consisting of computer, printer and Chemstation software, or an equivalent chromatographic data system.

6.2 Microliter pipetting syringes.

6.3 20 ml headspace vials with caps and septa.

6.4 Headspace vial crimper.

6.5 Laboratory shaker or tumbler suitable for the headspace vials.

6.6 Personal protective equipment required for sampling the process such as rubber gloves and face and eye protection.

7.0 Reagents and Standards

7.1 Toluene, 99.9+% purity, HPLC grade.

7.2 Styrene, 99.9+% purity, HPLC grade.

7.3 Dry rubber of same type as the stripper crumb samples.

7.4 Headspace vial crimper.

7.6 Microliter pipetting syringes.

7.7 Drying oven at 100 deg C vented into cold trap or other means of trapping hydrocarbons released.

7.8 Laboratory shaker or tumbler suitable for the headspace vials.

7.9 Personal protective equipment required for sampling the process such as rubber gloves and face and eye protection.

8.0 Sample Collection, Preservation and Storage

8.1 Collect a sample of crumb in a manner appropriate for the process equipment being sampled.

8.1.1 If conditions permit, this may be done by passing a stream of the crumb slurry through a strainer, thus separating the crumb from the water. Allow the water to drain freely, do not attempt to squeeze any water from the crumb. Results will not depend on the exact water content of the samples. Immediately place several pieces of crumb directly into a headspace vial. This should be done with rubber gloves to protect the hands from both the heat and from contact with residual hydrocarbons. The vial should be between ¹/₄ and ¹/₃ full. Results do not depend on sample size as long as there is sufficient sample to reach an equilibrium vapor pressure in the headspace of the vial. Cap and seal the vial. Prepare each sample at least in duplicate. This is to minimize the effect of the variation that naturally occurs in the composition of non homogeneous crumb. The free water is not analyzed by this method and should be disposed of appropriately along with any unused rubber crumb.

8.1.2 Alternatively the process can be sampled in a specially constructed sealed bomb which can then be transported to the laboratory. The bomb is then cooled to ambient temperature by applying a stream of running water. The bomb can then be opened and the crumb separated from the water and the vials filled as described in section 8.1.1 of this method. The bomb may be stored up to 8 hours prior to transferring the crumb into vials.

8.2 The sealed headspace vials may be run immediately or may be stored up to 72 hours prior to running. It is possible that even longer storage times may be acceptable, but this must be verified for the particular type of sample being analyzed (see section 9.2.3 of this method). The main concern here is that some types of rubber eventually may flow, thus compacting the crumb so that the surface area is reduced. This may have some effect on the headspace equilibration.

9.0 Quality Control

9.1 The laboratory is required to operate a formal quality control program. This consists of an initial demonstration of the capability of the method as well as ongoing analysis of standards, blanks and spiked samples to demonstrate continued performance.

9.1.1 When the method is first set up a calibration is run (described in section 10 of this method) and an initial demonstration of method capability is performed (described in section 9.2 of this method). Also recovery efficiency for each type of sample must be determined (see section 9.4 of this method).

9.1.2 It is permissible to modify this method in order to improve separations or make other improvements, provided that all performance specifications are met. Each time a modification to the method is made it is necessary to repeat the calibration (section 10 of this method), the demonstration of method performance (section 9.2 of this method) and the recovery efficiency for each type of sample (section 9.4 of this method).

9.1.3 Ongoing performance should be monitored by running a spiked rubber standard. If this test fails to demonstrate that the analysis is in control, then corrective action must be taken. This method is described in section 9.3 of this method.

9.1.4 If new types of samples are being analyzed then recovery efficiency for each new type of sample must be determined. New type includes any change, such as polymer...
type, physical form or a significant change in the composition of the matrix.

9.2 Initial demonstration of method capability to establish the accuracy and precision of the method. This is to be run following the calibration described in section 10 of this method.

9.2.1 Prepare a series of identical spiked rubber standards as described in section 9.3 of this method. A sufficient number to determine statistical information on the test should be run. Ten may be a suitable number, depending on the quality control methodology used at the laboratory running the tests. These are run in the same manner as unknown samples (see section 11 of this method).

9.2.2 Determine mean and standard deviation for the results. Use these to determine the capability of the method and to calculate suitable control limits for the ongoing performance check which will utilize the same standards.

9.2.3 Prepare several additional spiked rubber standards and run 2 each day to determine the suitability of storage of the samples for 24, 48 and 72 hours or longer if longer storage times are desired.

9.3 A spiked rubber standard should be run on a regular basis to verify system performance. This would probably be done daily if samples are run daily. This is prepared in the same manner as the calibration standards (section 10.1 of this method), except that only one concentration of toluene and styrene is prepared. Choose concentrations of toluene and styrene that fall in the middle of the range expected in the stripper crumb and then do not change these unless there is a major change in the composition of the unknowns. If it becomes necessary to change the composition of this standard the initial performance demonstration must be repeated with the new standard (section 9.2 of this method).

9.3.1 Each day prepare one spiked rubber standard to be run the following day. The dry rubber may be prepared in bulk and stored for any length of time consistent with the shelf life of the product. The addition of water and hydrocarbons must be performed daily and all the steps described under section 10.1 of this method must be followed.

9.3.2 Run the spiked rubber standard prepared the previous day. Record the results and plot on an appropriate control chart or other means of determining statistical control.

9.3.3 If the results for the standard indicate that the test is out of control then corrective action must be taken. This may include a check on procedures, instrument settings, maintenance or recalibration. Samples may be stored (see section 8.2 of this method) until compliance is demonstrated.

9.4 Recovery efficiency must be determined once for each sample type and whenever modifications are made to the method.

9.4.1 For each sample type collect 12 samples from the process (see section 8.1 of this method). This should be done when the process is operating in a normal manner and residual hydrocarbon levels are in the normal range. Half the vials and caps should be tared, labeled “spiked” and numbered 1 through 6. The other vials are labeled “unspiked” and need not be tared but are also numbered 1 through 6. Immediately on sampling, the vials should be capped to prevent loss of volatiles. Allow all the samples to cool completely to ambient temperature. Reweigh each of the vials labeled “spiked” to determine the weight of wet crumb inside.

9.4.2 The dry weight of rubber present in the wet crumb is estimated by multiplying the weight of wet crumb by the fraction of nonvolatile typical for the sample. If this is not known, an additional quantity of crumb may be sampled, weighed, dried in an oven and reweighed to determine the fraction of volatiles and nonvolatiles prior to starting this procedure.

9.4.3 To the vials labeled “spiked” add an amount of a mixture of toluene and styrene that is between 40 and 60 % of the amount expected in the crumb. This is done by removing the cap, adding the mixture by syringe, touching the tip of the needle to the sample in order to remove the drop and then immediately recapping the vials. The mixture is not added through the septum, because a punctured septum may leak and vent vapors as the vial is heated. The weights of toluene and styrene added may be calculated from the volumes of the mixture added, its composition and density, or may be determined by the weight of the vials and caps prior to and after addition. The exact dry weight of rubber present and the concentration of residual toluene and styrene are not known at this time so an exact calculation of the concentration of hydrocarbons is not possible until the test is completed.

9.4.4 Place all the vials onto a shaker or tumbler for 24 ± 2 hours. This is essential in order for the hydrocarbons to be evenly distributed and completely absorbed into the rubber. If this is not followed the toluene and styrene will be mostly at the surface of the rubber and high results will be obtained.

9.4.5 Remove the vials from the shaker and tap them so that all the crumb settles to the bottom of the vials. Allow them to stand for 1 hour prior to analysis to allow any liquid to drain fully to the bottom.

9.4.6 Run the spiked and unspiked samples in the normal manner. Record the concentrations of toluene and styrene reported for each pair of spiked and unspiked samples with the same vial number.

9.4.7 Open each of the vials labeled “spiked”, remove all the rubber crumb and
place it into a tarred drying pan. Place in a 100 °C oven for two hours, cool and reweigh. Subtract the weight of the tare to give the dry weight of rubber in each spiked vial. This will be slightly different for each vial since the weights of dry rubber will be different.

9.4.8 For each hydrocarbon calculate the average recovery efficiency (R) using the following equations:

\[ R = \frac{\sum (P_{n} \times R_{n})}{6} \]

\[ R_{n} = \frac{C_{n}}{C_{ns}} \]

Where:

- \( R \) = recovery efficiency
- \( n \) = vial number
- \( C_{ns} \) = concentration of compound measured in spiked sample number \( n \)
- \( C_{nu} \) = concentration of compound measured in unspiked sample number \( n \)
- \( S_{n} \) = theoretical concentration of compound spiked into sample \( n \) calculated in step 9.4.7

9.4.9 A different \( R \) value should be obtained for each compound (styrene and toluene) and for each sample type.

9.4.10 A value of \( R \) between 0.70 and 1.30 is acceptable.

9.4.11 \( R \) is used to correct all reported results for each compound by dividing the measured results of each compound by the \( R \) for that compound for the same sample type (see section 12.2 of this method.)

10.0 Calibration

10.1 Calibration standards are prepared by dosing known amounts of the hydrocarbons of interest into vials containing known amounts of rubber and water.

10.1.1 Cut a sufficient quantity of dry rubber of the same type as will be analyzed into pieces about the same size as that of the crumb. Place these in a single layer on a piece of aluminum foil or other suitable surface and place into a forced air oven at 100 °C for four hours. This is to remove any residual hydrocarbons that may be present. This step may be performed in advance.

10.1.2 Into each of a series of vials add 3.0 g of the dry rubber.

10.1.3 Into each vial add 1.0 ml distilled water or an amount that is close to the amount that will be present in the unknowns. The exact amount of water present does not have much effect on the analysis, but it is necessary to have a saturated environment. The water will also aid in the uniform distribution of the spiked hydrocarbons over the surface of the rubber after the vials are placed on the shaker (in step 10.1.5 of this method).

10.1.4 Into each vial add varying amounts of toluene and styrene by microliter syringe and cap the vials immediately to prevent loss. The tip of the needle should be carefully touched to the rubber in order to transfer the last drop to the rubber. Toluene and styrene may first be mixed together in suitable proportions and added together if desired. The weights of toluene and styrene added may be calculated from the volumes of the mixture added, its composition and density, or may be determined by the weight of the vials and caps prior to and after addition. Concentrations of added hydrocarbons are calculated as percent of the dry rubber weight. At least 5 standards should be prepared with the amounts of hydrocarbons added being calculated to cover the entire range possible in the unknowns. Retain two samples with no added hydrocarbons as blanks.

10.1.5 Place all the vials onto a shaker or tumbler for 24 ± 2 hours. This is essential in order for the hydrocarbons to be evenly distributed and completely absorbed into the rubber. If this is not followed the toluene and styrene will be mostly at the surface of the rubber and high results will be obtained.

10.1.6 Remove the vials from the shaker and tap them so that all the crumb settles to the bottom of the vials. Allow them to stand for 1 hour prior to analysis to allow any liquid to drain fully to the bottom.

10.2 Run the standards and blanks in the same manner as described for unknowns (section 11 of this method), starting with a blank, then in order of increasing hydrocarbon content and ending with the other blank.

10.3 Verify that the blanks are sufficiently free from toluene and styrene or any interfering hydrocarbons.

10.3.1 It is possible that trace levels may be present even in dry product. If levels are high enough that they will interfere with the calibration then the drying procedure in section 10.1.1 of this method should be reviewed and modified as needed to ensure that suitable standards can be prepared.

10.3.2 It is possible that the final blank is contaminated by the previous standard. If this is the case review and modify the sampler parameters as needed to eliminate this problem. If necessary it is possible to run blank samples between regular samples in order to reduce this problem, though it should not be necessary if the sampler is properly set up.

10.4 Enter the amounts of toluene and styrene added to each of the samples (as calculated in section 10.1.4 of this method) into the calibration table and perform a calibration utilizing the external standard method of analysis.

10.5 At low concentrations the calibration should be close to linear. If a wide range of levels are to be determined it may be desirable to apply a nonlinear calibration to get the best fit.
11.0 Procedure

11.1 Place the vials in the tray of the headspace sampler. Enter the starting and ending positions through the console of the sampler. For unknown samples each is run in duplicate to minimize the effect of variations in crumb composition. If excessive variation is noted it may be desirable to run more than two of each sample.

11.2 Make sure the correct method is loaded on the Chemstation. Turn on the gas flows and light the FID flame.

11.3 Start the sequence on the Chemstation. Press the START button on the headspace unit. The samples will be automatically injected after equilibrating for 30 minutes in the oven. As each sample is completed the Chemstation will calculate and print out the results as percent toluene and styrene in the crumb based on the dry weight of rubber.

12.0 Data Analysis and Calculations

12.1 For each set of duplicate samples calculate the average of the measured concentration of toluene and styrene. If more than two replicates of each sample are run calculate the average over all replicates.

12.2 For each sample correct the measured amounts of toluene and styrene using the following equation:

\[
\text{Corrected Result} = \frac{C_m}{R}
\]

Where:

- \( C_m \): Average measured concentration for that compound.
- \( R \): Recovery efficiency for that compound in the same sample type (see section 9.4 of this method)

12.3 Report the recovery efficiency (R) and the corrected results of toluene and styrene for each sample.

13.0 Method Performance

13.1 This method can be very sensitive and reproducible. The actual performance depends largely on the exact nature of the samples being analyzed. Actual performance must be determined by each laboratory for each sample type.

13.2 The main source of variation is the actual variation in the composition of non homogeneous crumb in a stripping system and the small sample sizes employed here. It therefore is the responsibility of each laboratory to determine the optimum number of replicates of each sample required to obtain accurate results.

14.0 Pollution Prevention

14.1 Samples should be kept sealed when possible in order to prevent evaporation of hydrocarbons.

14.2 When drying of samples is required it should be done in an oven which vents into a suitable device that can trap the hydrocarbons released.

14.3 Dispose of samples as described in section 15.

15.0 Waste Management

15.1 Excess stripper crumb and water as well as the contents of the used sample vials should be properly disposed of in accordance with local and federal regulations.

15.2 Preferably this will be accomplished by having a system of returning unused and spent samples to the process.

16.0 References


METHOD 313B—THE DETERMINATION OF RESIDUAL HYDROCARBON IN SOLUTION POLYMERS BY CAPILLARY GAS CHROMATOGRAPHY

1.0 Scope

1.1 This method is applicable to solution polymerized polybutadiene (PBD).

1.2 This method quantitatively determines \( n \)-hexane in wet crumb polymer at levels from 0.08 to 0.15% by weight.

1.3 This method may be extended to the determination of other hydrocarbons in solution produced polymers with proper experimentation and documentation.

2.0 Principle of Method

2.1 A weighed sample of polymer is dissolved in chloroform and the cement is coagulated with an isopropyl alcohol solution containing a specific amount of alpha-methyl styrene (AMS) as the internal standard. The extract of this coagulation is then injected into a gas chromatograph and separated into individual components. Quantification is achieved by the method of internal standardization.

3.0 Definitions

3.1 The definitions are included in the text as needed.

4.0 Interferences

[Reserved]

5.0 Safety

5.1 This method may involve hazardous materials, operations, and equipment. This method does not purport to address all of the safety problems associated with its use. It is the responsibility of the user of this method to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.
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6.0 Equipment and Supplies

6.1 Analytical balance, 160 g capacity, 0.1 mg resolution

6.2 Bottles, 2-oz capacity with poly-cap screw lids

6.3 Mechanical shaker

6.4 Syringe, 10-μl capacity

6.5 Syringe, 2.5-ml capacity, with 22 gauge 1.25 inch needle, PP/PE material, disposable

6.6 Gas chromatograph, Hewlett-Packard model 5890, or equivalent, configured with FID, split injector packed with silanized glass wool.

6.6.1 Establish the following gas chromatographic conditions, and allow the system to thoroughly equilibrate before use.

6.6.2 Injector parameters:
- Injection technique=Split
- Injector split flow=86 ml/min
- Injector temperature=225 deg C

6.6.3 Oven temperature program:
- Initial temperature=40 deg C
- Initial time=6 min
- Program rate=10 deg C/min
- Upper limit temperature=175 deg C
- Upper limit interval=10 min

6.6.4 Detector parameters:
- Detector temperature=300 deg C
- Hydrogen flow=30 ml/min
- Air flow=350 ml/min
- Nitrogen make up=26 ml/min

6.7 Gas chromatographic columns: SE-54 (5%-phenyl) (1%-vinyl)-methylpolysiloxane, 15 M × 0.53 mm ID with a 1.2 micron film thickness, and a Carbowax 20M (polyethylene glycol), 15 M × 0.53 mm ID with a 1.2 micron film thickness.

6.7.1 Column assembly: using a 0.53 mm ID butt connector union, join the 15 M × 0.53 mm SE-54 column to the 15 M × 0.53 mm Carbowax 20M. The SE-54 column will be inserted into the injector and the Carbowax 20M inserted into the detector after they have been joined.

6.7.2 Column parameters:
- Helium flow=2.8 ml/min
- Helium headpressure=2 psig

6.8 Centrifuge

6.9 Data collection system, Hewlett-Packard Model 3396, or equivalent

6.10 Pipet, 25-ml capacity, automatic dispensing, and 2-liter reservoir

6.11 Pipet, 2-ml capacity, volumetric delivery, class A

6.12 Flasks, 100 and 1000-ml capacity, volumetric, class A

6.13 Vial, serum, 50-ml capacity, red rubber septa and crimp ring seals

6.14 Sample collection basket fabricated out of wire mesh to allow for drainage

7.0 Chemicals and Reagents

CHEMICALS:

7.1 alpha-Methyl Styrene, C9H10, 99+% purity, CAS 98-83-9

7.2 n-Hexane, C6H14, 99+% purity, CAS 110-54-3

7.3 Isopropyl alcohol, C3H8O 99.5+% purity, reagent grade, CAS 67-63-0

7.4 Chloroform, CHCl3, 99% min., CAS 67-66-3

REAGENTS:

7.5 Internal Standard Stock Solution: 10 mg/25 ml AMS in isopropyl alcohol.

7.5.1 Into a 25-ml beaker, weigh 0.4 g of AMS to the nearest 0.1 mg.

7.5.2 Quantitatively transfer this AMS into a 1-L volumetric flask. Dilute to the mark with isopropyl alcohol.

7.5.3 Transfer this solution to the automatic dispensing pipet reservoir. This will be labeled the AMS STOCK SOLUTION.

7.6 n-Hexane Stock Solution: 13 mg/2 ml hexane in isopropyl alcohol.

7.6.1 Into a 100-ml volumetric flask, weigh 0.65 g of n-hexane to the nearest 0.1 mg.

7.6.2 Dilute to the mark with isopropyl alcohol. This solution will be labeled the n-HEXANE STOCK SOLUTION.

8.0 Sample Collection, Preservation and Storage

8.1 A sampling device similar to Figure 1 is used to collect a non-vented crumb rubber sample at a location that is after the striping operation but before the sample is exposed to the atmosphere.

8.2 The crumb rubber is allowed to cool before opening the sampling device and removing the sample.

8.3 The sampling device is opened and the crumb rubber sample is collected in the sampling basket.

8.4 One pound of crumb rubber sample is placed into a polyethylene bag. The bag is labeled with the time, date and sample location.

8.5 The sample should be delivered to the laboratory for testing within one hour of sampling.

8.6 Laboratory testing will be done within 3 hours of the sampling time.

8.7 No special storage conditions are required unless the storage time exceeds 3 hours in which case refrigeration of the samples is recommended.

9.0 Quality Control

9.1 For each sample type, 12 samples shall be obtained from the process for the recovery study. Half of the vials and caps shall be tared, labeled “spiked”, and numbered 1 through 6. The other vials shall be labeled “unspiked” and need not be tared, but are also numbered 1 through 6.

9.2 Determine the % moisture content of the crumb sample. After determining the % moisture content, the correction factor for

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calculating the dry crumb weight can be determined by using the equation in section 12.2 of this method.

9.3 Run the spiked and unspiked samples in the normal manner. Record the concentrations of the n-hexane content of the mixed hexane reported for each pair of spiked and unspiked samples.

9.4 For the recovery study, each sample of crumb shall be dissolved in chloroform containing a known amount of mixed hexane solvent.

9.5 For each hydrocarbon, calculate the recovery efficiency (R) using the following equations:

\[
R = \frac{M_r}{S}
\]

Where:

- \(M_r\) = Measured amount of compound in the spiked sample
- \(M_s\) = Measured amount of compound in the unspiked sample
- \(S\) = Amount of compound added to the spiked sample

9.6 Normally a value of R between 0.70 and 1.30 is acceptable.

9.7 R is used to correct all reported results for each compound by dividing the measured results of each compound by the R for that compound for the same sample type.

10.0 Calibration

10.1 Using the AMS STOCK SOLUTION equipped with the automatic dispensing pipet (7.5.3 of this method), transfer 25.0 ml of the internal standard solution into an unsealed 50-ml serum vial.

10.2 Using a 2.0 ml volumetric pipet, quantitatively transfer 2.0 ml of the n-HEXANE STOCK SOLUTION (7.6.2 of this method) into the 50-ml serum vial and cap. This solution will be labeled the CALIBRATION SOLUTION.

10.3 Using the conditions prescribed (6.6 of this method), inject 1 µl of the supernate.

10.4 Obtain the peak areas and calculate the response factor as described in the calculations section (12.1 of this method).

11.0 Procedure

11.1 Determination of Dry Polymer Weight

11.1.1 Remove wet crumb from the polyethylene bag and place on paper towels to absorb excess surface moisture.

11.1.2 Cut small slices or cubes from the center of the crumb sample to improve sample uniformity and further eliminate surface moisture.

11.1.3 A suitable gravimetric measurement should be made on a sample of this wet crumb to determine the correction factor needed to calculate the dry polymer weight.

11.2 Determination of n-Hexane in Wet Crumb

11.2.1 Remove wet crumb from the polyethylene bag and place on paper towels to absorb excess surface moisture.

11.2.2 Cut small slices or cubes from the center of the crumb sample to improve sample uniformity and further eliminate surface moisture.

11.2.3 Into a tared 2 oz bottle, weigh 1.5 g of wet polymer to the nearest 0.1 mg.

11.2.4 Add 25 ml of chloroform to the 2 oz bottle and cap.

11.2.5 Using a mechanical shaker, shake the bottle until the polymer dissolves.

11.2.6 Using the autodispensing pipet, add 25.0 ml of the AMS STOCK SOLUTION (7.5.3 of this method) to the dissolved polymer solution and cap.

11.2.7 Using a mechanical shaker, shake the bottle for 10 minutes to coagulate the dissolved polymer.

11.2.8 Centrifuge the sample for 3 minutes at 2000 rpm.

11.2.9 Using the conditions prescribed (6.6 of this method), chromatograph 1 µl of the supernate.

11.2.10 Obtain the peak areas and calculate the concentration of the component of interest as described in the calculations (12.2 of this method).

12.0 Calculations

12.1 Calibration:

\[
RF_x = \frac{(W_x \times A_{is})}{(W_{is} \times A_x)}
\]

Where:

- \(RF_x\) = the relative response factor for n-hexane
- \(W_x\) = the weight (g) of the dry polymer corrected for moisture
- \(W_{is}\) = the weight (g) of the wet crumb in section 9.6
- \(A_{is}\) = the area of AMS
- \(A_x\) = the area of n-hexane

12.2 Procedure:

12.2.1 Correction Factor for calculating dry crumb weight.

\[
F = 1 - \frac{\% \text{ moisture}}{100}
\]

Where:

\(F\) = Correction factor for calculating dry crumb weight
\(\% \text{ moisture}\) = moisture determined by appropriate method

12.2.2 Moisture adjustment for chromatographic determination.

\[
W = F \times W_c
\]

Where:

- \(W\) = the weight (g) of the dry polymer corrected for moisture
- \(W_c\) = the weight (g) of the wet crumb

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12.2.3 Concentration (ppm) of hexane in the wet crumb.

\[ \text{ppm} = \frac{A_x \cdot RF_x \cdot W_{is} \cdot 10000}{A_{is} \cdot W_s} \]

Where:

- \( \text{ppm} \) = parts per million of n-hexane in the polymer
- \( A_x \) = the area of n-hexane
- \( RF_x \) = the relative response factor for n-hexane
- \( W_{is} \) = the weight (g) of AMS in the sample solution
- \( A_{is} \) = the area of AMS
- \( W_s \) = the weight (g) of the dry polymer corrected for moisture

13.0 Method Performance

13.1 Precision for the method was determined at the 0.08% level. The standard deviation was 0.01 and the percent relative standard deviation (RSD) was 16.3% with five degrees of freedom.

14.0 Waste Generation

14.1 Waste generation should be minimized where possible.

15.0 Waste Management

15.1 Discard liquid chemical waste into the chemical waste drum.

15.2 Discard polymer waste into the polymer waste container.

16.0 References

16.1 This method is based on Goodyear Chemical Division Test Method E-964.

METHOD 315—DETERMINATION OF PARTICULATE AND METHYLENE CHLORIDE EXTRACTABLE MATTER (MCEM) FROM SELECTED SOURCES AT PRIMARY ALUMINUM PRODUCTION FACILITIES

NOTE: This method does not include all of the specifications (e.g., equipment and supplies) and procedures (e.g., sampling and analytical) essential to its performance. Some material is incorporated by reference from other methods in this part. Therefore, to obtain reliable results, persons using this method should have a thorough knowledge of at least the following additional test methods: Method 1, Method 2, Method 3, and Method 5 of 40 CFR part 60, appendix A.

1.0 Scope and Application

1.1 Analytes. Particulate matter (PM). No CAS number assigned. Methylene chloride extractable matter (MCEM). No CAS number assigned.

1.2 Applicability. This method is applicable for the simultaneous determination of PM and MCEM when specified in an applicable regulation. This method was developed by consensus with the Aluminum Association and the U.S. Environmental Protection Agency (EPA) and has limited precision estimates for MCEM; it should have similar precision to Method 5 for PM in 40 CFR part 60, appendix A since the procedures are similar for PM.

1.3 Data quality objectives. Adherence to the requirements of this method will enhance the quality of the data obtained from air pollutant sampling methods.

2.0 Summary of Method

Particulate matter and MCEM are withdrawn isokinetically from the source. PM is collected on a glass fiber filter maintained at a temperature in the range of 120 ± 14 °C (248 ± 25 °F) or such other temperature as specified by an applicable subpart of the standards or approved by the Administrator for a particular application. The PM mass, which includes any material that condenses on the probe and is subsequently removed in an acetone rinse or on the filter at or above the filtration temperature, is determined gravimetrically after removal of uncombined water. MCEM is then determined by adding a methylene chloride rinse of the probe and filter holder, extracting the condensable hydrocarbons collected in the impinger water, adding an acetone rinse followed by a methylene chloride rinse of the sampling train components after the filter and before the silica gel impinger, and determining residue gravimetrically after evaporating the solvents.

3.0 Definitions. [Reserved]

4.0 Interferences. [Reserved]

5.0 Safety

This method may involve hazardous materials, operations, and equipment. This method does not purport to address all of the safety problems associated with its use. It is the responsibility of the user of this method to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to performing this test method.

6.0 Equipment and Supplies

NOTE: Mention of trade names or specific products does not constitute endorsement by the EPA.

6.1 Sample collection. The following items are required for sample collection:

6.1.1 Sampling train. A schematic of the sampling train used in this method is shown in Figure 5-1, Method 5, 40 CFR part 60, appendix A. Complete construction details are given in APTD-0581 (Reference 2 in section 17.0 of this method); commercial models of this train are also available. For changes from APTD-0581 and for allowable modifications of the train shown in Figure 5-1, Method 5, 40 CFR part 60, appendix A, see the following subsections.
NOTE: The operating and maintenance procedures for the sampling train are described in APTD-0576 (Reference 3 in section 17.0 of this method). Since correct usage is important to obtaining valid results, all users should read APTD-0576 and adopt the operating and maintenance procedures outlined in it, unless otherwise specified herein. The use of grease for sealing sampling train components is not recommended because many greases are soluble in methylene chloride. The sampling train consists of the following components:

6.1.1.1 Probe nozzle. Glass or glass lined with sharp, tapered leading edge. The angle of taper shall be ≤3°, and the taper shall be on the outside to preserve a constant internal diameter. The probe nozzle shall be of the button-hook or elbow design, unless otherwise specified by the Administrator. Other materials of construction may be used, subject to the approval of the Administrator. A range of nozzle sizes suitable for isokinetic sampling should be available. Typical nozzle sizes range from 0.32 to 1.27 cm (1/8 to 1/2 in.) inside diameter (ID) in increments of 0.16 cm (5/64 in.). Larger nozzle sizes are also available if higher volume sampling trains are used. Each nozzle shall be calibrated according to the procedures outlined in section 10.0 of this method.

6.1.1.2 Probe liner. Borosilicate or quartz glass tubing with a heating system capable of maintaining a probe gas temperature at the exit end during sampling of 120±14°C (248±25°F), or such other temperature as specified by an applicable subpart of the standards or approved by the Administrator for a particular application. Because the actual temperature at the outlet of the probe is not usually monitored during sampling, probes constructed according to APTD-0581 and using the calibration curves of APTD-0576 (or calibrated according to the procedure outlined in APTD-0576) will be considered acceptable. Either borosilicate or quartz glass probe liners may be used for stack temperatures up to about 480°C (900°F); quartz liners shall be used for temperatures between 480 and 900°C (900 and 1,650°F). Both types of liners may be used at higher temperatures than specified for short periods of time, subject to the approval of the Administrator. The softening temperature for borosilicate glass is 820°C (1,500°F) and for quartz glass it is 1,500°C (2,700°F).

6.1.1.3 Pitot tube. Type S, as described in section 6.1 of Method 2, 40 CFR part 60, appendix A, or other device approved by the Administrator. The pitot tube shall be attached to the probe (as shown in Figure 5-1 of Method 5, 40 CFR part 60, appendix A) to allow constant monitoring of the stack gas velocity. The impact (high pressure) opening plane of the pitot tube shall be even with or above the nozzle entry plane (see Method 2, Figure 2-6b, 40 CFR part 60, appendix A) during sampling. The Type S pitot tube assembly shall have a known coefficient, determined as outlined in section 10.0 of Method 2, 40 CFR part 60, appendix A.

6.1.1.4 Differential pressure gauge. Inclined manometer or equivalent device (two), as described in section 6.2 of Method 2, 40 CFR part 60, appendix A. One manometer shall be used for velocity head (Dp) readings, and the other, for orifice differential pressure readings.

6.1.1.5 Filter holder. Borosilicate glass, with a glass frit filter support and a silicone rubber gasket. The holder design shall provide a positive seal against leakage from the outside or around the filter. The holder shall be attached immediately at the outlet of the probe (or cyclone, if used).

6.1.1.6 Filter heating system. Any heating system capable of maintaining a temperature around the filter holder of 120±14°C (248±25°F) during sampling, or such other temperature as specified by an applicable subpart of the standards or approved by the Administrator for a particular application. Alternatively, the tester may opt to operate the equipment at a temperature lower than that specified. A temperature gauge capable of measuring temperature to within ±3°C (±5°F) shall be installed so that the temperature around the filter holder can be regulated and monitored during sampling. Heating systems other than the one shown in APTD-0581 may be used.

6.1.1.7 Temperature sensor. A temperature sensor capable of measuring temperature to within ±3°C (±5°F) shall be installed so that the sensing tip of the temperature sensor is in direct contact with the sample gas, and the temperature around the filter holder can be regulated and monitored during sampling.

6.1.1.8 Condenser. The following system shall be used to determine the stack gas moisture content: four glass impingers connected in series with leak-free ground glass fittings. The first, third, and fourth impingers shall be of the Greenburg-Smith design, modified by replacing the tip with a 1.3 cm (1/2 in.) ID glass tube extending to about 1.3 cm (1/2 in.) from the bottom of the flask. The second impinger shall be of the Greenburg-Smith design with the standard tip. The first and second impingers shall contain known quantities of water (section 8.3.1 of this method), the third shall be empty, and the fourth shall contain a known weight of silica gel or equivalent desiccant. A temperature sensor capable of measuring temperature to within ±1°C (±2°F) shall be placed at the outlet of the fourth impinger for monitoring.

6.1.1.9 Metering system. Vacuum gauge, leak-free pump, temperature sensors capable of measuring temperature to within ±3°C (±5°F), dry gas meter (DGM) capable of measuring volume to within 2 percent, and
related equipment, as shown in Figure 5-1 of Method 5, 40 CFR part 60, appendix A. Other metering systems capable of maintaining sampling rates within 10 percent of isokinetic and of determining sample volumes to within 2 percent may be used, subject to the approval of the Administrator. When the metering system is used in conjunction with a sampling probe, the system shall allow periodic checks of isokinetic rates.

6.1.1.10 Sampling systems using metering systems designed for higher flow rates than that described in APTD-0581 or APTD-0576 may be used provided that the specifications of this method are met.

6.1.2 Barometer. Mercury, aneroid, or other barometer capable of measuring atmospheric pressure to within 2.5 mm (0.1 in.) Hg.

**NOTE:** The barometric reading may be obtained from a nearby National Weather Service station. In this case, the station value (which is the absolute barometric pressure) shall be requested and an adjustment for elevation differences between the weather station and sampling point shall be made at a rate of minus 2.5 mm (0.1 in.) Hg per 30 m (100 ft) elevation increase or plus 2.5 mm (0.1 in.) Hg per 30 m (100 ft) elevation decrease.

6.1.3 Gas density determination equipment. Temperature sensor and pressure gauge, as described in sections 6.3 and 6.4 of Method 2, 40 CFR part 60, appendix A, and gas analyzer, if necessary, as described in Method 3, 40 CFR part 60, appendix A. The temperature sensor shall, preferably, be permanently attached to the pitot tube or sampling probe in a fixed configuration, such that the tip of the sensor extends beyond the leading edge of the probe sheath and does not touch any metal. Alternatively, the sensor may be attached just prior to use in the field. Note, however, that if the temperature sensor is attached in the field, the sensor must be placed in an interference-free arrangement with respect to the Type S pitot tube openings (see Method 2, Figure 2-4, 40 CFR part 60, appendix A). As a second alternative, if a difference of not more than 1 percent in the average velocity measurement is to be introduced, the temperature sensor need not be attached to the probe or pitot tube. (This alternative is subject to the approval of the Administrator.)

6.2 Sample recovery. The following items are required for sample recovery:

6.2.1 Probe-liner and probe-nozzle brushes. Nylon or Teflon® bristle brushes with stainless steel wire handles. The probe brush shall have extensions (at least as long as the probe) constructed of stainless steel, nylon, Teflon®, or similarly inert material. The brushes shall be properly sized and shaped to brush out the probe liner and nozzle.

6.2.2 Wash bottles. Glass wash bottles are recommended. Polyethylene or tetrafluoroethylene (TFE) wash bottles may be used, but they may introduce a positive bias due to contamination from the bottle. It is recommended that acetone not be stored in polyethylene or TFE bottles for longer than a month.

6.2.3 Glass sample storage containers. Chemically resistant, borosilicate glass bottles, for acetone and methylene chloride washes and impinger water, 500 ml or 1,000 ml. Screw-cap liners shall either be rubber-backed Teflon® or shall be constructed so as to be leak-free and resistant to chemical attack by acetone or methylene chloride. (Narrow-mouth glass bottles have been found to be less prone to leakage.) Alternatively, polyethylene bottles may be used.

6.2.4 Petri dishes. For filter samples, glass, unless otherwise specified by the Administrator.

6.2.5 Graduated cylinder and/or balance. To measure condensed water, acetone wash and methylene chloride wash used during field recovery of the samples, to within 1 ml or 1 g. Graduated cylinders shall have subdivisions no greater than 2 ml. Most laboratory balances are capable of weighing to the nearest 0.5 g or less. Any such balance is suitable for use here and in section 6.3.4 of this method.

6.2.6 Plastic storage containers. Air-tight containers to store silica gel.

6.2.7 Funnel and rubber policeman. To aid in transfer of silica gel to container; not necessary if silica gel is weighed in the field.

6.2.8 Funnel. Glass or polyethylene, to aid in sample recovery.

6.3 Sample analysis. The following equipment is required for sample analysis:

6.3.1 Glass or Teflon® weighing dishes.

6.3.2 Desiccator. It is recommended that fresh desiccant be used to minimize the chance for positive bias due to absorption of organic material during drying.

6.3.3 Analytical balance. To measure to within 0.1 mg.

6.3.4 Balance. To measure to within 0.5 g.

6.3.5 Beakers. 250 ml.

6.3.6 Hygrometer. To measure the temperature of the laboratory environment.

6.3.7 Temperature sensor. To measure the temperature of the laboratory environment.

6.3.8 Buchner fritted funnel. 30 ml size, fine (<50 micron)-porosity fritted glass.

6.3.9 Pressure filtration apparatus.

6.3.10 Aluminum dish. Flat bottom, smooth sides, and flanged top, 18 mm deep and with an inside diameter of approximately 60 mm.

7.0 Reagents and Standards.

7.1 Sample collection. The following reagents are required for sample collection:

7.1.1 Filters. Glass fiber filters, without organic binder, exhibiting at least 99.95 percent efficiency (<0.05 percent penetration) on
0.3 micron dioctyl phthalate smoke particles. The filter efficiency test shall be conducted in accordance with ASTM Method D 2956-85A (incorporated by reference in §63.941 of this part). Test data from the supplier’s quality control program are sufficient for this purpose. In sources containing SO₂ or SO₃, the filter material must be of a type that is unreactive to SO₂ or SO₃. Reference 10 in section 17.0 of this method may be used to select the appropriate filter.

7.1.2 Silica gel. Indicating type, 6 to 16 mesh. If previously used, dried at 175°C (350°F) for 2 hours. New silica gel may be used as received. Alternatively, other types of desiccants (equivalent or better) may be used, subject to the approval of the Administrator.

7.1.4 Crushed ice.

7.1.5 Stopcock grease. Acetone-insoluble, heat-stable silicone grease. This is not necessary if screw-on connectors with Teflon® sleeves, or similar, are used. Alternatively, other types of stopcock grease may be used, subject to the approval of the Administrator. [Caution: Many stopcock greases are acetone-insoluble. Use sparingly and carefully remove prior to recovery to prevent contamination of the MCEM analysis.]

7.1.6 Crushed ice.

7.2 Sample recovery. The following reagents are required for sample recovery:

7.2.1 Acetone. Acetone with blank values <1 ppm, by weight residue, is required. Acetone blanks may be run prior to field use, and only acetone with low blank values may be used. In no case shall a blank value of greater than 1E-06 of the weight of acetone used be subtracted from the sample weight.

NOTE: This is more restrictive than Method 5, 40 CFR part 60, appendix A. At least one vendor (Supelco Incorporated located in Bellefonte, Pennsylvania) lists <1 mg/l as residue for its Environmental Analysis Solvents-grade acetone.

7.2.2 Methylene chloride. Methylene chloride with a blank value <3.5 ppm, by weight, residue. Methylene chloride blanks may be run prior to field use, and only methylene chloride with low blank values may be used. In no case shall a blank value of greater than 1E-06 of the weight of methylene chloride used be subtracted from the sample weight.

NOTE: This is more restrictive than Method 5, 40 CFR part 60, appendix A. At least one vendor quotes <1 mg/l for its Environmental Analysis Solvents-grade methylene chloride.

7.3 Sample analysis. The following reagents are required for sample analysis:

7.3.1 Acetone. Same as in section 7.2.1 of this method.

7.3.2 Desiccant. Anhydrous calcium sulfate, indicating type. Alternatively, other types of desiccants may be used, subject to the approval of the Administrator.

7.3.3 Acetone blanks may be run prior to field use to eliminate a high blank value. In no case shall a blank value greater than 1E-06 of the weight of acetone be used. In no case shall a blank value of acetone blank value >1.5 ppm, by weight residue, is required. Methylene chloride blanks may be run prior to field use, and only methylene chloride with a blank value <1.5 ppm, by weight, residue for its Environmental Analysis Solvents-grade methylene chloride.

8.0 Sample Collection, Preservation, Storage, and Transport.

NOTE: The complexity of this method is such that, in order to obtain reliable results, testers should be trained and experienced with the test procedures.

8.1 Pretest preparation. It is suggested that sampling equipment be maintained according to the procedures described in APTD-0576.

8.1.1 Weigh several 200 g to 300 g portions of silica gel in airtight containers to the nearest 0.5 g. Record the total weight of the silica gel plus container. As an alternative, the silica gel need not be preweighed but may be weighed directly in its impinger or sampling holder just prior to train assembly.

8.1.2 A batch of glass fiber filters, no more than 50 at a time, should be placed in a soxhlet extraction apparatus and extracted using methylene chloride for at least 16 hours. After extraction, check filters visually against light for irregularities, flaws, or pinhole leaks. Label the shipping containers (glass or plastic petri dishes), and keep the filters in these containers at all times except during sampling and weighing.

8.1.3 Weigh the filters at 20 ±0.5°C (68 ±10°F) and ambient pressure for at least 24 hours and weigh at intervals of at least 6 hours to a constant weight, i.e., <0.5 mg change from previous weighing; record results to the nearest 0.1 mg. During each weighing the filter must not be exposed to the laboratory atmosphere for longer than 2 minutes and a relative humidity above 50 percent. Alternatively (unless otherwise specified by the Administrator), the filters may be oven-dried at 104°C (220°F) for 2 to 3 hours, desiccated for 2 hours, and weighed. Procedures other than those described, which account for relative humidity effects, may be used, subject to the approval of the Administrator.

8.2 Preliminary determinations.

8.2.1 Select the sampling site and the minimum number of sampling points according to Method 1, 40 CFR part 60, appendix A; it is recommended that a leak check of the pitot lines (see section 8.1 of Method 2, 40 CFR part 60, appendix A) be performed. Determine the moisture content using Approximation Method 4 (section 1.2 of Method 4, 40 CFR part 60, appendix A) or its alternatives to make isokinetic sampling rate settings. Determine the stack gas dry molecular weight,
8.2.2 Select a nozzle size based on the range of velocity heads such that it is not necessary to change the nozzle size in order to maintain isokinetic sampling rates. During the run, do not change the nozzle size. Ensure that the proper differential pressure gauge is chosen for the range of velocity heads encountered (see section 8.2 of Method 2, 40 CFR part 60, appendix A).

8.2.3 Select a suitable probe liner and probe length such that all traverse points can be sampled. For large stacks, consider sampling from opposite sides of the stack to reduce the required probe length.

8.2.4 Select a total sampling time greater than or equal to the minimum total sampling time specified in the test procedures for the specific industry such that: (1) The sampling time per point is not less than 2 minutes (or some greater time interval as specified by the Administrator); and (2) the sample volume taken (corrected to standard conditions) will exceed the required minimum total gas sample volume. The latter is based on an approximate average sampling rate.

8.2.5 The sampling time at each point shall be the same. It is recommended that the number of minutes sampled at each point be an integer or an integer plus one-half minute, in order to eliminate timekeeping errors.

8.2.6 In some circumstances (e.g., batch cycles), it may be necessary to sample for shorter times at the traverse points and to obtain smaller gas sample volumes. In these cases, the Administrator's approval must first be obtained.

8.3 Preparation of sampling train.

8.3.1 During preparation and assembly of the sampling train, keep all openings where contamination can occur covered until just prior to assembly or until sampling is about to begin. Place 100 ml of water in each of the first two impingers, leave the third impinger empty, and transfer approximately 200 to 300 g of preweighed silica gel from its container to the fourth impinger. More silica gel may be used, but care should be taken to ensure that it is not entrained and carried out from the impinger during sampling. Place the container in a clean place for later use in the sample recovery. Alternatively, the weight of the silica gel plus impinger may be determined to the nearest 0.5 g and recorded.

8.3.2 Using a tweezer or clean disposable surgical gloves, place a labeled (identified) and weighed filter in the filter holder. Be sure that the filter is properly centered and the gasket properly placed so as to prevent the sample gas stream from circumventing the filter. Check the filter for tears after assembly is completed.

8.3.3 When glass liners are used, install the selected nozzle using a Viton A O-ring when stack temperatures are less than 260°C (500°F) and an asbestos string gasket when temperatures are higher. See APTD-0576 for details. Mark the probe with heat-resistant tape or by some other method to denote the proper distance into the stack or duct for each sampling point.

8.3.4 Set up the train as in Figure 5-1 of Method 5, 40 CFR part 60, appendix A, using (if necessary) a very light coat of silicone grease on all ground glass joints, greasing only the outer portion (see APTD-0576) to avoid possibility of contamination by the silicone grease. Subject to the approval of the Administrator, a glass cyclone may be used between the probe and filter holder when the total particulate catch is expected to exceed 100 mg or when water droplets are present in the stack gas.

8.3.5 Place crushed ice around the impingers.

8.4 Leak-check procedures.

8.4.1 Leak check of metering system shown in Figure 5-1 of Method 5, 40 CFR part 60, appendix A. That portion of the sampling train from the pump to the orifice meter should be leak-checked prior to initial use and after each shipment. Leakage after the pump will result in less volume being recorded than is actually sampled. The following procedure is suggested (see Figure 5-2 of Method 5, 40 CFR part 60, appendix A): Close the main valve on the meter box. Insert a one-hole rubber stopper with rubber tubing attached into the orifice exhaust pipe. Disconnect and vent the low side of the orifice manometer. Close off the low side orifice tap. Pressurize the system to 13 to 18 cm (5 to 7 in.) water column by blowing into the rubber tubing. Pinch off the tubing, and observe the manometer for 1 minute. A loss of pressure on the manometer indicates a leak in the meter box; leaks, if present, must be corrected.

8.4.2 Pretest leak check. A pretest leak check is recommended but not required. If the pretest leak-check is conducted, the following procedure should be used.

8.4.2.1 After the sampling train has been assembled, turn on and set the filter and probe heating systems to the desired operating temperatures. Allow time for the temperatures to stabilize. If a Viton A O-ring or other leak-free connection is used in assembling the probe nozzle to the probe liner, leak-check the train at the sampling site by plugging the nozzle and pulling a 380 mm (15 in.) Hg vacuum.

NOTE: A lower vacuum may be used, provided that it is not exceeded during the test.
8.4.2.2 If an asbestos string is used, do not connect the probe to the train during the leak check. Instead, leak-check the train by first plugging the inlet to the filter holder, and then pulling a 380 mm (15 in.) Hg vacuum. (See NOTE in section 8.4.2.1 of this method). Then connect the probe to the train and perform the leak check at approximately 25 mm (1 in.) Hg vacuum; alternatively, the probe may be leak-checked with the rest of the sampling train, in one step, at 380 mm (15 in.) Hg vacuum. Leakage rates in excess of 4 percent of the average sampling rate or 0.00057 m³/min (0.02 cfm), whichever is less, are unacceptable.

8.4.2.3 The following leak check instructions for the sampling train described in APTD-0576 and APTD-0581 may be helpful. Start the pump with the bypass valve fully open and the coarse adjust valve completely closed. Partially open the coarse adjust valve and slowly close the bypass valve until the desired vacuum is reached. Do not reverse the direction of the bypass valve, as this will cause water to back up into the filter holder. If the desired vacuum is exceeded, either leak-check this higher vacuum or end the leak check as shown below and start over.

8.4.2.4 When the leak check is completed, first slowly remove the plug from the inlet to the probe, filter holder, or cyclone (if applicable) and immediately turn off the vacuum pump. This prevents the water in the impingers from being forced backward into the filter holder and the silica gel from being entrained backward into the third impinger.

8.4.3 Leak checks during sample run. If, during the sampling run, a component (e.g., filter assembly or impinger) change becomes necessary, a leak check shall be conducted immediately before the change is made. The leak check shall be done according to the procedure outlined in section 8.4.2 of this method, except that it shall be done at a vacuum equal to or greater than the maximum value recorded up to that point in the test. If the leakage rate is found to be no greater than 0.00057 m³/min (0.02 cfm) or 4 percent of the average sampling rate ( whichever is less), the results are acceptable, and no correction need be applied to the total volume of dry gas metered. If, however, a higher leakage rate is obtained, either record the leakage rate and correct the sample volume, as shown in section 12.4 of this method, or void the sampling run.

8.5 Sampling train operation. During the sampling run, maintain an isokinetic sampling rate (within 10 percent of true isokinetic unless otherwise specified by the Administrator) and a temperature around the filter of 120°F (248°F), or such other temperature as specified by an applicable subpart of the standards or approved by the Administrator.

8.5.1 For each run, record the data required on a data sheet such as the one shown in Figure 5-2 of Method 5, 40 CFR part 60, appendix A. Be sure to record the initial reading. Record the DGM readings at the beginning and end of each sampling time increment, when changes in flow rates are made, before and after each leak-check, and when sampling is halted. Take other readings indicated by Figure 5-2 of Method 5, 40 CFR part 60, appendix A at least once at each sample point during each time increment and additional readings when significant changes (10 percent variation in velocity head readings) necessitate additional adjustments in flow rate. Level and zero the manometer. Because the manometer level and zero may drift due to vibrations and temperature changes, make periodic checks during the traverse.

8.5.2 Clean the portholes prior to the test run to minimize the chance of sampling deposited material. To begin sampling, remove the nozzle cap and verify that the filter and probe heating systems are up to temperature and that the pitot tube and probe are properly positioned. Position the nozzle at the first traverse point with the tip pointing directly into the gas stream. Immediately start the pump and adjust the flow to isokinetic conditions. Nomographs are available, which aid in the rapid adjustment of the isokinetic sampling rate without excessive computations. These nomographs are designed for use when the Type S pitot tube coefficient (Cp) is 0.85 ± 0.02 and the stack gas equivalent density (dry molecular weight) is 29 ± 4. APTD-0576 details the procedure for using the nomographs. If Cp and Ms are outside the above-stated ranges, do not use the nomographs unless appropriate steps (see Reference 7 in section 17.0 of this method) are taken to compensate for the deviations.

8.5.3 When the stack is under significant negative pressure (height of impinger stem), close the coarse adjust valve before inserting...
8.5.4 When the probe is in position, block off the openings around the probe and port-hole to prevent unrepresentative dilution of the gas stream.

8.5.5 Traverse the stack cross-section, as required by Method 1, 40 CFR part 60, appendix A or as specified by the Administrator, being careful not to bump the probe nozzle into the stack walls when sampling near the walls or when removing or inserting the probe through the port-holes; this minimizes the chance of extracting deposited material.

8.5.6 During the test run, make periodic adjustments to keep the temperature around the filter holder at the proper level; add more ice and, if necessary, salt to maintain a temperature of less than 20°C (68°F) at the condenser/silica gel outlet. Also, periodically check the level and zero of the manometer.

8.5.7 If the pressure drop across the filter becomes too high, making isokinetic sampling difficult to maintain, the filter may be replaced in the midst of the sample run. It is recommended that another complete filter assembly be used rather than attempting to change the filter itself. Before a new filter assembly is installed, conduct a leak check (see section 8.4.3 of this method). The total PM weight shall include the summation of the filter assembly catches.

8.5.8 A single train shall be used for the entire sample run, except in cases where simultaneous sampling is required in two or more separate ducts or at two or more different locations within the same duct, or in cases where equipment failure necessitates a change of trains. In all other situations, the use of two or more trains will be subject to the approval of the Administrator.

Note: When two or more trains are used, separate analyses of the front-half and (if applicable) impinger catches from each train shall be performed, unless identical nozzle sizes were used in all trains, in which case the front-half catches from the individual trains may be combined (as may the impinger catches) and one analysis of the front-half catch and one analysis of the impinger catch may be performed.

8.5.9 At the end of the sample run, turn off the coarse adjust valve, remove the probe and nozzle from the stack, turn off the pump, record the final DGM reading, and then conduct a post-test leak check, as outlined in section 8.4.4 of this method. Also leak-check the pitot lines as described in section 8.1 of Method 2, 40 CFR part 60, appendix A. The lines must pass this leak check in order to validate the velocity head data.

8.6 Calculation of percent isokinetic. Calculate percent isokinetic (see Calculations, section 12.12 of this method) to determine whether a run was valid or another test run should be made. If there was difficulty in maintaining isokinetic rates because of source conditions, consult the Administrator for possible variance on the isokinetic rates.

8.7 Sample recovery.

8.7.1 Proper cleanup procedure begins as soon as the probe is removed from the stack at the end of the sampling period. Allow the probe to cool.

8.7.2 When the probe can be safely handled, wipe off all external PM near the tip of the probe nozzle and place a cap over it to prevent losing or gaining PM. Do not cap off the probe tip tightly while the sampling train is cooling down. This would create a vacuum in the filter holder, thus drawing water from the impingers into the filter holder.

8.7.3 Before moving the sample train to the cleanup site, remove the probe from the sample train, wipe off the silicone grease, and cap the open outlet of the probe. Be careful not to lose any condensate that might be present. Wipe off the silicone grease from the filter inlet where the probe was fastened and cap it. Remove the umbilical cord from the last impinger and cap the impinger. If a flexible line is used between the first impinger or condenser and the filter holder, disconnect the line at the filter holder and let any condensed water or liquid drain into the impingers or condenser. After wiping off the silicone grease, cap off the filter holder outlet and impinger inlet. Ground-glass stoppers, plastic caps, or serum caps may be used to close these openings.

8.7.4 Transfer the probe and filter-impinger assembly to the cleanup area. This area should be clean and protected from the wind so that the chances of contaminating or losing the sample will be minimized.

8.7.5 Save a portion of the acetone and methylene chloride used for cleanup as blanks. Take 200 ml of each solvent directly from the wash bottle being used and place it in glass sample containers labeled “acetone blank” and “methylene chloride blank,” respectively.

8.7.6 Inspect the train prior to and during disassembly and note any abnormal conditions. Treat the samples as follows:

8.7.6.1 Container No. 1. Carefully remove the filter from the filter holder, and place it in its identified petri dish container. Use a pair of tweezers and/or clean disposable surgical gloves to handle the filter. If it is necessary to fold the filter, do so such that the PM cake is inside the fold. Using a dry nylon bristle brush and/or a sharp-edged blade, carefully transfer to the petri dish any PM and/or filter fibers that adhere to the filter holder gasket. Seal the container.

8.7.6.2 Container No. 2. Taking care to see that dust on the outside of the probe or other...
chloride washings and PM have been collected in the proper sample containers, tighten the lid on the sample containers so that acetone and methylene chloride will not leak out when it is shipped to the laboratory. Mark the height of the fluid level to determine whether leakage occurs during transport. Label each container to identify clearly its contents.

8.7.6.3 Container No. 3. Note the color of the indicating silica gel to determine whether it has been completely spent, and make a notation of its condition. Transfer the silica gel from the fourth impinger to its original container and seal the container. A funnel may make it easier to pour the silica gel without spilling. A rubber policeman may be used as an aid in removing the silica gel from the impinger. It is not necessary to remove the small amount of dust particles that may adhere to the impinger wall and are difficult to remove. Since the gain in weight is to be used for moisture calculations, do not use any water or other liquids to transfer the silica gel. If a balance is available in the field, follow the procedure for Container No. 3 in section 11.2.3 of this method.

8.7.6.4 Impinger water. Treat the impingers as follows:

8.7.6.4.1 Make a notation of any color or film in the liquid catch. Measure the liquid that is in the first three impingers to within 1 ml by using a graduated cylinder or by weighing it to within 0.5 g by using a balance (if one is available). Record the volume or weight of liquid present. This information is required to calculate the moisture content of the effluent gas.

8.7.6.4.2 Following the determination of the volume of liquid present, rinse the back half of the train with water, add it to the impinger catch, and store it in a container labeled 3W (water).

8.7.6.4.3 Following the water rinse, rinse the back half of the train with acetone to remove the excess water to enhance subsequent organic recovery with methylene chloride. Quantitatively recover to a container labeled 3S (solvent) followed by at least three sequential rinsings with aliquots of methylene chloride. Quantitatively recover to the same container labeled 3S. Record separately the amount of both acetone and methylene chloride used to the nearest 1 ml or 0.5 g.

Note: Because the subsequent analytical finish is gravimetric, it is okay to recover both solvents to the same container. This would not be recommended if other analytical finishes were required.

8.8 Sample transport. Whenever possible, containers should be shipped in such a way that they remain upright at all times.
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9.0 Quality Control.

9.1 Miscellaneous quality control measures.

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9.2 Volume metering system checks. The following quality control procedures are suggested to check the volume metering system calibration values at the field test site prior to sample collection. These procedures are optional.

9.2.1 Meter orifice check. Using the calibration data obtained during the calibration procedure described in section 10.3 of this method, determine the \( \Delta H \) for the metering system orifice. The \( \Delta H \) is the orifice pressure differential in units of in. Hg that correlates to 0.75 cfm of air at 528°R and 29.92 in. Hg. The \( \Delta H \) is calculated as follows:

\[
\Delta H_a = 0.0319 \Delta H - \frac{T_m \Theta^2}{P_{bar} Y^2 V_m^2}
\]

Where

\[
0.0319 = \frac{(0.0567 \text{ in. Hg/°R})(0.75 \text{ cfm})^2}{10}
\]

\( \Delta H \) = Average pressure differential across the orifice meter, in. Hg; 
\( T_m \) = Absolute average DGM temperature, °R; 
\( \Theta \) = Total sampling time, min; 
\( P_{bar} \) = Barometric pressure, in. Hg; 
\( Y \) = DGM calibration factor, dimensionless; 
\( V_m \) = Volume of gas sample as measured by DGM, dcf.

9.2.1.1 Before beginning the field test (a set of three runs usually constitutes a field test), operate the metering system (i.e., pump, volume meter, and orifice) at the \( \Delta H \) pressure differential for 10 minutes. Record the volume collected, the DGM temperature, and the barometric pressure. Calculate a DGM calibration check value, \( Y_c \), as follows:

\[
Y_c = \frac{10}{V_m} \left[ \frac{0.0319 T_m^2}{P_{bar} Y^2 V_m^2} \right]
\]

Where

\( Y_c \) = DGM calibration check value, dimensionless; 
10 = Run time, min.

9.2.1.2 Compare the \( Y_c \) value with the dry gas meter calibration factor \( Y \) to determine that: 0.97 \( Y \) \( < \) \( Y_c \) \( < \) 1.03 \( Y \). If the \( Y_c \) value is not within this range, the volume metering system should be investigated before beginning the test.

9.2.2 Calibrated critical orifice. A calibrated critical orifice, calibrated against a wet test meter or spirometer and designed to be inserted at the inital of the sampling meter box, may be used as a quality control check by following the procedure of section 16.2 of this method.

10.0 Calibration and Standardization.

NOTE: Maintain a laboratory log of all calibrations.

10.1 Probe nozzle. Probe nozzles shall be calibrated before their initial use in the field. Using a micrometer, measure the ID of the nozzle to the nearest 0.025 mm (0.001 in.). Make three separate measurements using different diameters each time, and obtain the average of the measurements. The difference between the high and low numbers shall not exceed 0.1 mm (0.004 in.). When nozzles become nicked, dented, or corroded, they shall be reshaped, sharpened, and recalibrated before use. Each nozzle shall be permanently and uniquely identified.

10.2 Pitot tube assembly. The Type S pitot tube assembly shall be calibrated according to the procedure outlined in section 10.1 of Method 2, 40 CFR part 60, appendix A.

10.3 Metering system. 10.3.1 Calibration prior to use. Before its initial use in the field, the metering system shall be calibrated as follows: Connect the metering system inlet to the outlet of a wet test meter that is accurate to within 1 percent. Refer to Figure 5-5 of Method 5, 40 CFR part 60, appendix A. The wet test meter should have a capacity of 30 liters/revolution (1 ft³/rev). A spirometer of 400 liters (14 ft³) or more capacity, or equivalent, may be used for this calibration, although a wet test meter is usually more practical. The wet test meter should be periodically calibrated with a spirometer or a liquid displacement meter to ensure the accuracy of the wet test meter. Spirometers or wet test meters of other sizes may be used, provided that the specified accuracies of the procedure are maintained. Run the metering system pump for about 15 minutes with the orifice manometer indicating a median reading, as expected in field use, to allow the pump to warm up and to
permit the interior surface of the wet test meter to be thoroughly wetted. Then, at each of a minimum of three orifice manometer settings, pass an exact quantity of gas through the wet test meter and note the gas volume indicated by the DGM. Also note the barometric pressure and the temperatures of the wet test meter, the inlet of the DGM, and the outlet of the DGM. Select the highest and lowest orifice settings to bracket the expected field operating range of the orifice. Use a minimum volume of 0.15 m³ (5 cf) at all orifice settings. Record all the data on a form similar to Figure 5-6 of Method 5, 40 CFR part 60, appendix A, and calculate Y (the DGM calibration factor) and ΔH, (the orifice calibration factor) at each orifice setting, as shown on Figure 5-6 of Method 5, 40 CFR part 60, appendix A. Allowable tolerances for individual Y and ΔH, values are given in Figure 5-6 of Method 5, 40 CFR part 60, appendix A. Use the average of the Y values in the calculations in section 12 of this method.

10.3.1.1 Before calibrating the metering system, it is suggested that a leak check be conducted. For metering systems having diaphragm pumps, the normal leak check procedure will not detect leakages within the pump. For these cases the following leak check procedure is suggested: make a 10-minute calibration run at 0.00057 m³/min (0.02 cfm); at the end of the run, take the difference of the measured wet test meter and DGM volumes; divide the difference by 10 to get the leak rate. The leak rate should not exceed 0.00057 m³/min (0.02 cfm).

10.3.2 Calibration after use. After each field use, the calibration of the metering system shall be checked by performing three calibration runs at a single, intermediate orifice setting (based on the previous field test) with the vacuum set at the maximum value reached during the test series. To adjust the vacuum, insert a valve between the wet test meter and the inlet of the metering system. Calculate the average value of the DGM calibration factor. If the value has changed by more than 5 percent, recalibrate the meter over the full range of orifice settings, as previously detailed.

NOTE: Alternative procedures, e.g., rechecking the orifice meter coefficient, may be used, subject to the approval of the Administrator.

10.3.3 Acceptable variation in calibration. If the DGM coefficient values obtained before and after a test series differ by more than 5 percent, either the test series shall be voided or calculations for the test series shall be performed using whichever meter coefficient value (i.e., before or after) gives the lower value of total sample volume.

10.4 Probe heater calibration. Use a heat source to generate air heated to selected temperatures that approximate those expected to occur in the sources to be sampled. Pass this air through the probe at a typical sample flow rate while measuring the probe inlet and outlet temperatures at various probe heater settings. For each air temperature generated, construct a graph of probe heating system setting versus probe outlet temperature. The procedure outlined in APTD-0576 can also be used. Probes constructed according to APTD-0581 need not be calibrated if the calibration curves in APTD-0576 are used. Also, probes with outlet temperature monitoring capabilities do not require calibration.

NOTE: The probe heating system shall be calibrated before its initial use in the field.

10.5 Temperature sensors. Use the procedure in section 10.3 of Method 2, 40 CFR part 60, appendix A to calibrate in-stack temperature sensors. Dial thermometers, such as are used for the DGM and condenser outlet, shall be calibrated against mercury-in-glass thermometers.

10.6 Barometer. Calibrate against a mercury barometer.

11.0 Analytical Procedure.

11.1 Record the data required on a sheet such as the one shown in Figure 315-1 of this method.

11.2 Handle each sample container as follows:

11.2.1 Container No. 1.

11.2.1.1 PM analysis. Leave the contents in the shipping container or transfer the filter and any loose PM from the sample container to a tared glass weighing dish. Desiccate for 24 hours in a desiccator containing anhydrous calcium sulfate. Weigh to a constant weight and report the results to the nearest 0.1 mg. For purposes of this section, the term “constant weight” means a difference of no more than 0.5 mg or 1 percent of total weight less tare weight, whichever is greater, between two consecutive weighings, with no less than 6 hours of desiccation time between weighings (overnight desiccation is a common practice). If a third weighing is required and it agrees within ±0.5 mg, then the results of the second weighing should be used. For quality assurance purposes, record and report each individual weighing; if more than three weighings are required, note this in the results for the subsequent MCEM results.

11.2.1.2 MCEM analysis. Transfer the filter and contents quantitatively into a beaker. Add 100 ml of methylene chloride and cover with aluminum foil. Sonicate for 3 minutes then allow to stand for 20 minutes. Set up the filtration apparatus. Decant the solution into a clean Buchner fritted funnel. Immediately pressure filter the solution through the tube into another clean, dry beaker. Continue decanting and pressure filtration until all the solvent is transferred.
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Rinse the beaker and filter with 10 to 20 ml methylene chloride, decant into the Buchner fritted funnel and pressure filter. Place the beaker on a low-temperature hot plate (maximum 40°C) and slowly evaporate almost to dryness. Transfer the remaining few milliliters of solution quantitatively from the beaker (using at least three aliquots of methylene chloride rinses) to a tared clean dry aluminum dish and evaporate to complete dryness. Remove from heat once solvent is evaporated. Reweigh the dish after a 30-minute equilibrium in the balance room and determine the weight to the nearest 0.1 mg. Conduct a methylene chloride blank run in an identical fashion.

11.2.2 Container No. 2.

11.2.2.1 PM analysis. Note the level of liquid in the container, and confirm on the analysis sheet whether leakage occurred during transport. If a noticeable amount of leakage has occurred, either void the sample or use methods, subject to the approval of the Administrator, to correct the final results. Measure the liquid in this container either volumetrically to ±1 ml or gravimetrically to ±0.5 g. Transfer the contents to a tared 250 ml beaker and evaporate to dryness at ambient temperature and pressure. Desiccate for 24 hours, and weigh to a constant weight. Report the results to the nearest 0.1 mg.

11.2.2.2 MCEM analysis. Add 25 ml methylene chloride to the beaker and cover with aluminum foil. Sonicate for 3 minutes then allow to stand for 20 minutes; combine with contents of Container No. 2M and pressure filter and evaporate as described for Container 1 in section 11.2.1.2 of this method.

Notes for MCEM Analysis

1. Light finger pressure only is necessary on 24/40 adaptor. A Chemplast adapter (15055-240 has been found satisfactory.

2. Avoid aluminum dishes made with fluted sides, as these may promote solvent “creep,” resulting in possible sample loss.

3. If multiple samples are being run, rinse the Buchner fritted funnel twice between samples with 5 ml solvent using pressure filtration. After the second rinse, continue the flow of air until the glass frit is completely dry. Clean the Buchner fritted funnels thoroughly after filtering five or six samples.

11.2.3 Container No. 3. Weigh the spent silica gel (or silica gel plus impinger) to the nearest 0.5 g using a balance. This step may be conducted in the field.

11.2.4 Container 3W (impinger water).

11.2.4.1 MCEM analysis. Transfer the solution into a 1,000 ml separatory funnel quantitatively with methylene chloride washes. Add enough solvent to total approximately 50 ml, if necessary. Shake the funnel for 1 minute, allow the phases to separate, and drain the solvent layer into a 250 ml beaker.

Repeat the extraction twice. Evaporate with low heat (less than 40°C) until near dryness. Transfer the remaining few milliliters of solvent quantitatively with small solvent washes into a clean, dry, tared aluminum dish and evaporate to dryness. Remove from heat once solvent is evaporated. Reweigh the dish after a 30-minute equilibration in the balance room and determine the weight to the nearest 0.1 mg.

11.2.5 Container 3S (solvent).

11.2.5.1 MCEM analysis. Transfer the mixed solvent to 250 ml beaker(s). Evaporate and weigh following the procedures detailed for container 3W in section 11.2.4 of this method.

11.2.6 Blank containers. Measure the distilled water, acetone, or methylene chloride in each container either volumetrically or gravimetrically. Transfer the “solvent” to a tared 250 ml beaker, and evaporate to dryness at ambient temperature and pressure. (Conduct a solvent blank on the distilled demineralized water blank in an identical fashion to that described in section 11.2.4.4 of this method.) Desiccate for 24 hours, and weigh to a constant weight. Report the results to the nearest 0.1 mg.

NOTE: The contents of Containers No. 2, 3W, and 3M as well as the blank containers may be evaporated at temperatures higher than ambient. If evaporation is done at an elevated temperature, the temperature must be below the boiling point of the solvent; also, to prevent “bumping,” the evaporation process must be closely supervised, and the contents of the beaker must be swirled occasionally to maintain an even temperature. Use extreme care, as acetone and methylene chloride are highly flammable and have a low flash point.

12.0 Data Analysis and Calculations.

12.1 Carry out calculations, retaining at least one extra decimal figure beyond that of the acquired data. Round off figures after the final calculation. Other forms of the equations may be used as long as they give equivalent results.

12.2 Nomenclature.

A = Cross-sectional area of nozzle, m² (ft²).

B = Water vapor in the gas stream, proportion by volume.

C = Acetone blank residue concentration, mg/g.

Cₚ = Concentration of particulate matter in stack gas, dry basis, corrected to standard conditions, g/dscm (g/scf).

I = Percent of isokinetic sampling.

Lₐ = Maximum acceptable leakage rate for either a pretest leak check or for a leak check following a component change; equal to 0.00057 m³/min (0.02 cfm) or 4 percent of the average sampling rate, whichever is less.
L_i = Individual leakage rate observed during the leak check conducted prior to the ‘‘i-th’’ component change (i = 1, 2, 3...n), m^3/min (cfm).

L_p = Leakage rate observed during the post-test leak check, m^3/min (cfm).

m_r = Mass of residue of acetone after evaporation, mg.

m_a = Total amount of particulate matter collected, mg.

M_w = Molecular weight of water, 18.0 g/g-mole.

M_c = Total volume liquid collected in impingers and silica gel (see Figure 5-2 of Method 5, 40 CFR part 60, appendix A), ml.

V = Volume of gas sample as measured by the dry gas meter, dcm (dcf).

V_b = Volume of acetone blank, ml.

V_c = Volume of acetone used in wash, ml.

V_w = Volume of methylene chloride blank, ml.

V_ea = Volume of acenone used in wash, ml.

V_m = Volume of methylene chloride used in wash, ml.

V_l = Total volume liquid collected in impingers and silica gel (see Figure 5-2 of Method 5, 40 CFR part 60, appendix A), ml.

V_n = Volume of gas sample as measured by the dry gas meter, corrected to standard conditions, dscm (dcf).

V_wd = Volume of water vapor in the gas sample, corrected to standard conditions, scm (scf).

V_s = Stack gas velocity, calculated by Equation 2-9 in Method 2, 40 CFR part 60, appendix A, using data obtained from Method 5, 40 CFR part 60, appendix A, m/sec (ft/sec).

W_r = Weight of residue in acetone wash, mg.

Y = Dry gas meter calibration factor.

\[ \Delta H = \text{Average pressure differential across the orifice meter (see Figure 5-2 of Method 5, 40 CFR part 60, appendix A), mm H}_2\text{O (in H}_2\text{O).} \]

\[ \rho_a = \text{Density of acetone, 785.1 mg/ml (or see label on bottle).} \]

\[ \rho_w = \text{Density of water, 0.9982 g/ml (0.00220 lb/ml).} \]

\[ \rho_c = \text{Density of methylene chloride, 1316.8 mg/ml (or see label on bottle).} \]

\[ \Theta = \text{Total sampling time, min.} \]

\[ \Theta_1 = \text{Sampling time interval, from the beginning of a run until the first component change.} \]

\[ \Theta_2 = \text{Sampling time interval, between two successive component changes, beginning with the interval between the first and second changes, min.} \]

\[ \Theta_3 = \text{Sampling time interval, from the final (n-th) component change until the end of the sampling run, min.} \]

1.36 = Specific gravity of mercury.

60 = Sec/min.

100 = Conversion to percent.

12.3 Average dry gas meter temperature and average orifice pressure drop. See data sheet (Figure 5-2 of Method 5, 40 CFR part 60, appendix A).

12.4 Dry gas volume. Correct the sample volume measured by the dry gas meter to standard conditions (20°C, 760 mm Hg or 68°F, 29.92 in Hg) by using Equation 315-1.

\[ V = V_m \frac{T_{\text{std}}}{T_m} \left( \frac{P_{\text{bar}} + \frac{\Delta H}{13.6}}{P_{\text{std}}} \right) = V = K_1 V_m \frac{P_{\text{bar}} + \frac{\Delta H}{13.6}}{T_m} \]

\text{Eq. 315-1}

Where

\[ K_1 = 0.3858 \text{ K/mm Hg for metric units,} \]

\[ = 17.64 \text{ R/in Hg for English units.} \]

\text{Note: Equation 315-1 can be used as written unless the leakage rate observed during any of the mandatory leak checks (i.e., the post-test leak check or leak checks conducted prior to component changes) exceeds L_i. If L_i or L_p exceeds L_r, Equation 315-1 must be modified as follows:}

\[ V_{\text{wad}} = \begin{cases} V_m & \text{if} \ L_i \leq L_r, \\ V_m - (L_i - L_r) \Theta & \text{if} \ L_i > L_r \end{cases} \]

(a) Case I. No component changes made during sampling run. In this case, replace \( V_{\text{wad}} \) in Equation 315-1 with the expression:

\[ \left[ V_{\text{wad}} - (L_i - L_r) \Theta \right] \]

(b) Case II. One or more component changes made during the sampling run. In this case, replace \( V_{\text{wad}} \) in Equation 315-1 by the expression:
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\[
\left[ V_m - (L_1 - L_a) \Theta_1 - \sum_{i=2}^{n} (L_i - L_a) \Theta_i - (L_p - L_a) \Theta_p \right]
\]

and substitute only for those leakage rates \((L_i \text{ or } L_p)\) which exceed \(L_a\).

12.5 Volume of water vapor condensed.

\[
V_{w(\text{std})} = V_{i} \frac{\rho_w RT_{\text{std}}}{M_w p_{\text{std}}} = K_2 V_{i} \quad \text{Eq. 315-2}
\]

Where

\[
K_2 = 0.001333 \text{ m}^3/\text{ml} \quad \text{for metric units;}
= 0.04706 \text{ ft}^3/\text{ml} \quad \text{for English units.}
\]

12.6 Moisture content.

\[
B_{ws} = \frac{V_{w(\text{std})}}{V_{m(\text{std})} + V_{w(\text{std})}} \quad \text{Eq. 315-3}
\]

**NOTE:** In saturated or water droplet-laden gas streams, two calculations of the moisture content of the stack gas shall be made, one from the impinger analysis (Equation 315-3), and a second from the assumption of saturated conditions. The lower of the two values of \(B_{ws}\) shall be considered correct. The procedure for determining the moisture content based upon assumption of saturated conditions is given in section 4.0 of Method 4, 40 CFR part 60, appendix A. For the purposes of this method, the average stack gas temperature from Figure 5-2 of Method 5, 40 CFR part 60, appendix A may be used to make this determination, provided that the accuracy of the in-stack temperature sensor is \(\pm 1^\circ C\) (\(\pm 2^\circ F\)).

12.7 Acetone blank concentration.

\[
C_a = \frac{M_a}{V_a \rho_a} \quad \text{Eq. 315-4}
\]

12.8 Acetone wash blank.

\[
W_a = C_a V_{aw} \rho_a \quad \text{Eq. 315-5}
\]

12.9 Total particulate weight. Determine the total PM catch from the sum of the weights obtained from Containers I and 2 less the acetone blank associated with these two containers (see Figure 315-3).

**NOTE:** Refer to section 8.5.8 of this method to assist in calculation of results involving two or more filter assemblies or two or more sampling trains.

12.10 Particulate concentration.

\[
c_s = \frac{K_3 m}{V_{\text{m(}\text{std})}} \quad \text{Eq. 315-6}
\]

where

\[
K = 0.001 \text{ g/mg} \quad \text{for metric units;}
= 0.0154 \text{ gr/mg} \quad \text{for English units.}
\]

12.11 Conversion factors.

<table>
<thead>
<tr>
<th>From</th>
<th>To</th>
<th>Multiply by</th>
</tr>
</thead>
<tbody>
<tr>
<td>ft$^3$</td>
<td>m$^3$</td>
<td>0.02832</td>
</tr>
<tr>
<td>gr</td>
<td>mg</td>
<td>64.80004</td>
</tr>
<tr>
<td>gr/ft$^3$</td>
<td>mg/m$^3$</td>
<td>2288.4</td>
</tr>
<tr>
<td>mg</td>
<td>g</td>
<td>0.001</td>
</tr>
<tr>
<td>gr</td>
<td>lb</td>
<td>1.429×10$^{-4}$</td>
</tr>
</tbody>
</table>

12.12 Isokinetic variation.

12.12.1 Calculation from raw data.

\[
I = \frac{100T_s}{60} \left[ K_4 V_{i} \left( \frac{V_{\text{m}} Y_{s}}{T_m} \right) \left( P_{\text{bar}} + \frac{\Delta H}{13.6} \right) \right] \quad \text{Eq. 315-7}
\]

where

\[
K_4 = 0.003454 \quad \text{[mm Hg/(m$^3$)]/[m$^3$/(°K)]} \quad \text{for metric units;}
= 0.002669 \quad \text{[(in Hg)/(ft$^3$)]/[m$^3$/(°R)]} \quad \text{for English units.}
\]

12.12.2 Calculation from intermediate values.

597
where

\[ K_1 = 4.320 \text{ for metric units; } \]
\[ = 0.09450 \text{ for English units.} \]

12.12.3 Acceptable results. If 90 percent \( \leq I \leq 110 \) percent, the results are acceptable. If the PM or MCEM results are low in comparison to the standard, and “I” is over 110 percent or less than 90 percent, the Administrator may opt to accept the results. Reference 4 in the Bibliography may be used to make acceptability judgments. If “I” is judged to be unacceptable, reject the results, and repeat the test.

12.13 Stack gas velocity and volumetric flow rate. Calculate the average stack gas velocity and volumetric flow rate, if needed, using data obtained in this method and the equations in sections 5.2 and 5.3 of Method 2, 40 CFR part 60, appendix A.

12.14 MCEM results. Determine the MCEM concentration from the results from Containers 1, 2, 2M, 3W, and 3S less the acetone, methylene chloride, and filter blanks value as determined in the following equation:

\[ m_{mecm} = S \frac{V_w}{t_w} \cdot w_{ds} \cdot f_b \]

13.0 Method Performance. [Reserved]

14.0 Pollution Prevention. [Reserved]

15.0 Waste Management. [Reserved]

16.0 Alternative Procedures.

16.1 Dry gas meter as a calibration standard. A DGM may be used as a calibration standard for volume measurements in place of the wet test meter specified in section 16.1 of this method, provided that it is calibrated initially and recalibrated periodically as follows:

16.1.1 Standard dry gas meter calibration.

16.1.1.1 The DGM to be calibrated and used as a secondary reference meter should be of high quality and have an appropriately sized capacity, e.g., 3 liters/rev (0.1 ft ²/rev). A spirometer (400 liters or more capacity), or equivalent, may be used for this calibration, although a wet test meter is usually more practical. The wet test meter should have a capacity of 30 liters/rev (1 ft ²/rev) and be capable of measuring volume to within 1.0 percent; wet test meters should be checked against a spirometer or a liquid displacement meter to ensure the accuracy of the wet test meter. Spirometers or wet test meters of other sizes may be used, provided that the specified accuracies of the procedure are maintained.

16.1.1.2 Set up the components as shown in Figure 5-7 of Method 5, 40 CFR part 60, appendix A. A spirometer, or equivalent, may be used in place of the wet test meter in the system. Run the pump for at least 5 minutes at a flow rate of about 10 liters/min (0.35 cfm) to condition the interior surface of the wet test meter. The pressure drop indicated by the manometer at the inlet side of the DGM should be minimized (no greater than 100 mm H₂O [4 in. H₂O] at a flow rate of 30 liters/min [1 cfm]). This can be accomplished by using large-diameter tubing connections and straight pipe fittings.

16.1.1.3 Collect the data as shown in the example data sheet (see Figure 5-8 of Method 5, 40 CFR part 60, appendix A). Make tripslicate runs at each of the flow rates and at no less than five different flow rates. The range of flow rates should be between 10 and 34 liters/min (0.35 and 1.2 cfm) or over the expected operating range.

16.1.1.4 Calculate flow rate, \( Q \), for each run using the wet test meter volume, \( V_w \), and the run time, \( q \). Calculate the DGM coefficient, \( Y_{ds} \), for each run. These calculations are as follows:

\[ Q = K_1 \frac{P_{bar} V_w}{(t_w + t_{std})} \]

\[ Y_{ds} = \frac{V_w (T_{ds} + T_{std}) P_{bar}}{V_{ds} (T_w + T_{std}) (P_{bar} + \frac{\Delta p}{13.6})} \]
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\[ t_{n.t} = 273°C \text{ for SI units; } 460°F \text{ for English units; } \]
\[ \theta = \text{Run time, min; } \]
\[ t_{a.} = \text{Average dry gas meter temperature, °C (°F); } \]
\[ V_{m} = \text{Dry gas meter volume, liter (ft³); } \]
\[ \Delta p = \text{Dry gas meter inlet differential pressure, mm H}_{2}O \text{ (in H}_{2}O). \]

16.1.1.5 Compare the three \( Y_{o.a} \) values at each of the flow rates and determine the maximum and minimum values. The difference between the maximum and minimum values at each flow rate should be no greater than 0.030. Extra sets of triplicate runs may be made in order to complete this requirement. In addition, the meter coefficients specified in section 16.2 and 1.05 if these specifications cannot be met in three sets of successive triplicate runs, the meter is not suitable as a calibration standard and should not be used as such. If these specifications are met, average the three \( Y_{o.a} \) values at each flow rate resulting in five average meter coefficients, \( Y_{o.a.} \).

16.1.1.6 Prepare a curve of meter coefficient, \( Y_{o.a.} \) versus flow rate, \( Q \), for the DGM. This curve shall be used as a reference when the meter is used to calibrate other DGMs and to determine whether recalibration is required.

16.1.2 Standard dry gas meter recalibration.

16.1.2.1 Recalibrate the standard DGM against a wet test meter or spirometer annually or after every 200 hours of operation, whichever comes first. This requirement is valid provided the standard DGM is kept in a laboratory and, if transported, cared for as any other laboratory instrument. Abuse to the standard meter may cause a change in the calibration and will require more frequent recalibrations.

16.1.2.2 As an alternative to full recalibration, a two-point calibration check may be made. Follow the same procedure and equipment arrangement as for a full recalibration, but run the meter at only two flow rates (suggested rates are 14 and 28 liters/min [0.5 and 1.0 cfm]). Calculate the meter coefficients for these two points, and compare the values with the meter calibration curve. If the two coefficients are within 1.5 percent of the calibration curve values at the same flow rates, the meter need not be recalibrated until the next date for a recalibration check.

6.2 Critical orifices as calibration standards. Critical orifices may be used as calibration standards in place of the wet test meter specified in section 10.3 of this method, provided that they are selected, calibrated, and used as follows:

16.2.1 Selection of critical orifices.

16.2.1.1 Before calibrating the meter box, leak-check the system as follows: Fully open the coarse adjust valve and completely close the bypass valve. Plug the inlet. Then turn on the pump and determine whether there is any leakage. The leakage rate shall be zero; i.e., no detectable movement of the DGM dial shall be seen for 1 minute.

16.2.1.2 Check also for leaks in that portion of the sampling train between the pump and the orifice meter. See section 5.6 of Method 5, 40 CFR part 60, appendix A for the procedure; make any corrections, if necessary. If leakage is detected, check for cracked gaskets, loose fittings, worn O-rings, etc. and make the necessary repairs.

16.2.1.3 After determining that the meter box is leakless, calibrate the meter box according to the procedure given in section 5.3 of Method 5, 40 CFR part 60, appendix A. Make sure that the wet test meter meets the requirements stated in section 7.1.11 of Method 5, 40 CFR part 60, appendix A. Check the water level in the wet test meter. Record the DGM calibration factor, \( Y_{o.a.} \).

16.2.2 Critical orifice calibration. The procedure described in this section uses the Method 5 meter box configuration with a DGM as described in section 6.1.19 of this method to calibrate the critical orifices. Other schemes may be used, subject to the approval of the Administrator.

16.2.2.1 Calibration of meter box. The critical orifices must be calibrated in the same configuration as they will be used; i.e., there should be no connections to the inlet of the orifice.

16.2.2.1.1 Before calibrating the meter box, leak-check the system as follows: Fully open the coarse adjust valve and completely close the bypass valve. Plug the inlet. Then turn on the pump and determine whether there is any leakage. The leakage rate shall be zero; i.e., no detectable movement of the DGM dial shall be seen for 1 minute.

16.2.2.1.2 Check also for leaks in that portion of the sampling train between the pump and the orifice meter. See section 5.6 of Method 5, 40 CFR part 60, appendix A for the procedure; make any corrections, if necessary. If leakage is detected, check for cracked gaskets, loose fittings, worn O-rings, etc. and make the necessary repairs.

16.2.2.1.3 After determining that the meter box is leakless, calibrate the meter box according to the procedure given in section 5.3 of Method 5, 40 CFR part 60, appendix A. Make sure that the wet test meter meets the requirements stated in section 7.1.11 of Method 5, 40 CFR part 60, appendix A. Check the water level in the wet test meter. Record the DGM calibration factor, \( Y_{o.a.} \).

16.2.2.2 Calibration of critical orifices. Set up the apparatus as shown in Figure 5-10 of Method 5, 40 CFR part 60, appendix A.
the temperature conditions through the DGM.

16.2.2.2.2 Leak-check the system as in section 7.2.2.1.1 of Method 5, 40 CFR part 60, appendix A. The leakage rate shall be zero.

16.2.2.2.3 Before calibrating the critical orifice, determine its suitability and the appropriate operating vacuum as follows: turn on the pump, fully open the coarse adjust valve, and adjust the bypass valve to give a vacuum reading corresponding to about half of atmospheric pressure. Observe the meter box orifice manometer reading, DH. Slowly increase the vacuum reading until a stable reading is obtained on the meter box orifice manometer. Record the critical vacuum for each orifice. Orifices that do not reach a critical value shall not be used.

16.2.2.2.4 Obtain the barometric pressure using a barometer as described in section 6.1.2 of this method. Record the barometric pressure, \( P_{bar} \), in mm Hg (in. Hg).

16.2.2.2.5 Conduct duplicate runs at a vacuum of 25 to 50 mm Hg (1 to 2 in. Hg) above the critical vacuum. The runs shall be at least 5 minutes each. The DGM volume readings shall be in increments of complete revolutions of the DGM. As a guideline, the times should not differ by more than 3.0 seconds (this includes allowance for changes in the DGM temperatures) to achieve 5% percent in \( K' \). Record the information listed in Figure 5-11 of Method 5, 40 CFR part 60, appendix A.

16.2.2.2.6 Calculate \( K' \) using Equation 315-11.

\[
K' = \frac{K_y V_m (P_{bar} + \Delta H/13.6)}{P_{bar} T_m \theta} \quad \text{Eq. 315-11}
\]

where

\( K' \) = Critical orifice coefficient, \([\text{m}^3/\text{min}] / [\text{mm Hg} / \text{min}] \times 16.2.2.2.7 \text{ Average the } K' \text{ values. The individual } K' \text{ values should not differ by more than } \pm 0.5 \text{ percent from the average.}

16.2.3 Using the critical orifices as calibration standards.

16.2.3.1 Record the barometric pressure.

16.2.3.2 Calibrate the metering system according to the procedure outlined in sections 7.2.2.1.2 to 7.2.2.2.5 of Method 5, 40 CFR part 60, appendix A. Record the information listed in Figure 5-12 of Method 5, 40 CFR part 60, appendix A.

16.2.3.3 Calculate the standard volumes of air passed through the DGM and the critical orifices, and calculate the DGM calibration factor, \( Y \), using the equations below:

\[
V_{(0s)} = K_y V_m (P_{bar} + \Delta H / 13.6) / T_m \quad \text{Eq. 315-12}
\]

\[
V_{(0s)} = K_y (P_{bar} \theta) / T_m \quad \text{Eq. 315-13}
\]

\[
y = V_{(0s)} N_{final} \quad \text{Eq. 315-14}
\]

where

\[ y \] = Volume of gas sample passed through the critical orifice, corrected to standard conditions, dscf (dsfc).

16.2.3.4 Average the DGM calibration values for each of the flow rates. The calibration factor, \( Y \), at each of the flow rates should not differ by more than \( \pm 2 \) percent from the average.

16.2.3.5 To determine the need for recalibrating the critical orifices, compare the DGM \( Y \) factors obtained from two adjacent orifices each time a DGM is calibrated; for example, when checking orifice 13/2.5, use orifices 12/10.2 and 13/5.1. If any critical orifice yields a DGM \( Y \) factor differing by more than 2 percent from the others, recalibrate the critical orifice according to section 7.2.2.2 of Method 5, 40 CFR part 60, appendix A.

17.0 References.


18.0 Tables, Diagrams, Flowcharts, and Validation Data

TABLE 315-1. FLOW RATES FOR VARIOUS NEEDLE SIZES AND TUBE LENGTHS.

<table>
<thead>
<tr>
<th>Gauge/length (cm)</th>
<th>Flow rate (liters/min)</th>
<th>Gauge/length (cm)</th>
<th>Flow rate (liters/min)</th>
</tr>
</thead>
<tbody>
<tr>
<td>12/7.6</td>
<td>32.56</td>
<td>14/2.5</td>
<td></td>
</tr>
<tr>
<td>12/10.2</td>
<td>30.02</td>
<td>14/5.1</td>
<td></td>
</tr>
<tr>
<td>13/2.5</td>
<td>25.77</td>
<td>14/7.6</td>
<td></td>
</tr>
<tr>
<td>13/5.1</td>
<td>23.50</td>
<td>15/3.2</td>
<td></td>
</tr>
<tr>
<td>13/7.8</td>
<td>22.37</td>
<td>15/7.8</td>
<td></td>
</tr>
<tr>
<td>13/10.2</td>
<td>20.67</td>
<td>15/10.2</td>
<td></td>
</tr>
</tbody>
</table>

FIGURE 315-1. PARTICULATE AND MCEM ANALYSES

Particulate Analysis

<table>
<thead>
<tr>
<th>Container No. 1</th>
<th>Final weight (mg)</th>
<th>Tare weight (mg)</th>
<th>Weight gain (mg)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Container No. 2</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Total</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Less Acetone blank</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Weight of particulate matter</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Moisture Analysis

<table>
<thead>
<tr>
<th>Impingers</th>
<th>Initial volume (mg)</th>
<th>Liquid collected (mg)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Note 1</td>
<td>Note 1</td>
<td></td>
</tr>
<tr>
<td>Silica gel</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Total</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Note 1: Convert volume of water to weight by multiplying by the density of water (1 g/ml).

<table>
<thead>
<tr>
<th>Container No.</th>
<th>Final weight (mg)</th>
<th>Tare of aluminum dish (mg)</th>
<th>Weight gain</th>
<th>Acetone wash volume (ml)</th>
<th>Methylene chloride wash volume (ml)</th>
</tr>
</thead>
</table>
METHOD 316—SAMPLING AND ANALYSIS FOR FORMALDEHYDE EMISSIONS FROM STATIONARY SOURCES IN THE MINERAL WOOL AND WOOL FIBERGLASS INDUSTRIES

1.0 Introduction

This method is applicable to the determination of formaldehyde, CAS Registry number 50-00-0, from stationary sources in the mineral wool and wool fiber glass industries. High purity water is used to collect the formaldehyde. The formaldehyde concentrations in the stack samples are determined using the modified pararosaniline method. Formaldehyde can be detected as low as $8.8 \times 10^{10}$ lbs/cu ft (11.3 ppbv) or as high as $1.8 \times 10^{3}$ lbs/cu ft (23,000,000 ppbv), at standard conditions over a 1 hour sampling period, sampling approximately 30 cu ft.

2.0 Summary of Method

Gaseous and particulate pollutants are withdrawn isokinetically from an emission source and are collected in high purity water. Formaldehyde present in the emissions is highly soluble in high purity water. The high purity water containing formaldehyde is then analyzed using the modified pararosaniline method. Formaldehyde in the sample reacts with acidic pararosaniline, and the sodium sulfite, forming a purple chromophore. The intensity of the purple color, measured spectrophotometrically, provides an accurate and precise measure of the formaldehyde concentration in the sample.

3.0 Definitions

See the definitions in the General Provisions of this Subpart.

4.0 Interferences

Sulfite and cyanide in solution interfere with the pararosaniline method. A procedure to overcome the interference by each compound has been described by Miksch, et al.

5.0 Safety. (Reserved)

6.0 Apparatus and Materials

6.1 A schematic of the sampling train is shown in Figure 1. This sampling train configuration is adapted from EPA Method 5, 40 CFR part 60, appendix A, procedures.
The sampling train consists of the following components: probe nozzle, probe liner, pitot tube, differential pressure gauge, impingers, metering system, barometer, and gas density determination equipment.

6.1.1 Probe Nozzle: Quartz, glass, or stainless steel with sharp, tapered (30° angle) leading edge. The taper shall be on the outside to preserve a constant inner diameter. The nozzle shall be buttonhook or elbow design. A range of nozzle sizes suitable for isokinetic sampling should be available in increments of 0.15 cm (1/16 in), e.g., 0.32 to 1.27 cm (1/8 to 1/2 in), or larger if higher volume sampling trains are used. Each nozzle shall be calibrated according to the procedure outlined in Section 10.1.

6.1.2 Probe Liner: Borosilicate glass or quartz shall be used for the probe liner. The probe shall be maintained at a temperature of 120°C ± 14°C (248°F ± 25°F).

6.1.3 Pitot Tube: The pitot tube shall be Type S, as described in Section 2.1 of EPA Method 2, 40 CFR part 60, appendix A, or any other appropriate device. The pitot tube shall be attached to the probe to allow constant monitoring of the stack gas velocity. The impact (high pressure) opening plane of the pitot tube shall be even with or above the nozzle entry plane (see Figure 2-6b, EPA Method 2, 40 CFR part 60, appendix A) during sampling. The Type S pitot tube assembly shall have a known coefficient, determined as outlined in Section 4 of EPA Method 2, 40 CFR part 60, appendix A.

6.1.4 Differential Pressure Gauge: The differential pressure gauge shall be an inclined manometer or equivalent device as described in Section 2.2 of EPA Method 2, 40 CFR part 60, appendix A. One manometer shall be used for velocity-head reading and the other for orifice differential pressure readings.

6.1.5 Impingers: The sampling train requires a minimum of four impingers, connected as shown in Figure 1, with ground glass (or equivalent) vacuum-tight fittings. For the first, third, and fourth impingers, use the Greenburg-Smith design, modified by replacing the tip with a 1.3 cm inside diameter (1/2 in) glass tube extending to 1.3 cm (1/2 in) from the bottom of the flask. For the second impinger, use a Greenburg-Smith impinger with the standard tip. Place a thermometer capable of measuring temperature...
6.1 Metering System: The necessary components are a vacuum gauge, leak-free pump, thermometers capable of measuring temperatures within 3°C (5.4°F), dry-gas meter capable of measuring volume to within 1 percent, and related equipment as shown in Figure 1. At a minimum, the pump should be capable of 4 cfm free flow, and the dry gas meter should have a recording capacity of 0.999.9 cu ft with a resolution of 0.005 cu ft. Other metering systems may be used which are capable of maintaining sample volumes to within 2 percent. The metering system may be used in conjunction with a pitot tube to enable checks of isokinetic sampling rates.

6.1.6 Barometer: The barometer may be mercury, aneroid, or other barometer capable of measuring barometric pressure to within 2.5 mm Hg (0.1 in Hg). In many cases, the barometric reading may be obtained from a nearby National Weather Service Station, in which case the station value (which is the absolute barometric pressure) is requested and an adjustment for elevation differences between the weather station and sampling point is applied at a rate of minus 2.5 mm Hg (0.1 in Hg) per 30 m (100 ft) elevation increase (rate is plus 2.5 mm Hg per 30 m (100 ft) of elevation decrease).

6.1.7 Gas Density Determination Equipment: Temperature sensor and pressure gauge (as described in Sections 2.3 and 2.3.3 of EPA Method 2, 40 CFR part 60, appendix A), and gas analyzer, if necessary (as described in EPA Method 3, 40 CFR part 60, appendix A). The temperature sensor ideally should be permanently attached to the pitot tube or sampling probe in a fixed configuration such that the top of the sensor extends beyond the leading edge of the probe sheath and does not touch any metal. Alternatively, the sensor may be attached just prior to use in the field. Note, however, that if the temperature sensor is attached in the field, the sensor must be placed in an interference-free arrangement with respect to the Type S pitot openings (see Figure 2-7, EPA Method 2, 40 CFR part 60, appendix A). As a second alternative, if a difference of no more than 1 percent in the average velocity measurement is to be introduced, the temperature gauge need not be attached to the probe or pitot tube.

6.2 Sample Recovery

6.2.1 Probe Liner: Probe nozzle and brushes; bristle brushes with stainless steel wire handles are required. The probe brush shall have extensions of stainless steel, Teflon™, or inert material at least as long as the probe. The brushes shall be properly sized and shaped to brush out the probe liner, the probe nozzle, and the impingers.

6.2.2 Wash Bottles: One wash bottle is required. Polyethylene, Teflon™, or glass wash bottles may be used for sample recovery.

6.2.3 Graduated Cylinder and/or Balance: A graduated cylinder or balance is required to measure condensate water to the nearest 1 ml or 1 g. Graduated cylinders shall have divisions not >2 ml. Laboratory balances capable of weighing to ±0.5 g are required.

6.2.4 Polyethylene Storage Containers: 500 ml wide-mouth polyethylene bottles are required to store impinger water samples.

6.2.5 Rubber Policeman and Funnel: A rubber policeman and funnel are required to aid the transfer of material into and out of containers in the field.

6.3 Sample Analysis

6.3.1 Spectrophotometer—B&L 70, 710, 2000, etc., or equivalent; 1 cm pathlength cuvette holder.

6.3.2 Disposable polystyrene cuvettes, pathlength 1 cm, volume of about 4.5 ml.

6.3.3 Pipetters—Fixed-volume Oxford pipet (250 µl; 500 µl; 1000 µl); adjustable volume Oxford or equivalent pipetter 1-5 ml model, set to 2.50 ml.

6.3.4 Pipet tips for pipettors above.

6.3.5 Parafilm, 2’ wide; cut into about 1” squares.

7.0 Reagents

7.1 High purity water: All references to water in this method refer to high purity water (ASTM Type I water or equivalent). The water purity will dictate the lower limits of formaldehyde quantification.

7.2 Silica Gel: Silica gel shall be indicating type, 6-16 mesh. If the silica gel has been used previously, dry at 175°C (350°F) for 2 hours before using. New silica gel may be used as received. Alternatively, other types of desiccants (equivalent or better) may be used.

7.3 Crushed Ice: Quantities ranging from 10-50 lbs may be necessary during a sampling run, depending upon ambient temperature. Samples which have been taken must be stored and shipped cold; sufficient ice for this purpose must be allowed.

7.4 Quaternary ammonium compound stock solution: Prepare a stock solution of dodecyltrimethylammonium chloride (98 percent minimum assay, reagent grade) by dissolving 1.0 gram in 1000 ml water. This solution contains nominally 1000 µg/ml quaternary ammonium compound, and is used as a biocide for some sources which are prone to microbial contamination.

7.5 Pararosaniline: Weigh 0.16 grams pararosaniline (free base, assay of 95 percent or greater, C.I. 42500; Sigma P7632 has been found to be acceptable) into a 100 ml flask. Exercise care, since pararosaniline is a dye and will stain. Using a wash bottle with
high-purity water, rinse the walls of the flask. Add no more than 25 ml water. Then, carefully add 20 ml of concentrated hydrochloric acid to the flask. The flask will become warm after the addition of acid. Add a magnetic stir bar to the flask, cap, and place on a magnetic stirrer for approximately 4 hours. Then, add additional water so the total volume is 100 ml. This solution is stable for several months when stored tightly capped at room temperature.

7.6 Sodium sulfite: Weigh 0.10 grams anhydrous sodium sulfite into a 100 ml flask. Dilute to the mark with high-purity water. Invert 15-20 times to mix and dissolve the sodium sulfite. This solution must be prepared fresh every day.

7.7 Formaldehyde standard solution: Pipet exactly 2.70 ml of 37 percent formaldehyde stock solution into a 1000 ml volumetric flask which contains about 500 ml of high-purity water. Dilute to the mark with high-purity water. This solution contains nominally 1000 µg/ml formaldehyde, and is used to prepare the working formaldehyde standards. The exact formaldehyde concentration may be determined if needed by suitable modification of the sodium sulfite method (Reference: J.F. Walker, Formaldehyde (Third Edition), 1964.). The 1000 µg/ml formaldehyde stock solution is stable for at least a year if kept tightly closed, with the neck of the flask sealed with Parafilm. Store at room temperature.

7.8 Working formaldehyde standards: Pipet exactly 10.0 ml of the 1000 µg/ml formaldehyde stock solution into a 100 ml volumetric flask which is about half full of high-purity water. Dilute to the mark with high-purity water, and invert 15-20 times to mix thoroughly. This solution contains nominally 100 µg/ml formaldehyde. Prepare the working standards from this 100 µg/ml standard solution and using the Oxford pipets:

<table>
<thead>
<tr>
<th>Working standard, µg/mL</th>
<th>µL or 100 µg/mL solution</th>
<th>Volumetric flask volume (dilute to mark with water)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.250</td>
<td>250</td>
<td>100</td>
</tr>
<tr>
<td>0.500</td>
<td>500</td>
<td>100</td>
</tr>
<tr>
<td>1.00</td>
<td>1000</td>
<td>100</td>
</tr>
<tr>
<td>2.00</td>
<td>2000</td>
<td>100</td>
</tr>
<tr>
<td>3.00</td>
<td>1500</td>
<td>50</td>
</tr>
</tbody>
</table>

The 100 µg/ml stock solution is stable for 4 weeks if kept refrigerated between analyses. The working standards (0.25-3.00 µg/ml) should be prepared fresh every day, consistent with good laboratory practice for trace analysis. If the laboratory water is not of high purity, it may be necessary to prepare the working standards every day. The laboratory must establish that the working standards are stable—DO NOT assume that your working standards are stable for more than a day unless you have verified this by actual testing for several series of working standards.

8.0 Sample Collection

8.1 Because of the complexity of this method, field personnel should be trained in and experienced with the test procedures in order to obtain reliable results.

8.2 Laboratory Preparation

8.2.1 All the components shall be maintained and calibrated according to the procedure described in APTD-0576, unless otherwise specified.

8.2.2 Weigh several 200 to 300 g portions of silica gel in airtight containers to the nearest 0.5 g. Record on each container the total weight of the silica gel plus containers. As an alternative to preweighing the silica gel, it may instead be weighed directly in the impinger or sampling holder just prior to train assembly.

8.3 Preliminary Field Determinations

8.3.1 Select the sampling site and the minimum number of sampling points according to EPA Method 1, 40 CFR part 60, appendix A, or other relevant criteria. Determine the stack pressure, temperature, and range of velocity heads using EPA Method 2, 40 CFR part 60, appendix A, A leak-check of the pitot lines according to Section 3.1 of EPA Method 2, 40 CFR part 60, appendix A, must be performed. Determine the stack gas moisture content using EPA Approximation Method 4, 40 CFR part 60, appendix A, or its alternatives to establish estimates of isokinetic sampling rate settings. Determine the stack gas dry molecular weight, as described in EPA Method 2, 40 CFR part 60, appendix A, Section 3.6. If integrated EPA Method 3, 40 CFR part 60, appendix A, sampling is used for molecular weight determination, the integrated bag sample shall be taken simultaneously with, and for the same total length of time as, the sample run.

8.3.2 Select a nozzle size based on the range of velocity heads so that it is not necessary to change the nozzle size in order to maintain isokinetic sampling rates below 28 l/min (1.0 cfm). During the run do not change the nozzle. Ensure that the proper differential pressure gauge is chosen for the range of velocity heads encountered (see Section 2.2 of EPA Method 2, 40 CFR part 60, appendix A).

8.3.3 Select a suitable probe liner and probe length so that all traverse points can be sampled. For large stacks, to reduce the length of the probe, consider sampling from opposite sides of the stack.

8.3.4 A minimum of 30 cu ft of sample volume is suggested for emission sources with stack concentrations not greater than 25,000,000 ppbv. Additional sample volume...
shall be collected as necessitated by the capacity of the water reagent and analytical detection limit constraint. Reduced sample volume may be collected as long as the final concentration of formaldehyde in the stack sample is greater than 10 (ten) times the detection limit.

8.3.5 Determine the total length of sampling time needed to obtain the identified minimum volume by comparing the anticipated average sampling rate with the volume requirement. Allocate the same time to all traverse points defined by EPA Method 1, 40 CFR part 60, appendix A. To avoid timekeeping errors, the length of time sampled at each traverse point should be an integer or an integer plus 0.5 min.

8.3.6 In some circumstances (e.g., batch cycles) it may be necessary to sample for shorter times at the traverse points and to obtain smaller gas-volume samples. In these cases, careful documentation must be maintained in order to allow accurate calculations of concentrations.

8.4 Preparation of Collection Train

8.4.1 During preparation and assembly of the sampling train, keep all openings where contamination can occur covered with Teflon™ film or aluminum foil until just prior to assembly or until sampling is about to begin.

8.4.2 Place 100 ml of water in each of the first two impingers, and leave the third impinger empty. If additional capacity is required for high expected concentrations of formaldehyde in the stack gas, 200 ml of water per impinger may be used or additional impingers may be used for sampling. Transfer approximately 200 to 300 g of preweighed silica gel from its container to the fourth impinger. Care should be taken to ensure that the silica gel is not entrained and carried out from the impinger during sampling. Place the silica gel container in a clean place for later use in the sample recovery. Alternatively, the weight of the silica gel plus impinger may be determined to the nearest 0.5 g and recorded.

8.4.3 With a glass or quartz liner, install the selected nozzle using a Viton-A O-ring when stack temperatures are <260°C (500°F) and a woven glass-fiber gasket when temperatures are higher. See APTD±0576 for details. Other connection systems utilizing either 316 stainless steel or Teflon™ ferrules may be used. Mark the probe with heat-resistant tape or by some other method to denote the proper distance into the stack or duct for each sampling point.

8.4.4 Assemble the train as shown in Figure 1. During assembly, a very light coating of silicone grease may be used on ground-glass joints of the impingers, but the silicone grease should be limited to the outer portion (see APTD±0576) of the ground-glass joints to minimize silicone grease contamination. If necessary, Teflon™ tape may be used to seal leaks. Connect all temperature sensors to an appropriate potentiometer/display unit. Check all temperature sensors at ambient temperatures.

8.4.5 Place crushed ice all around the impingers.

8.4.6 Turn on and set the probe heating system at the desired operating temperature. Allow time for the temperature to stabilize.

8.5 Leak-Check Procedures

8.5.1 Pre-test Leak-Check: Recommended, but not required. If the tester elects to conduct the pre-test leak-check, the following procedure shall be used.

8.5.1.1 After the sampling train has been assembled, turn on and set probe heating system at the desired operating temperature. Allow time for the temperature to stabilize. If a Viton-A O-ring or other leak-free connection is used in assembling the probe nozzle to the probe liner, leak-check the train at the sampling site by plugging the nozzle and pulling a 381 mm Hg (15 in Hg) vacuum.

NOTE: A liquid vacuum may be used, provided that the lower vacuum is not exceeded during the test.

8.5.1.2 The following leak-check instructions for the sampling train described in APTD±0576 and APTD±0581 may be helpful. Start the pump with the fine-adjust valve fully open and coarse-valve completely closed. Partially open the coarse-adjust valve and slowly close the fine-adjust valve until the desired vacuum is reached. Do not reverse direction of the fine-adjust valve, as liquid will back up into the train. If the desired vacuum is exceeded, either perform the leak-check at this higher vacuum or end the leak-check, as described below, and start over.

8.5.1.3 When the leak-check is completed, first slowly remove the plug from the inlet to the probe. When the vacuum drops to 127 mm (5 in) Hg or less, immediately close the coarse-adjust valve. Switch off the pumping system and reopen the fine-adjust valve. Do not reopen the fine-adjust valve until the
coarse-adjust valve has been closed to prevent the liquid in the impingers from being forced backward in the sampling line and silica gel from being entrained backward into the third impinger.

8.5.2 Leak-checks During Sampling Run:

8.5.2.1 If, during the sampling run, a component change (e.g., impinger) becomes necessary, a leak-check shall be conducted immediately after the interruption of sampling and before the change is made. The leak-check shall be done according to the procedure described in Section 10.3.3, except that it shall be done at a vacuum greater than or equal to the maximum value recorded up to that point in the test. If the leakage rate is found to be no greater than 0.0057 m³/min (0.02 cfm) or 4 percent of the average sampling rate (whichever is less), the results are acceptable. If a higher leakage rate is obtained, the tester shall record the leakage rate and void the sampling run.

NOTE: Any correction of the sample volume by calculation reduces the integrity of the pollutant concentration data generated and must be avoided.

8.5.2.2 Immediately after component changes, leak-checks are optional. If performed, the procedure described in section 8.5.1.1 shall be used.

8.5.3 Post-test Leak-check:

8.5.3.1 A leak-check is mandatory at the conclusion of each sampling run. The leak-check shall be done with the same procedures as the pre-test leak-check, except that the post-test leak-check shall be conducted at a vacuum greater than or equal to the maximum value reached during the sampling run. If the leakage rate is found to be no greater than 0.00057 m³/min (0.002 cfm) or 4 percent of the average sampling rate (whichever is less), the results are acceptable. If, however, a higher leakage rate is obtained, the tester shall record the leakage rate and void the sampling run.

8.6 Sampling Train Operation

8.6.1 During the sampling run, maintain an isokinetic sampling rate to within 10 percent of true isokinetic, below 28 l/min (1.0 cfm). Maintain a temperature around the probe of 120°C ± 14°C (248°F ± 25°F).

8.6.2 For each run, record the data on a data sheet such as the one shown in Figure 2. Be sure to record the initial dry-gas meter reading. Record the dry-gas meter readings at the beginning and end of each sampling time increment, when changes in flow rates are made, before and after each leak-check, and when sampling is halted. Take other readings required by Figure 2 at least once at each sample point during each time increment and additional readings when significant adjustments (20 percent variation in velocity head readings) necessitate additional adjustments in flow rate. Level and zero the manometer. Because the manometer level and zero may drift due to vibrations and temperature changes, make periodic checks during the traverse.
Figure 2 - Formaldehyde Field Data

Plant ............
Location ..........
Operator ..........
Date .............
Run No ...........
Sample box No ... 
Meter box No ....
Meter ΔH .......... 
C Factor .......... 
Pitot tube coefficient, Op

Ambient temperature ..........
Barometric pressure ....... 
Assumed moisture, percent ...
Probe length, m (ft) .......
Nozzle Identification No ...
Average calibrated nozzle diameter, cm (in.) .......
Probe heater setting ..... 
Leak rate, m³/min (cfm) ...
Probe liner material ..... 
Static pressure, mm Hg (in. Hg) .
Filter No. .............
<table>
<thead>
<tr>
<th>Traverse point number</th>
<th>Sampling time (e) min.</th>
<th>Vacuum mm Hg (in. Hg)</th>
<th>Stack temperature (T) °C (°F)</th>
<th>Velocity head (ΔP) mm (in) H₂O</th>
<th>Pressure differential across orifice meter mm H₂O (in. H₂O)</th>
<th>Gas sample volume m³ (ft³)</th>
<th>Gas sample temperature at dry gas meter</th>
<th>Filter holder temperature °C (°F)</th>
<th>Temperature of gas leaving condenser or last iminger °C (°F)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
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<td></td>
<td></td>
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<td></td>
<td></td>
<td></td>
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<tr>
<td>Total</td>
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<td></td>
</tr>
<tr>
<td>Average</td>
<td></td>
<td></td>
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<td></td>
<td></td>
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<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>
8.6.3 Clean the stack access ports prior to the test run to eliminate the chance of sampling deposited material. To begin sampling, remove the nozzle cap, verify that the probe heating system are at the specified temperature, and verify that the pitot tube and probe are properly positioned. Position the nozzle at the first traverse point, with the tip pointing directly into the gas stream. Immediately start the pump and adjust the flow to isokinetic conditions. Nomographs, which aid in the rapid adjustment of the isokinetic sampling rate without excessive computations, are available. These nomographs are designed for use when the Type S pitot tube coefficient is 0.94 ± 0.02 and the stack gas equivalent density (dry molecular weight) is equal to 29 ± 4. APTD-0576 details the procedure for using the nomographs. If the stack gas molecular weight and the pitot tube coefficient are outside the above ranges, do not use the nomographs unless appropriate steps are taken to compensate for the deviations.

8.6.4 When the stack is under significant negative pressure (equivalent to the height of the impinger stem), take care to close the coarse-adjust valve before inserting the probe into the stack in order to prevent liquid from backing up through the train. If necessary, a low vacuum on the train may have to be started prior to entering the stack.

8.6.5 When the probe is in position, block off the openings around the probe and stack access port to prevent unrepresentative dilution of the gas stream.

8.6.6 Traverse the stack cross section, as required by EPA Method 1, 40 CFR part 60, appendix A, being careful not to bump the probe nozzle into the stack walls when sampling near the walls or when removing or inserting the probe through the access port, in order to minimize the chance of extracting deposited material.

8.6.7 During the test run, make periodic adjustments to keep the temperature around the probe at the proper levels. Add more ice and, if necessary, salt, to maintain a temperature of <20°C (68°F) at the silica gel outlet.

8.6.8 A single train shall be used for the entire sampling run, except in cases where simultaneous sampling is required in two or more separate ducts or at two or more different locations within the same duct, or in cases where equipment failure necessitates a change of trains. An additional train or trains may also be used for sampling when the capacity of a single train is exceeded.

8.6.9 When two or more trains are used, separate analyses of components from each train shall be performed. If multiple trains have been used because the capacity of a single train would be exceeded, first impingers from each train may be combined, and second impingers from each train may be combined.

8.6.10 At the end of the sampling run, turn off the coarse-adjust valve, remove the probe and nozzle from the stack, turn off the pump, record the final dry gas meter reading, and conduct a post-test leak-check. Also, check the pitot lines as described in EPA Method 2, 40 CFR part 60, appendix A. The lines must pass this leak-check in order to validate the velocity-head data.

8.6.11 Calculate percent isokineticity (see Method 2) to determine whether the run was valid or another test should be made.

8.7 Sample Preservation and Handling

8.7.1 Samples from most sources applicable to this method have acceptable holding times using normal handling practices (shipping samples iced, storing in refrigerator at 2°C until analysis). However, forming section stacks and other sources using waste water sprays may be subject to microbial contamination. For these sources, a biocide (quaternary ammonium compound solution) may be added to collected samples to improve sample stability and method ruggedness.

8.7.2 Sample holding time: Samples should be analyzed within 14 days of collection. Samples must be refrigerated and kept cold for the entire period preceding analysis. After the samples have been brought to room temperature for analysis, any analyses needed should be performed on the same day. Repeated cycles of warming the samples to room temperature/refrigerating/rewarming, then analyzing again, etc., have not been investigated in depth to evaluate if analyte levels remain stable for all sources.

8.7.3 Additional studies will be performed to evaluate whether longer sample holding times are feasible for this method.

8.8 Sample Recovery

8.8.1 Preparation:

8.8.1.1 Proper cleanup procedure begins as soon as the probe is removed from the stack at the end of the sampling period. Allow the probe to cool. When the probe can be handled safely, wipe off all external particulate matter near the tip of the probe nozzle and place a cap over the tip to prevent losing or gaining particulate matter. Do not cap the probe tightly while the sampling train is cooling because a vacuum will be created, drawing liquid from the impingers back through the sampling train.

8.8.1.2 Before moving the sampling train to the cleanup site, remove the probe from the sampling train and cap the open outlet, being careful not to lose any condensate that might be present. Remove the umbilical cord from the last impinger and cap the impinger. If a flexible line is used, let any condensed water or liquid drain into the impingers. Cap off any open impinger inlets and outlets. Ground glass stoppers, Teflon™ caps, or...
 caps of other inert materials may be used to seal all openings.

8.8.1.3 Transfer the probe and impinger assembly to an area that is clean and protected from wind so that the chances of contaminating or losing the sample are minimized.

8.8.1.4 Inspect the train before and during disassembly, and note any abnormal conditions.

8.8.1.5 Save a portion of the washing solution (high purity water) used for cleanup as a blank.

8.8.2 Sample Containers:

8.8.2.1 Container 1: Probe and Impinger Catches. Using a graduated cylinder, measure to the nearest ml, and record the volume of the solution in the first three impingers. Alternatively, the solution may be weighed to the nearest 0.5 g. Include any condensate in the probe in this determination. Transfer the combined impinger solution from the graduated cylinder into the polyethylene bottle. Taking care that dust on the outside of the probe or other exterior surfaces does not get into the sample, clean all surfaces to which the sample is exposed (including the probe nozzle, probe fitting, probe liner, first three impingers, and impinger connectors) with water. Use less than 400 ml for the entire wash (250 ml would be better, if possible). Add the rinse water to the sample container.

8.8.2.1.1 Carefully remove the probe nozzle and rinse the inside surface with water from a wash bottle. Brush with a bristle brush and rinse until the rinse shows no visible particles, after which make a final rinse of the inside surface. Brush and rinse the inside parts of the Swagelok (or equivalent) fitting with water in a similar way.

8.8.2.1.2 Rinse the probe liner with water. While squirting the water into the upper end of the probe, tilt and rotate the probe so that all inside surfaces will be wetted with water. Let the water drain from the lower end into the sample container. The tester may use a funnel (glass or polyethylene) to aid in transferring the liquid washes to the container. Follow the rinse with a bristle brush. Hold the probe in an inclined position, and squirt water into the upper end as the probe brush is being pushed with a twisting action through the probe. Hold the sample container underneath the lower end of the probe, and catch any water and particulate matter that is brushed from the probe. Run the brush through the probe three times or more. Rinse the brush with water and quantitatively collect these washings in the sample container. After the brushing, make a final rinse of the probe as described above.

NOTE: Two people should clean the probe in order to minimize sample losses. Between sampling runs, brushes must be kept clean and free from contamination.

8.8.2.1.3 Rinse the inside surface of each of the first three impingers (and connecting tubing) three separate times. Use a small portion of water for each rinse, and brush the surface to which the sample is exposed with a bristle brush to ensure recovery of fine particulate matter. Make a final rinse of each surface and of the brush, using water.

8.8.2.1.4 After all water washings, if particulate matter have been collected in the sample container, tighten the lid so the sample will not leak out when the container is shipped to the laboratory. Mark the height of the fluid level to determine whether leakage occurs during transport. Label the container clearly to identify its contents.

8.8.2.1.5 If the first two impingers are to be analyzed separately to check for breakthrough, separate the contents and rinses of the two impingers into individual containers. Care must be taken to avoid physical carryover from the first impinger to the second. Any physical carryover of collected moisture into the second impinger will invalidate a breakthrough assessment.

8.8.2.2 Container 2: Sample Blank. Prepare a blank by using a polyethylene container and adding a volume of water equal to the total volume in Container 1. Process the blank in the same manner as Container 1.

8.8.2.3 Container 3: Silica Gel. Note the color of the indicating silica gel to determine whether it has been completely spent and make a notation of its condition. The impinger containing the silica gel may be used as a sample transport container with both ends sealed with tightly fitting caps or plugs. Ground-glass stoppers or Teflon caps may be used. The silica gel impinger should then be labeled, covered with aluminum foil, and packaged on ice for transport to the laboratory. If the silica gel is removed from the impinger, the tester may use a funnel to pour the silica gel and a rubber policeman to remove the silica gel from the impinger. It is not necessary to remove the small amount of dust particles that may adhere to the impinger wall and are difficult to remove. Since the gain in weight is to be used for moisture calculations, do not use water or other liquids to transfer the silica gel. If a balance is available in the field, the spent silica gel (or silica gel plus impinger) may be weighed to the nearest 0.5 g.

8.8.2.4 Sample containers should be placed in a cooler, cooled by (although not in contact with) ice. Putting sample bottles in Zip-Lock™ bags can aid in maintaining the integrity of the sample labels. Sample containers should be placed vertically to avoid leakage during shipment. Samples should be cooled during shipment so they will be received cold at the laboratory. It is critical that samples be chilled immediately after recovery. If the source is susceptible to microbial contamination from wash water (e.g.
forming section stack), add biocide as directed in section 8.2.5.

8.8.2.5 A quaternary ammonium compound can be used as a biocide to stabilize samples against microbial degradation following collection. Using the stock quaternary ammonium compound (QAC) solution; add 2.5 ml QAC solution for every 100 ml of sample volume (estimate of volume is satisfactory) immediately after collection. The total volume of QAC solution must be accurately known and recorded, to correct for any dilution caused by the QAC solution addition.

8.8.3 Sample Preparation for Analysis 8.8.3.1 The sample should be refrigerated if the analysis will not be performed on the day of sampling. Allow the sample to warm at room temperature for about two hours (if it has been refrigerated) prior to analyzing.

8.8.3.2 Analyze the sample by the pararosaniline method, as described in Section 11. If the color-developed sample has an absorbance above the highest standard, a suitable dilution in high purity water should be prepared and analyzed.

9.0 Quality Control

9.1 Sampling: See EPA Manual 600/4-77-02b for Method 5 quality control.

9.2 Analysis: The quality assurance program required for this method includes the analysis of the field and method blanks, and procedure validations. The positive identification and quantitation of formaldehyde are dependent on the integrity of the samples received and the precision and accuracy of the analytical methodology. Quality assurance procedures for this method are designed to monitor the performance of the analytical methodology and to provide the required information to take corrective action if problems are observed in laboratory operations or in field sampling activities.

9.2.1 Field Blanks: Field blanks must be submitted with the samples collected at each sampling site. The field blanks include the sample bottles containing aliquots of sample recover water, and water reagent. At a minimum, one complete sampling train will be assembled in the field staging area, taken to the sampling area, and leak-checked at the beginning and end of the testing (or for the same total number of times as the actual sampling train). The probe of the blank train must be heated during the sample test. The train will be recovered as if it were an actual test sample. No gaseous sample will be passed through the blank sampling train.

9.2.2 Blank Correction: The field blank formaldehyde concentrations will be subtracted from the appropriate sample formaldehyde concentrations. Blank formaldehyde concentrations above 0.25 µg/mL should be considered suspect, and subtraction from the sample formaldehyde concentrations should be performed in a manner acceptable to the Administrator.

9.2.3 Method Blanks: A method blank must be prepared for each set of analytical operations, to evaluate contamination and artifacts that can be derived from glassware, reagents, and sample handling in the laboratory.

10 Calibration

10.1 Probe Nozzle: Probe nozzles shall be calibrated before their initial use in the field. Using a micrometer, measure the inside diameter of the nozzle to the nearest 0.025 mm (0.001 in). Make measurements at three separate places across the diameter and obtain the average of the measurements. The difference between the high and low numbers shall not exceed 0.1 mm (0.004 in). When the nozzle becomes nicked or corroded, it shall be repaired and calibrated, or replaced with a calibrated nozzle before use. Each nozzle must be permanently and uniquely identified.

10.2 Pitot Tube: The Type S pitot tube assembly shall be calibrated according to the procedure outlined in Section 4 of EPA Method 2, or assigned a nominal coefficient of 0.84 if it is not visibly nicked or corroded and if it meets design and intercomponent spacing specifications.

10.3 Metering System

10.3.1 Before its initial use in the field, the metering system shall be calibrated according to the procedure outlined in APTD-0576. Instead of physically adjusting the dry-gas meter dial readings to correspond to the wet-test meter readings, calibration factors may be used to correct the gas meter dial readings mathematically to the proper values. Before calibrating the metering system, it is suggested that a leak-check be conducted. For metering systems having diaphragm pumps, the normal leak-check procedure will not delete leakages with the pump. For these cases, the following leak-check procedure will apply: Make a ten-minute calibration run at 0.00057 m³/min (0.02 cfm). At the end of the run, take the difference of the measured wet-test and dry-gas meter volumes and divide the difference by 10 to get the leak rate. The leak rate should not exceed 0.00057 m³/min (0.02 cfm).

10.3.2 After each field use, check the calibration of the metering system by performing three calibration runs at a single intermediate orifice setting (based on the previous field test). Set the vacuum at the maximum value reached during the test series. To adjust the vacuum, insert a valve between the wet-test meter and the inlet of the metering system. Calculate the average...
value of the calibration factor. If the calibration has changed by more than 5 percent, re-calibrate the meter over the full range of orifice settings, as outlined in APTD-0576.

10.3.3 Leak-check of metering system: The portion of the sampling train from the pump to the orifice meter (see Figure 1) should be leak-checked prior to initial use and after each shipment. Leakage after the pump will result in less volume being recorded than is actually sampled. Use the following procedure:

Procedure: Close the main valve on the meter box. Insert a one-hole rubber stopper with rubber tubing attached into the orifice exhaust pipe. Disconnect and vent the low side of the orifice manometer. Close off the low side orifice tap. Pressurize the system to 13-18 cm (5-7 in) water column by blowing into the rubber tubing. Pinch off the tubing and observe the manometer for 1 min. A loss of pressure on the manometer indicates a leak in the meter box. Leaks must be corrected.

NOTE: If the dry-gas meter coefficient values obtained before and after a test series differ by >5 percent, either the test series must be voided or calculations for test series must be performed using whichever meter coefficient value (i.e., before or after) gives the lower value of total sample volume.

10.4 Probe Heater: The probe heating system must be calibrated before its initial use in the field according to the procedure outlined in APTD-0576. Probes constructed according to APTD-0581 need not be calibrated if the calibration curves in APTD-0576 are used.

10.5 Temperature gauges: Use the procedure in section 4.3 of USEPA Method 2 to calibrate in-stack temperature gauges. Dial thermometers such as are used for the dry gas meter and condenser outlet, shall be calibrated against mercury-in-glass thermometers.

10.6 Barometer: Adjust the barometer initially and before each test series to agree to within ±2.5 mm Hg (0.1 in Hg) of the mercury barometer. Alternately, if a National Weather Service Station (NWSS) is located at the same altitude above sea level as the test site, the barometric pressure reported by the NWSS may be used.

10.7 Balance: Calibrate the balance before each test series, using Class S standard weights. The weights must be within ±0.5 percent of the standards, or the balance must be adjusted to meet these limits.

11.0 Procedure for Analysis.

The working formaldehyde standards (0.25, 0.50, 1.0, 2.0, and 3.0 µg/ml) are analyzed and a calibration curve is calculated for each day’s analysis. The standards should be analyzed first to ensure that the method is working properly prior to analyzing the samples. In addition, a sample of the high-purity water should also be analyzed and used as a “0” formaldehyde standard.

The procedure for analysis of samples and standards is identical: Using the pipet set to 2.50 ml, pipet 2.50 ml of the solution to be analyzed into a polystyrene cuvette. Using the 250 µl pipet, pipet 250 µl of the pararosaniline reagent solution into the cuvette. Seal the top of the cuvette with a Parafilm square and shake at least 30 seconds to ensure the solution in the cuvette is well-mixed. Peel back a corner of the Parafilm so the next reagent can be added. Using the 250 µl pipet, pipet 250 µl of the sodium sulfite reagent solution into the cuvette. Reseal the cuvette with the Parafilm, and again shake for about 30 seconds to mix the solution in the cuvette. Record the time of addition of the sodium sulfite and let the color develop at room temperature for 60 minutes. Set the spectrophotometer to 570 nm and set to read in Absorbance Units. The spectrophotometer should be equipped with a holder for the 1-cm pathlength cuvettes. Place cuvette(s) containing high-purity water in the spectrophotometer and adjust to read 0.000 AU.

After the 60 minutes color development period, read the standard and samples in the spectrophotometer. Record the absorbance reading for each cuvette. The calibration curve is calculated by linear regression, with the formaldehyde concentration as the “x” coordinate of the pair, and the absorbance reading as the “y” coordinate. The procedure is very reproducible, and typically will yield values similar to these for the calibration curve:

Correlation Coefficient: 0.9999
Slope: 0.50
Y-Intercept: 0.000

The formaldehyde concentration of the samples can be found by using the trend-line feature of the calculator or computer program used for the linear regression. For example, the TI-55 calculators use the “X” key (this gives the predicted formaldehyde concentration for the value of the absorbance you key in for the sample). Multiply the formaldehyde concentration from the sample by the dilution factor, if any, for the sample to give the formaldehyde concentration of the original, undiluted, sample (units will be micrograms/ml).

11.1 Notes on the Pararosaniline Procedure

11.1.1 The pararosaniline method is temperature-sensitive. However, the small fluctuations typical of a laboratory will not significantly affect the results.

11.1.2 The calibration curve is linear to beyond 4.0 µg/ml formaldehyde, however, a
research-grade spectrophotometer is required to reproducibly read the high absorbance values. Consult your instrument manual to evaluate the capability of the spectrophotometer.

11.1.3 The quality of the laboratory water used to prepare standards and make dilutions is critical. It is important that the cautions given in the Reagents section be observed. This procedure allows quantitation of formaldehyde at very low levels, and thus it is imperative to avoid contamination from other sources of formaldehyde and to exercise the degree of care required for trace analyses.

11.1.4 The analyst should become familiar with the operation of the Oxford or equivalent pipettors before using them for an analysis. Follow the instructions of the manufacturer; one can pipet water into a tared container on any analytical balance to check pipet accuracy and precision. This will also establish if the proper technique is being used. Always use a new tip for each pipetting operation.

11.1.5 This procedure follows the recommendations of ASTM Standard Guide D 3614, reading all solutions versus water in the reference cell. This allows the absorbance of the blank to be tracked on a daily basis. Refer to ASTM D 3614 for more information.

12.0 Calculations

Carry out calculations, retaining at least one extra decimal figure beyond that of the acquired data. Round off figures after final calculations.

12.1 Calculations of Total Formaldehyde

12.1.1 To determine the total formaldehyde in mg, use the following equation if biocide was not used:

\[
\text{Total mg formaldehyde} = C_d \times V \times \text{DF} \times 0.001 \text{ mg/µg}
\]

Where:

- \( C_d \) = measured conc. formaldehyde, µg/ml
- \( V \) = total volume of stack sample, ml
- \( \text{DF} \) = dilution factor

12.1.2 To determine the total formaldehyde in mg, use the following equation if biocide was used:

\[
\text{Total mg formaldehyde} = \frac{C_d \times V}{(V - B) \times \text{DF} \times 0.001 \text{ mg/µg}}
\]

Where:

- \( C_d \) = measured conc. formaldehyde, µg/ml
- \( V \) = total volume of stack sample, ml
- \( B \) = total volume of biocide added to sample, ml
- \( \text{DF} \) = dilution factor

12.2 Formaldehyde concentration (mg/m³) in stack gas. Determine the formaldehyde concentration (mg/m³) in the stack gas using the following equation:

\[
\frac{K \times [\text{total formaldehyde, mg}]}{V_m(\text{std})}
\]

Where:

- \( K = 35.31 \text{ cu ft/m}^3 \) for \( V_m(\text{std}) \) in English units, or
- \( K = 1.00 \text{ m}^3/\text{m}^3 \) for \( V_m(\text{std}) \) in metric units
- \( V_m(\text{std}) \) = volume of gas sample measured by a dry gas meter, corrected to standard conditions, dscm (dscf)

12.3 Average dry gas meter temperature and average orifice pressure drop are obtained from the data sheet.

12.4 Dry Gas Volume: Calculate \( V_m(\text{std}) \) and adjust for leakage, if necessary, using the equation in Section 6.3 of EPA Method 5, 40 CFR part 60, appendix A.

12.5 Volume of Water Vapor and Moisture Content: Calculated the volume of water vapor and moisture content from equations 5-2 and 5-3 of EPA Method 5.

13.0 Method Performance

The precision of this method is estimated to be better than ±5 percent, expressed as ± the percent relative standard deviation.

14.0 Pollution Prevention. (Reserved)

15.0 Waste Management. (Reserved)

16.0 References


**METHOD 318—EXTRACTIVE FTIR METHOD FOR THE MEASUREMENT OF EMISSIONS FROM THE MINERAL WOOL AND WOOL FIBERGLASS INDUSTRIES**

1.0 Scope and Application

This method has been validated and approved for mineral wool and wool fiberglass sources. This method may not be applied to other source categories without validation and approval by the Administrator according to the procedures in Test Method 301, 40 CFR part 63, appendix A. For sources seeking to apply FTIR to other source categories, Test Method 320 (40 CFR part 63, appendix A) may be utilized.

1.1 Scope. The analytes measured by this method and their CAS numbers are:

- Carbon Monoxide 630-08-0
- Carbonyl Sulfide 463-58-1
- Formaldehyde 50-00-0
- Methanol 1455-13-6
- Phenol 108-95-2
1.2 Applicability

1.2.1 This method is applicable for the determination of formaldehyde, phenol, methanol, carbonyl sulfide (COS) and carbon monoxide (CO) concentrations in controlled and uncontrolled emissions from manufacturing processes using phenolic resins. The compounds are analyzed in the mid-infrared spectral region (about 400 to 4000 cm⁻¹ or 25 to 2.5 µm). Suggested analytical regions are given below (Table 1). Slight deviations from these recommended regions may be necessary due to variations in moisture content and ammonia concentration from source to source.

<table>
<thead>
<tr>
<th>Compound</th>
<th>Analytical region (cm⁻¹) FLₘ – FUₘ</th>
<th>Potential interferants</th>
</tr>
</thead>
<tbody>
<tr>
<td>Formaldehyde</td>
<td>2840.93 – 2679.83</td>
<td>Water, Methane.</td>
</tr>
<tr>
<td>Phenol</td>
<td>1231.32 – 1131.47</td>
<td>Water, Ammonia, Methane.</td>
</tr>
<tr>
<td>Methanol</td>
<td>1041.56 – 1019.95</td>
<td>Water, Ammonia.</td>
</tr>
<tr>
<td>COS</td>
<td>2028.4 – 2091.9</td>
<td>Water, CO₂, CO.</td>
</tr>
<tr>
<td>CO</td>
<td>2092.1 – 2191.8</td>
<td>Water, CO₂, COS.</td>
</tr>
</tbody>
</table>

* Suggested analytical regions assume about 15 percent moisture and CO₂, and that COS and CO have about the same absorbance (in the range of 10 to 50 ppm). If CO and COS are hundreds of ppm or higher, then CO₂ and moisture interference is reduced. If CO or COS is present at high concentration and the other at low concentration, then a shorter cell pathlength may be necessary to measure the high concentration component.

1.2.2 This method does not apply when: (a) Polymerization of formaldehyde occurs, (b) moisture condenses in either the sampling system or the instrumentation, and (c) when moisture content of the gas stream is so high relative to the analyte concentrations that it causes severe spectral interference.

1.3 Method Range and Sensitivity

1.3.1 The analytical range is a function of instrumental design and composition of the gas stream. Theoretical detection limits depend, in part, on (a) the absorption coefficient of the compound in the analytical frequency region, (b) the spectral resolution, (c) interferometer sampling time, (d) detector sensitivity and response, and (e) absorption pathlength.

1.3.2 Practically, there is no upper limit to the range. The practical lower detection limit is usually higher than the theoretical value, and depends on (a) moisture content of the flue gas, (b) presence of interferants, and (c) losses in the sampling system. In general, a 22 meter pathlength cell in a suitable sampling system can achieve practical detection limits of 1.5 ppm for three compounds (formaldehyde, phenol, and methanol) at moisture levels up to 15 percent by volume. Sources with uncontrolled emissions of CO and COS may require a 4 meter pathlength cell due to high concentration levels. For these two compounds, make sure absorbance of highest concentration component is <1.0.

1.4 Data Quality Objectives

1.4.1 In designing or configuring the system, the analyst first sets the data quality objectives, i.e., the desired lower detection limit (DLᵢ) and the desired analytical uncertainty (AUᵢ) for each compound. The instrumental parameters (factors b, c, d, and e in Section 1.3.1) are then chosen to meet these requirements, using Appendix D of the FTIR Protocol.

1.4.2 Data quality for each application is determined, in part, by measuring the RMS (Root Mean Square) noise level in each analytical spectral region (Appendix C of the FTIR Protocol). The RMS noise is defined as the RMSD (Root Mean Square Deviation) of the absorbance values in an analytical region from the mean absorbance value of the region. Appendix D of the FTIR Protocol defines the MAUᵢ (minimum analyte uncertainty) for the iᵗʰ analyte in the mᵗʰ analytical region. The MAU is the minimum analyte concentration for which the analytical uncertainty limit (AUᵢ) can be maintained: if the measured analyte concentration is less than MAUᵢ, then data quality is unacceptable. Table 2 gives some example DL and AU values along with calculated areas and MAU values using the protocol procedures.
<table>
<thead>
<tr>
<th>Protocol value</th>
<th>Form</th>
<th>Phenol</th>
<th>Methanol</th>
<th>Protocol appendix</th>
</tr>
</thead>
</table>
| Reference concentration 
(ppm-meters)/K                | 3.016     | 3.017     | 5.064     |                   |
| Reference Band Area          | 8.2544    | 16.6417   | 4.9416    | B                 |
| DL (ppm-meters)/K            | 0.1117    | 0.1117    | 0.1117    | B                 |
| AU                           | 0.2       | 0.2       | 0.2       | B                 |
| CL                           | 0.02234   | 0.02234   | 0.02234   | B                 |
| FL                           | 2679.83   | 1131.47   | 1019.95   | B                 |
| FU                           | 294.03    | 1231.32   | 1041.56   | B                 |
| Fc                           | 2750.38   | 1181.355  | 1030.755  | B                 |
| AAI (ppm-meters)/K           | 0.18440   | 0.01201   | 0.00132   | B                 |
| RMSD                         | 2.28E-03  | 1.21E-03  | 1.07E-03  | C                 |
| MAU (ppm-meters)/K           | 4.45E-02  | 7.26E-03  | 4.68E-03  | D                 |
| MAU (ppm at 22)              | 0.0797    | 0.0130    | 0.0084    | D                 |

*Concentration units are: ppm concentration of the reference sample (ASC), times the path length of the FTIR cell used when the reference spectrum was measured (meters), divided by the absolute temperature of the reference sample in Kelvin (K), or (ppm-meters)/K.
Environmental Protection Agency

2. Summary of Method

2.1 Principle

2.1.1 Molecules are composed of chemically bonded atoms, which are in constant motion. The atomic motions result in bond deformations (bond stretching and bond-angle bending). The number of fundamental (or independent) vibrational motions depends on the number of atoms \((N)\) in the molecule. At typical testing temperatures, most molecules are in the ground-state vibrational state for most of their fundamental vibrational motions. A molecule can undergo a transition from its ground state (for a particular vibration) to the first excited state by absorbing a quantum of light at a frequency characteristic of the molecule and the molecular motion. Molecules also undergo rotational transitions by absorbing energies in the far-infrared or microwave spectral regions. Rotational transition absorbencies are superimposed on the vibrational absorbencies to give a characteristic shape to each rotational-vibrational absorbance "band."

2.1.2 Most molecules exhibit more than one absorbance band in several frequency regions to produce an infrared spectrum (a characteristic pattern of bands or a "fingerprint") that is unique to each molecule. The infrared spectrum of a molecule depends on its structure (bond lengths, bond angles, bond strengths, and atomic masses). Even small differences in structure can produce significantly different spectra.

2.1.3 Spectral band intensities vary with the concentration of the absorbing compound. Within constraints, the relationship between absorbance and sample concentration is linear. Same spectra are compared to reference spectra to determine the species and their concentrations.

2.2 Sampling and Analysis

2.2.1 Flue gas is continuously extracted from the source, and the gas or a portion of the gas is conveyed to the FTIR gas cell, where a spectrum of the flue gas is recorded. Absorptions band intensities are related to sample concentrations by Beer’s Law. Where:

\[ A_v = \sum a_i b_i c_i \]

where:

- \(A_v\) = absorbance of the \(i^{th}\) component at the given frequency, \(v\).  
- \(a_i\) = absorption coefficient of the \(i^{th}\) component at the frequency, \(v\).  
- \(b_i\) = path length of the cell.  
- \(c_i\) = concentration of the \(i^{th}\) compound in the sample at frequency \(v\).

2.2.2 After identifying a compound from the infrared spectrum, its concentration is determined by comparing band intensities in the sample spectrum to band intensities in "reference spectra" of the formaldehyde, phenol, methanol, COS and CO. These reference spectra are available in a permanent soft copy from the EPA spectral library on the EMTIC bulletin board. The source may also prepare reference spectra according to Section 4.5 of the FTIR Protocol.

**Note:** Reference spectra not prepared according to the FTIR Protocol are not acceptable for use in this test method. Documentation detailing the FTIR Protocol steps used in preparing any non-EPA reference spectra shall be included in each test report submitted by the source.

2.3 Operator Requirements. The analyst must have some knowledge of source sampling and of infrared spectral patterns to operate the sampling system and to choose a suitable instrument configuration. The analyst should also understand FTIR instrument operation well enough to choose an instrument configuration consistent with the data quality objectives.

3.0 Definitions

See Appendix A of the FTIR Protocol.

4.0 Interferences

4.1 Analytical (or Spectral) Interferences. Water vapor. High concentrations of ammonia (hundreds of ppm) may interfere with the analysis of low concentrations of methanol (1 to 5 ppm). For CO, carbon dioxide and water may be interferants. In cases where COS levels are low relative to CO levels, CO and water may be interferants.

4.2 Sampling System Interferences. Water, if it condenses, and ammonia, which reacts with formaldehyde.

5.0 Safety

5.1 Formaldehyde is a suspected carcinogen; therefore, exposure to this compound must be limited. Proper monitoring and safety precautions must be practiced in any atmosphere with potentially high concentrations of CO.

5.2 This method may involve sampling at locations having high positive or negative pressures, high temperatures, elevated heights, high concentrations of hazardous or toxic pollutants, or other diverse sampling conditions. It is the responsibility of the tester(s) to ensure proper safety and health practices, and to determine the applicability of regulatory limitations before performing this test method.

6.0 Equipment and Supplies

The equipment and supplies are based on the schematic of a sampling train shown in Figure 1. Either the evacuated or purged sampling technique may be used with this sampling train. Alternatives may be used,
provided that the data quality objectives of this method are met.

6.1 Sampling Probe. Glass, stainless steel, or other appropriate material of sufficient length and physical integrity to sustain heating, prevent adsorption of analytes, and to reach gas sampling point.

6.2 Particulate Filters. A glass wool plug (optional) inserted at the probe tip (for large particulate removal) and a filter rated at 1-micron (e.g., Balston™) for fine particulate removal, placed immediately after the heated probe.

6.3 Sampling Line/Heating System. Heated (maintained at 250 ± 25 degrees F) stainless steel, Teflon™, or other inert material that does not adsorb the analytes, to transport the sample to analytical system.

6.4 Stainless Steel Tubing. Type 316, e.g., 3/8 in. diameter, and appropriate length for heated connections.

6.5 Gas Regulators. Appropriate for individual gas cylinders.

6.6 Teflon™ Tubing. Diameter (e.g., 3/8 in.) and length suitable to connect cylinder regulators.

6.7 Sample Pump. A leak-free pump (e.g., KNF™), with by-pass valve, capable of pulling sample through entire sampling system at a rate of about 10 to 20 L/min. If placed before the analytical system, heat the pump and use a pump fabricated from materials non-reactive to the target pollutants. If the...
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6.8 Gas Sample Manifold. A heated manifold that diverts part of the sample stream to the analyzer, and the rest to the by-pass discharge vent or other analytical instrumentation.

6.9 Rotameter. A calibrated 0 to 20 L/min range rotameter.

6.10 FTIR Analytical System. Spectrometer and detector, capable of measuring formaldehyde, phenol, methanol, COS and CO to the predetermined minimum detectable level. The system shall include a personal computer with compatible software that prompts the operator to obtain at least 8 sample spectra in 1 hour.

6.11 FTIR Cell Pump. Required for the evacuated sampling technique, capable of evacuating the FTIR cell volume within 2 minutes. The FTIR cell pump should allow the operator to obtain at least 8 sample spectra in 1 hour.

6.12 Absolute Pressure Gauge. Heatable and capable of measuring pressure from 0 to 1000 mmHg to within ±2.5 mmHg (e.g., Baratron™).

6.13 Temperature Gauge. Capable of measuring the cell temperature to within ±2°C.

7.0 Reagents and Standards

7.1 Ethylene (Calibration Transfer Standard). Obtain NIST traceable (or Protocol) cylinder gas.

7.2 Nitrogen. Ultra high purity (UHP) grade.

7.3 Reference Spectra. Obtain reference spectra for the target pollutants at concentrations that bracket (in ppm-meter/K) the emission source levels. Also, obtain reference spectra for SF₆ and ethylene. Suitable concentrations are 0.012 to 0.112 (ppm-meter/K) for SF₆ and 5.6L (ppm-meter/K) or less for ethylene. The reference spectra shall meet the criteria for acceptance outlined in Section 2.2.2. The optical density (ppm-meters/K) of the reference spectrum must match the optical density of the sample spectrum within (less than) 25 percent.

8.0 Sample Collection, Preservation, and Storage

Sampling should be performed in the following sequence: Collect background, collect CTS spectrum, collect samples, collect post-test CTS spectrum, verify that two copies of all data were stored on separate computer media.

8.1 Pretest Preparations and Evaluations. Using the procedure in Section 4.0 of the FTIR Protocol, determine the optimum sampling system configuration for sampling the target pollutants. Table 2 gives some example values for AU, DL, and MAU. Based on a study (Reference 1), an FTIR system using 1 cm⁻¹ resolution, 22 meter path length, and a broad band MCT detector was suitable for meeting the requirements in Table 2. Other factors that must be determined are:

a. Test requirements: AU, CMAX, DL, OFU, and UI, for each.
b. Interferants: See Table 1.

c. Sampling system: LS, Pmin, P′, T′, TSS, VSS, fractional error, MIL.
d. Analytical regions: 1 through N, FL, FC, and FU plus interferants, FFU, FFL, wave number range FNU to 4N L. See Tables 1 and 2.

8.1.1 If necessary, sample and acquire an initial spectrum. Then determine the proper operational pathlength of the instrument to obtain non-saturated absorbances of the target analytes.

8.1.2 Set up the sampling train as shown in Figure 1.

8.2 Sampling System Leak-check. Leak-check from the probe tip to pump outlet as follows: Connect a 0- to 250-mL/min rate meter (rotameter or bubble meter) to the outlet of the pump. Close off the inlet to the probe, and note the leakage rate. The leakage rate shall be ≤200 mL/min.

8.3 Analytical System Leak-check.

8.3.1 For the evacuated sample technique, close the valve to the FTIR cell, and evacuate the absorption cell to the minimum absolute pressure Pmin. Close the valve to the pump, and determine the change in pressure ΔP after 2 minutes.

8.3.2 For both the evacuated sample and purging techniques, pressurize the system to about 100 mmHg above atmospheric pressure. Isolate the pump and determine the change in pressure ΔP after 2 minutes.

8.3.3 Measure the barometric pressure, Pb, in mmHg.

8.3.4 Determine the percent leak volume %V, for the signal integration time tSS, and for ΔPmax, i.e., the larger of ΔPv or ΔPp, as follows:

\[
%V_L = 50 \frac{\Delta P_{\text{max}}}{p_{\text{SS}}} \times 100
\]

Where:

\( \frac{50}{2} = 100\% \) divided by the leak-check time of 2 minutes.

8.3.5 Leak volumes in excess of 4 percent of the sample system volume VSS are unacceptable.

8.4 Background Spectrum. Evacuate the gas cell to ≤5 mmHg, and fill with dry nitrogen gas to ambient pressure. Verify that no significant amounts of absorbing species (for example water vapor and CO₂) are present. Collect a background spectrum, using a signal averaging period equal to or greater than the averaging period for the sample spectra. Assign a unique file name to the background
spectrum. Store the spectra of the background interferogram and processed single-beam background spectrum on two separate computer media (one is used as the back-up). If continuous sampling will be used during sample collection, collect the background spectrum with nitrogen gas flowing through the cell at the same pressure and temperature as will be used during sampling.

8.5 Pre-Test Calibration Transfer Standard. Evacuate the gas cell to ≤5 mmHg absolute pressure, and fill the FTIR cell to atmospheric pressure with nitrogen gas. Or, purge the cell with 10 cell volumes of CTS gas. Record the spectrum. If continuous sampling will be used during sample collection, collect a CTS spectrum with CTS gas flowing through the cell at the same pressure and temperature as will be used during sampling.

8.6 Samples

8.6.1 Evacuated Samples. Evacuate the absorbance cell to ≤5 mmHg absolute pressure. Fill the cell with flue gas to ambient pressure and record the spectrum. Before taking the next sample, evacuate the cell until no further evidence of absorption exists. Repeat this procedure to collect at least 8 separate spectra (samples) in 1 hour.

8.6.2 Purge Sampling. Purge the FTIR cell with 10 cell volumes of flue gas and at least for about 10 minutes. Discontinue the gas cell purge, isolate the cell, and record the sample spectrum and the pressure. Before taking the next sample, purge the cell with 10 cell volumes of flue gas.

8.6.3 Continuous Sampling. Spectra can be collected continuously while the FTIR cell is being purged. The sample integration time, t_, the sample flow rate through the FTIR gas cell, and the total run time must be chosen so that the collected data consist of at least 10 spectra with each spectrum being of a separate cell volume of flue gas. More spectra can be collected over the run time and the total run time (and number of spectra) can be extended as well.

8.7 Sampling QA, Data Storage and Reporting

8.7.1 Sample integration times should be sufficient to achieve the required signal-to-noise ratios. Obtain an absorbance spectrum by filling the cell with nitrogen. Measure the RMSD in each analytical region in this absorbance spectrum. Verify that the number of scans is sufficient to achieve the target MAU (Table 2).

8.7.2 Identify all sample spectra with unique file names.

8.7.3 Store on two separate computer media a copy of sample interferograms and processed spectra. The data shall be available to the Administrator on request for the length of time specified in the applicable regulation.

8.7.4 For each sample spectrum, document the sampling conditions, the sampling time (while the cell was being filled), the time the spectrum was recorded, the instrumental conditions (path length, temperature, pressure, resolution, integration time), and the spectral file name. Keep a hard copy of these data sheets.

8.8 Signal Transmittance. While sampling, monitor the signal transmittance through the instrumental system. If signal transmittance (relative to the background) drops below 95 percent in any spectral region where the sample does not absorb infrared energy, obtain a new background spectrum.

8.9 Post-run CTS. After each sampling run, record another CTS spectrum.

8.10 Post-test QA

8.10.1 Inspect the sample spectra immediately after the run to verify that the gas matrix composition was close to the expected (assumed) gas matrix.

8.10.2 Verify that the sampling and instrumental parameters were appropriate for the conditions encountered. For example, if the moisture is much greater than anticipated, it will be necessary to use a shorter path length or dilute the sample.

8.10.3 Compare the pre and post-run CTS spectra. They shall agree to within 5 percent. See FTIR Protocol, Appendix E.

9.0 Quality Control

Follow the quality assurance procedures in the method, including the analysis of pre and post-run calibration transfer standards (Sections 8.5 and 8.9) and the post-test quality assurance procedures in Section 8.10.

10.0 Calibration and Standardization

10.1 Signal-to-Noise Ratio (S/N). The S/N shall be sufficient to meet the MAU in each analytical region.

10.2 Absorbance Pathlength. Verify the absorbance path length by comparing CTS spectra to reference spectra of the calibration gas(es). See FTIR Protocol, Appendix E.

10.3 Instrument Resolution. Measure the line width of appropriate CTS band(s) and compare to reference CTS spectra to verify instrumental resolution.

10.4 Apodization Function. Choose appropriate apodization function. Determine any appropriate mathematical transformations that are required to correct instrumental errors by measuring the CTS. Any mathematical transformations must be documented and reproducible.

10.5 FTIR Cell Volume. Evacuate the cell to ≤5 mmHg. Measure the initial absolute temperature (T_i) and absolute pressure (P_i). Connect a wet test meter (or a calibrated dry gas meter), and slowly draw room air into the cell. Measure the meter volume (V_m), meter absolute temperature (T_m), and meter
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absolute pressure ($P_a$), and the cell final absolute temperature ($T_f$) and absolute pressure ($P_f$). Calculate the FTIR cell volume $V_{ss}$, including that of the connecting tubing, as follows:

$$V_{ss} = \frac{V_m P_m}{T_m}$$

(8)

As an alternative to the wet test meter/calibrated dry gas meter procedure, measure the inside dimensions of the cell cylinder and calculate its volume.

11.0 Procedure

Refer to Sections 4.6-4.11, Sections 5, 6, and 7, and the appendices of the FTIR Protocol.

12.0 Data Analysis and Calculations

a. Data analysis is performed using appropriate reference spectra whose concentrations can be verified using CTS spectra. Various analytical programs are available to relate sample absorbance to a concentration standard. Calculated concentrations should be verified by analyzing spectral baselines after mathematically subtracting scaled reference spectra from the sample spectra. A full description of the data analysis and calculations may be found in the FTIR Protocol (Sections 4.0, 5.0, 6.0 and appendices).

b. Correct the calculated concentrations in sample spectra for differences in absorption pathlength between the reference and sample spectra by:

$$C_{corr} = C_{calc} \left( \frac{L_s}{L_i} \right) \left( \frac{T_s}{T_i} \right)$$

(9)

Where:

- $C_{corr}$ = The pathlength corrected concentration.
- $C_{calc}$ = The initial calculated concentration (output of the Multicomp program designed for the compound).
- $L_s$ = The pathlength associated with the reference spectra.
- $L_i$ = The pathlength associated with the sample spectra.
- $T_s$ = The absolute temperature (K) of the sample gas.
- $T_i$ = The absolute gas temperature (K) at which reference spectra were recorded.

13.0 Reporting and Recordkeeping

All interferograms used in determining source concentration shall be stored for the period of time required in the applicable regulation. The Administrator has the option of requesting the interferograms recorded during the test in electronic form as part of the test report.

14.0 Method Performance

Refer to the FTIR Protocol.

15.0 Pollution Prevention. [Reserved]

16.0 Waste Management

Laboratory standards prepared from the formaldehyde and phenol are handled according to the instructions in the materials safety data sheets (MSDS).

17.0 References


(2) “Method 301—Field Validation of Pollutant Measurement Methods from Various Waste Media,” 40 CFR part 63, appendix A.

METHOD 319—DETERMINATION OF FILTRATION EFFICIENCY FOR PAINT OVERSPRAY ARRESTORS

1.0 Scope and Application.

1.1 This method applies to the determination of the initial, particle size dependent, filtration efficiency for paint arrestors over the particle diameter range from 0.3 to 10 µm. The method applies to single and multiple stage paint arrestors or paint arrestor media. The method is applicable to efficiency determinations from 0 to 99 percent. Two test aerosols are used—one liquid phase and one solid phase. Oleic acid, a low-volatility liquid (CAS Number 112-80-1), is used to simulate the behavior of wet paint overspray. The solid-phase aerosol is potassium chloride salt (KCl, CAS Number 7447-40-7) and is used to simulate the behavior of a dry overspray. The method is limited to determination of the initial, clean filtration efficiency of the arrestor. Changes in efficiency (either increase or decrease) due to the accumulation of paint overspray on and within the arrestor are not evaluated.

1.2 Efficiency is defined as 1—Penetration (e.g., 70 percent efficiency is equal to 0.30 penetration). Penetration is based on the ratio of the downstream particle concentration to the upstream concentration. It is often more useful, from a mathematical or statistical point of view, to discuss the upstream and downstream counts in terms of penetration rather than the derived efficiency value. Thus, this document uses both penetration and efficiency as appropriate.
1.3 For a paint arrestor system or sub-system which has been tested by this method, adding additional filtration devices to the system or subsystem shall be assumed to result in an efficiency of at least that of the original system without the requirement for additional testing. (For example, if the final stage of a three-stage paint arrestor system has been tested by itself, then the addition of the other two stages shall be assumed to maintain, as a minimum, the filtration efficiency provided by the final stage alone. Thus, in this example, if the final stage has been shown to meet the filtration requirements of Table 1 of §63.745 of subpart GG, then the final stage in combination with any additional paint arrestor stages also passes the filtration requirements.)

2.0 Summary of Method.

2.1 This method applies to the determination of the fractional (i.e., particle-size dependent) aerosol penetration of several types of paint arrestors. Fractional penetration is computed from aerosol concentrations measured upstream and downstream of an arrestor installed in a laboratory test rig. The aerosol concentrations upstream and downstream of the arrestors are measured with an aerosol analyzer that simultaneously counts and sizes the particles in the aerosol stream. The aerosol analyzer covers the particle diameter size range from 0.3 to 10 µm in a minimum of 12 contiguous sizing channels. Each sizing channel covers a narrow range of particle diameters. For example, Channel 1 may cover from 0.3 to 0.4 µm, Channel 2 from 0.4 to 0.5 µm, * * * By taking the ratio of the downstream to upstream counts on a channel by channel basis, the penetration is computed for each of the sizing channels.

2.2 The upstream and downstream aerosol measurements are made while injecting the test aerosol into the air stream upstream of the arrestor (ambient aerosol is removed with HEPA filters on the inlet of the test rig). This test aerosol spans the particle size range from 0.3 to 10 µm and provides sufficient upstream concentration in each of the optical particle counter (OPC) sizing channels to allow accurate calculation of penetration, down to penetrations of approximately 0.01 (i.e., 1 percent penetration; 99 percent efficiency). Results are presented as a graph and a data table showing the aerodynamic particle diameter and the corresponding fractional efficiency.

3.0 Definitions.

Aerodynamic Diameter—diameter of a unit density sphere having the same aerodynamic properties as the particle in question.

Efficiency is defined as equal to 1—Penetration.

Optical Particle Counter (OPC)—an instrument that counts particles by size using light scattering. An OPC gives particle diameters based on size, index of refraction, and shape.

Penetration—the fraction of the aerosol that penetrates the filter at a given particle diameter. Penetration equals the downstream concentration divided by the upstream concentration.

4.0 Interferences.

4.1 The influence of the known interferences (particle losses) are negated by correction of the data using blanks.

5.0 Safety.

5.1 There are no specific safety precautions for this method above those of good laboratory practice. This standard does not purport to address all of the safety problems, if any, associated with its use. It is the responsibility of the user of this method to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

6.0 Equipment and Supplies.

6.1 Test Facility. A schematic diagram of a test duct used in the development of the method is shown in Figure 319-1.
6.1.1 The test section, paint spray section, and attached transitions are constructed of stainless and galvanized steel. The upstream and downstream ducting is 20 cm diameter polyvinyl chloride (PVC). The upstream transition provides a 7° angle of expansion to provide a uniform air flow distribution to the paint arrestors. Aerosol concentration is
measured upstream and downstream of the test section to obtain the challenge and penetrating aerosol concentrations, respectively. Because the downstream ducting runs back under the test section, the challenge and penetrating aerosol taps are located physically near each other, thereby facilitating aerosol sampling and reducing sample-line length. The inlet nozzles of the upstream and downstream aerosol probes are designed to yield isokinetic sampling conditions.

6.2 Aerosol Generator. The aerosol generator is used to produce a stable aerosol covering the particle size range from 0.3 to 10 \( \mu \text{m} \) diameter. The generator used in the development of this method consists of an air atomizing nozzle positioned at the top of a 0.30-m (12-in.) diameter, 1.3-m (51-in.) tall, acrylic, transparent, spray tower. This tower allows larger sized particles, which would otherwise foul the test duct and sample lines, to fall out of the aerosol. It also adds drying air to ensure that the KCl droplets dry to solid salt particles. After generation, the aerosol passes through an aerosol neutralizer (K108 radioactive source) to neutralize any electrostatic charge on the aerosol (electrostatic charge is an unavoidable consequence of most aerosol generation methods). To improve the mixing of the aerosol with the air stream, the aerosol is injected counter to the airflow. Generators of other designs may be used, but they must produce a stable aerosol concentration over the 0.3 to 10 \( \mu \text{m} \) diameter size range; provide a means of ensuring the complete drying of the KCl aerosol; and utilize a charge neutralizer to neutralize any electrostatic charge on the aerosol. The resultant challenge aerosol must meet the minimum count per channel and maximum concentration criteria of Table 319-1.

6.3 Installation of Paint Arrestor. The paint arrestor is to be installed in the test duct in a manner that precludes air bypassing the arrestor. Since arrestor media are often sold unmounted, a mounting frame may be used to provide back support for the media in addition to sealing it into the duct. The mounting frame for 20 x 20 in. arrestors will have minimum open internal dimensions of 18 in. square. Mounting frames for 24 in. x 24 in. arrestors will have minimum open internal dimensions of 22 in. square. The open internal dimensions of the mounting frame shall not be less than 75 percent of the approach duct dimensions.

### Table 319-1.—QC Control Limits

<table>
<thead>
<tr>
<th>Frequency and description</th>
<th>Control limits</th>
</tr>
</thead>
<tbody>
<tr>
<td>OPC zero count</td>
<td>&lt;50 counts per minute.</td>
</tr>
<tr>
<td>OPC sizing accuracy check</td>
<td>Peak of distribution should be in correct OPC channel.</td>
</tr>
<tr>
<td>Minimum counts per channel for challenge aerosol</td>
<td>Minimum total of 500 particle counts per channel.</td>
</tr>
<tr>
<td>Maximum particle concentration</td>
<td>&lt;10% of manufacturer's claimed upper limit corresponding to a 10% count error.</td>
</tr>
<tr>
<td>Standard Deviation of Penetration</td>
<td>&lt;0.10 for 0.3 to 3 ( \mu \text{m} ) diameter.</td>
</tr>
<tr>
<td>0% Penetration</td>
<td>&lt;0.30 for &gt;3 ( \mu \text{m} ) diameter.</td>
</tr>
<tr>
<td>100% Penetration—KCl</td>
<td>&lt;0.01.</td>
</tr>
<tr>
<td>100% Penetration—Oleic Acid</td>
<td>0.3 to 1 ( \mu \text{m} ): 0.90 to 1.10.</td>
</tr>
<tr>
<td></td>
<td>1 to 3 ( \mu \text{m} ): 0.75 to 1.25.</td>
</tr>
<tr>
<td></td>
<td>3 to 10 ( \mu \text{m} ): 0.50 to 1.50.</td>
</tr>
<tr>
<td></td>
<td>0.3 to 1 ( \mu \text{m} ): 0.90 to 1.10.</td>
</tr>
<tr>
<td></td>
<td>1 to 3 ( \mu \text{m} ): 0.75 to 1.25.</td>
</tr>
<tr>
<td></td>
<td>3 to 10 ( \mu \text{m} ): 0.50 to 1.50.</td>
</tr>
</tbody>
</table>
6.4 Optical Particle Counter. The upstream and downstream aerosol concentrations are measured with a high-resolution optical particle counter (OPC). To ensure comparability of test results, the OPC shall utilize an optical design based on wide-angle light scattering and provided a minimum of 12 contiguous particle sizing channels from 0.3 to 10\(\mu\)m diameter (based on response to PSL) where, for each channel, the ratio of the diameter corresponding to the upper channel bound to the lower channel bound must not exceed 1.5.

6.5 Aerosol Sampling System. The upstream and downstream sample lines must be made of rigid electrically-grounded metallic tubing having a smooth inside surface, and they must be rigidly secured to prevent movement during testing. The upstream and downstream sample lines are to be nominally identical in geometry. The use of a short length (100 mm maximum) of straight flexible tubing to make the final connection to the OPC is acceptable. The inlet nozzles of the upstream and downstream probes must be sharp-edged and of appropriate entrance diameter to maintain isokinetic sampling within 20 percent of the air velocity.

6.5.1 The sampling system may be designed to acquire the upstream and downstream counts using (a) sequential upstream-downstream sampling with a single OPC, (b) simultaneous upstream and downstream sampling with two OPC’s, or (c) sequential upstream-downstream sampling with two OPC’s.

6.5.2 When two particle counters are used to acquire the upstream and downstream counts, they must be closely matched in flowrate and optical design.

6.6 Airflow Monitor. The volumetric airflow through the system shall be measured with a calibrated orifice plate, flow nozzle, or laminar flow element. The measurement device must have an accuracy of 5 percent or better.

7.0 Reagents and Standards.

7.1 The liquid test aerosol is reagent grade, 98 percent pure, oleic acid (Table 319-2). The solid test aerosol is KCl aerosolized from a solution of KCl in water. In addition to the test aerosol, a calibration aerosol of monodisperse polystyrene latex (PSL) spheres is used to verify the calibration of the OPC.

<table>
<thead>
<tr>
<th>Refractive index</th>
<th>Density, g/cm(^3)</th>
<th>Shape</th>
</tr>
</thead>
<tbody>
<tr>
<td>Oleic Acid</td>
<td>1.46 nonabsorbing</td>
<td>0.89 Spherical</td>
</tr>
<tr>
<td>KCl</td>
<td>1.49</td>
<td>1.98 Cubic or agglomerated cubes</td>
</tr>
<tr>
<td>(solid-phase challenge aerosol)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>PSL (calibration aerosol)</td>
<td>1.59 nonabsorbing</td>
<td>1.05 Spherical</td>
</tr>
</tbody>
</table>

8.0 Sample Collection, Preservation, and Storage.

8.1 In this test, all sampling occurs in real-time, thus no samples are collected that require preservation or storage during the test. The paint arrestors are shipped and stored to avoid structural damage or soiling. Each arrestor may be shipped in its original box from the manufacturer or similar cardboard box. Arrestors are stored at the test site in a location that keeps them clean and dry. Each arrestor is clearly labeled for tracking purposes.

9.0 Quality Control.

9.1 Table 319-1 lists the QC control limits.

9.2 The standard deviation (\(\sigma\)) of the penetration (P) for a given test at each of the 15 OPC sizing channels is computed from the coefficient of variation (CV, the standard deviation divided by the mean) of the upstream and downstream measurements as:

\[
\sigma = P \sqrt{(CV_{\text{upstream}}^2 + CV_{\text{downstream}}^2)} \quad \text{(Eq. 3194)}
\]

For a properly operating system, the standard deviation of the penetration is less than 0.10 at particle diameters from 0.3 to 3 \(\mu\)m and less than 0.30 at diameters > 3 \(\mu\)m.

9.3 Data Quality Objectives (DQO).

9.3.1 Fractional Penetration. From the triplicate tests of each paint arrestor model, the standard deviation for the penetration measurements at each particle size (i.e., for each sizing channel of the OPC) is computed as:

\[
\sigma = P \sqrt{(CV_{\text{upstream}}^2 + CV_{\text{downstream}}^2)} \quad \text{(Eq. 3194)}
\]
\[ s = \left[ \sum (P_i - \bar{P})^2 / (n - 1) \right]^{1/2} \]

(Eq. 319-2)

where \( P_i \) represents an individual penetration measurement, and \( \bar{P} \) the average of the 3 \((n = 3)\) individual measurements.

9.3.2 Bias of the fractional penetration values is determined from triplicate no-filter and HEPA filter tests. These tests determine the measurement bias at 100 percent penetration and 0 percent penetration, respectively.

9.3.3 PSL-Equivalent Light Scattering Diameter. The precision and bias of the OPC sizing determination are based on sampling a known diameter of PSL and noting whether the particle counts peak in the correct channel of the OPC. This is a pass/fail measurement with no calculations involved.

9.3.4 Airflow. The precision of the measurement must be within 5 percent of the set point.

10.0 Calibration and Standardization.

10.1 Optical Particle Counter. The OPC must have an up-to-date factory calibration. Check the OPC zero at the beginning and end of each test by sampling HEPA-filtered air. Verify the sizing accuracy on a daily basis (for days when tests are performed) with 1-µm PSL spheres.

10.2 Airflow Measurement. Airflow measurement devices must have an accuracy of 5 percent or better. Manometers used in conjunction with the orifice plate must be inspected prior to use for proper level, zero, and mechanical integrity. Tubing connections to the manometer must be free from kinks and have secure connections.

10.3 Pressure Drop. Measure pressure drop across the paint arrestor with an inclined manometer readable to within 0.01 in. H₂O. Prior to use, the level and zero of the manometer, and all tubing connections, must be inspected and adjusted as needed.

11.0 Procedure.

11.1 Filtration Efficiency. For both the oleic acid and KCl challenges, this procedure is performed in triplicate using a new arrestor for each test.

11.1.1 General Information and Test Duct Preparation

11.1.1.1 Use the “Test Run Sheet” form (Figure 319-2) to record the test information.

**RUN SHEET**

**Part 1. General Information**

Date and Time: ____________________________

Test Operator: ____________________________

Test #: ____________________________

Paint Arrestor: ____________________________

Brand/Model ____________________________

Arrester Assigned ID # ____________________________

Condition of arrestor (i.e., is there any damage? Must be new condition to proceed): ____________________________

Manometer zero and level confirmed? ____________________________

**Part 2. Clean Efficiency Test**

Date and Time: ____________________________

Optical Particle Counter: ____________________________

20 min. warm up ____________________________

Zero count (<50 counts/min) ____________________________

Daily PSL check ____________________________

PSL Diam: ______µm ____________________________

File name for OPC data: ____________________________

Test Conditions: ____________________________

Air Flow: ____________________________

Temp & RH: Temp ______°F RH ______% ____________________________

Atm. Pressure: ______ in. Hg ____________________________

(from mercury barometer)

Aerosol Generator: (record all operating parameters) ____________________________

Test Aerosol: ____________________________

(Oleic acid or KCl) ____________________________

Arrester: ____________________________

Pressure drop: at start ______ in. H₂O ____________________________

at end ______ in. H₂O ____________________________

Condition of arrestor at end of test (note any physical deterioration): ____________________________

**Figure 319-2. Test Run Sheet**

Other report formats which contain the same information are acceptable.

11.1.12 Record the date, time, test operator, Test #, paint arrestor brand/model and its assigned ID number. For tests with no arrestor, record none.

11.1.13 Ensure that the arrestor is undamaged and in “new” condition.

11.1.14 Mount the arrestor in the appropriate frame. Inspect for any airflow leak paths.

11.1.15 Install frame-mounted arrestor in the test duct. Examine the installed arrestor to verify that it is sealed in the duct. For tests with no arrestor, install the empty frame.
11.1.1.6 Visually confirm the manometer zero and level. Adjust as needed.
11.1.2 Clean Efficiency Test.
11.1.2.1 Record the date and time upon beginning this section.
11.1.2.2 Optical Particle Counter.
11.1.2.2.1 General: Operate the OPC per the manufacturer’s instructions allowing a minimum of 20 minutes warm up before making any measurements.
11.1.2.2.2 Overload: The OPC will yield inaccurate data if the aerosol concentration it is attempting to measure exceeds its operating limit. To ensure reliable measurements, the maximum aerosol concentration will not exceed 10 percent of the manufacturer’s claimed upper concentration limit corresponding to a 10 percent count error. If this value is exceeded, reduce the aerosol concentration until the acceptable conditions are met.
11.1.2.2.3 Zero Count: Connect a HEPA capsule to the inlet of the OPC and obtain printouts for three samples (each a minimum of 1-minute each). Record maximum cumulative zero count. If the count rate exceeds 50 counts per minute, the OPC requires servicing before continuing.
11.1.2.2.4 PSL Check of OPC Calibration: Confirm the calibration of the OPC by sampling a known size PSL aerosol. Aerosolize the PSL using an appropriate nebulizer. Record whether the peak count is observed in the proper channel. If the peak is not seen in the appropriate channel, have the OPC recalibrated.
11.1.2.3 Test Conditions:
11.1.2.3.1 Airflow: The test airflow corresponds to a nominal face velocity of 120 FPM through the arrestor. For arrestors having nominal 20 in. x 20 in. face dimensions, this measurement corresponds to an airflow of 333 cfm. For arrestors having nominal face dimensions of 24 in. x 24 in., this measurement corresponds to an airflow of 480 cfm.
11.1.2.3.2 Temperature and Relative Humidity: The temperature and relative humidity of the challenge air stream will be measured to within an accuracy of ±2 °F and ±10 percent RH. To protect the probe from fouling, it may be removed during periods of aerosol generation.
11.1.2.3.3 Barometric Pressure: Use a mercury barometer. Record the atmospheric pressure.
11.1.2.4 Upstream and Downstream Background Counts.
11.1.2.4.1 With the arrestor installed in the test duct and the airflow set at the proper value, turn on the data acquisition computer and bring up the data acquisition program.
11.1.2.4.2 Set the OPC settings for the appropriate test sample duration with output for both printer and computer data collection.
11.1.2.4.3 Obtain one set of upstream-downstream background measurements.
11.1.2.4.4 After obtaining the upstream-downstream measurements, stop data acquisition.
11.1.2.5 Efficiency Measurements:
11.1.2.5.1 Record the arrestor pressure drop.
11.1.2.5.2 Turn on the Aerosol Generator. Begin aerosol generation and record the operating parameters.
11.1.2.5.3 Monitor the particle counts. Allow a minimum of 5 minutes for the generator to stabilize.
11.1.2.5.4 Confirm that the total particle count does not exceed the predetermined upper limit. Adjust generator as needed.
11.1.2.5.5 Confirm that a minimum of 50 particle counts are measured in the upstream sample in each of the OPC channels per sample. (A minimum of 50 counts per channel per sample will yield the required minimum 500 counts per channel total for the 10 upstream samples as specified in Table 319-1.) Adjust generator or sample time as needed.
11.1.2.5.6 If you are unable to obtain a stable concentration within the concentration limit and with the 50 count minimum per channel, adjust the aerosol generator.
11.1.2.5.7 When the counts are stable, perform repeated upstream-downstream sampling until 10 upstream-downstream measurements are obtained.
11.1.2.5.8 After collection of the 10 upstream-downstream samples, stop data acquisition and allow 2 more minutes for final purging of generator.
11.1.2.5.9 Obtain one additional set of upstream-downstream background samples.
11.1.2.5.10 After obtaining the upstream-downstream background samples, stop data acquisition.
11.1.2.5.11 Record the arrestor pressure drop.
11.1.2.5.12 Turn off blower.
11.1.2.5.13 Remove the paint arrestor assembly from the test duct. Note any signs of physical deterioration.
11.1.2.5.14 Remove the arrestor from the frame and place the arrestor in an appropriate storage bag.
11.2 Control Test: 100 Percent Penetration Test. A 100 percent penetration test must be performed immediately before each individual paint arrestor test using the same challenge aerosol substance (i.e., oleic acid or KCl) as to be used in the arrestor test. These tests are performed with no arrestor installed in the test housing. This test is a relatively stringent test of the adequacy of the overall duct, sampling, measurement, and aerosol generation system. The test is performed as a normal penetration test except the paint arrestor is not used. A perfect system would yield a measured penetration of 1 at all particle sizes. Deviations from 1
can occur due to particle losses in the duct, differences in the degree of aerosol uniformity (i.e., mixing) at the upstream and downstream probes, and differences in particle transport efficiency in the upstream and downstream sampling lines.

11.3 Control Test: 0 Percent Penetration.

One 0 percent penetration test must be performed at least monthly during testing. The test is performed by using a HEPA filter rather than a paint arrestor. This test assesses the adequacy of the instrument response time and sample line lag.

12.0 Data Analysis and Calculations.

12.1 Analysis. The analytical procedures for the fractional penetration and flow velocity measurements are described in Section 11. Note that the primary measurements, those of the upstream and downstream aerosol concentrations, are performed with the OPC which acquires the sample and analyzes it in real time. Because all the test data are collected in real time, there are no analytical procedures performed subsequent to the actual test, only data analysis.

12.2 Calculations.

12.2.1 Penetration.

Nomenclature

\[ U = \text{Upstream particle count} \]
\[ D = \text{Downstream particle count} \]
\[ U_b = \text{Upstream background count} \]
\[ D_b = \text{Downstream background count} \]
\[ P_{100} = \text{100 percent penetration value determined immediately prior to the arrestor test computed for each channel as:} \]

\[
P = \frac{D - D_b}{U - U_b} \]

\[ P = \text{Penetration of the arrestor corrected for } P_{100} \]
\[ \rho = \text{sample standard deviation} \]
\[ CV = \text{coefficient of variation} = \frac{\rho}{\text{mean}} \]
\[ E = \text{Efficiency}. \]

Overbar denotes arithmetic mean of quantity.

Analysis of each test involves the following quantities:

- \( P_{100} \) value for each sizing channel from the 100 percent penetration control test,
- 2 upstream background values,
- 2 downstream background values,
- 10 upstream values with aerosol generator on, and
- 10 downstream values with aerosol generator on.

Using the values associated with each sizing channel, the penetration associated with each particle-sizing channel is calculated as:

\[
P = \left( \frac{D - D_b}{U - U_b} \right) / P_{100} \quad (\text{Eq. 319-3})
\]

\[ E = 1 - P \quad (\text{Eq. 319-4}) \]

Most often, the background levels are small compared to the values when the aerosol generator is on.

12.3 The relationship between the physical diameter (\( D_{\text{Physical}} \)) as measured by the OPC to the aerodynamic diameter (\( D_{\text{Aero}} \)) is given by:

\[
D_{\text{Aero}} = D_{\text{Physical}} \sqrt{\frac{\rho_{\text{Particle}}}{\rho_o}} \frac{\text{CCF}_{\text{Physical}}}{\text{CCF}_{\text{Aero}}} \quad (\text{Eq. 319-5})
\]

Where:

\[ \rho_o = \text{unit density of } 1 \text{ g/cm}^3 \]
\[ \rho_{\text{Particle}} = \text{the density of the particle, } 0.89 \text{ g/cm}^3 \text{ for oleic acid.} \]
\[ \text{CCF}_{\text{Physical}} = \text{the Cunningham Correction Factor at } D_{\text{Physical}} \]
\[ \text{CCF}_{\text{Aero}} = \text{the Cunningham Correction Factor at } D_{\text{Aero}} \]

12.4 Presentation of Results. For a given arrestor, results will be presented for:

- Triplicate arrestor tests with the liquid-phase challenge aerosol,
- Triplicate arrestor tests with the solid-phase challenge aerosol,
- Triplicate 100 percent challenge aerosol tests with the liquid-phase challenge aerosol,
- Triplicate 100 percent challenge aerosol tests with the solid-phase challenge aerosol, and
- One 0 percent filter test (using either the liquid-phase or solid-phase aerosol and performed at least monthly).

12.4.1 Results for the paint arrestor test must be presented in both graphical and tabular form. The X-axis of the graph will be a logarithmic scale of aerodynamic diameter from 0.1 to 100 \( \mu m \). The Y-axis will be efficiency (%) on a linear scale from 0 to 100.

Plots for each individual run and a plot of
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the average of triplicate solid-phase and of
the average triplicate liquid-phase tests
must be prepared. All plots are to be based
on point-to-point plotting (i.e., no curve fit-
ing) is to be used. The data are to be plotted
based on the geometric mean diameter of
each of the OPC's sizing channels.

12.4.2 Tabulated data from each test must
be provided. The data must include the upper
and lower diameter bound and geometric
mean diameter of each of the OPC sizing
channels, the background particle counts for
each channel for each sample, the upstream
particle counts for each channel for each
sample, the downstream particle counts for
each channel for each sample, the 100 percent
penetration values computed for each chan-
nel, and the 0 percent penetration values
computed for each channel.

13.0 Pollution Prevention.

13.1 The quantities of materials to be
aerosolized should be prepared in accord with
the amount needed for the current tests so
as to prevent wasteful excess.

14.0 Waste Management.

14.1 Paint arrestors may be returned to
originator, if requested, or disposed of with
regular laboratory waste.

15.0 References.

"Fractional Penetration of Paint Overspray
Arrestors, Draft Final Report." EPA Cooper-
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Removal Air Cleaners Used in General Ven-
tilation." Final Report, 671-RP, American
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1994.

Test Method 330—Measurement of Vapor
Phase Organic and Inorganic Emissions
By Extractive Fourier Transform Infrar-
ed (FTIR) Spectroscopy

1.0 Introduction.

Persons unfamiliar with basic elements of
FTIR spectroscopy should not attempt to
use this method. This method describes sam-
ping and analytical procedures for extract-
ing emission measurements using Fourier
transform infrared (FTIR) spectroscopy. De-
tailed analytical procedures for interpreting
infrared spectra are described in the "Pro-
tocol for the Use of Extractive Fourier
Transform Infrared (FTIR) Spectroscopy in
Analyses of Gaseous Emissions from Sta-
tionary Sources," hereafter referred to as
the "Protocol." Definitions not given in this
method are given in appendix A of the Pro-
tocol. References to specific sections in the
Protocol are made throughout this Method.

For additional information refer to ref-
ences 1 and 2, and other EPA reports,
which describe the use of FTIR spectrometry
in specific field measurement applications
and validation tests. The sampling procedure
described here is extractive. Flue gas is ex-
tracted through a heated gas transport and
handling system. For some sources, sample
conditioning systems may be applicable.
Some examples are given in this method.

NOTE: sample conditioning systems may be
used providing the method validation re-
quirements in Sections 9.2 and 13.0 of this
method are met.

1.1 Scope and Applicability.

1.1.1 Analytes. Analytes include hazardous
air pollutants (HAPs) for which EPA ref-
ereence spectra have been developed. Other
compounds can also be measured with this
method if reference spectra are prepared ac-
ording to section 4.6 of the protocol.

1.1.2 Applicability. This method applies to
the analysis of vapor phase organic or inor-
ganic compounds which absorb energy in the
mid-infrared spectral region, about 400 to
4000 cm⁻¹ (25 to 2.5 µm). This method is used
to determine compound-specific concentra-
tions in a multi-component vapor phase sam-
ple, which is contained in a closed-path gas
 cell. Spectra of samples are collected using
double beam infrared absorption spectro-
copy. A computer program is used to analyze
spectra and report compound concentrations.

1.2 Method Range and Sensitivity. Analyt-
ical range and sensitivity depend on the fre-
quency-dependent analyte absorptivity, in-
strument configuration, data collection pa-
rameters, and gas stream composition. In-
strument factors include: (a) spectral resolu-
tion, (b) interferometer signal averaging
time, (c) detector sensitivity and response,
and (d) absorption path length.

1.2.1 For any optical configuration the an-
alytical range is between the absorbance val-
ues of about 0.01 (infrared transmittance re-
ative to the background = 0.98) and 1.0
(T = 0.1). (For absorbance > 1.0 the relation
between absorbance and concentration may
not be linear.)

1.2.2 The concentrations associated with
this absorbance range depend primarily on
the cell path length and the sample tempera-
ture. An analyte absorbance greater than 1.0,
can be lowered by decreasing the optical
path length. Analyte absorbance increases
with a longer path length. Analyte detection
also depends on the presence of other species
exhibiting absorbance in the same analytical

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**Data Quality.** Data quality shall be determined by executing Protocol pre-test procedures in appendices I and J of the protocol.

1.3 Sensitivity. The limit of sensitivity for an optical configuration and integration time is determined using appendix D of the Protocol: Minimum Analyte Uncertainty, (MAU). The MAU depends on the RMSD noise in an analytical region, and on the absorbance (A) limit (A = 0.03) depends on the root mean square deviation (RMSD) noise in the analytical region.

1.2.3 The concentration range of this method is determined by the choice of optical configuration.

1.2.3.1 The absorbance for a given concentration can be decreased by increasing the cell path length or by diluting the sample. There is no practical upper limit to the measurement range.

1.2.3.2 The analyte absorbance for a given concentration may be increased by increasing the cell path length or (to some extent) using a higher resolution. Both modifications also cause a corresponding increased absorbance for all compounds in the sample, and a decrease in the signal throughput. For this reason the practical lower detection range (quantitation limit) usually depends on sample characteristics such as moisture content of the gas, the presence of other interferants, and losses in the sampling system.

1.4 Data Quality. Data quality shall be determined by executing Protocol pre-test procedures in appendices B to H of the protocol and post-test procedures in appendices I and J of the protocol.

1.4.1 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

1.4.2 An instrumental configuration shall be selected. An estimate of gas composition shall be made based on previous test data, data from a similar source or information gathered in a pre-test site survey. Spectral interferers shall be identified using the selected DL, and AU, and band areas from reference spectra and interferent spectra. The baseline noise of the system shall be measured in each analytical region to determine the MAU of the instrument configuration for each analyte and interferent (MIU).

1.4.3 Data quality for the application shall be determined, in part, by measuring the RMS (root mean square) noise level in each analytical spectral region (appendix C of the Protocol). The RMS noise is defined as the RMS of the absorbance values in an analytical region from the mean absorbance value in the region.

1.4.4 The MAU is the minimum analyte concentration for which the AU, can be maintained; if the measured analyte concentration is less than MAU, then data quality are unacceptable.

1.4.5 The MAU depends on the RMSD noise in an analytical region, and on the absorbance (A) limit (A = 0.03) depends on the root mean square deviation (RMSD) noise in the analytical region.

1.4.6 The MAU is the minimum analyte concentration for which the AU, can be maintained; if the measured analyte concentration is less than MAU, then data quality are unacceptable.

2.1 Principle. References 4 through 7 provide background material on infrared spectroscopy and quantitative analysis. A summary is given in this section.

2.1.1 Infrared absorption spectroscopy is performed by directing an infrared beam through a sample to a detector. The frequency-dependent infrared absorbance of the sample is measured by comparing this detector signal (single beam spectrum) to a signal obtained without a sample in the beam path (background).

2.1.2 Most molecules absorb infrared radiation and the absorbance occurs in a characteristic and reproducible pattern. The infrared spectrum measures fundamental molecular properties and a compound can be identified from its infrared spectrum alone.

2.1.3 Within constraints, there is a linear relationship between infrared absorption and compound concentration. If this frequency dependent relationship (absorptivity) is known (measured), it can be used to determine compound concentration in a sample mixture.

2.1.4 Absorptivity is measured by preparing, in the laboratory, standard samples of compounds at known concentrations and measuring the FTIR "reference spectra" of these standard samples. These "reference spectra" are then used in sample analysis: (1) Compounds are detected by matching sample absorbance bands with bands in reference spectra, and (2) concentrations are measured by comparing sample band intensities with reference band intensities.

2.1.5 This method is self-validating provided that the results meet the performance requirement of the QA spike in sections 8.6.2 and 9.0 of this method, and results from a previous method validation study support the use of this method in the application.

1.2.3.1 The absorbance for a given concentration can be decreased by decreasing the path length or by diluting the sample. There is no practical upper limit to the measurement range.

2.2.1 The digitized infrared spectrum of the sample is measured by comparing reference spectra and interferent spectra. The baseline noise of the system shall be measured in each analytical region to determine the MAU of the instrument configuration for each analyte and interferent (MIU).

2.2.2 The digitized infrared spectrum of the sample is measured by comparing reference spectra and interferent spectra. The baseline noise of the system shall be measured in each analytical region to determine the MAU of the instrument configuration for each analyte and interferent (MIU).

2.2.3 Data quality for the application shall be determined, in part, by measuring the RMS (root mean square) noise level in each analytical spectral region (appendix C of the Protocol). The RMS noise is defined as the RMS of the absorbance values in an analytical region from the mean absorbance value in the region.

2.2.4 The MAU is the minimum analyte concentration for which the AU, can be maintained; if the measured analyte concentration is less than MAU, then data quality are unacceptable.

2.2.5 The MAU is the minimum analyte concentration for which the AU, can be maintained; if the measured analyte concentration is less than MAU, then data quality are unacceptable.

3.1.4 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.1.5 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.1.6 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.2.1 The absorbance for a given concentration can be decreased by decreasing the path length or by diluting the sample. There is no practical upper limit to the measurement range.

3.2.2 The absorbance for a given concentration can be decreased by decreasing the path length or by diluting the sample. There is no practical upper limit to the measurement range.

3.2.3 The absorbance for a given concentration can be decreased by decreasing the path length or by diluting the sample. There is no practical upper limit to the measurement range.

3.3.1 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.3.2 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.3.3 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.4.1 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.4.2 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.4.3 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.5.1 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.5.2 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

3.5.3 Measurement objectives shall be established by the choice of detection limit (DL) and analytical uncertainty (AU) for each analyte.

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Section 3.0 Definitions

See appendix A of the Protocol for definitions relating to infrared spectroscopy. Additional definitions are given in sections 3.1 through 3.20.

3.1 Analyte. A compound that this method is used to measure. The term ''target analyte'' is also used. This method is multi-component and a number of analytes can be targeted for a test.

3.2 Reference Spectrum. Infrared spectrum of an analyte prepared under controlled, documented, and reproducible laboratory conditions according to procedures in section 4.6 of the Protocol. A library of reference spectra is used to measure analytes in gas samples.

3.3 Standard Spectrum. A spectrum that has been prepared from a reference spectrum through a (documented) mathematical operation. A common example is de-resolving of reference spectra to lower-resolution standard spectra (Protocol, appendix K to the addendum of this method). Standard spectra, prepared by approved, and documented, procedures can be used as reference spectra for analysis.

3.4 Concentration. In this method concentration is expressed as a molar concentration, in ppm-meters, or in (ppm-meters)/K, where K is the absolute temperature (Kelvin). The latter units allow the direct comparison of concentrations from systems using different optical configurations or sampling temperatures.

3.5 Interferant. A compound in the sample matrix whose infrared spectrum overlaps with part of an analyte spectrum. The most accurate analyte measurements are achieved when reference spectra of interferants are used in the quantitative analysis with the analyte reference spectra. The presence of an interferant can increase the analytical uncertainty in the measured analyte concentration.

3.6 Gas Cell. A gas containment cell that can be evacuated. It is equipped with the optical components to pass the infrared beam through the sample to the detector. Important cell features include: path length (or range if variable), temperature range, materials of construction, and total gas volume.

3.7 Sampling System. Equipment used to extract the sample from the test location and transport the sample gas to the FTIR analyzer. This includes sample conditioning systems.

3.8 Sample Analysis. The process of interpreting the infrared spectra to obtain sample analyte concentrations. This process is usually automated using a software routine employing a classical least squares (cLS), partial least squares (pLS), or K- or P-matrix method.

3.9 One hundred percent line. A double beam transmittance spectrum obtained by combining two background single beam spectra. Ideally, this line is equal to 100 percent transmittance (or zero absorbance) at every frequency in the spectrum. Practically, a zero absorbance line is used to measure the baseline noise in the spectrum.

3.10 Background Deviation. A deviation from 100 percent transmittance in any region of the 100 percent line. Deviations greater than ±5 percent in an analytical region are unacceptable (absorbance of 0.021 to 0.022). Such deviations indicate a change in the instrument throughput relative to the background single beam.

3.11 Batch Sampling. A procedure where spectra of discreet, static samples are collected. The gas cell is filled with sample and the cell is isolated. The spectrum is collected. Finally, the cell is evacuated to prepare for the next sample.

3.12 Continuous Sampling. A procedure where spectra are collected while sample gas...
is flowing through the cell at a measured rate.

3.13 Sampling resolution. The spectral resolution used to collect sample spectra.

3.14 Truncation. Measurements to determine a number of interferogram data points by deleting points farthest from the center burst (zero path difference, ZPD).

3.15 Zero filling. The addition of points to the interferogram. The position of each added point is interpolated from neighboring real data points. Zero filling adds no information to the interferogram, but affects line shapes in the absorbance spectrum (and possibly analytical results).

3.16 Reference CTS. Calibration Transfer Standard spectra that were collected with reference spectra.

3.17 CTS Standard. CTS spectrum produced by applying a de-resolution procedure to a reference CTS.

3.18 Test CTS. CTS spectra collected at the sampling resolution using the same optical configuration as for sample spectra. Test spectra help verify the resolution, temperature and path length of the FTIR system.

3.19 RMSD. Root Mean Square Difference, defined in EPA FTIR Protocol, appendix A.

3.20 Sensitivity. The noise-limited compound-dependent detection limit for the FTIR system configuration. This is estimated by the MAU. It depends on the RMSD in an analytical region of a zero absorbance line.

3.21 Quantitation Limit. The lower limit of detection for the FTIR system configuration in the sample spectra. This is estimated by mathematically subtracting scaled reference spectra of analytes and interferences from sample spectra, then measuring the RMSD in an analytical region of the subtracted spectrum. Since the noise in subtracted sample spectra may be much greater than in a zero absorbance spectrum, the quantitation limit is generally much higher than the sensitivity. Removing spectral interferences from the sample or improving the spectral subtraction can lower the quantitation limit toward (but not below) the sensitivity.

3.22 Independent Sample. A unique volume of sample gas; there is no mixing of gas between two consecutive independent samples. In continuous sampling two independent samples are separated by at least 5 cell volumes. The interval between independent measurements depends on the cell volume and the sample flow rate (through the cell).

3.23 Measurement. A single spectrum of flue gas contained in the FTIR cell.

3.24 Run. A run consists of a series of measurements. At a minimum a run includes 8 independent measurements spaced over 1 hour.

3.25 Validation. Validation of FTIR measurements is described in sections 13.0 through 13.4 of this method. Validation is used to verify the test procedures for measuring specific analytes at a source. Validation provides proof that the method works under certain test conditions.

3.26 Validation Run. A validation run consists of at least 24 independent samples. Half of the samples are spiked and half are not spiked. The length of the run is determined by the interval between independent samples.

3.27 Spiking. Screening is used when there is little or no available information about a source. The purpose of screening is to determine what analytes are emitted and to obtain information about important sample characteristics such as moisture, temperature, and interferences. Screening results are semi-quantitative (estimated concentrations) or qualitative (identification only). Various optical and sampling configurations may be used. Sample conditioning systems may be evaluated for their effectiveness in removing interferences. It is unnecessary to perform a complete run under any set of sampling conditions. Spiking is not necessary, but spiking can be a useful screening tool for evaluating the sampling system, especially if a reactive or soluble analyte is used for the spike.

3.28 Emissions Test. An FTIR emissions test is performed according specific sampling and analytical procedures. These procedures, for the target analytes and the source, are based on previous screening and validation results. Emission results are quantitative. A QA spike (sections 8.6.2 and 9.2 of this method) is performed under each set of sampling conditions using a representative analyte. Flow, gas temperature and diluent data are recorded concurrently with the FTIR measurements to provide mass emission rates for detected compounds.

3.29 Surrogate. A surrogate is a compound that is used in a QA spike procedure (section 8.6.2 of this method) to represent other compounds. The chemical and physical properties of a surrogate shall be similar to the compounds it is chosen to represent. Under given sampling conditions, usually a single sampling factor is of primary concern for measuring the target analytes: for example, the surrogate spike results can be representative for analytes that are more reactive, more soluble, have a lower absorptivity, or have a lower vapor pressure than the surrogate itself.

4.0 Interferences

Interferences are divided into two classifications: analytical and sampling.

4.1 Analytical Interferences. An analytical interference is a spectral feature that complicates (in extreme cases may prevent) the analysis of an analyte. Analytical interferences are classified as background or spectral interference.

4.1.1 Background Interference. This results from a change in throughput relative to the
single beam background. It is corrected by collecting a new background and proceeding with the test. In severe instances the cause must be identified and corrected. Potential causes include: (1) deposits on reflective surfaces or transmitting windows, (2) changes in detector sensitivity, (3) a change in the infrared source output, or (4) failure in the instrument electronics. In routine sampling throughput may degrade over several hours. Periodically a new background must be collected, but no other corrective action will be required.

4.1.2 Spectral Interference. This results from the presence of interfering compound(s) (interferant) in the sample. Interferent spectral features overlap analyte spectral features. Any compound with an infrared spectrum, including analytes, can potentially be an interferent. The Protocol measures absorbance band overlap in each analytical region to determine if potential interferents shall be classified as known interferents (FTIR Protocol, section 4.9 and appendix B). Water vapor and CO₂ are common spectral interferents. Both of these compounds have strong infrared spectra and are present in many sample matrices at high concentrations relative to analytes. The extent of interference depends on the (1) interferent concentration, (2) analyte concentration, and (3) the degree of band overlap. Choosing an alternate analytical region can minimize or avoid the spectral interference. For example, CO₂ interferes with the analysis of the 670 cm⁻¹ benzene band. However, benzene can also be measured near 3000 cm⁻¹ (with less sensitivity).

4.2 Sampling System Interferences. These prevent analytes from reaching the instrument. The analyte spike procedure is designed to measure sampling system interference, if any.

4.2.1 Temperature. A temperature that is too low causes condensation of analytes or water vapor. The materials of the sampling system and the FTIR gas cell usually set the upper limit of temperature.

4.2.2 Reactive Species. Anything that reacts with analytes. Some analytes, like formaldehyde, polymerize at lower temperatures, preventing adsorption of analytes, and the analysis of the 670 cm⁻¹ benzene band. However, benzene can also be measured near 3000 cm⁻¹ (with less sensitivity).

4.2.3 Materials. Poor choice of material for probe, or sampling line may remove some analytes. For example, HF reacts with glass components.

5.0 Safety

The hazards of performing this method are those associated with any stack sampling method and the same precautions shall be followed. Many HAPs are suspected carcinogens or present other serious health risks. Exposure to these compounds should be avoided in all circumstances. For instructions on the safe handling of any particular compound, refer to its material safety data sheet. When using analyte standards, always ensure that gases are properly vented and that the gas handling system is leak free. (Always perform a leak check with the system under maximum vacuum and, again, with the system at greater than ambient pressure.) Refer to section 8.2 of this method for leak check procedures. This method does not address all of the potential safety risks associated with its use. Anyone performing this method must follow safety and health practices consistent with applicable legal requirements and with prudent practice for each application.

5.0 Equipment and Supplies

NOTE: Mention of trade names or specific products does not constitute endorsement by the Environmental Protection Agency.

The equipment and supplies are based on the schematic of a sampling system shown in Figure 1. Either the batch or continuous sampling procedures may be used with this sampling system. Alternative sampling configurations may also be used, provided that the data quality objectives are met as determined in the post-analysis evaluation. Other equipment or supplies may be necessary, depending on the design of the sampling system or the specific target analytes.

6.1. Sampling Probe. Glass, stainless steel, or other appropriate material of sufficient length and physical integrity to sustain heating, prevent adsorption of analytes, and to transport analytes to the infrared gas cell. Special materials or configurations may be required in some applications. For instance, high stack sample temperatures may require special steel or cooling the probe. For very high moisture sources it may be desirable to use a dilution probe.

6.2. Particulate Filters. A glass wool plug (optional) inserted at the probe tip (for large particulate removal) and a filter (required) rated for 99 percent removal efficiency at 1-micron (e.g., Balston®) connected at the outlet of the heated probe.

6.3. Sampling Line/Heating System. Heated (sufficient to prevent condensation) stainless steel, polytetrafluoroethylene, or other material inert to the analytes.

6.4. Gas Distribution Manifold. A heated manifold allowing the operator to control flows of gas standards and samples directly to the FTIR system or through sample conditioning systems. Usually includes heated flow meter, heated valve for selecting and sending sample to the analyzer, and a bypass vent. This is typically constructed of stainless steel tubing and fittings, and high-temperature valves.

6.5. Stainless Steel Tubing. Type 316, appropriate diameter (e.g., 38 in.) and length for...
heated connections. Higher grade stainless steel may be desirable in some applications.

6.1 Calibration/Analyte Spike Assembly. A three way valve assembly (or equivalent) to introduce analyte or surrogate spikes into the sampling system at the outlet of the probe upstream of the out-of-stack particulate filter and the FTIR analytical system.

6.2 Mass Flow Meter (MFM). These are used for measuring analyte spike flow. The MFM shall be calibrated in the range of 0 to $2\frac{\text{L}}{\text{min}}$ and be accurate to ± 2 percent (or better) of the flow meter span.

6.3 Gas Regulators. Appropriate for individual gas standards.

6.4 Polytetrafluoroethylene Tubing. Diameter (e.g., % in.) and length suitable to connect cylinder regulators to gas standard manifold.

6.5 Sample Pump. A leak-free pump (e.g., KNF®), with by-pass valve, capable of producing a sample flow rate of at least 10 $\frac{\text{L}}{\text{min}}$ through 100 ft of sample line. If the pump is positioned upstream of the distribution manifold and FTIR system, use a heated pump that is constructed from materials non-reactive to the analytes. If the pump is located downstream of the FTIR system, the gas cell sample pressure will be lower than ambient pressure and it must be recorded at regular intervals.

6.6 Gas Sample Manifold. Secondary manifold to control sample flow at the inlet to the FTIR manifold. This is optional, but includes a by-pass vent and heated rotometer.

6.7 Rotameter. A 0 to 20 $\frac{\text{L}}{\text{min}}$ rotometer. This meter need not be calibrated.

6.8 Gas Pressure Gauge. Capable of measuring pressure from 0 to 1000 mmHg to within ± 2.5 mmHg (e.g., Baratron®).

6.9 Temperature Gauge. Capable of measuring the cell temperature to within ± 2°C.

6.10 Sample Conditioning. One option is a condenser system, which is used for moisture removal. This can be helpful in the measurement of some analytes. Other sample conditioning procedures may be devised for the removal of moisture or other interfering species.

6.11 FTIR Analytical System. Spectrometer and detector, capable of measuring the analytes to the chosen detection limit. The system shall include a personal computer with compatible software allowing automated collection of spectra.

6.12 FTIR Cell Pump. Required for the batch sampling technique, capable of evacuating the FTIR cell volume within 2 minutes. The pumping speed shall allow the operator to obtain 8 sample spectra in 1 hour.

6.13 Absolute Pressure Gauge. Capable of measuring pressure from 0 to 1000 mmHg to within ± 2.5 mmHg (e.g., Baratron®).

6.14 FTIR Cell Volume. Required for the batch sampling technique, capable of evacuating the FTIR cell volume within 2 minutes. The pumping speed shall allow the operator to obtain 8 sample spectra in 1 hour.

6.15 FTIR Cell Temperature. Capable of measuring the cell temperature to within ± 2°C.

6.16 Temperature Control. The analyte spike procedure of section 9.2 of this method, the QA spike procedure of section 8.6 of this method, and the validation procedure of section 13 of this method demonstrate whether the sample conditioning affects analyte concentrations. Alternatively, measurements can be made with two parallel FTIR systems; one measuring conditioned sample, the other measuring unconditioned sample.

6.17.2 Another option is sample dilution. The dilution factor measurement must be documented and accounted for in the reported concentrations. An alternative to dilution is to lower the sensitivity of the FTIR system by decreasing the cell path length, or to use a short-path cell in conjunction with a long path cell to measure more than one concentration range.

7.0 Reagents and Standards

7.1 Analyte(s) and Tracer Gas. Obtain a certified gas cylinder mixture containing all of the analyte(s) at concentrations within ± 2 percent of the emission source levels (expressed in ppm-meter/K). If practical, the analyte standard cylinder shall also contain the tracer gas at a concentration which gives a measurable absorbance at a dilution factor of at least 10:1. Two ppm SF₆ is sufficient for a path length of 22 meters at 250°F.

7.2 Calibration Transfer Standard(s). Select the calibration transfer standards (CTS) according to section 4.5 of the FTIR Protocol. Obtain a National Institute of Standards and Technology (NIST) traceable gravimetric standard of the CTS (± 2 percent).

7.3 Reference Spectra. Obtain reference spectra for each analyte, interferant, surrogate, CTS, and tracer. If EPA reference spectra are not available, use reference spectra prepared according to procedures in section 4.6 of the EPA FTIR Protocol.

8.0 Sampling and Analysis Procedure

Three types of testing can be performed: (1) Screening, (2) emissions test, and (3) validation. Each is defined in section 3 of this method. Determine the purpose(s) of the FTIR test. Test requirements include: (a) AU, DL, overall fractional uncertainty, OFU, maximum expected concentration (CMAX), and TAN for each, (b) potential interferants, (c) sampling system factors, e.g., minimum absolute cell pressure, $P_{\text{abs}}$, FTIR cell volume $V_{\text{cell}}$, estimated sample absorption pathlength, $L_{\text{abs}}$, signal integration time (t$_{\text{int}}$), minimum instrumental linewidth, MIL, fractional error, and (d) analytical regions, e.g., m=1 to M, lower wavenumber position, FLₘ, center wavenumber position, FCₘ, and upper wavenumber position, FUₘ, plus interferants, upper wavenumber position of the CTS absorption band, $F_{\text{LU}}$, lower wavenumber position of the CTS absorption band, $F_{\text{LL}}$, wavenumber range FNU to FNL. If necessary, sample and acquire an initial spectrum. From analysis of this preliminary spectrum determine a suitable operational path length. Set up the sampling train as shown in Figure 1 or use an appropriate alternative configuration. Sections 8.1 through 8.11 of this method provide guidance on pre-
test calculations in the EPA protocol, sampling and analytical procedures, and post-test protocol calculations.

8.1 Pretest Preparations and Evaluations. Use sections 4.0 of the FTIR Protocol, determine the optimum sampling system configuration for measuring the target analytes. Use available information to make reasonable assumptions about moisture content and other interferences.

8.1.1 Analytes. Select the required detection limit (DL) and the maximum permissible analytical uncertainty (AU) for each analyte (labeled from 1 to i). Estimate, if possible, the maximum expected concentration for each analyte, CMAX. The expected measurement range is fixed by DL and CMAX, for each analyte (i).

8.1.2 Potential Interferants. List the potential interferants. This usually includes water vapor and CO₂, but may also include some analytes and other compounds.

8.1.3 Optical Configuration. Choose an optical configuration that can measure all of the analytes within the absorbance range of 0.01 to 1.0 (this may require more than one path length). Use Protocol sections 4.3 to 4.8 for guidance in choosing a configuration and measuring CTS.

8.1.4 Fractional Reproducibility Uncertainty (FRU). The FRU is determined for each analyte by comparing CTS spectra taken before and after the reference spectra were measured. The EPA para-xylene reference spectra were collected on 10/31/91 and 11/01/91 with corresponding CTS spectra "cts1031a," and "cts1101b." The CTS spectra are used to estimate the reproducibility (FRU) in the system that was used to collect the references. The FRU must be < AU. Appendix E of the protocol is used to calculate the FRU from CTS spectra. Figure 2 plots results for 0.25 cm⁻³ CTS spectra in EPA reference library: S₀, (cts1101b−cts1031a), and S₁ [(cts1101b−cts1031a)/2]. The RMSD (SRMS) is calculated in the same region of the averaged CTS spectrum, S₀.

8.1.5 Known Interferants. Use appendix B of the EPA FTIR Protocol.

8.1.6 Calculate the Minimum Analyte Uncertainty, MAU (section 1.3 of this method discusses MAU and protocol appendix D gives the MAU procedure). The MAU for each analyte, i, and each analytical region, m, depend on the RMS noise.

8.1.7 Analytical Program. See FTIR Protocol, section 4.10. Prepare computer program based on the chosen analytical technique. Use as input reference spectra of all target analytes and expected interferants. Reference spectra of additional compounds shall also be included in the program if their presence (even if transient) in the samples is considered possible. The program output shall be in ppm (or ppb) and shall be corrected for differences between the reference path length, Lᵣ, temperature, Tᵣ, and pressure, Pᵣ, and the conditions used for collecting the sample spectra. If sampling is performed at ambient pressure, then any pressure correction is usually small relative to corrections for path length and temperature, and may be neglected.

8.2 Leak-Check

8.2.1 Sampling System. A typical FTIR extractive sampling train is shown in Figure 1. Leak check from the probe tip to pump outlet as follows: Connect a 0-to 250-mL/min rate meter (rotameter or bubble meter) to the outlet of the pump. Close off the inlet to the probe, and record the leak rate. The leak rate shall be ≤ 100 mL/min.

8.2.2 Analytical System Leak check. Leak check the FTIR cell under vacuum and under pressure (greater than ambient). Leak check connecting tubing and inlet manifold under pressure.

8.2.2.1 For the evacuated sample technique, close the valve to the FTIR cell, and evacuate the absorption cell to the minimum absolute pressure Pᵥᵥ. Close the valve to the pump, and determine the change in pressure ΔPᵥ after 2 minutes.

8.2.2.2 For both the evacuated sample and purging techniques, pressurize the system to about 100 mmHg above atmospheric pressure. Isolate the pump and determine the change in pressure ΔPᵥ after 2 minutes.

8.2.2.3 Measure the barometric pressure, Pᵥ, in mmHg.

8.2.2.4 Determine the percent leak volume %Vᵥ, for the signal integration time tᵥ, and for ΔPᵥ max, i.e., the larger of ΔPᵥ or ΔPᵥ. as follows:

\[
\%Vᵥ = \frac{50 \cdot tᵥ \cdot ΔPᵥ_{\text{max}}}{Pᵥ \cdot SS}
\]

where 50=100% divided by the leak-check time of 2 minutes. 8.2.2.5 Leak volumes in excess of 4 percent of the FTIR system volume Vᵥᵥ are unacceptable.

8.3 Detector Linearity. Once an optical configuration is chosen, use one of the procedures of sections 8.3.1 through 8.3.3 to verify that the detector response is linear. If the detector response is not linear, decrease the aperture, or attenuate the infrared beam. After a change in the instrument configuration perform a linearity check until it is demonstrated that the detector response is linear.

8.3.1 Vary the power incident on the detector by modifying the aperture setting.

Measure the background and CTS at three instrument aperture settings: (1) at the aperture setting to be used in the testing, (2) at one half this aperture and (3) at twice the proposed testing aperture. Compare the
three CTS spectra. CTS band areas shall agree to within the uncertainty of the cylinder standard and the RMSD noise in the system. If test aperture is the maximum aperture and the RMSD noise in the IR throughput by half. Collect a second background and CTS at the smaller aperture setting and compare the spectra again. Use neutral density filters to attenuate the infrared beam. Set up the FTIR system as it will be used in the test measurements. Collect a CTS spectrum. Use a neutral density filter to attenuate the infrared beam (either immediately after the source or the interferometer) to approximately 1/4 its original intensity. Collect a second CTS spectrum. Use another filter to attenuate the infrared beam to approximately 1/2 its original intensity. Collect a third background and CTS spectrum. Compare the CTS spectra. CTS band areas shall agree to within the uncertainty of the cylinder standard and the RMSD noise in the system.

8.3.3 Observe the single beam instrument response in a frequency region where the detector response is "flat" and equal to zero in these regions.

8.4 Data Storage Requirements. All field test spectra shall be stored on a computer disk and a second backup copy must stored on a separate disk. The stored information includes sample interferograms, processed absorbance spectra, background interferograms, CTS sample interferograms and CTS absorbance spectra. Additionally, documentation of all sample conditions, instrument settings, and test records must be recorded on hard copy or on computer medium. Table 1 gives a sample presentation of documentation.

8.5 Background Spectrum. Evacuate the gas cell to ≤5 mmHg absolute pressure, and fill with dry nitrogen gas to ambient pressure (or purge the cell with 10 volumes of dry nitrogen). Collect a background spectrum. Use another filter to attenuate the infrared beam to approximately 1/4 its original intensity. Collect a second background and CTS spectrum. Compare the CTS spectra. CTS band areas shall agree to within the uncertainty of the cylinder standard and the RMSD noise in the system.

8.5.1 Interference Spectra. If possible, collect spectra of known and suspected major interferences using the same optical system that will be used in the field measurements. This can be done on-site or earlier. A number of gases, e.g. CO₂, SO₂, CO, NH₃, are readily available from cylinder gas suppliers.

8.5.2 Water vapor spectra can be prepared by the following procedure. Fill a sample tube with distilled water. Evacuate above the sample and remove dissolved gasses by alternately freezing and thawing the water while evacuating. Allow water vapor into the FTIR cell, then dilute to atmospheric pressure with nitrogen or dry air. If quantitative water spectra are required, follow the reference spectrum procedure for neat samples (protocol, section 4.6). Often, interference spectra need not be quantitative, but for best results the absorbance must be comparable to the interference absorbance in the sample spectra.

8.6 Pre-Test Calibrations

8.6.1 Calibration Transfer Standard. Evacuate the gas cell to ≤5 mmHg absolute pressure, and fill the FTIR cell to atmospheric pressure with the CTS gas. Alternatively, purge the cell with 10 cell volumes of CTS gas. (If purge is used, verify that the CTS concentration in the cell is stable by collecting two spectra 2 minutes apart as the CTS gas continues to flow. If the absorbance in the second spectrum is no greater than in the first, within the uncertainty of the gas standard, then this can be used as the CTS spectrum.) Record the spectrum.

8.6.2 QA Spike. This procedure assumes that the method has been validated for at least some of the target analytes at the source. For emissions testing perform a QA spike. Use a certified standard, if possible, of an analyte, which has been validated at the source. One analyte standard can serve as a QA surrogate for other analytes which are less reactive or less soluble than the standard. Perform the spike procedure of section 9.2 of this method. Record spectra of at least three independent (section 3.2 of this method) spiked samples. Calculate the spiked component of the analyte concentration. If the average spiked concentration is within 0.7 to 1.3 times the expected concentration, then proceed with the testing. If applicable, apply the correction factor from the Method 301 of this appendix validation test (not the result from the QA spike).

8.7 Sampling. If analyte concentrations vary rapidly with time, continuous sampling is preferable using the smallest cell volume, fastest sampling rate and fastest spectra collection rate possible. Continuous sampling requires the least operator intervention even without an automated sampling system. For continuous monitoring at one location over long periods, Continuous sampling is preferred. Batch sampling and continuous static sampling are used for screening and performing test runs of finite duration. Either technique is preferred for sampling several locations in a matter of days. Batch sampling gives reasonably good time resolution and ensures that each spectrum measures a discreet (and unique) sample volume. Continuous static (and continuous) sampling provides a very stable background over long periods. Like batch sampling, continuous static
sampling also ensures that each spectrum measures a unique sample volume. It is essential that the leak check procedure under vacuum (section 8.2 of this method) is passed if the batch sampling procedure is used. It is essential that the leak check procedure under positive pressure is passed if the continuous static or continuous sampling procedures are used. The sampling techniques are described in sections 8.7.1 through 8.7.2 of this method.

8.7.1 Batch Sampling. Evacuate the absorbance cell to 5 mmHg absolute pressure. Fill the cell with exhaust gas to ambient pressure, isolate the cell, and record the spectrum. Before taking the next sample, evacuate the cell until no spectral evidence of sample absorption remains. Repeat this procedure to collect eight spectra of separate samples in 1 hour.

8.7.2 Continuous Static Sampling. Purge the FTIR cell with 10 cell volumes of sample gas. Isolate the cell, collect the spectrum of the static sample and record the pressure. Before measuring the next sample, purge the cell with 10 more cell volumes of sample gas.

8.8 Sampling QA and Reporting

8.8.1 Sample integration times shall be sufficient to achieve the required signal-to-noise ratio. Obtain an absorbance spectrum by filling the cell with N2. Measure the RMSD in each analytical region in this absorbance spectrum. Verify that the number of scans used is sufficient to achieve the target MAU.

8.8.2 Assign a unique file name to each spectrum.

8.8.3 Store two copies of sample interferograms and processed spectra on separate computer disks.

8.8.4 For each sample spectrum, document the sampling conditions, the sampling time (while the cell was being filled), the time the spectrum was recorded, the instrumental conditions (path length, temperature, pressure, resolution, signal integration time), and the spectral file name. Keep a hard copy of these data sheets.

8.9 Signal Transmittance. While sampling, monitor the signal transmittance. If signal transmittance (relative to the background) changes by 5 percent or more (absorbance = \pm 0.02 to 0.00) in any analytical spectral region, obtain a new background spectrum.

8.10 Post-test CTS. After the sampling run, record another CTS spectrum.

8.11 Post-test QA

8.11.1 Inspect the sample spectra immediately after the run to verify that the gas matrix composition was close to the expected (assumed) gas matrix.

8.11.2 Verify that the sampling and instrumental parameters were appropriate for the conditions encountered. For example, if the moisture is much greater than anticipated, it may be necessary to use a shorter path length or dilute the sample.

8.11.3 Compare the pre- and post-test CTS spectra. The peak absorbance in pre- and post-test CTS must be \pm 5 percent of the mean value. See appendix E of the FTIR Protocol.

9.0 Quality Control

Use analyte spiking (sections 8.6.2, 9.2 and 13.0 of this method) to verify that the sampling system can transport the analytes from the probe to the FTIR system.

9.1 Spike Materials. Use a certified standard (accurate to \pm 2 percent) of the target analyte, if one can be obtained. If a certified standard cannot be obtained, follow the procedures in section 4.6.2.2 of the FTIR Protocol.

9.2 Spiking Procedure. QA spiking (section 8.6.2 of this method) is a calibration procedure used before testing. QA spiking involves following the spike procedure of sections 9.2.1 through 9.2.3 of this method to obtain at least three spiked samples. The analyte concentrations in the spiked samples shall be compared to the expected spike concentration to verify that the sampling/analytical system is working properly. Usually, when QA spiking is used, the method has already been validated at a similar source for the analyte in question. The QA spike demonstrates that the validated sampling/analytical conditions are being duplicated. If the QA spike fails then the sampling/analytical system shall be repaired before testing proceeds. The method validation procedure (section 13.0 of this method) involves a more extensive use of the analyte spike procedure of sections 9.2.1 through 9.2.3 of this method. Spectra of at least 12 independent spiked and 12 independent unspiked samples are recorded. The concentration results are analyzed statistically to determine if there is a systematic bias in the method for measuring a particular analyte. If there is a systematic bias, within the limits allowed by Method 301 of this appendix, then a correction factor shall be applied to the analytical results. If the systematic bias is greater than the allowed limits, this method is not valid and cannot be used.

9.2.1 Introduce the spike/tracer gas at a constant flow rate of \pm 10 percent of the total sample flow, when possible.

NOTE: Use the rotameter at the end of the sampling train to estimate the required spike/tracer gas flow rate.

Use a flow device, e.g., mass flow meter (+2 percent), to monitor the spike flow rate. Record the spike flow rate every 10 minutes.

9.2.2 Determine the response time (RT) of the system by continuously collecting spectra of the spiked effluent until the spectrum of the spiked component is constant for 5 minutes. The RT is the interval from the
first measurement until the spike becomes constant. Wait for twice the duration of the RT, then collect spectra of two independent spiked gas samples. Duplicate analyses of the spiked concentration shall be within 5 percent of the mean of the two measurements.

\[
CS = DF \times \text{Spike}_{\text{dir}} + \text{Unspike} \times (1 - DF)
\]  

\(DF = \text{Dilution factor of the spike gas; this value shall be} \geq 10\).  
\(SF_{\text{6(dir)}} = SF_{\text{a}} \) (or tracer gas) concentration measured directly in undiluted spike gas.  
\(SF_{\text{6(spk)}} = \text{Diluted SF}_{\text{a}} \) (or tracer gas) concentration measured in a spiked sample.  
\(\text{Spike}_{\text{dir}} = \text{Concentration of the analyte in the spike standard measured by filling the FTIR cell directly.} \)  
\(\text{Unspike} = \text{Native concentration of analytes in unspiked samples.} \)  

10.0 Calibration and Standardization  

10.1 Signal-to-Noise Ratio (S/N). The RMSD in the noise must be less than one tenth of the minimum analyte peak absorbance in each analytical region. For example if the minimum peak absorbance is 0.01 at the required DL, then RMSD measured over the entire analytical region must be \(\leq 0.001\).  

10.2 Absorbance Path length. Verify the absorbance path length by comparing reference CTS spectra to test CTS spectra. See appendix E of the FTIR Protocol.  

10.3 Instrument Resolution. Measure the line width of appropriate test CTS band(s) to verify instrument resolution. Alternatively, compare CTS spectra to a reference CTS spectrum, if available, measured at the nominal resolution.  

10.4 Apodization Function. In transforming the sample interferograms to absorbance spectra use the same apodization function that was used in transforming the reference spectra.  

10.5 FTIR Cell Volume. Evacuate the cell to \(\leq 5\) mmHg. Measure the initial absolute temperature \((T_i)\) and absolute pressure \((P_i)\). Connect a wet test meter (or a calibrated dry gas meter), and slowly draw room air into the cell. Measure the meter volume \((V_m)\), meter absolute temperature \((T_m)\), and meter absolute pressure \((P_m)\); and the cell final absolute temperature \((T_f)\) and absolute pressure \((P_f)\). Calculate the FTIR cell volume \(V_{SS}\), including that of the connecting tubing, as follows:

\[
V_{SS} = \frac{\left(\frac{P_m}{T_m}\right) - \left(\frac{P_f}{T_f}\right)}{T_f - T_i}
\]  

11.0 Data Analysis and Calculations  

Analyte concentrations shall be measured using reference spectra from the EPA FTIR spectral library. When EPA library spectra are not available, the procedures in section 4.6 of the Protocol shall be followed to prepare reference spectra of all the target analytes.  

11.1 Spectral De-resolution. Reference spectra can be converted to lower resolution standard spectra (section 3.3 of this method) by truncating the original reference sample and background interferograms. Appendix K of the FTIR Protocol gives specific de-resolution procedures. Deresolved spectra shall be transformed using the same apodization function and level of zero filling as the sample spectra. Additionally, pre-test FTIR protocol calculations (e.g., FRU, MAU, FCU) shall be performed using the de-resolved standard spectra.  

11.2 Data Analysis. Various analytical programs are available for relating sample absorbance to a concentration standard. Calculated concentrations shall be verified by analyzing residual baselines after mathematically subtracting scaled reference spectra from the sample spectra. A full description of the data analysis and calculations is contained in the FTIR Protocol (sections 4.0, 5.0, 6.0 and appendices). Correct the calculated concentrations in the sample spectra for differences in absorption path length and temperature between the reference and sample spectra using equation 6.

\[
C_{\text{corr}} = \left(\frac{L_C}{L_s}\right) \left(\frac{T_h}{T_s}\right) \left(\frac{P_L}{P_s}\right) C_{\text{calc}}
\]  

Where:  
\(C_{\text{corr}} = \text{Concentration, corrected for path length.} \)
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\[ C_{\text{in}} = \text{Concentration, initial calculation (output of the analytical program designed for the compound).} \]
\[ L_s = \text{Reference spectra path length.} \]
\[ L = \text{Sample spectra path length.} \]
\[ T_r = \text{Absolute temperature of the sample gas, K.} \]
\[ T_s = \text{Absolute gas temperature of reference spectra, K.} \]
\[ P_c = \text{Sample cell pressure.} \]
\[ P_r = \text{Reference spectrum sample pressure.} \]

12.0 Method Performance

12.1 Spectral Quality. Refer to the FTIR Protocol appendices for analytical requirements, evaluation of data quality, and analysis of uncertainty.

12.2 Sampling QA/QC. The analyte spike procedure of section 9 of this method, the QA spike of section 8.6.2 of this method, and the validation procedure of section 13 of this method are used to evaluate the performance of the sampling system and to quantify sampling system effects, if any, on the measured concentrations. This method is self-verifying provided that the results meet the performance requirement of the QA spike in sections 9.0 and 8.6.2 of this method and results from a previous method validation study support the use of this method in the application. Several factors can contribute to uncertainty in the measurement of spiked samples. Factors which can be controlled to provide better accuracy in the spiking procedure are listed in sections 12.2.1 through 12.2.4 of this method.

12.2.1 Flow meter. An accurate mass flow meter is accurate to \( \pm 1\% \) of its span. If a flow of 1 L/min is monitored with such a MFM, which is calibrated in the range of 0-5 L/min, the flow measurement has an uncertainty of 5 percent. This may be improved by re-calibrating the meter at the specific flow rate to be used.

12.2.2 Calibration gas. Usually the calibration standard is certified to within \( \pm 2\% \) percent. With reactive analytes, such as HCl, the certified accuracy in a commercially available standard may be no better than \( \pm 5\% \).

12.2.3 Temperature. Temperature measurements of the cell shall be quite accurate. If practical, it is preferable to measure sample temperature directly, by inserting a thermocouple into the cell chamber instead of monitoring the cell outer wall temperature.

12.2.4 Pressure. Accuracy depends on the accuracy of the barometer, but fluctuations in pressure throughout a day may be as much as 2.5 percent due to weather variations.

13.0 Method Validation Procedure

This validation procedure, which is based on EPA Method 301 (40 CFR part 63, appendix A), may be used to validate this method for the analytes in a gas matrix. Validation at one source may also apply to another type of source, if it can be shown that the exhaust gas characteristics are similar at both sources.

13.1 Section 5.3 of Method 301 (40 CFR part 63, appendix A), the Analyte Spike procedure, is used with these modifications. The statistical analysis of the results follows section 6.3 of EPA Method 301. Section 3 of this method defines terms that are not defined in Method 301.

13.1.1 The analyte spike is performed dynamically. This means the spike flow is continuous and constant as spiked samples are measured.

13.1.2 The spike gas is introduced at the back of the sample probe.

13.1.3 Spiked effluent is carried through all sampling components downstream of the probe.

13.1.4 A single FTIR system (or more) may be used to collect and analyze spectra (not quadruplicate integrated sampling trains).

13.1.5 All of the validation measurements are performed sequentially in a single "run" (section 3.26 of this method).

13.1.6 The measurements analyzed statistically are each independent (section 3.22 of this method).

13.1.7 A validation data set can consist of more than 12 spiked and 12 unspiked measurements.

13.2 Batch Sampling. The procedure in sections 13.2.1 through 13.2.2 may be used for stable processes. If process emissions are highly variable, the procedure in section 13.2.3 shall be used.

13.2.1 With a single FTIR instrument and sampling system, begin by collecting spectra of two unspiked samples. Introduce the spike flow into the sampling system and allow 10 cell volumes to purge the sampling system and FTIR cell. Collect spectra of two spiked samples. Turn off the spike and allow 10 cell volumes of unspiked sample to purge the FTIR cell. Repeat this procedure until the 24 (or more) samples are collected.

13.2.2 In batch sampling, collect spectra of 24 distinct samples. (Each distinct sample consists of filling the cell to ambient pressure after the cell has been evacuated.)

13.2.3 Alternatively, a separate probe assembly, line, and sample pump can be used for spiked sample. Verify and document that sampling conditions are the same in both the spiked and the unspiked sampling systems. This can be done by wrapping both sample lines in the same heated bundle. Keep the same flow rate in both sample lines. Measure samples in sequence in pairs. After two spiked samples are measured, evacuate the FTIR cell, and take the manifold valve so that spiked sample flows to the FTIR cell. Allow the connecting line from the manifold to the FTIR cell to purge thoroughly (the
time depends on the line length and flow rate. Collect a pair of spiked samples. Repeat the procedure until at least 24 measurements are completed.

13.3 Simultaneous Measurements With Two FTIR Systems. If unspiked effluent concentrations of the target analyte(s) vary significantly with time, it may be desirable to perform synchronized measurements of spiked and unspiked sample. Use two FTIR systems, each with its own cell and sampling system to perform simultaneous spiked and unspiked measurements. The optical configurations shall be similar, if possible. The sampling configurations shall be the same. One sampling system and FTIR analyzer shall be used to measure spiked effluent. The other sampling system and FTIR analyzer shall be used to measure unspiked flue gas. Both systems shall use the same sampling procedure (i.e., batch or continuous).

13.3.1 If batch sampling is used, synchronize the cell evacuation, cell filling, and collection of spectra. Fill both cells at the same rate (in cell volumes per unit time).

13.3.2 If continuous sampling is used, adjust the sample flow through each gas cell so that the same number of cell volumes pass through each cell in a given time (i.e., $T_C = T_C$).

13.4 Statistical Treatment. The statistical procedure of EPA Method 301 of this appendix, section 6.3 is used to evaluate the bias and precision. For FTIR testing a validation “run” is defined as spectra of 24 independent samples, $12$ of which are spiked with the analyte(s) and $12$ of which are not spiked.

13.4.1 Bias. Determine the bias (defined by EPA Method 301 of this appendix, section 6.3.2) using equation 7:

$$B = S_m - CS \quad (7)$$

Where:

- $B$ = Bias at spike level.
- $S_m$ = Mean concentration of the analyte spiked samples.
- $CS$ = Expected concentration of the spiked samples.

13.4.2 Correction Factor. Use section 6.3.2.2 of Method 301 of this appendix to evaluate the statistical significance of the bias. If it is determined that the bias is significant, then use section 6.3.3 of Method 301 to calculate a correction factor (CF). Analytical results of the test method are multiplied by the correction factor, if $0.7 \leq CF \leq 1.3$. If is determined that the bias is significant and $CF > 1.3$ percent, then the test method is considered to "not valid."

13.4.3 If measurements do not pass validation, evaluate the sampling system, instrument configuration, and analytical system to determine if improper set-up or a malfunction was the cause. If so, repair the system and repeat the validation.

14.0 Pollution Prevention. The extracted sample gas is vented outside the enclosure containing the FTIR system and gas manifold after the analysis. In typical method applications the vented sample volume is a small fraction of the source volumetric flow and its composition is identical to that emitted from the source. When analyte spiking is used, spiked pollutants are vented with the extracted sample gas. Approximately $1.6 \times 10^{-4}$ to $3.2 \times 10^{-4}$ lbs of a single HAP may be vented to the atmosphere in a typical validation run of 3 hours. (This assumes a molar mass of 50 to 100g, spike rate of 1.0 L/min, and a standard concentration of 100 ppm). Minimize emissions by keeping the spike flow off when not in use.

15.0 Waste Management.

Small volumes of laboratory gas standards can be vented through a laboratory hood. Neat samples must be packed and disposed according to applicable regulations. Surplus materials may be returned to supplier for disposal.

16.0 References.


### Table 1.—Example Presentation of Sampling Documentation

<table>
<thead>
<tr>
<th>Sample time</th>
<th>Spectrum file</th>
<th>Background file name</th>
<th>Sample conditioning</th>
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Environmental Protection Agency
Figure 1. Extractive FTIR sampling system.

Figure 2. Fractional Reproducibility. Top: average of cts1031a and cts1101b. Bottom: Reference spectrum of p-xylene.
Environmental Protection Agency

ADDENDUM TO TEST METHOD 320—PROTOCOL FOR THE USE OF EXTRACTIVE FOURIER TRANSFORM IR SPECTROSCOPY FOR THE ANALYSES OF GASEOUS EMISSIONS FROM STATIONARY SOURCES

1.0 Introduction

The purpose of this addendum is to set general guidelines for the use of modern FTIR spectroscopic methods for the analysis of gas samples extracted from the effluent of stationary emission sources. This addendum outlines techniques for developing and evaluating such methods and sets basic requirements for reporting and quality assurance procedures.

1.1 Nomenclature

1.1.1 Appendix A to this addendum lists definitions of the symbols and terms used in this Protocol, many of which have been taken directly from American Society for Testing and Materials (ASTM) publication E 131-90a, entitled “Terminology Relating to Molecular Spectroscopy.”

1.1.2 Except in the case of background spectra or where otherwise noted, the term “spectrum” refers to a double-beam spectrum in units of absorbance vs. wavenumber (cm⁻¹).

1.1.3 The term “Study” in this addendum refers to a publication that has been subjected to EPA peer review.

2.0 Applicability and Analytical Principle

2.1 Applicability. This Protocol applies to the determination of compound-specific concentrations in single- and multiple-component gas phase samples using double-beam absorption spectroscopy in the mid-infrared band. It does not specifically address other FTIR applications, such as single-beam spectroscopy, analysis of open-path (non-enclosed) samples, and continuous measurement techniques. If multiple spectrometers, absorption cells, or instrumental linewidths are used in such analyses, each distinct operational configuration of the system must be evaluated separately according to this Protocol.

2.2 Analytical Principle

2.2.1 In the mid-infrared band, most molecules exhibit characteristic gas phase absorption spectra that may be recorded by FTIR systems. Such systems consist of a source of mid-infrared radiation, an interferometer, an enclosed sample cell of known absorption pathlength, an infrared detector, optical elements for the transfer of infrared radiation between components, and gas flow control and measurement components. Adjunct and integral computer systems are used for controlling the instrument, processing the signal, and for performing both Fourier transforms and quantitative analyses of spectral data.

2.2.2 The absorption spectra of pure gases and of mixtures of gases are described by a linear absorbance theory referred to as Beer’s Law. Using this law, modern FTIR systems use computerized analytical programs to quantify compounds by comparing the absorption spectra of known (reference) gas samples to the absorption spectrum of the sample gas. Some standard mathematical techniques used for comparisons are classical least squares, inverse least squares, cross-correlation, factor analysis, and partial least squares. Reference A describes several of these techniques, as well as additional techniques, such as differentiation methods, linear baseline corrections, and non-linear absorbance corrections.

3.0 General Principles of Protocol Requirements

The characteristics that distinguish FTIR systems from gas analyzers used in instrumental gas analysis methods (e.g., Methods 6C and 7E of appendix A to part 60 of this chapter) are: (1) Computers are necessary to obtain and analyze data; (2) chemical concentrations can be quantified using previously recorded infrared reference spectra; and (3) analytical assumptions and results, including possible effects of interfering compounds, can be evaluated after the quantitative analysis. The following general principles and requirements of this Protocol are based on these characteristics.

3.1 Verifiability and Reproducibility of Results. Store all data and document data analysis techniques sufficient to allow an independent agent to reproduce the analytical results from the raw interferometric data.

3.2 Transfer of Reference Spectra. To determine whether reference spectra recorded under one set of conditions (e.g., optical bench, instrumental linewidth, absorption pathlength, detector performance, pressure, and temperature) can be used to analyze sample spectra taken under a different set of conditions, quantitatively compare “calibration transfer standards” (CTS) and reference spectra as described in this Protocol.

NOTE: The CTS may, but need not, include analytes of interest. To effect this, record the absorption spectra of the CTS (a) immediately before and immediately after recording reference spectra and (b) immediately after recording sample spectra.

3.3 Evaluation of FTIR Analyses. The applicability, accuracy, and precision of FTIR measurements are influenced by a number of interrelated factors, which may be divided into two classes:

3.3.1 Sample-independent Factors. Examples are system configuration and performance (e.g., detector sensitivity and infrared source output), quality and applicability of reference absorption spectra, and type of
mathematical analyses of the spectra. These factors define the fundamental limitations of FTIR measurements for a given system configuration. These limitations may be estimated from evaluations of the system before samples are available. For example, the detection limit for the absorbing compound under a given set of conditions may be estimated from the system noise level and the strength of a particular absorption band. Similarly, the accuracy of measurements may be estimated from the analysis of the reference spectra.

3.3.2 Sample-Dependent Factors. Examples are spectral interferants (e.g., water vapor and CO₂) or the overlap of spectral features of different compounds and contamination deposits on reflective surfaces or transmitting windows. To maximize the effectiveness of the mathematical techniques used in spectral analysis, identification of interferants (a standard initial step) and analysis of samples (includes effect of other analytical errors) are necessary. Thus, the Protocol requires post-analysis calculation of measurement concentration uncertainties for the detection of these potential sources of measurement error.

4.0 Pre-Test Preparations and Evaluations

Before testing, demonstrate the suitability of FTIR spectrometry for the desired application according to the procedures of this section.

4.1 Identify Test Requirements. Identify and record the test requirements described in sections 4.1.1 through 4.1.4 of this addendum. These values set the desired or required goals of the proposed analysis; the description of methods for determining whether these goals are actually met during the analysis comprises the majority of this Protocol.

4.1.1 Analytes (specific chemical species). Label the analytes from i = 1 to N.

4.1.2 Analytical uncertainty limit (AU). The AU is the maximum permissible fractional uncertainty of analysis for the i\(^{\text{th}}\) analyte concentration, expressed as a fraction of the analyte concentration in the sample.

4.1.3 Required detection limit for each analyte (DL\(_i\), ppm). The detection limit is the lowest concentration of an analyte for which its overall fractional uncertainty (OFU) is required to be less than its analytical uncertainty limit (AU).

4.1.4 Maximum expected concentration of each analyte (C\(_{\text{MAX}}\), ppm).

4.2 Identify Potential Interferants. Considering the chemistry of the process or results of previous studies, identify potential interferants, i.e., the major effluent constituents and any relatively minor effluent constituents that possess either strong absorption characteristics or strong structural similarities to any analyte of interest. Label them 1 through N, where the subscript “i” pertains to potential interferants. Estimate the concentrations of these compounds in the effluent (CPOT\(_i\), ppm).

4.3 Select and Evaluate the Sampling System. Considering the source, e.g., temperature and pressure profiles, moisture content, analyte characteristics, and particulate concentration, select the equipment for extracting gas samples. Recommended are a particulate filter, heating system to maintain sample temperature above the dew point for all sample constituents at all points within the sampling system (including the filter), and sample conditioning system (e.g., coolers, water-permeable membranes that remove water or other compounds from the sample, and dilution devices) to remove spectral interferants or to protect the sampling and analytical components. Determine the minimum absolute sample system pressure (P\(_{\text{abs}}\), mmHg) and the infrared absorption cell volume (V\(_{\text{ss}}\), liter). Select the techniques and/or equipment for the measurement of sample pressures and temperatures.

4.4 Select Spectroscopic System. Select a spectroscopic configuration for the application. Approximate the absorption pathlength (L\(_{\text{sc}}\), meter), sample pressure (P\(_{\text{sc}}\), kPa), absolute sample temperature T\(_{\text{sc}}\), and signal integration period (t\(_{\text{int}}\), seconds) for the analysis. Specify the nominal minimum instrumental linewidth (MIL) of the system. Verify that the fractional error at the approximate values P\(_{\text{sc}}\) and T\(_{\text{sc}}\) is less than one half the smallest value AU, (see section 4.1.2 of this addendum).

4.5 Select Calibration Transfer Standards (CTS's). Select CTS's that meet the criteria listed in sections 4.5.1, 4.5.2, and 4.5.3 of this addendum. Note: It may be necessary to choose preliminary analytical regions (see section 4.7 of this addendum), identify the minimum analyte linewidths, or estimate the system noise level (see section 4.12 of this addendum) before selecting the CTS. More than one compound may be needed to meet the criteria; if so, obtain separate cylinders for each compound.

4.5.1 The central wavenumber position of each analytical region shall lie within 25 percent of the wavenumber position of at least one CTS absorption band.

4.5.2 The absorption bands in section 4.5.1 of this addendum shall exhibit peak absorbances greater than ten times the value RMS\(_{\text{EST}}\) (see section 4.12 of this addendum) but less than 1.5 absorbance units.

4.5.3 At least one absorption CTS band within the operating range of the FTIR instrument shall have an instrument-independent linewidth no greater than the narrowest analyte absorption band. Perform and document measurements or cite Studies to determine analyte and CTS compound linewidths.
4.5.4 For each analytical region, specify the upper and lower wavenumber positions (FFU and FFLO, respectively) that bracket the CTS absorption band or bands for the associated analytical region. Specify the wavenumber range, FROM to FNL, containing the absorption band that meets the criterion of section 4.5.3 of this addendum.

4.5.5 Associate, whenever possible, a single set of CTS gas cylinders with a set of reference spectra. Replacement CTS gas cylinders shall contain the same compounds at concentrations within 5 percent of that of the original CTS cylinders; the entire absorption spectra (not individual spectral segments) of the replacement gas shall be scaled by a factor between 0.95 and 1.05 to match the original CTS spectra.

4.6 Prepare Reference Spectra

**NOTE:** Reference spectra are available in a permanent soft copy from the EPA spectral library on the EMTIC (Emission Measurement Technical Information Center) computer bulletin board; they may be used if applicable.

4.6.1 Select the reference absorption pathlength (L) of the cell.

4.6.2 Obtain or prepare a set of chemical standards for each analyte, potential and known spectral interferants, and CTS. Select the concentrations of the chemical standards to correspond to the top of the desired range.

4.6.2.1 Commercially-Prepared Chemical Standards. Chemical standards for many compounds may be obtained from independent sources, such as a specialty gas manufacturer, chemical company, or commercial laboratory. These standards (accurate to within ±2 percent) shall be prepared according to EPA Traceability Protocol (see Reference D) or shall be traceable to NIST standards. Obtain from the supplier an estimate of the stability of the analyte concentration. Obtain and follow all of the supplier's recommendations for recertifying the analyte concentration.

4.6.2.2 Self-Prepared Chemical Standards. Chemical standards may be prepared by diluting certified commercially prepared chemical gases or pure analytes with ultra-pure carrier (UPC) grade nitrogen according to the barometric and volumetric techniques generally described in Reference A, section 4.6.6.

4.6.3 Record a set of the absorption spectra of the CTS (R1), then a set of the reference spectra at two or more concentrations in duplicate over the desired range (the top of the range must be less than 10 times that of the bottom), followed by a second set of CTS spectra (R2). (If self-prepared standards are used, see section 4.6.5 of this addendum before disposing of any of the standards.) The maximum accepted standard concentration-pathlength product (ASCPP) for each compound shall be higher than the maximum estimated concentration-pathlength products for both analytes and known interferants in the effluent gas. For each analyte, the minimum ASCPP shall be no greater than ten times the concentration-pathlength product of that analyte at its required detection limit.

4.6.4 Permanently store the background and interferograms in digitized form. Document details of the mathematical process for generating the spectra from these interferograms. Record the sample pressure (P), sample temperature (T), reference absorption pathlength (L), and interferogram signal integration period (IS). Signal integration periods for the background interferograms shall be 2τIR. Values of P, L, and τ shall not deviate by more than ±1 percent from the time of recording [R1] to that of recording [R2].

4.6.5 If self-prepared chemical standards are employed and spectra of only two concentrations are recorded for one or more compounds, verify the accuracy of the dilution technique by analyzing the prepared standards for those compounds with a secondary (non-FTIR) technique in accordance with sections 4.6.5.1 through 4.6.5.4 of this addendum.

4.6.5.1 Record the response of the secondary technique to each of the four standards prepared.

4.6.5.2 Perform a linear regression of the response values (dependant variable) versus the accepted standard concentration (ASC) values (independent variable), with the regression constrained to pass through the zero-response, zero ASC point.

4.6.5.3 Calculate the average fractional difference between the actual response values and the regression-predicted values (those calculated from the regression line using the four ASC values as the independent variable).

4.6.5.4 If the average fractional difference value calculated in section 4.6.5.3 of this addendum is larger for any compound than the corresponding AU, the dilution technique is not sufficiently accurate and the reference spectra prepared are not valid for the analyte.

4.7 Select Analytical Regions. Using the general considerations in section 7 of Reference A and the spectral characteristics of the analytes and interferants, select the analytical regions for the application. Label them m = 1 to M. Specify the lower, center and upper wavenumber positions of each analytical region (FFLO, FC, and FFH, respectively). Specify the analytes and interferants which exhibit absorption in each region.

4.8 Determine Fractional Reproducibility Uncertainties. Using appendix E of this addendum, calculate the fractional reproducibility uncertainty for each analyte (FRU) from a comparison of [R1] and [R2]. If FRU > AU, for any analyte, the reference spectra generated.
in accordance with section 4.6 of this addendum are not valid for the application.

4.9 Identify Known Interferants. Using appendix B of this addendum, determine which potential interferants affect the analyte concentration determinations. Relabel these potential interferants as "known" interferants, and designate these compounds from \( k = 1 \) to \( k \). Appendix B to this addendum also provides criteria for determining whether the selected analytical regions are suitable.

4.10 Prepare Computerized Analytical Programs

4.10.1 Choose or devise mathematical techniques (e.g., classical least squares, inverse least squares, cross-correlation, and factor analysis) based on equation 4 of Reference A that are appropriate for analyzing spectral data by comparison with reference spectra.

4.10.2 Following the general recommendations of Reference A, prepare a computer program or set of programs that analyzes all of the analytes and known interferants, based on the selected analytical regions (section 4.7 of this addendum) and the prepared reference spectra (section 4.6 of this addendum). Specify the baseline correction technique (e.g., determining the slope and intercept of a linear baseline contribution in each analytical region) for each analytical region, including all relevant wavenumber positions.

4.10.3 Use programs that provide as output (at the reference absorption pathlength \( L_s \), reference gas temperature \( T_s \), and reference gas pressure \( P_s \)) the analyte concentrations, the known interferent concentrations, and the baseline slope and intercept values. If the sample absorption pathlength \( L_s \), sample gas temperature \( T_s \), or sample gas pressure \( P_s \) during the actual sample analyses differ from \( L_s \), \( T_s \), and \( P_s \), use a program or set of programs that applies multiplicative corrections to the derived concentrations to account for these variations, and that provides as output both the corrected and uncorrected values. Include in the report of the analysis (see section 7.0 of this addendum) the details of any transformations applied to the original reference spectra and data spectra alone.

4.11 Determine the Fractional Calibration Uncertainty. Calculate the fractional calibration uncertainty for each analyte (FCU) according to appendix F of this addendum, and compare these values to the fractional uncertainty limits (AU; see section 4.1.2 of this addendum). If \( FCU > AU \), either the reference spectra or analytical programs for that analyte are unsuitable.

4.12 Verify System Configuration Suitability. Using appendix C of this addendum, measure or obtain estimates of the noise level (\( \text{RMS}_{\text{est}} \), absorbance) of the FTIR system. Alternatively, construct the complete spectrometer system and determine the values \( \text{RMS}_{\text{est}} \) using appendix G of this addendum. Estimate the minimum measurement uncertainty for each analyte (MAU, ppm) and known interferent (MIU, ppm) using appendix D of this addendum. Verify that (a) MAU, < (AU)(DL), FRUi < AU, and FCUi < AU for each analyte and that (b) the CTS chosen meets the requirements listed in sections 4.5.1 through 4.5.5 of this addendum.

5.0 Sampling and Analysis Procedure

5.1 Analysis System Assembly and Leak-Test. Assemble the analysis system. Allow sufficient time for all system components to reach the desired temperature. Then, determine the leak-rate \( (L_u) \) and leak volume \( (V_u) \), where \( V_u = L_u \cdot T_u \cdot S \). Leak volumes shall be ≤ 4 percent of \( V_s \).

5.2 Verify Instrumental Performance. Measure the noise level of the system in each analytical region using the procedure of appendix G of this addendum. If any noise level is higher than that estimated for the system in section 4.12 of this addendum, repeat the calculations of appendix D of this addendum and verify that the requirements of section 4.12 of this addendum are met; if they are not, adjust or repair the instrument and repeat this section.

5.3 Determine the Sample Absorption Pathlength.

Record a background spectrum. Then, fill the absorption cell with CTS at the pressure \( P_u \) and record a set of CTS spectra [R3]. Store the background and unscaled CTS single beam interferograms and spectra. Using appendix H of this addendum, calculate the sample absorption pathlength \( L_s \) for each analytical region. The values \( L_s \) shall not differ from the approximated sample pathlength \( L_s' \) (see section 4.4 of this addendum) by more than 5 percent.

5.4 Record Sample Spectrum. Connect the sample line to the source. Either evacuate the absorption cell to an absolute pressure below 5 mmHg before extracting a sample from the effluent stream into the absorption cell, or pump at least ten cell volumes of sample through the cell before obtaining a sample. Record the sample pressure \( P_s \). Generate the absorbance spectrum of the sample. Store the background and sample single beam interferograms, and document the process by which the absorbance spectra are generated from these data. (If necessary, apply the spectral transformations developed in section 5.6.2 of this addendum). The resulting sample spectrum is referred to below as \( S_s \).

NOTE: Multiple sample spectra may be recorded according to the procedures of section...
5.4 of this addendum before performing sections 5.5 and 5.6 of this addendum.

5.5 Quantify Analyte Concentrations. Calculate the unscaled analyte concentrations RSA and unscaled interferent concentrations RSI using the programs developed in section 4 of this addendum. To correct for pathlength and pressure variations between the reference and sample spectra, calculate the scaling factor, R_{LPS} using equation A.1.

\[ R_{LPS} = \frac{(L_R P_R T_S)}{(L_S P_S T_R)} \]  
(A.1)

Calculate the final analyte and interferant concentrations RSA and RSI using equations A.2 and A.3.

\[ RSA_i = R_{LPS} RUA_i \]  
(A.2)

\[ RSI_k = R_{LPS} RUI_k \]  
(A.3)

5.6 Determine Fractional Analysis Uncertainty. Fill the absorption cell with CTS at the pressure P_c. Record a set of CTS spectra (R4). Store the background and CTS single beam interferograms. Using appendix H of this addendum, calculate the fractional analysis uncertainty (FAU) for each analytical region. If the FAU indicated for any analytical region is greater than the required accuracy requirements determined in sections 4.1.1 through 4.1.4 of this addendum, then comparisons to previously recorded reference spectra are invalid in that analytical region, and the analyst shall perform one or both of the procedures of sections 5.6.1 through 5.6.2 of this addendum.

5.6.1 Perform instrumental checks and adjust the instrument to restore its performance to acceptable levels. If adjustments are made, repeat sections 5.3, 5.4 (except for the recording of a sample spectrum), and 5.5 of this addendum to demonstrate that acceptable uncertainties are obtained in all analytical regions.

5.6.2 Apply appropriate mathematical transformations (e.g., frequency shifting, zero-filling, apodization, smoothing) to the spectra (or to the interferograms upon which the spectra are based) generated during the procedures of section 5.3 of this addendum. Document these transformations and their reproducibility. Do not apply multiplicative scaling of the spectra, or any set of transformations that is mathematically equivalent to multiplicative scaling. Different transformations may be applied to different analytical regions. Frequency shifts shall be less than one-half the minimum instrumental linewidth, and must be applied to all spectral data points in an analytical region. The mathematical transformations may be retained for the analysis if they are also applied to the appropriate analytical regions of all sample spectra recorded, and if all original sample spectra are digitally stored. Repeat sections 5.3, 5.4 (except the recording of a sample spectrum), and 5.5 of this addendum to demonstrate that these transformations lead to acceptable calculated concentration uncertainties in all analytical regions.

6.0 Post-Analysis Evaluations

Estimate the overall accuracy of the analyses performed in accordance with sections 5.1 through 5.6 of this addendum using the procedures of sections 6.1 through 6.3 of this addendum.

6.1 Qualitatively Confirm the Assumed Matrix. Examine each analytical region of the sample spectrum for spectral evidence of un-expected or unidentified interferants. If found, identify the interfering compounds (see Reference C for guidance) and add them to the list of known interferants. Repeat the procedures of section 4 of this addendum to include the interferants in the uncertainty calculations and analysis procedures. Verify that the MAU and FCU values do not increase beyond acceptable levels for the application requirements. Re-calculate the analyte concentrations (section 5.5 of this addendum) in the affected analytical regions.

6.2 Quantitatively Evaluate Fractional Model Uncertainty (FMU). Perform the procedures of either section 6.2.1 or 6.2.2 of this addendum:

6.2.1 Using appendix I of this addendum, determine the fractional model error (FMU) for each analyte.

6.2.2 Provide statistically determined uncertainties FMU for each analyte which are equivalent to two standard deviations at the 95 percent confidence level. Such determinations, if employed, must be based on mathematical examinations of the pertinent sample spectra (not the reference spectra alone). Include in the report of the analysis (see section 7.0 of this addendum) a complete description of the determination of the concentration uncertainties.

6.3 Estimate Overall Concentration Uncertainty (OCU). Using appendix J of this addendum, determine the overall concentration uncertainty (OCU) for each analyte. If the OCU is larger than the required accuracy for any analyte, repeat sections 4 and 6 of this addendum.

7.0 Reporting Requirements
[Documentation pertaining to virtually all the procedures of sections 4, 5, and 6 will be required. Software copies of reference spectra and sample spectra will be retained for some minimum time following the actual testing.]

8.0 References
(A) Standard Practices for General Techniques of Infrared Quantitative Analysis
Interferogram, $I(\sigma)$

Baseline means any line drawn on an absorption spectrum to establish a reference point that represents a function of the radiant power incident on a sample at a given wavelength.

Beer's law means the direct proportionality of the absorbance of a compound in a homogeneous sample to its concentration.

Calibration transfer standard (CTS) gas means a gas standard of a compound used to achieve and/or demonstrate suitable quantitative agreement between sample spectra and the reference spectra; see section 4.5.1 of this addendum.

Infrared means the portion of the electromagnetic spectrum containing wavelengths from approximately 0.78 to 800 microns.

Interferogram, $I(\nu)$ means record of the modulated component of the interference spectrum to establish a reference spectrum to achieve and/or demonstrate suitable quantitative agreement between sample spectra and the reference spectra; see section 4.5.1 of this addendum.

Compound means a substance possessing a distinct, unique molecular structure.

Concentration means the quantity of a compound contained in a unit quantity of sample. The unit “ppm” (number, or mole, basis) is recommended.

Concentration-pathlength product means the mathematical product of concentration of the species and absorption pathlength. For reference spectra, this is a known quantity; for sample spectra, it is the quantity directly determined from Beer's law. The units “centimeters-ppm” or “meters-ppm” are recommended.

Derivative absorption spectrum means a plot of rate of change of absorbance or of any function of absorbance with respect to wavelength or any function of wavelength.

Double beam spectrum means a transmission or absorbance spectrum derived by dividing the sample single beam spectrum by the background spectrum.

NOTE: The term “double-beam” is used elsewhere to denote a spectrum in which the sample and background interferograms are collected simultaneously along physically distinct absorption paths. Here, the term denotes a spectrum in which the sample and background interferograms are collected at different times along the same absorption path.

Fast Fourier transform (FFT) means a method of speeding up the computation of a discrete FT by factoring the data into sparse matrices containing mostly zeros.

Flyback means interferometer motion during which no data are recorded.

Fourier transform (FT) means the mathematical process for converting an amplitude-time spectrum to an amplitude-frequency spectrum, or vice versa.

Fourier transform infrared (FTIR) spectrometer means an analytical system that employs a source of mid-infrared radiation, an interferometer, an enclosed sample cell of known absorption pathlength, an infrared detector, optical elements that transfer infrared radiation between components, and a computer system. The time-domain detector response (interferogram) is processed by a Fourier transform to yield a representation of the detector response vs. infrared frequency.

NOTE: When FTIR spectrometers are interfaced with other instruments, a slash should be used to denote the interface; e.g., GC/FTIR; HPCL/FTIR, and the use of FTIR should be explicit; i.e., FTIR not IR.

Frequency, $\nu$ means the number of cycles per unit time.

Infrared means the portion of the electromagnetic spectrum containing wavelengths from approximately 0.78 to 800 microns.

NOTE: The term “double-beam” is used elsewhere to denote a spectrum in which the sample and background interferograms are collected simultaneously along physically distinct absorption paths. Here, the term denotes a spectrum in which the sample and background interferograms are collected at different times along the same absorption path.

Fast Fourier transform (FFT) means a method of speeding up the computation of a discrete FT by factoring the data into sparse matrices containing mostly zeros.

Flyback means interferometer motion during which no data are recorded.

Fourier transform (FT) means the mathematical process for converting an amplitude-time spectrum to an amplitude-frequency spectrum, or vice versa.

Fourier transform infrared (FTIR) spectrometer means an analytical system that employs a source of mid-infrared radiation, an interferometer, an enclosed sample cell of known absorption pathlength, an infrared detector, optical elements that transfer infrared radiation between components, and a computer system. The time-domain detector response (interferogram) is processed by a Fourier transform to yield a representation of the detector response vs. infrared frequency.

NOTE: When FTIR spectrometers are interfaced with other instruments, a slash should be used to denote the interface; e.g., GC/FTIR; HPCL/FTIR, and the use of FTIR should be explicit; i.e., FTIR not IR.

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Frequency, $\nu$ means the number of cycles per unit time.
signal measured as a function of retardation by the detector.

Interferometer means device that divides a beam of radiant energy into two or more paths, generates an optical path difference between the beams, and combines them in order to produce repetitive interference maxima and minima as the optical retardation is varied.

Linewidth means the full width at half maximum of an absorption band in units of wavenumbers (cm⁻¹).

Mid-infrared means the region of the electromagnetic spectrum from approximately 400 to 5000 cm⁻¹.

Reference spectra means absorption spectra of gases with known chemical compositions, recorded at a known absorption pathlength, which are used in the quantitative analysis of gas samples.

Retardation, σ means optical path difference between two beams in an interferometer; also known as “optical path difference” or “optical retardation.”

Scan means digital representation of the detector output obtained during one complete motion of the interferometer’s moving assembly or assemblies.

Scaling means application of a multiplicative factor to the absorbance values in a spectrum.

Single beam spectrum means Fourier-transformed interferogram, representing the detector response vs. wavenumber.

Standard reference material means a reference material, the composition or properties of which are certified by a recognized standardizing agency or group.

Transmittance, T means the ratio of radiant power transmitted by the sample to the radiant power incident on the sample. Estimated in FTIR spectroscopy by forming the ratio of the single-beam sample and background spectra.

Wavenumber, ν means the number of waves per unit length.

Zero-filling means the addition of zero-valued points to the end of a measured interferogram.

NOTE: Performing the FT of a zero-filled interferogram results in correctly interpolated points in the computed spectrum.

A.2 Definitions of Mathematical Symbols
The symbols used in equations in this protocol are defined as follows:

1. A, absorbance = the logarithm to the base 10 of the reciprocal of the transmittance (T).

A = \log_{10}\left(\frac{1}{T}\right) = -\log_{10} T

2. AAI = band area of the iⁿ analyte in the mⁿ analytical region, at the concentration (CL) corresponding to the product of its required detection limit (DL) and analytical uncertainty limit (AU).

(2) AAI = \frac{\text{band area of the } iⁿ \text{ analyte in the } mⁿ \text{ analytical region, at the concentration (CL) corresponding to the product of its required detection limit (DL) and analytical uncertainty limit (AU)}}{

3. AAV = average absorbance of the iⁿ analyte in the mⁿ analytical region, at the concentration (CL) corresponding to the product of its required detection limit (DL) and analytical uncertainty limit (AU).

(3) AAV = \frac{\text{average absorbance of the } iⁿ \text{ analyte in the } mⁿ \text{ analytical region, at the concentration (CL) corresponding to the product of its required detection limit (DL) and analytical uncertainty limit (AU)}}{

4. ASC, accepted standard concentration = the concentration value assigned to a chemical standard.

5. ASCPP, accepted standard concentration-pathlength product = for a chemical standard, the product of the ASC and the sample absorption pathlength. The units “centimeters-ppm” or “meters-ppm” are recommended.

(6) ASCPP = \text{accepted standard concentration-pathlength product = for a chemical standard, the product of the ASC and the sample absorption pathlength. The units “centimeters-ppm” or “meters-ppm” are recommended.}

6. AU, analytical uncertainty limit = the maximum permissible fractional uncertainty of analysis for the iⁿ analyte concentration, expressed as a fraction of the analyte concentration determined in the analysis.

(7) AVT = \text{average estimated total absorbance in the } mⁿ \text{ analytical region.}

7. CKWN = \text{estimated concentration of the } kⁿ \text{ known interferant.}

8. CMAX = \text{estimated maximum concentration of the } iⁿ \text{ analyte.}

9. CPOT = \text{estimated concentration of the } jⁿ \text{ potential interferant.}

10. (11) \text{DL} = \text{required detection limit = for the } iⁿ \text{ analyte, the lowest concentration of the analyte for which its overall fractional uncertainty (OFU) is required to be less than the analytical uncertainty limit (AU).}

12. FC = \text{center wavenumber position of the } mⁿ \text{ analytical region.}

13. FCU, fractional analytical uncertainty = \text{calculated uncertainty in the measured concentration of the } iⁿ \text{ analyte because of errors in the mathematical comparison of reference and sample spectra.}

14. FCU, fractional calibration uncertainty = \text{calculated uncertainty in the measured concentration of the } iⁿ \text{ analyte because of errors in Beer’s law modeling of the reference spectra concentrations.}
(15) \( FF_L = \) lower wavenumber position of the CTS absorption band associated with the \( m \)th analytical region.

(16) \( FF_U = \) upper wavenumber position of the CTS absorption band associated with the \( m \)th analytical region.

(17) \( FL_L = \) lower wavenumber position of the \( m \)th analytical region.

(18) \( FM_{U_i} = \) fractional model uncertainty = calculated uncertainty in the measured concentration of the \( i \)th analyte because of errors in the absorption model employed.

(19) \( FN_L = \) lower wavenumber position of the CTS spectrum containing an absorption band at least as narrow as the analyte absorption bands.

(20) \( FN_U = \) upper wavenumber position of the CTS spectrum containing an absorption band at least as narrow as the analyte absorption bands.

(21) \( FRU_{i} = \) fractional reproducibility uncertainty = calculated uncertainty in the measured concentration of the \( i \)th analyte because of errors in the reproducibility of spectra from the FTIR system.

(22) \( FU_L = \) upper wavenumber position of the \( m \)th analytical region.

(23) \( IA_{U} = \) band area of the \( j \)th potential interferant in the \( m \)th analytical region, at its expected concentration (CPOT).

(24) \( IA_{V_{ij}} = \) average absorbance of the \( i \)th analyte in the \( m \)th analytical region, at its expected concentration (CPOT).

(25) \( IS_{i} = \) indicated standard concentration = the concentration from the computerized analytical program for a single-compound reference spectrum for the \( i \)th analyte or \( k \)th known interferant.

(26) \( kPa = \) kilo-Pascal (see Pascal).

(27) \( L_S = \) reference absorption pathlength.

(28) \( L_S = \) actual sample absorption pathlength.

(29) \( MAU = \) mean of the MAU over the appropriate analytical regions.

(30) \( MAU_{\text{min}} = \) minimum analyte uncertainty = the calculated minimum concentration for which the analyte uncertainty limit (AU) in the measurement of the \( i \)th analyte, based on spectral data in the \( m \)th analytical region, can be maintained.

(31) \( MIU_{\text{min}} = \) minimum interferant uncertainty = the calculated minimum concentration for which the interferant uncertainty limit (IFU) in the measurement of the \( j \)th interferant, based on spectral data in the \( m \)th analytical region, can be maintained.

(32) \( MI_{U_i} = \) mean of the MIU over the appropriate analytical regions.

(33) \( MIL = \) minimum instrumental linewidth = the minimum linewidth from the FTIR system, in wavenumbers.

NOTE: The MIL of a system may be determined by observing an absorption band known (through higher resolution examinations) to be narrower than indicated by the system. The MIL is fundamentally limited by the retardation of the interferometer, but is also affected by other operational parameters (e.g., the choice of apodization).

(34) \( N_i = \) number of interferants.

(35) \( N_k = \) number of known interferants.

(36) \( N_{\text{scan}} = \) the number of scans averaged to obtain an interferogram.

(37) \( OF_{U_i} = \) overall fractional uncertainty in the analyte concentration determined in the analysis (OFU = MAX[FRU, FCU, FAU, FMU]).

(38) \( P_s = \) reference pressure.

(39) \( P_{\text{act}} = \) actual sample pressure.

(40) \( RMS_{\text{scan}} = \) measured noise level of the FTIR system in the \( m \)th analytical region.

(41) \( RMSD = \) root mean square difference = a measure of accuracy determined by the following equation:

\[
RMSD = \sqrt{\frac{1}{n} \sum_{i=1}^{n} e_i^2}
\]

Where:

\( n = \) the number of observations for which the accuracy is determined.

\( e_i = \) the difference between a measured value of a property and its mean value over the \( n \) observations.

NOTE: The RMSD value “between a set of \( n \) contiguous absorbance values (\( A_i \)) and the mean of the values” (\( A_M \)) is defined as

\[
RMSD = \sqrt{\frac{1}{n} \sum_{i=1}^{n} (A_i - A_M)^2}
\]

(42) \( P_{\text{min}} = \) minimum pressure of the sampling system during the sampling procedure.

(43) \( P_{\text{act}} = \) estimated sample pressure.

(44) \( P_{\text{act}} = \) actual sample pressure.

(45) \( RMS_{\text{scan}} = \) measured noise level of the FTIR system in the \( m \)th analytical region.

(46) \( RMSD = \) root mean square difference = a measure of accuracy determined by the following equation:

\[
RMSD = \sqrt{\frac{1}{n} \sum_{i=1}^{n} e_i^2}
\]

Where:

\( n = \) the number of observations for which the accuracy is determined.

\( e_i = \) the difference between a measured value of a property and its mean value over the \( n \) observations.

NOTE: The RMSD value “between a set of \( n \) contiguous absorbance values (\( A_i \)) and the mean of the values” (\( A_M \)) is defined as

\[
RMSD = \sqrt{\frac{1}{n} \sum_{i=1}^{n} (A_i - A_M)^2}
\]

(47) \( RSA_i = \) the (calculated) final concentration of the \( i \)th analyte.

(48) \( RSS_i = \) the (calculated) final concentration of the \( k \)th known interferant.

(49) \( t_{\text{scan}} = \) scan time = time used to acquire a single scan, not including flyback.

(50) \( t_{\text{scan}} = \) scan time = time used to acquire a single scan, not including flyback.

(51) \( t_{\text{scan}} = \) signal integration period used in recording reference spectra.

(52) \( t_{\text{scan}} = \) signal integration period used in recording sample spectra.

(53) \( T_S = \) absolute temperature of gases used in recording reference spectra.

(54) \( T_S = \) absolute temperature of sample gas as sample spectra are recorded.
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(55) TP, Throughput = manufacturer’s estimate of the fraction of the total infrared power transmitted by the absorption cell and transfer optics from the interferometer to the detector.

(56) \( V_{SC} \) = volume of the infrared absorption cell, including parts of attached tubing.

(57) \( W_k \) = weight used to average over analytical regions \( k \) for quantities related to the analyte \( i \); see appendix D of this addendum.

APPENDIX B TO ADDENDUM TO METHOD 320—IDENTIFYING SPECTRAL INTERFERANTS

B.1 General

B.1.1 Assume a fixed absorption pathlength equal to the value \( L_{SC}' \).

B.1.2 Use band area calculations to compare the relative absorption strengths of the analytes and potential interferants. In the \( m \)th analytical region (\( FL_m \) to \( FU_m \)), use either rectangular or trapezoidal approximations to determine the band areas described below (see Reference A, sections A.3.1 through A.3.3). Document any baseline corrections applied to the spectra.

B.1.3 Use the average total absorbance of the analytes and potential interferants in each analytical region to determine whether the analytical region is suitable for analyte concentration determinations.

NOTE: The average absorbance in an analytical region is the band area divided by the width of the analytical region in wavenumbers. The average total absorbance in an analytical region is the sum of the average absorbances of all analytes and potential interferants.

B.2 Calculations

B.2.1 Prepare spectral representations of each analyte at the concentration \( CL_i = (DL_i)(AU_i) \), where \( DL_i \) is the required detection limit and \( AU_i \) is the maximum permissible analytical uncertainty. For the \( m \)th analytical region, calculate the band area (\( AAI_{im} \)) and average absorbance (\( AAV_{im} \)) from these scaled analyte spectra.

B.2.2 Prepare spectral representations of each potential interferant at its expected concentration (\( CPOT_j \)). For the \( m \)th analytical region, calculate the band area (\( IAI_{jm} \)) and average absorbance (\( IAV_{jm} \)) from these scaled potential interferant spectra.

B.2.3 Repeat the calculation for each analytical region, and record the band area results in matrix form as indicated in Figure B.1.

B.2.4 If the band area of any potential interferant in an analytical region is greater than the one-half the band area of any analyte (i.e., \( IAI_{jm} > 0.5 AAI_{im} \) for any pair \( ij \) and any \( m \)), classify the potential interferant as a known interferant. Label the known interferants \( k = 1 \) to \( K \). Record the results in matrix form as indicated in Figure B.2.

B.2.5 Calculate the average total absorbance (\( AVT_m \)) for each analytical region and record the values in the last row of the matrix described in Figure B.2. Any analytical region where \( AVT_m > 2.0 \) is unsuitable.
### FIGURE B.1 Presentation of Potential Interferant Calculations

**Analytical Regions**

1 . . . M

**Analyte Labels**

<table>
<thead>
<tr>
<th>1</th>
<th>AAI_{11} . . . AAI_{1M}</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
</tr>
<tr>
<td>1</td>
<td>AAI_{11} . . . AAI_{1M}</td>
</tr>
</tbody>
</table>

**Potential Interferant Labels**

<table>
<thead>
<tr>
<th>1</th>
<th>IAI_{11} . . . IAI_{1M}</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
</tr>
<tr>
<td>J</td>
<td>IAI_{J1} . . . IAI_{JM}</td>
</tr>
</tbody>
</table>

### FIGURE B.2 Presentation of Known Interferant Calculations

**Analytical Regions**

1 . . . M

**Analyte Labels**

<table>
<thead>
<tr>
<th>1</th>
<th>AAI_{11} . . . AAI_{1M}</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
</tr>
<tr>
<td>1</td>
<td>AAI_{11} . . . AAI_{1M}</td>
</tr>
</tbody>
</table>

**Known Interferant Labels**

<table>
<thead>
<tr>
<th>1</th>
<th>IAI_{11} . . . IAI_{1M}</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
</tr>
<tr>
<td>K</td>
<td>IAI_{K1} . . . IAI_{KM}</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Total Average Absorbance</th>
<th>AVT_{1}</th>
<th>AVT_{n}</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>
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APPENDIX C TO ADDENDUM TO METHOD 320—
ESTIMATING NOISE LEVELS

C.1 General

C.1.1 The root-mean-square (RMS) noise level is the standard measure of noise in this addendum. The RMS noise level of a contiguous segment of a spectrum is defined as the RMS difference (RMSD) between the absorbance values which form the segment and the mean value of that segment (see appendix A of this addendum).

C.1.2 The RMS noise value in double-beam absorbance spectra is assumed to be inversely proportional to: (a) the square root of the signal integration period of the sample single beam spectra from which it is formed, and (b) the total infrared power transmitted through the interferometer and absorption cell.

C.1.3 Practically, the assumption of C.1.2 allows the RMS noise level of a complete system to be estimated from the quantities described in sections C.1.3.1 through C.1.3.4:

C.1.3.1 RMS$^{\text{MAN}}$, the noise level of the system (in absorbance units), without the absorption cell and transfer optics, under those conditions necessary to yield the specified minimum instrumental linewidth, e.g., Jacquinot stop size.

C.1.3.2 $t_{\text{MAN}}$, the manufacturer's signal integration time used to determine RMS$^{\text{MAN}}$.

C.1.3.3 $t_{\text{SS}}$, the signal integration time for the analyses.

C.1.3.4 TP, the manufacturer's estimate of the fraction of the total infrared power transmitted by the absorption cell and transfer optics from the interferometer to the detector.

C.2 Calculations

C.2.1 Obtain the values of RMS$^{\text{MAN}}$, $t_{\text{MAN}}$, and TP from the manufacturers of the equipment, or determine the noise level by direct measurements with the completely constructed system proposed in section 4 of this addendum.

C.2.2 Calculate the noise value of the system (RMS$^{\text{EST}}$) using equation C.1.

$$\text{RMS}^{\text{EST}} = \text{RMS}^{\text{MAN}} \left(\frac{t_{\text{SS}}}{t_{\text{MAN}}}\right)$$

APPENDIX D TO ADDENDUM TO METHOD 320—
ESTIMATING MINIMUM CONCENTRATION MEASUREMENT UNCERTAINTIES (MAU AND MIU)

D.1 General

Estimate the minimum concentration measurement uncertainties for the $i^{th}$ analyte (MAU$_i$) and $j^{th}$ interferant (MIU$_j$) based on the spectral data in the $m^{th}$ analytical region by comparing the analyte band area in the analytical region (AAI$_{im}$) and estimating or measuring the noise level of the system (RMS$_{EST}$ or RMS$_{SM}$).

NOTE: For a single analytical region, the MAU or MIU value is the concentration of the analyte or interferant for which the band area is equal to the product of the analytical region width (in wavenumbers) and the noise level of the system (in absorbance units). If data from more than one analytical region are used in the determination of an analyte concentration, the MAU or MIU is the mean of the separate MAU or MIU values calculated for each analytical region.

D.2 Calculations

D.2.1 For each analytical region, set RMS = RMS$_{SM}$ if measured (appendix G of this addendum), or set RMS = RMS$_{EST}$ if estimated (appendix C of this addendum).

D.2.2 For each analyte associated with the analytical region, calculate MAU$_{im}$ using equation D.1.

$$\text{MAU}_{im} = \left(\text{RMS} \cdot (\text{DL}_i) \cdot (\text{AU}_j) \right) \frac{\left(\text{FU}_m - \text{FL}_m\right)}{\text{AAI}_{im}}$$

D.2.3 If only the $m^{th}$ analytical region is used to calculate the concentration of the $i^{th}$ analyte, set MAU$_i$ = MAU$_{im}$.

D.2.4 If more than one analytical region is used to calculate the concentration of the $i^{th}$ analyte, set MAU$_i$ equal to the weighted mean of the appropriate MAU$_{im}$ values calculated above; the weight for each term in the mean is equal to the fraction of the total wavenumber range used for the calculation.
represented by each analytical region. Mathematically, if the set of analytical regions employed is \( \{m^i\} \), then the MAU for each analytical region is given by equation D.2.

\[
\text{MAU}_{ik} = \sum_{k \in \{m\}} W_{ik} \text{MAU}_{ik}
\]

where the weight \( W_{ik} \) is defined for each term in the sum as

\[
W_{ik} = (FM_k - FL_k) \left( \sum_{p \in \{m\}} (FM_p - FL_p) \right)^{-1}
\]

D.2.5 Repeat sections D.2.1 through D.2.4 of this appendix to calculate the analogous values MIU for the interferants \( j = 1 \) to \( J \).

Replace the value \( (AU_i) (DL_i) \) in equation D.1 with \( CPOT_{ij} \) and replace the value \( (AAI_j) \) in equation D.1 with \( IAI_{jm} \).

APPENDIX E TO ADDENDUM TO METHOD 320—DETERMINING FRACTIONAL REPRODUCIBILITY UNCERTAINTIES (FRU)

E.1 General

To estimate the reproducibility of the spectroscopic results of the system, compare the CTS spectra recorded before and after preparing the reference spectra. Compare the difference between the spectra to their average band area. Perform the calculation for each analytical region on the portions of the CTS spectra associated with that analytical region.

E.2 Calculations

E.2.1 The CTS spectra \( \{R_i\} \) consist of \( N \) spectra, denoted by \( S_{1i} \), \( i = 1 \) to \( N \). Similarly, the CTS spectra \( \{R_i\} \) consist of \( N \) spectra, denoted by \( S_{2i} \), \( i = 1 \) to \( N \). Each \( S_{ki} \) is the spectrum of a single compound, where \( i \) denotes the compound and \( k \) denotes the set \( \{R_k\} \) of which \( S_{ki} \) is a member. Form the spectra \( S_r \) according to \( S_r = S_{1i} - S_{2i} \) for each \( i \). Form the spectra \( S_s \) according to \( S_s = (S_{1i} + S_{2i})/2 \) for each \( i \).

E.2.2 Each analytical region \( m \) is associated with a portion of the CTS spectra \( S_{1i} \) and \( S_{2i} \), for a particular \( i \), with lower and upper wavenumber limits \( FFL_m \) and \( FFU_m \), respectively.

E.2.3 For each \( m \) and the associated \( i \), calculate the band area of \( S_s \) in the wavenumber range \( FFU_m \) to \( FFL_m \). Follow the guidelines of section B.1.2 of this addendum for this band area calculation. Denote the result by \( BAV_m \).

E.2.4 For each \( m \) and the associated \( i \), calculate the RMSD of \( S_r \) between the absorbance values and their mean in the wavenumber range \( FFU_m \) to \( FFL_m \). Denote the result by \( SRMS_m \).

E.2.5 For each analytical region \( m \), calculate \( FM_m \) using equation E.1.

\[
FM_m = \frac{SRMS_m (FFU_m - FFL_m)}{BAV_m}
\]

E.2.6 If only the \( m^\text{th} \) analytical region is used to calculate the concentration of the \( i^\text{th} \) analyte, set \( FRU_i = FM_m \).

E.2.7 If a number \( p \) of analytical regions are used to calculate the concentration of the \( i^\text{th} \) analyte, set \( FRU_i = FM_m \), equal to the weighted mean of the appropriate \( FM_m \) values calculated according to section E.2.5. Mathematically, if the set of analytical regions employed is \( \{m^i\} \), then \( FRU_i \) is given by equation E.2.

\[
FRU_i = \sum_{k \in \{m^i\}} W_{ik} FM_k
\]

where the \( W_{ik} \) are calculated as described in appendix D of this addendum.

APPENDIX F OF ADDENDUM TO METHOD 320—DETERMINING FRACTIONAL CALIBRATION UNCERTAINTIES (FCU)

F.1 General

F.1.1 The concentrations yielded by the computerized analytical program applied to each single-compound reference spectrum are defined as the indicated standard concentrations (ISC’s). The ISC values for a single compound spectrum should ideally equal the accepted standard concentration (ASC) for one analyte or interferant, and should ideally be zero for all other compounds. Variations from these results are caused by errors in the ASC values, variations from the Beer’s law (or modified Beer’s law) model
used to determine the concentrations, and noise in the spectra. When the first two effects dominate, the systematic nature of the errors is often apparent and the analyst shall take steps to correct them.

F.1.2 When the calibration error appears non-systematic, apply the procedures of sections F.2.1 through F.2.3 of this appendix to estimate the fractional calibration uncertainty (FCU) for each compound. The FCU is defined as the mean fractional error between the ASC and the ISC for all reference spectra with non-zero ASC for that compound. The FCU for each compound shall be less than the required fractional uncertainty specified in section 4.1 of this addendum.

F.1.3 The computerized analytical programs shall also be required to yield acceptably low concentrations for compounds with ISC = 0 when applied to the reference spectra. The ISC of each reference spectrum for each analyte or interferant shall not exceed that compound's minimum measurement uncertainty (MAU or MIU).

F.2 Calculations

F.2.1 Apply each analytical program to each reference spectrum. Prepare a similar table to that in Figure F.1 to present the ISC and ASC values for each analyte and interferant in each reference spectrum. Maintain the order of reference file names and compounds employed in preparing Figure F.1.

F.2.2 For all reference spectra in Figure F.1, verify that the absolute values of the ISC's are less than the compound's MAU (for analytes) or MIU (for interferants).

F.2.3 For each analyte reference spectrum, calculate the quantity (ASC±ISC)/ASC. For each analyte, calculate the mean of these values (the FCU, for the i th analyte) over all reference spectra. Prepare a similar table to that in Figure F.2 to present the FCU, and analytical uncertainty limit (AU) for each analyte.

**Figure F.1.—Presentation of Accepted Standard Concentrations (ASC's) and Indicated Standard Concentrations (ISC's)**

<table>
<thead>
<tr>
<th>Compound name</th>
<th>Reference spectrum file name</th>
<th>ASC (ppm)</th>
<th>ISC (ppm)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**Figure F.2—Presentation of Fractional Calibration Uncertainties (FCU's) and Analytical Uncertainties (AU's)**

<table>
<thead>
<tr>
<th>Analyte name</th>
<th>FCU (%)</th>
<th>AU (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**Appendix G to Addendum to Method 320—Measuring Noise Levels**

G.1 General

The root-mean-square (RMS) noise level is the standard measure of noise. The RMS noise level of a contiguous segment of a spectrum is the RMSD between the absorbance values that form the segment and the mean value of the segment (see appendix A of this addendum).


APPENDIX H OF ADDENDUM TO METHOD 320—
DETERMINING SAMPLE ABSORPTION
PATHLENGTH (Lₚ) AND FRACTIONAL ANALYTICAL
UNCERTAINTY (FAU)

H.1 General

Reference spectra recorded at absorption pathlength (Lₛ), gas pressure (Pₛ), and gas absolute temperature (Tₛ), may be used to determine analyte concentrations in samples whose spectra are recorded at conditions different from that of the reference spectra, i.e., at absorption pathlength (Lₛ), absolute temperature (Tₛ), and pressure (Pₛ). This appendix describes the calculations for estimating the fractional uncertainty (FAU) of this practice. It also describes the calculations for determining the sample absorption pathlength from comparison of CTS spectra, and for preparing spectra for further instrumental and procedural checks.

H.1.1 Before sampling, determine the sample absorption pathlength using least squares analysis. Determine the ratio Lₛ/Lₓ by comparing the spectral sets ([R₁] and [R₃]), which are recorded using the same CTS at Lₛ and Lₓ, and Tₛ and Tₓ, but both at Pₓ.

H.1.2 Determine the fractional analysis uncertainty (FAU) for each analyte by comparing a scaled CTS spectral set, recorded at Lₛ, Tₛ, and Pₛ, to the CTS reference spectra of the same gas, recorded at Lₓ, Tₓ, and Pₓ. Perform the quantitative comparison after recording the sample spectra, based on band areas of the spectra in the CTS absorbance band associated with each analyte.

$$\text{FAU} = \frac{\text{NRMS}}{\text{IA}_{AV}}$$

(H.4)

APPENDIX I TO ADDENDUM TO METHOD 320—
DETERMINING FRACTIONAL MODEL UNCERTAINTIES (FMU)

I.1 General

To prepare analytical programs for FTIR analyses, the sample constituents must first be assumed. The calculations in this appendix, based upon a simulation of the sample spectrum, shall be used to verify the appropriateness of these assumptions. The simulated spectra consist of the sum of single compound reference spectra scaled to represent their contributions to the sample absorbance spectrum; scaling factors are based on the indicated standard concentrations (ISC) and measured (sample) analyte and interferent concentrations, the sample and reference absorption pathlengths, and the sample and reference gas pressures. No bandshape correction for differences in the temperature of the sample and reference spectra gases is made; such errors are included in the FMU estimate. The actual and simulated sample spectra are quantitatively compared to determine the fractional model uncertainty; this comparison uses the reference
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spectra band areas and residuals in the difference spectrum formed from the actual and simulated sample spectra.

1.2 Calculations

1.2.1 For each analyte (with scaled concentration RSA), select a reference spectrum SAC, with indicated standard concentration ISC. Calculate the scaling factors, RA,

\[ RA_i = \frac{T_R L_P RSA_i}{T_S L_P ISC_i} \] (I.1)

Form the spectra SAC by scaling each SA, by the factor RA,

1.2.2 For each interferant, select a reference spectrum SIC, with indicated standard concentration ISC. Calculate the scaling factors, RI,

\[ RI_k = \frac{T_R L_P SIC_k}{T_S L_P ISC_k} \] (I.2)

Form the spectra SAC by scaling each SA, by the factor RI,

1.2.3 For each analytical region, determine by visual inspection which of the spectra SAC and SIC exhibit absorbance bands within the analytical region. Subtract each spectrum SAC and SIC, exhibiting absorbance from the sample spectrum S to form the spectrum SUB. To save analysis time and to avoid the introduction of unwanted noise into the subtracted spectrum, it is recommended that the calculation be made (1) only for those spectral data points within the analytical regions, and (2) for each analytical region separately using the original spectrum S.

1.2.4 For each analytical region m, calculate the RMSD of SUB between the absorbance values and their mean in the region FFU to FFL. Denote the result by RMSDm.

1.2.5 For each analyte i, calculate FMm using equation I.3.

\[ FM_m = \frac{\text{RMSD}_m (\text{FFU}_m - \text{FFL}_m)}{\text{AAL} \cdot \text{RSA}_i} \] (I.3)

for each analytical region associated with the analyte.

1.2.6 If only the m analytical region is used to calculate the concentration of the i analytical, set FMU ≡ FMm.

1.2.7 If a number of analytical regions are used to calculate the concentration of the i analytical, set FM equal to the weighted mean of the appropriate FM values calculated using equation I.3. Mathematically, if the set of analytical regions employed is (m), then the fractional model uncertainty, FMU, is given by equation I.4.

\[ FMU_i = \sum_{k=1}^{m} W_k FM_k \] (I.4)

where Wa is calculated as described in appendix D of this addendum.

APPENDIX J OF ADDENDUM TO METHOD 320—DETERMINING OVERALL CONCENTRATION UNCERTAINTIES (OCU)

The calculations in this addendum estimate the measurement uncertainties for various FTIR measurements. The lowest possible overall concentration uncertainty (OCU) for an analyte is its MAU value, which is an estimate of the absolute concentration uncertainty when spectral noise dominates the measurement error. However, if the product of the largest fractional concentration uncertainty (FRU, FCU, FAU, or FMU) and the measured concentration of an analyte exceeds the MAU for the analyte, then the OCU is this product. In mathematical terms, set OFU = MAX(FRU, FCU, FAU, FMU) and OCU = MAX(RSA • OFU, MAU).

TEST METHOD 321—MEASUREMENT OF GASEOUS HYDROGEN CHLORIDE EMISSIONS AT PORTLAND CEMENT KILNS BY FOURIER TRANSFORM INFRARED (FTIR) SPECTROSCOPY

1.0 Introduction

This method should be performed by those persons familiar with the operation of Fourier Transform Infrared (FTIR) instrumentation in the application to source sampling. This document describes the sampling procedures for use in the application of FTIR spectrometry for the determination of vapor phase hydrogen chloride (HCl) concentrations both before and after particulate matter control devices installed at Portland cement kilns. A procedure for analyte spiking is included for quality assurance. This method is considered to be self validating provided that the requirements listed in section 9 of this method are followed. The analytical procedures for interpreting infrared spectra from emission measurements are described in the "Protocol For The Use of Extractive
Fourier Transform Infrared (FTIR) Spectrometry in Analyses of Gaseous Emissions
From Stationary Industrial Sources^"^, included as an addendum to proposed Method
320 of this appendix (hereafter referred to as the “FTIR Protocol”). References 1 and 2
describe the use of FTIR spectrometry in field measurements. Sample transport presents
the principal difficulty in directly measuring HCl emissions. This identical problem must
be overcome by any extractive measurement method. HCl is reactive and water soluble.
The sampling system must be adequately designed to prevent sample condensation in the
system.

1.1 Scope and Application
This method is specifically designed for the application of FTIR Spectrometry in ex-
tractive measurements of gaseous HCl concent-
trations in portland cement kiln emis-
sions.

1.2 Applicability
This method applies to the measurement of HCl [CAS No. 7647-01-0]. This method can be
applied to the determination of HCl concentra-
tions both before and after particulate
matter control devices installed at portland
cement manufacturing facilities. This meth-
od applies to either continuous flow through
measurement (with isolated sample analysis)
or grab sampling (batch analysis). HCl is
measured using the mid-infrared spectral re-
gion for analysis (about 400 to 4000 cm^−1 or 25
to 2.5 µm). Table 1 lists the suggested analyt-
cal region for quantification of HCl taking
the interference from water vapor into con-
sideration.

<table>
<thead>
<tr>
<th>Compound</th>
<th>Analytical region (cm^−1)</th>
<th>Potential interferants</th>
</tr>
</thead>
<tbody>
<tr>
<td>Hydrogen chloride</td>
<td>2679–2840</td>
<td>Water</td>
</tr>
</tbody>
</table>

1.3 Method Range and Sensitivity
1.3.1 The analytical range is determined by the instrumental design and the composi-
tion of the gas stream. For practical pur-
poses there is no upper limit to the range be-
cause the pathlength may be reduced or the
sample may be diluted. The lower detection
range depends on (1) the absorption coeffi-
cient of the compound in the analytical fre-
cquency region, (2) the spectral resolution, (3)
the interferometer sampling time, (4) the de-
tector sensitivity and response, and (5) the
absorption pathlength.

1.3.2 The practical lower quantification
range is usually higher than the instrument
sensitivity allows and is dependent upon (1)
the presence of interfering species in the ex-
hauat gas including H2O, CO2, and SO2, (2)
analyte losses in the sampling system, (3)
the optical alignment of the gas cell and
transfer optics, and (4) the quality of the re-
flexive surfaces in the cell (cell through-
put). Under typical test conditions (moisture
content of up to 30% and CO2 concentrations
from 1 to 15 percent), a 22 meter path length
cell with a suitable sampling system may
achieve a lower quantification range of from
1 to 5 ppm for HCl.

1.4 Data Quality Objectives
1.4.1 In designing or configuring the ana-
litical system, data quality is determined by
measuring of the root mean square deviation
(RMSE) of the absorbance values within a
chosen spectral (analytical) region. The
RMSE provides an indication of the signal-
to-noise ratio (S/N) of the spectral baseline.
Appendix D of the FTIR Protocol (the adden-
dum to Method 320 of this appendix) presents
a discussion of the relationship between the
RMSE, lower detection limit, DL, and ana-
lytical uncertainty, AU. It is important to
consider the target analyte quantification
limit when performing testing with FTIR in-
strumentation, and to optimize the system
to achieve the desired detection limit.

1.4.2 Data quality is determined by meas-
uring the root mean square (RMS) noise level in each analytical spectral region (ap-
pendix C of the FTIR Protocol). The RMS
noise is defined as the root mean square de-
viation (RMSD) of the absorbance values in
an analytical region from the mean absorb-
bance value in the same region. Appendix D of
the FTIR Protocol defines the minimum
analyte uncertainty (MAU), and how the
RMSE is used to calculate the MAU. The
MAU is the minimum concentration of the
ith analyte in the mth analytical region for
which the analytical uncertainty limit can
be maintained. Table 2 presents example val-
ues of AU and MAU using the analytical re-

<table>
<thead>
<tr>
<th></th>
<th>HCl</th>
</tr>
</thead>
<tbody>
<tr>
<td>Reference concentraion (ppm-meters)/K</td>
<td>11.2</td>
</tr>
<tr>
<td>Reference Band area</td>
<td>2.881</td>
</tr>
<tr>
<td>DL (ppm-meters)/K</td>
<td>0.117</td>
</tr>
<tr>
<td>AU</td>
<td>0.2</td>
</tr>
<tr>
<td>CL (DL × AU)</td>
<td>0.02234</td>
</tr>
</tbody>
</table>
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TABLE 2.—EXAMPLE PRE-TEST PROTOCOL CALCULATIONS FOR HYDROGEN CHLORIDE—Continued

<table>
<thead>
<tr>
<th>HCl</th>
</tr>
</thead>
<tbody>
<tr>
<td>FL (cm⁻¹)</td>
</tr>
<tr>
<td>FU (cm⁻¹)</td>
</tr>
<tr>
<td>FG (cm⁻¹)</td>
</tr>
<tr>
<td>AAI (ppm-meters)/K</td>
</tr>
<tr>
<td>RMSD</td>
</tr>
<tr>
<td>MAU (ppm-meters)/K</td>
</tr>
<tr>
<td>MAU ppm at 22 meters and 250 °F</td>
</tr>
</tbody>
</table>

2.0 Summary of Method

2.1 Principle

See Method 320 of this appendix. HCl can also undergo rotation transitions by absorbing energy in the far-infrared spectral region. The rotational transitions are superimposed on the vibrational fundamental to give a series of lines centered at the fundamental vibrational frequency, 2885 cm⁻¹. The frequencies of absorbance and the pattern of rotational/vibrational lines are unique to HCl. When this distinct pattern is observed in an infrared spectrum of an unknown sample, it unequivocally identifies HCl as a component of the mixture. The infrared spectrum of HCl is very distinctive and cannot be confused with the spectrum of any other compound. See Reference 6.

2.2 Sampling and Analysis. See Method 320 of this appendix.

2.3 Operator Requirements. The analyst must have knowledge of spectral patterns to choose an appropriate absorption path length or determine if sample dilution is necessary. The analyst should also understand FTIR instrument operation well enough to choose instrument settings that are consistent with the objectives of the analysis.

3.0 Definitions

See appendix A of the FTIR Protocol.

4.0 Interferences

This method will not measure HCl under conditions: (1) where the sample gas stream can condense in the sampling system or the instrumentation, or (2) where a high moisture content sample relative to the analyte concentrations imparts spectral interference due to the water vapor absorbance bands. For measuring HCl the first (sampling) consideration is more critical. Spectral interference from water vapor is not a significant problem except at very high moisture levels and low HCl concentrations.

4.1 Analytical Interferences. See Method 320 of this appendix.

4.1.1 Background Interferences. See Method 320 of this appendix.

4.1.2 Spectral Interferences. Water vapor can present spectral interference for FTIR gas analysis of HCl. Therefore, the water vapor in the spectra of kiln gas samples must be accounted for. This means preparing at least one spectrum of a water vapor sample where the moisture concentration is close to that in the kiln gas.

4.2 Sampling System Interferences. The principal sampling system interferant for measuring HCl is water vapor. Steps must be taken to ensure that no condensation forms anywhere in the probe assembly, sample lines, or analytical instrumentation. Cold spots anywhere in the sampling system must be avoided. The extent of sampling system bias in the FTIR analysis of HCl depends on concentrations of potential interferants, moisture content of the gas stream, temperature of the gas stream, temperature of sampling system components, sample flow rate, and reactivity of HCl with other species in the gas stream (e.g., ammonia). For measuring HCl in a wet gas stream the temperatures of the gas stream, sampling components, and the sample flow rate are of primary importance. Analyte spiking with HCl is performed to demonstrate the integrity of the sampling system for transporting HCl vapor in the flue gas to the FTIR instrument. See section 9 of this method for a complete description of analyte spiking.

5.0 Safety

5.1 Hydrogen chloride vapor is corrosive and can cause irritation or severe damage to respiratory system, eyes and skin. Exposure to this compound should be avoided.

5.2 This method may involve sampling at locations having high positive or negative pressures, or high concentrations of hazardous or toxic pollutants, and can not address all safety problems encountered under these diverse sampling conditions. It is the responsibility of the tester(s) to ensure proper safety and health practices, and to determine the applicability of regulatory limitations before performing this test method. Leak-check procedures are outlined in section 8.2 of Method 320 of this appendix.

6.0 Equipment and Supplies

NOTE: Mention of trade names or specific products does not constitute endorsement by the Environmental Protection Agency.

6.1 FTIR Spectrometer and Detector. An FTIR spectrometer system (interferometer, transfer optics, gas cell and detector) having the capability of measuring HCl to the predetermined minimum detectable level required (see section 4.1.3 of the FTIR Protocol). The system must also include an accurate means to control and/or measure the temperature of the FTIR gas analysis cell, and a personal computer with compatible software that provides real-time updates of the spectral profile during sample and spectral collection.

6.2 Pump. Capable of evacuating the FTIR cell volume to 1 Torr (133.3 Pascals) within two minutes (for batch sample analysis).

6.3 Mass Flow Meters/Controllers. To accurately measure gas flow rates. Having the appropriate calibrated range and a stated accuracy of ±2 percent of the absolute measurement value. This device must be calibrated with standard gases having the appropriate gas mixture.

6.4 Polytetrafluoroethylene (PTFE) tubing. Diameter and length suitable to connect cylinder regulators. Gas flow rates must be measured and verified using a calibrated flowmeter.

6.5 Stainless Steel tubing. Type 316 of appropriate length and diameter for heated connections.

6.6 Gas Regulators. Purgeable HCl regulators are required.

6.7 Pressure Gauge. Capable of measuring pressure from 0 to 1000 Torr (133.3 Pa to 1 Torr) within ±5 percent.

6.8 Sampling Probe. Glass, stainless steel or other appropriate material of sufficient length and physical integrity to sustain heating, prevent adsorption of analytes and capable of reaching gas sampling point.

6.9 Sampling Line. Heated 180 °C (360 °F) and fabricated of stainless steel, polytetrafluoroethylene or other material that prevents adsorption of HCl and transports effluent to analytical instrumentation. The extractive sample line must have the capability to transport sample gas to the analytical components as well as direct heated calibration spike gas to the calibration assembly located at the sample probe. It is important to minimize the length of heated sample line.

6.10 Particulate Filters. A sintered stainless steel filter rated at 20 microns or greater may be placed at the inlet of the pump for removal of large particulate matter. A heated filter (Balston or equivalent) rated at 1 micron is necessary for primary particulate removal, and shall be placed immediately after the heated probe. The filter holder temperature should be maintained at 180 °C (360 °F).

6.11 Calibration/Analyte Spike Assembly. A heated three-way valve assembly (or equivalent) to introduce surrogate spikes into the sampling system at the outlet of the probe before the primary particulate filter.

6.12 Sample Extraction Pump. A leak-free heated head pump (KNF Neuberger or equivalent) capable of extracting sample effluent through entire sampling system at a rate which prevents analyte losses and minimizes analyzer response time. The pump should have a heated by-pass and may be placed either before the FTIR instrument or after. If the sample pump is located upstream of the FTIR instrument, it must be fabricated from materials non-reactive to HCl. The sampling system and FTIR measurement system shall allow the operator to obtain at least six sample spectra during a one-hour period.

6.13 Barometer. For measurement of barometric pressure.


6.14.1 Delivery of calibration gas directly to the analytical instrumentation.

6.14.2 Delivery of calibration gas to the sample probe (system calibration or analyte spike) via a heated traced sample line.

6.14.3 Delivery of sample gas (kiln gas, spiked kiln gas, or system calibrations) to the analytical instrumentation.

6.14.4 Delivery (optional) of a humidified nitrogen sample stream.

6.15 Flow Measurement Device. Type S Pitot tube (or equivalent) and Magnahelic set for measurement of volumetric flow rate.

7.0 Reagents and Standards

HCl can be purchased in a standard compressed gas cylinder. The most stable HCl cylinder mixture available has a concentration certified at ±5 percent. Such a cylinder is suitable for performing analyte spiking because it will provide reproducible samples. The stability of the cylinder can be monitored over time by periodically performing direct FTIR analysis of cylinder samples. It is recommended that a 10-50 ppm cylinder of HCl be prepared having from 2±5 ppm SF6 as a tracer compound. (See sections 7.1 through 7.3 of Method 320 of this appendix for a complete description of the use of existing HCl reference spectra. See section 9.1 of Method 320 of this appendix for a complete discussion of standard concentration selection.)

8.0 Sample Collection, Preservation and Storage

See also Method 320 of this appendix.

8.1 Pretest. A screening test is ideal for obtaining proper data that can be used for preparing analytical program files. Information from literature surveys and source personnel is also acceptable. Information about the sampling location and gas stream composition is required to determine the optimum sampling system configuration for measuring HCl. Determine the percent moisture of the kiln gas by Method 4 of appendix A to part 60 of this chapter or by performing a preliminary traverse of the sample duct or stack and select the sampling point(s). Acquire an initial spectrum and determine the optimum operational pathlength of the instrument.
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8.2 Leak-Check. See Method 320 of this appendix, section 8.2 for direction on performing leak-checks.

8.3 Background Spectrum. See Method 320 of this appendix, section 8.3 for direction in background spectral acquisition.

8.4 Pre-Test Calibration Transfer Standard (Direct Instrument Calibration). See Method 320 of this appendix, section 8.4 for direction in CTS spectral acquisition.

8.5 Pre-Test System Calibration. See Method 320 of this appendix, sections 8.6.1 through 8.6.2 for direction in performing system calibration.

8.6 Sampling

8.6.1. Extractive System. An extractive system maintained at 180°C (360°F) or higher which is capable of directing a total flow of at least 12 L/min to the sample cell is required (differences 1 and 2). Insert the probe into the duct or stack at a point representing the average volumetric flow rate and 25 percent of the cross sectional area. Co-locate an appropriate flow monitoring device with the sample probe so that the flow rate is recorded at specified time intervals during emission testing (e.g., differential pressure measurements taken every 10 minutes during each run).

8.6.2. Batch Samples. Evacuate the absorbance cell to 5 Torr (or less) absolute pressure before taking first sample. Fill the cell with kiln gas to ambient pressure and record the infrared spectrum, then evacuate the cell until there is no further evidence of infrared absorption. Repeat this procedure, collecting a total of six separate sample spectra within a 1-hour period.

8.6.3 Continuous Flow Through Sampling. Purge the FTIR cell with kiln gas for a time period sufficient to equilibrate the entire sampling system and FTIR gas cell. The time required is a function of the mechanical response time of the system (determined by performing the system calibration with the CTS gas or equivalent), and by the chemical reactivity of the target analytes. If the effluent target analyte concentration is not variable, observation of the spectral up-date of the flowing gas sample should be performed until equilibration of the sample is achieved. Isolate the gas cell from the sample flow by directing the purge flow to vent. Record the spectrum and pressure of the sample gas. After spectral acquisition, allow the sample gas to purge the cell with at least three volumes of kiln gas. The time required to adequately purge the cell with the required volume of gas is a function of (1) cell volume, (2) flow rate through the cell, and (3) cell design. It is important that the gas introduction and removal for the FTIR cell provides a complete purge through the cell.

8.6.4 Continuous Sampling. In some cases it is possible to collect spectra continuously while the FTIR cell is purged with sample gas. The sample integration time, t_s, the sample flow rate through the gas cell, and the sample integration time must be chosen so that the collected data consist of at least 10 spectra with each spectrum being of a separate cell volume of flue gas. Sampling in this manner may only be performed if the native source analyte concentrations do not affect the test results.

8.7 Sample Conditioning

8.7.1 High Moisture Sampling. Kiln gas emitted from wet process cement kilns may contain 3- to 40 percent moisture. Zinc selenide windows or the equivalent should be used when attempting to analyze hot/wet kiln gas under these conditions to prevent dissolution of water soluble window materials (e.g., KBr).

8.7.2 Sample Dilution. The sample may be diluted using an in-stack dilution probe, or an external dilution device provided that the sample is not diluted below the instrument's quantification range. As an alternative to using a dilution probe, nitrogen may be dynamically spiked into the effluent stream in the same manner as analyte spiking. A constant dilution rate shall be maintained throughout the measurement process. It is critical to measure and verify the exact dilution ratio when using a dilution probe or the nitrogen spiking approach. Calibrating the system with a calibration gas containing an appropriate tracer compound will allow determination of the dilution ratio for most measurement systems. The tester shall specify the procedures used to determine the dilution ratio, and include these calibration results in the report.

8.8 Sampling QA, Data Storage and Reporting. See the FTIR Protocol. Sample integration times shall be sufficient to achieve the required signal-to-noise ratio, and all sample spectra should have unique file names. Two copies of sample interferograms and processed spectra will be stored on separate computer media. For each sample spectrum the analyst must document the sampling conditions, the sampling time (while the cell was being filled), the time the spectrum was recorded, the instrumental conditions (path length, temperature, pressure, resolution, integration time), and the spectral file name. A hard copy of these data must be maintained until the test results are accepted.

8.9 Signal Transmittance. Monitor the signal transmittance through the instrumental system. If signal transmittance (relative to the background) drops below 95 percent in any spectral region where the sample does not absorb infrared energy, then a new background spectrum must be obtained.
8.10 Post-test CTS. After the sampling run completion, record the CTS spectrum. Analysis of the spectral band area used for quantification from pre- and post-test CTS spectra should agree to within ±5 percent or corrective action must be taken.

8.11 Post-test QA. The sample spectra shall be inspected immediately after the run to verify that the spectrum of the completed sample run was close to the assumed gas matrix, (this is necessary to account for the concentrations of the interferants for use in the analytical analysis programs), and to confirm that the sampling and instrumental parameters were appropriate for the conditions encountered.

9.0 Quality Control

Use analyte spiking to verify the effectiveness of the sampling system for the target compounds in the actual kiln gas matrix. QA spiking shall be performed before and after each sample run. QA spiking shall be performed after the pre- and post-test CTS direct and system calibrations. The system biases calculated from the pre- and post-test dynamic analyte spiking shall be within ±30 percent for the spiked surrogate analytes for the measurements to be considered valid. See sections 9.1.1 through 9.1.2 for the required calculations. Measurement of the undiluted spike (direct-to-cell measurement) involves sending dry, spike gas to the FTIR cell, filling the cell to 1 atmosphere and obtaining the spectrum of this sample. The direct-to-cell measurement should be performed before each analyte spike so that the recovery of the dynamically spiked analytes may be calculated. Analyte spiking is only effective for assessing the integrity of the sampling system when the concentration of HCl in the source does not vary substantially. Any attempt to quantify an analyte recovery in a variable concentration matrix will result in errors in the expected concentration of the spiked sample. If the kiln gas target analyte concentrations vary by more than ±5 percent (or 5 ppm, whichever is greater) in the time required to acquire a sample spectrum, it may be necessary to: (1) use a dual sample probe approach, (2) use two independent FTIR measurement systems, (3) use alternate QA/QC procedures, or (4) postpone testing until stable emission concentrations are achieved. (See section 9.2.3 of this method). It is recommended that a laboratory evaluation be performed before attempting to employ this method under actual field conditions. The laboratory evaluation shall include (1) performance of all applicable calculations in section 4 of the FTIR Protocol; (2) simulated analyte spiking experiments in dry (ambient) and humidified sample matrices using HCl; and (3) performance of bias (recovery) calculations from analyte spiking experiments. It is not necessary to perform a laboratory evaluation before every field test. The purpose of the laboratory study is to demonstrate that the actual instrument and sampling system configuration used in field testing meets the requirements set forth in this method.

9.1 Spike Materials. Perform analyte spiking with an HCl standard to demonstrate the integrity of the sampling system.

9.1.1 An HCl standard of approximately 50 ppm in a balance of ultra pure nitrogen is recommended. The SF6 (tracer) concentration shall be 2 to 5 ppm depending upon the measurement pathlength. The spike ratio (spike flow/total flow) shall be no greater than 1:10, and an ideal spike concentration should approximate the native effluent concentration.

9.1.2 The ideal spike concentration may not be achieved because the target concentration cannot be accurately predicted prior to the field test, and limited calibration standards will be available during testing. Therefore, practical constraints must be applied that allow the tester to spike at an anticipated concentration. For these tests, the analyte concentration contributed by the HCl standard spike should be 1 to 5 ppm or should more closely approximate the native concentration if it is greater.

9.2 Spike Procedure

9.2.1 A spiking/sampling apparatus is shown in Figure 2. Introduce the spike/tracer gas mixture at a constant flow (±2 percent) rate at approximately 10 percent of the total sample flow. (For example, introduce the surrogate spike at 1 L/min 20 cc/min, into a total sample flow rate of 10 L/min). The spike must be pre-heated before introduction into the sample matrix to prevent a localized condensation of the gas stream at the spike introduction point. A heated sample transport line(s) containing multiple transport tubes within the heated bundle may be used to spike gas up through the sampling system to the spike introduction point. Use a calibrated flow device (e.g., mass flow meter/controller), to monitor the spike flow as indicated by a calibrated flow meter or controller, or alternately, the SF6 tracer ratio may be calculated from the direct measurement and the diluted measurement. It is often desirable to use the tracer approach in calculating the spike/total flow ratio because of the difficulty in accurately measuring hot/wet total flow. The tracer technique has been successfully used in past validation efforts (Reference 1).

9.2.2 Perform a direct-to-cell measurement of the dry, undiluted spike gas. Introduce the spike directly to the FTIR cell, bypassing the sampling system. Fill cell to 1 atmosphere and collect the spectrum of this sample. Ensure that the spike gas has equilibrated to the temperature of the measurement cell before acquisition of the spectra. Inspect the spectrum and verify that the gas
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is dry and contains negligible CO₂. Repeat the process to obtain a second direct-to-cell measurement. Analysis of spectral band areas for HCl from these duplicate measurements should agree to within ±5 percent of the mean.

9.2.3 Analyte Spiking. Determine whether the kiln gas contains native concentrations of HCl by examination of preliminary spectra. Determine whether the concentration varies significantly with time by observing a continuously updated spectrum of sample gas in the flow-through sampling mode. If the concentration varies by more than ±5 percent during the period of time required to acquire a spectrum, then an alternate approach should be used. One alternate approach uses two sampling lines to convey sample to the gas distribution manifold. One of the sample lines is used to continuously extract unspiked kiln gas from the source. The other sample line serves as the analyte spike line. One FTIR system can be used in this arrangement. Spiked or unspiked sample gas may be directed to the FTIR system from the gas distribution manifold, with the need to purge only the components between the manifold and the FTIR system. This approach minimizes the time required to acquire an equilibrated sample of spiked or unspiked kiln gas. If the source varies by more than ±5 percent (or 5 ppm, whichever is greater) in the time it takes to switch from the unspiked sample line to the spiked sample line, then analyte spiking may not be a feasible means to determine the effectiveness of the sampling system for the HCl in the sample matrix. A second alternative is to use two completely independent FTIR measurement systems. One system would measure unspiked samples, while the other system would measure the spiked samples. As a last option, where no other alternatives can be used, a humidified nitrogen stream may be generated in the field which approximates the moisture content of the kiln gas. Analyte spiking into this humidified stream can be employed to assure that the sampling system is adequate for transporting the HCl to the FTIR instrumentation.

9.2.3.1 Adjust the spike flow rate to approximately 10 percent of the total flow by metering spike gas through a calibrated mass flowmeter or controller. Allow spike flow to equilibrate within the sampling system before analyzing the first spiked kiln gas samples. A minimum of two consecutive spikes are required. Analysis of the spectral band area used for quantification should agree to within ±5 percent or corrective action must be taken.

9.2.3.2 After QA spiking is completed, the sampling system components shall be purged with nitrogen or dry air to eliminate traces of the HCl compound from the sampling system components. Acquire a sample spectra of the nitrogen purge to verify the absence of the calibration mixture.

9.2.3.3 Analyte spiking procedures must be carefully executed to ensure that meaningful measurements are achieved. The requirements of sections 9.2.3.1 through 9.2.3.4 shall be met.

9.2.3.3.1 The spike must be in the vapor phase, dry, and heated to (or above) the kiln gas temperature before it is introduced to the kiln gas stream.

9.2.3.3.2 The spike flow rate must be constant and accurately measured.

9.2.3.3.3 The total flow must also be measured continuously and reliably or the dilution ratio must otherwise be verified before and after a run by introducing a spike of a non-reactive, stable compound (i.e., tracer).

9.2.3.3.4 The tracer must be inert to the sampling system components, not contained in the effluent gas, and readily detected by the analytical instrumentation. Sulfur hexafluoride (SF₆) has been used successfully (References 1 and 2) for this purpose.

9.3 Calculations

9.3.1 Recovery. Calculate the percent recovery of the spiked analytes using equations 1 and 2.

\[
\% R = 100 \times \frac{S_m - S_{d}(1 - DF)}{DF \times C_s} \tag{1}
\]

\[
S_m = \text{Mean concentration of the analyte spiked effluent samples (observed)}.
\]

\[
C_s = \text{Expected concentration of the spiked samples (theoretical)}.
\]

\[
D_f = \text{Dilution Factor (Total flow} \times \text{Spike flow)}.
\]

\[
is a factor that takes into account the total flow rate of the effluent gas, the spike flow rate, and the ratio of the two.

\[
D_f = \frac{[SF_6]_{spike}}{[SF_6]_{direct}} \tag{3}
\]

[SF₆]_{spike} = \text{the diluted SF₆ concentration measured in a spiked sample.}

[SF₆]_{direct} = \text{the SF₆ concentration measured directly.}

9.3.2 Bias. The bias may be determined by the difference between the observed spike value and the expected response (i.e., the equivalent concentration of the spiked material plus the analyte concentration adjusted...
for spike dilution). Bias is defined by section 6.3.1 of EPA Method 301 of this appendix (Reference B) as,

$$B = S_m - C_e \quad (4)$$

Where:
- $B =$ Bias at spike level.
- $S_m =$ Mean concentration of the analyte spiked samples.
- $C_e =$ Expected concentration of the analyte in spiked samples.

Acceptable recoveries for analyte spiking are ±30 percent. Application of correction factors to the data based upon bias and recovery calculations is subject to the approval of the Administrator.

10.0 Calibration and Standardization

10.1 Calibration transfer standards (CTS). The EPA Traceability Protocol gases or NIST traceable standards, with a minimum accuracy of ±2 percent shall be used. For other requirements of the CTS, see the FTIR Protocol section 4.5.

10.2 Signal-to-Noise Ratio (S/N). The S/N shall be less than the minimum acceptable measurement uncertainty in the analytical regions to be used for measuring HCl.

10.3 Absorbance Pathlength. Verify the absorbance path length by comparing CTS spectra to reference spectra of the calibration gas(es).

10.4 Instrument Resolution. Measure the line width of appropriate CTS band(s) to verify instrumental resolution.

10.5 Apodization Function. Choose the appropriate apodization function. Determine any appropriate mathematical transformations that are required to correct instrumental errors by measuring the CTS. Any mathematical transformations must be documented and reproducible. Reference 9 provides additional information about FTIR instrumentation.

11.0 Analytical Procedure

A full description of the analytical procedures is given in sections 4.6-4.11, sections 5, 6, and 7, and the appendices of the FTIR Protocol. Additional description of quantitative spectral analysis is provided in References 10 and 11.

12.0 Data Analysis and Calculations

Data analysis is performed using appropriate reference spectra whose concentrations can be verified using CTS spectra. Various analytical programs (References 10 and 11) are available to relate sample absorbance to a concentration standard. Calculated concentrations should be verified by analyzing spectral baselines after mathematically subtracting scaled reference spectra from the sample spectra. A full description of the data analysis and calculations may be found in the FTIR Protocol (sections 4.0, 5.0, 6.0 and appendices).

12.1 Calculated concentrations in sample spectra are corrected for differences in absorption pathlength between the reference and sample spectra by

$$C_{corr} = \left(\frac{L_r}{L_s}\right) \times \left(\frac{T_s}{T_r}\right) \times C_{calc} \quad (5)$$

Where:
- $C_{corr} =$ The pathlength corrected concentration.
- $C_{calc} =$ The initial calculated concentration (output of the multicomponent analysis program designed for the compound).
- $L_r =$ The pathlength associated with the reference spectra.
- $L_s =$ The pathlength associated with the sample spectra.
- $T_s =$ The absolute temperature (K) of the sample gas.
- $T_r =$ The absolute temperature (K) at which reference spectra were recorded.

12.2 The temperature correction in equation 5 is a volumetric correction. It does not account for temperature dependence of rotational-vibrational relative line intensities. Whenever possible, the reference spectra used in the analysis should be collected at a temperature near the temperature of the FTIR cell used in the test to minimize the calculated error in the measurement (FTIR Protocol, appendix D). Additionally, the analytical region chosen for the analysis should be sufficiently broad to minimize errors caused by small differences in relative line intensities between reference spectra and the sample spectra.

13.0 Method Performance

A description of the method performance may be found in the FTIR Protocol. This method is self validating provided the results meet the performance specification of the QA spike in sections 9.0 through 9.3 of this method.

14.0 Pollution Prevention

This is a gas phase measurement. Gas is extracted from the source, analyzed by the instrumentation, and discharged through the instrument vent.
15.0 Waste Management

Gas standards of HCl are handled according to the instructions enclosed with the material safety data sheet.

16.0 References


Figure 1. FTIR Spectra of HCl and Water.
Figure 2. FTIR Sampling/Spiking System.
APPENDIX C TO PART 63—DETERMINATION OF THE FRACTION BIODEGRADED (F_{bio}) IN A BIOLOGICAL TREATMENT UNIT

I. Purpose

The purpose of this appendix is to define the procedures for an owner or operator to use to calculate the site specific fraction of organic compounds biodegraded (F_{bio}) in a biological treatment unit. If an acceptable level of organic compounds is destroyed rather than emitted to the air or remaining in the effluent, the biological treatment unit may be used to comply with the applicable treatment requirements without the unit being covered and vented through a closed vent system to an air pollution control device.

The determination of F_{bio} shall be made on a system as it would exist under the rule. The owner or operator should anticipate changes that would occur to the wastewater flow and concentration of organics, to be treated by the biological treatment unit, as a result of enclosing the collection and treatment system as required by the rule.

The forms presented in this appendix are designed to be applied to thoroughly mixed treatment units. A thoroughly mixed treatment unit is a unit that is designed and operated to approach or achieve uniform biodegradation and organic compound concentration throughout the wastewater system by quickly dispersing the recycled biomass and the wastewater entering the unit. Systems that are not thoroughly mixed treatment units should be subdivided into a series of zones that have uniform characteristics within each zone. The number of zones required to characterize a biological treatment system will depend on the design and operation of the treatment system. Each zone should then be modeled as a separate unit. The amount of air emissions and biodegradation from the modeling of these separate zones can then be added to reflect the entire system.

II. Definitions

Biological treatment unit = wastewater treatment unit designed and operated to promote the growth of bacteria to destroy organic materials in wastewater.

F_{bio} = The fraction of individual applicable organic compounds in the wastewater biodegraded in a biological treatment unit.

F_{tot} = The fraction of total applicable organic compounds in the wastewater biodegraded in a biological treatment unit.

F_{bio} = The fraction of total applicable organic compounds emitted from the wastewater to the atmosphere.

K1 = First order biodegradation rate constant, L/g MLVSS-hr

KL = Liquid-phase mass transfer coefficient, m/s

M = Compound specific mass flow weighted average of organic compounds in the wastewater, Mg/Yr

III. Procedures for Determination of F_{bio}

The first step in the analysis to determine if a biological treatment unit may be used without being covered and vented through a closed-vent system to an air pollution control device, is to determine the compound-specific F_{bio}. The following four procedures may be used to determine F_{bio}:

2. Performance data with and without biodegradation,
3. Inlet and outlet concentration measurements,

All procedures must be executed so that the resulting F_{bio} is based on the collection system and waste management units being
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in compliance with the regulation. If the collection system and waste management units meet the suppression requirements at the time of the test, any of the four procedures may be chosen. If the collection system and waste management units are not in compliance at the time of the performance test, then only Method 304A, 304B, or the Batch Test shall be chosen. If Method 304A, 304B, or the Batch Test is used, any anticipated changes to the influent of the full-scale biological treatment unit that will occur after the facility has enclosed the collection system must be represented in the influent feed to the benchtop bioreactor unit, or test unit.

Select one or more appropriate procedures from the four listed above based on the availability of site specific data. If the facility does not have site-specific data on the removal efficiency of its biological treatment unit, Procedure 1 or Procedure 4 may be used. Procedure 1 allows the use of a benchtop bioreactor to determine the first-order biodegradation rate constant. An owner or operator may elect to assume the first order biodegradation rate constant is zero for any regulated compound(s) present in the wastewater. Procedure 4 explains two types of batch tests which may be used to estimate the first order biodegradation rate constant. An owner or operator may elect to assume the first order biodegradation rate constant is zero for any regulated compound(s) present in the wastewater. Procedure 3 would be used if the facility has, or measures to determine, data on the inlet and outlet individual organic compound concentration for the biological treatment unit. Procedure 3 may only be used on a thoroughly mixed treatment unit. Procedure 2 is used if a facility has or obtains performance data on a biological treatment unit prior to and after addition of the microbial mass. An example where Procedure 2 could be used, is an activated sludge unit where measurements have been taken on inlet and exit concentration of organic compounds in the wastewater prior to seeding with the microbial mass and start-up of the unit. The flow chart in figure 1 outlines the steps to use for each of the procedures.

A. Method 304A or 304B (Procedure 1)

If the first procedure is selected, follow the instructions in appendix A of part 63 Method 304A “Method for the Determination of Biodegradation Rates of Organic Compounds (Vented Option)” or Method 304B “Method for the Determination of Biodegradation Rates of Organic Compounds (Scrubber Option).” Method 304A or 304B provides instruction on setting up and operating a self-contained benchtop bioreactor system which is operated under conditions representative of the target full-scale system. Method 304A uses a benchtop bioreactor system with a vent, and uses modeling to estimate any air emissions. Method 304B uses a benchtop bioreactor system which is equipped with a scrubber and is not vented.

There are some restrictions on which method a source may use if the facility is measuring the rate of biodegradation of compounds that may tend to react or hydrolyze in the scrubber of Method 304B, this method shall not be used and Method 304A is the required method. If a Henry’s law value is not available to use with Form V, then Method 304A shall not be used and Method 304B is the required method. When using either method, the feed flow to the benchtop bioreactor shall be representative of the flow and concentration of the wastewater that will be treated by the full-scale biological treatment unit after the collection and treatment system has been enclosed as required under the applicable subpart.

The conditions under which the full-scale biological treatment unit is run establish the operating parameters of Method 304A or 304B. If the biological treatment unit is operated under abnormal operating conditions (conditions outside the range of critical parameters examined and confirmed in the laboratory), the EPA believes this will adversely affect the biodegradation rate and is an unacceptable treatment option. The facility would be making multiple runs of the test method to simulate the operating range for its biological treatment unit. For wide ranges of variation in operating parameters, the facility shall demonstrate the biological treatment unit is achieving an acceptable level of control, as required by the regulation, across the ranges and not only at the endpoints.

If Method 304A is used, complete Form V initially. Form V is used to calculate K1 from the Method 304A results. Form V uses the Henry’s law constant to estimate the fraction lost from the benchtop reactor vent. The owner or operator shall use the Henry’s law values in Table I. Form V also gives direction for calculating an equivalent K. Note on Form V if the calculated number for line 11 is greater than the calculated value for line 13, this procedure shall be used to demonstrate the compound is biodegradable. If line 11 is greater than line 13, this is an indication the fraction emitted from the vent is greater than the fraction biodegraded. The equivalent K determined on Form V is used in Form II (line 6). Estimation of the Fe and fewn must be done following the steps in Form II. Form III uses the previously calculated values of K1 and KL (equivalent K), and site-specific parameters of the full-scale bioreactor as input to the calculations. Forms II, III, and V must be completed for each organic compound in the wastewater to determine Fe and fewn.

If Method 304B is used, perform the method and use the measurements to determine K1, which is the first-order biodegradation rate
constant. Form I lists the sequence of steps in the procedure for calculating $K_L$ from the Method 304B results. Once $K_L$ is determined, $KL$ must be calculated by use of mass transfer equations. Form II outlines the procedure to follow for use of mass transfer equations to determine $K_L$. A computer program which incorporates these mass transfer equations may be used. Water7 is a program that incorporates these mass transfer equations and may be used to determine $K_L$. Refer to Form II-A to determine $K_L$, if Water7 or the most recent update to this model is used. In addition, the Bay Area Sewage Toxics Emission (BASTE) model version 3.0 or equivalent upgrade and the TOXCHEM (Environment Canada’s Wastewater Technology Centre and Environmega, Ltd.) model version 1.10 or equivalent upgrade may also be used to determine $K_L$ for the biological treatment unit with several stipulations. The programs must be altered to output a $K_L$ value which is based on the site-specific parameters of the unit modeled, and the Henry’s law values listed in Table I must be substituted for the existing Henry’s law values in the programs. Input values used in the model and corresponding output values shall become documentation of the $f_{m0}$ determination. The owner or operator should be aware these programs do not allow modeling of certain units. To model these units, the owner or operator shall use one of the other appropriate procedures as outlined in this appendix. The owner or operator shall not use a default value for $K_L$. The $K_L$ value determined by use of these models shall be based on the site-specific parameters of the specific unit. This $K_L$ value shall be inserted in Form II (line 6). Estimation of the $F_e$ and $f_{m0}$ must be done following the steps in Form III. Form III uses the previously calculated values of $K_L$ and $KL$, and site-specific parameters of the full-scale bioreactor as input to the calculations. Forms I, II, and III must be completed for each organic compound in the wastewater to determine $F_e$ and $f_{m0}$.

B. Performance Data With and Without Biodegradation (Procedure 2)

Procedure 2 uses site-specific performance data that represents or characterizes operation of the unit both with and without biodegradation. As previously mentioned, proper determination of $f_{m0}$ must be made on a system as it would exist under the rule. Using Form IV, calculate $KL$ and $K_L$. After $KL$ and $K_L$ are determined, Form III is used to calculate $F_e$ and $f_{m0}$ for each organic compound present in the wastewater.

C. Inlet and Outlet Concentration Measurements (Procedure 3)

Procedure 3 uses measured inlet and outlet organic compound concentrations for the unit. This procedure may only be used on a thoroughly mixed treatment unit. Again, proper determination of $f_{m0}$ must be made on a system as it would exist under the rule. The first step in using this procedure is to calculate $KL$ using Form II. A computer model may be used. If the Water7 model or the most recent update to this model is used, then use Form II-A to calculate $KL$. After $KL$ is determined, use field data, complete Form VI to calculate $K_L$. The TOXCHEM or BASTE model may also be used to calculate $KL$ for the biological treatment unit, with the stipulations listed in procedure 304B. After $KL$ and $K_L$ are determined, Form III is used to calculate $F_e$ and $f_{m0}$ for each organic compound.

D. Batch Tests (Procedure 4)

Two types of batch tests which may be used to determine kinetic parameters are: (1) The aerated reactor test and (2) the sealed reactor test. The aerated reactor test is also known as the BOX test (batch test with oxygen addition). The sealed reactor test is also known as the serum bottle test. These batch tests should be conducted only by persons familiar with procedures for determining biodegradation kinetics. Detailed discussions of batch procedures for determining biodegradation kinetic parameters can be found in references 1-4.

For both batch test approaches, a biomass sample from the activated sludge unit of interest is collected, aerated, and stored for no more than 4 hours prior to testing. To collect sufficient data when biodegradation is rapid, it may be necessary to dilute the biomass sample. If the sample is to be diluted, the biomass sample shall be diluted using treated effluent from the activated sludge unit of interest to a concentration such that the biodegradation test will last long enough to make at least six concentration measurements. It is recommended that the tests not be terminated until the compound concentration falls below the limit of quantitation (LOQ). Measurements that are below the LOQ should not be used in the data analysis. Biomass concentrations shall be determined using standard methods for measurement of mixed liquor volatile suspended solids (MLVSS) (reference 5).

The change in concentration of a test compound may be monitored by either measuring the concentration in the liquid or in the reactor headspace. The analytical technique chosen for the test should be as sensitive as possible. For the batch test procedures described in this section, equilibrium conditions must exist between the liquid and gas phases of the experiments because the data analysis procedures are based on this premise. To use the headspace sampling approach, the reactor headspace must be in equilibrium with the liquid so that the headspace concentrations can be correlated.
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With the liquid concentrations. Before the biodegradation testing is conducted, the equilibrium assumption must be verified. A discussion of the equilibrium assumption verification is given below in sections D.1 and D.2 since different approaches are required for the two types of batch tests.

To determine biodegradation kinetic parameters in a batch test, it is important to choose an appropriate initial substrate (compound(s) of interest) concentration for the test. The outcome of the batch experiment may be influenced by the initial substrate ($S_o$) to biomass ($X_o$) ratio (see references 3, 4, and 6). This ratio is typically measured in chemical oxygen demand (COD) units. When the $S_o/X_o$ ratio is low, cell multiplication and growth in the batch test is negligible and the kinetics measured by the test are representative of the kinetics in the activated sludge unit of interest. The $S_o/X_o$ ratio for a batch test is determined with the following equation:

$$\frac{S_0}{X_0} = \frac{S_i}{1.42 X} \quad (\text{Eqn App. C - 1})$$

Where:

- $S_o$: initial substrate to biomass ratio on a COD basis
- $S_i$: initial substrate concentration in COD units (g COD/L)
- $X$: biomass concentration in the batch test (g MLVSS/L)
- 1.42: Conversion factor to convert to COD units

For the batch tests described in this section, the $S_o/X_o$ ratio (on a COD basis) must be initially less than 0.5.

1. Aerated Reactor Test. An aerated draft tube reactor may be used for the biokinetics testing (as an example see Figure 2 of appendix C). Other aerated reactor configurations may also be used. Air is bubbled through a porous frit at a rate sufficient to aerate and keep the reactor uniformly mixed. Aeration rates typically vary from 50 to 200 ml/min for a 1 liter system. A mass flow rate controller is used to carefully control the air flow rate because it is important to have an accurate measure of this rate. The dissolved oxygen (DO) concentration in the system must not fall below 2 mg/liter so that the biodegradation observed will not be DO-limited. Once the air flow rate is established, the test mixture (or compound) of interest is then injected into the reactor and the concentration of the compound(s) is monitored over time. Concentrations may be monitored in the liquid or in the headspace. A minimum of six samples shall be taken over the period of the test. However, it is necessary to collect samples until the compound concentration falls below the LOQ. If liquid samples are collected, they must be small enough such that the liquid volume in the batch reactor does not change by more than 10%.

Before conducting experiments with biomass, it is necessary to verify the equilibrium assumption. The equilibrium assumption can be verified by conducting a stripping experiment using the effluent (no biomass) from the activated sludge unit of interest. Effluent is filtered with a 0.45 um or smaller filter and placed in the draft tube reactor. Air is sparged into the system and the compound concentration in the liquid or headspace is monitored over time. This test with no biomass may provide an estimate of the Henry’s law constant. If the system is at equilibrium, the Henry’s law constant may be estimated with the following equation:

$$-\ln\left(\frac{C}{C_0}\right) = \left(\frac{GK_{eq}}{V}\right)t \quad (\text{Eqn App. C - 2})$$

Where:

- $C$: concentration at time, $t$ (min)
- $C_0$: concentration at $t=0$
- $G$: volumetric gas flow rate (ml/min)
- $V$: liquid volume in the batch reactor (ml)
- $K_{eq}$: Henry’s law constant (mg/L-gas)/(mg/L-liquid)
- $t$: time (min)

A plot of $-\ln(C/C_0)$ as a function of $t$ will have a slope equal to $GK_{eq}/V$. The equilibrium assumption can be verified by comparing the experimentally determined $K_{eq}$ for the system to literature values of the Henry’s Law constant (including those listed in this appendix). If $K_{eq}$ does not match the Henry’s law constant, $K_{eq}$ shall be determined from analysis of the headspace and liquid concentration in a batch system.

The concentration of a compound decreases in the bioreactor due to both biodegradation and stripping. Biodegradation processes are typically described with a Monod model. This model and a stripping expression are combined to give a mass balance for the aerated draft tube reactor.)
\[ \frac{ds}{dt} = \left( \frac{G K_{eq}}{V} \right) s + \left( \frac{Q_m X}{K_s + s} \right) s \]  
\text{(Eqn App. C - 3)}

Where:
- \( s \) = test compound concentration, mg/liter
- \( G \) = volumetric gas flow rate, liters/hr
- \( K_{eq} \) = Henry's Law constant measured in the system, (mg/liter gas)/(mg/liter liquid)
- \( V \) = volume of liquid in the reactor, liters
- \( X \) = biomass concentration (g MLVSS/liter)
- \( Q_m \) = maximum rate of substrate removal, mg/ g MLVSS/hr
- \( K_s \) = Monod biorate constant at half the maximum rate, mg/liter

Equation App. C-3 has the analytical solution:

\[ -t = \frac{V K_s}{A} \ln \left( \frac{s}{s_0} \right) + \frac{Q_m X V^2}{A B} \ln \left( \frac{A + Bs}{A + Bs_0} \right) \]  
\text{(Eqn App. C - 4)}

Where:
- \( A = G K_{eq} K_s + Q_m VX \)
- \( B = G K_m \)
- \( s_0 \) = test compound concentration at \( t=0 \)

This equation is used along with the substrate concentration versus time data to determine the best fit parameters \( (Q_m \) and \( K_s) \) to describe the biodegradation process in the aerated reactor. If the aerated reactor test is used, the following procedure is used to analyze the data. Evaluate \( K_{eq} \) for the compound of interest with Form XI. The concentration in the vented headspace or liquid is measured as a function of time and the data is entered on Form XI. A plot is made from the data and attached to the Form XI. The concentration is calculated from \( K_{eq} \) completing Form XI. The values of \( K_{eq} \) may differ because the theoretical value of \( K_{eq} \) may not be applicable to the system of interest. If the comparison of the calculated \( K_{eq} \) from the form and the expected value of Henry's law obtained from Form IX is satisfactory, the stripping constant is calculated from \( K_{eq} \) completing Form XI. The final result of the batch testing is the measurement of a biorate that can be used to estimate the fraction biodegraded, \( f_{bio} \). The number transferred to Form III is obtained from Form XII, line 9.

2. Sealed Reactor Test. This test uses a closed system to prevent losses of the test compound by volatilization. This test may be conducted using a serum bottle or a sealed draft tube reactor (see Figure 3 of appendix C). Since no air is supplied, it is necessary to ensure that sufficient oxygen is present in the system. The DO concentration in the system must not fall below 2 mg/liter so that the biodegradation observed will not be DO-limited. As an alternative, oxygen may be supplied by electrolysis as needed to maintain the DO concentration above 2 mg/liter. The reactor contents must be uniformly mixed, by stirring...
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or agitation using a shaker or similar apparatus. The test mixture (or compound) of interest is injected into the reactor and the concentration is monitored over time. A minimum of six samples shall be taken over the period of the test. However, it is necessary to monitor the concentration until it falls below the LOQ.

The equilibrium assumption must be verified for the batch reactor system. In this case, $K_{eq}$ may be determined by simultaneously measuring gas and liquid phase concentrations at different times within a given experiment. A constant ratio of gas/liquid concentrations indicates that equilibrium conditions are present and $K_{eq}$ is not a function of concentration. This ratio is then taken as the $K_{eq}$ for the specific compound in the test. It is not necessary to measure $K_{eq}$ for each experiment. If the ratio is not constant, the equilibrium assumption is not valid and it is necessary to (1) increase mixing energy for the system and retest for the equilibrium assumption, or (2) use a different type of test (for example, a collapsible volume reactor).

The concentration of a compound decreases in the bioreactor due to biodegradation according to Equation App. C-5:

$$\frac{ds}{dt} = \left[ \frac{-V_l}{V_g K_{eq} + V_l} \right] \left( \frac{Q_m X}{K_s + s} \right)_s$$  (Eqn App. C-5)

Where:

$s = \text{test compound concentration (mg/liters)}$
$V_l = \text{the average liquid volume in the reactor (liters)}$
$V_g = \text{the average gas volume in the reactor (liters)}$
$Q_m = \text{maximum rate of substrate removal (mg/g MLVSS/hr)}$

$K_{eq} = \text{Henry's Law constant determined for the test, (mg/liter gas)/(mg/liter liquid)}$
$K_s = \text{Monod biorate constant at one-half the maximum rate (mg/liter)}$
$t = \text{time (hours)}$
$X = \text{biomass concentration (g MLVSS/liter)}$
$s_0 = \text{test compound concentration at time t=0}$

Equation App. C-5 can be solved analytically to give:

$$t = \left[ \frac{V_l K_{eq} + V_l}{V_l Q_m X} \right] \left( s - s_0 \right) + K_s \ln \left( \frac{s}{s_0} \right)$$  (Eqn App. C-6)

This equation is used along with the substrate concentration versus time data to determine the best fit parameters ($Q_m$ and $K_s$) to describe the biodegradation process in the sealed reactor.

If the sealed reactor test is used, Form X is used to determine the headspace correction factor. The disappearance of a compound in the sealed reactor test is slowed because a fraction of the compound is not available for biodegradation because it is present in the headspace. If the compound is almost entirely in the liquid phase, the headspace correction factor is approximately one. If the headspace correction factor is substantially less than one, improved mass transfer or reduced headspace may improve the accuracy of the sealed reactor test. A preliminary sealed reactor test must be conducted to test the equilibrium assumption. As the compound of interest is degraded, simultaneous headspace and liquid samples should be collected and Form X should be used to evaluate $K_{eq}$. The ratio of headspace to liquid concentrations must be constant in order to confirm that equilibrium conditions exist. If equilibrium conditions are not present, additional mixing or an alternate reactor configuration may be required.

The compound-specific biorate constants are then calculated using Form XII. For the sealed reactor test, a stripping rate constant of zero and the headspace correction factor that was determined from Form X are entered on Form XII. The sealed reactor test may then be run, measuring the concentrations of each compound of interest as a function of time. If headspace concentrations are measured instead of liquid concentrations, then the corresponding liquid concentrations are calculated from the headspace measurements using $K_{eq}$ from Form X and entered on Form XII.

The concentration data on Form XII may contain scatter that can adversely influence the data interpretation. It is possible to
curve the concentration data and enter the concentrations on the fitted curve instead of the actual data. If curve fitting is used, the curve-fitting procedure must be based on equation App. C-6. When curve fitting is used, it is necessary to attach a plot of the actual data and the fitted curve to Form XII.

If a sealed collapsible reactor is used that has no headspace, the headspace correction factor will equal 1, but the stripping rate constant may not equal 0 due to diffusion losses through the reactor wall. The ratio of the rate of loss of compound to the concentration of the compound in the reactor (units of per hour) must be evaluated. This loss ratio has the same units as the stripping rate constant and may be entered as the stripping rate constant on line 1 of Form XII.

If the loss due to diffusion through the walls of the collapsible reactor is relatively large when compared to the biorate at low concentrations, it may be difficult to obtain accurate evaluations of the first-order biorate constant. In these cases, either replacing the materials used to construct the reactor with materials of low permeability or increasing the biomass concentration should be considered.

The final results of the batch testing is the measurement of a biorate that can be used to estimate the fraction biodegraded, \( f_{bio} \). The number transferred to Form III is obtained from Form XII, line 9.

The number on Form XII line 9 will equal the Monod first-order biorate constant if the full-scale system is operated in the first-order range. If the full-scale system is operated at concentrations above that of the Monod first-order range, the value of the number on line 9 will be somewhat lower than the Monod first-order biorate constant.

With supporting biorate data, the Monod model used in Form XII may be used to estimate the effective biorate constant \( K_1 \) for use in Form III.

If a reactor with headspace is used, analysis of the data using equation App. C-6 is valid only if \( V_1 \) and \( V_2 \) do not change more than 10% (i.e., they can be approximated as constant for the duration of the test). Since biodegradation is occurring only in the liquid, as the liquid concentration decreases it is necessary for mass to transfer from the gas to the liquid phase. This may require vigorous mixing and/or reducing the volume in the headspace of the reactor.

If there is no headspace (e.g., a collapsible reactor), equation App. C-6 is independent of \( V_1 \) and there are no restrictions on the liquid volume. If a membrane or bag is used as the collapsible-volume reactor, it may be important to monitor for diffusion losses in the system. To determine if there are losses, the bag should be used without biomass and spiked with the compound(s) of interest. The concentration of the compound(s) in the reactor should be monitored over time. The data are analyzed as described above for the sealed reactor test.

IV. Calculation of \( F_{bio} \)

At this point, the individual \( f_{bio} \) determined by the previously explained procedures must be summed to obtain the total \( F_{bio} \). To determine the \( F_{bio} \), multiply each compound specific \( f_{bio} \) by the compound-specific average mass flow rate of the organic compound in the wastewater stream (see regulation for instruction on calculation of average mass flow rate). Sum these products and divide by the total wastewater stream average mass flow rate of organic compounds.
\[ F_{bio} = \frac{\sum_{i=1}^{n} (f_{bio,i} \times M_i)}{\sum_{i=1}^{m} M_i} \]  

(Eqn App. C−7)

\( M \) = compound specific average mass flow rate of the organic compounds in the wastewater (Mg/yr)
\( n \) = number of organic compounds in the wastewater

The \( F_{bio} \) is then used in the applicable compliance equations in the regulation to determine if biodegradation may be used to comply with the treatment standard without covering and venting to an air pollution control device.

References

<table>
<thead>
<tr>
<th>Compound</th>
<th>( H_\ell @ 25°C ) (am/mole frac)</th>
<th>( H_\ell @ 100°C ) (am/mole frac)</th>
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<tbody>
<tr>
<td>1 Acetaldehyde</td>
<td>4.87e+00</td>
<td>5.64e+01</td>
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<td>3 Acetonitrile</td>
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<td>25 Chloroform</td>
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<tr>
<td>31 Cumene</td>
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<td>32 1,4-Dichlorobenzene</td>
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<td>33 Dichloroethyl ether</td>
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<td>34 1,3-Dichloropropene</td>
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<td>36 N,N-Dimethylsalinimine</td>
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<td>1.57e+01</td>
</tr>
<tr>
<td>42 Dimethyl sulfate</td>
<td>2.23e-01</td>
<td>1.43e+01</td>
</tr>
<tr>
<td>43 2,4-Dinitrophenol</td>
<td>2.84e-01</td>
<td>1.50e+02</td>
</tr>
<tr>
<td>44 2,4-Dinitrotoluene</td>
<td>4.00e-01</td>
<td>9.62e+00</td>
</tr>
<tr>
<td>45 1,4-Dioxane</td>
<td>3.08e-01</td>
<td>9.53e+00</td>
</tr>
<tr>
<td>47 Epichlorohydrin</td>
<td>1.86e+00</td>
<td>4.34e+01</td>
</tr>
<tr>
<td>48 Ethyl acrylate</td>
<td>1.41e+01</td>
<td>3.01e+02</td>
</tr>
<tr>
<td>49 Ethylbenzene</td>
<td>4.38e+02</td>
<td>4.27e+03</td>
</tr>
<tr>
<td>50 Ethyl chloride (chloroethane)</td>
<td>6.72e+02</td>
<td>3.10e+03</td>
</tr>
<tr>
<td>Compound</td>
<td>Hl @ 25°C (atm/mole frac)</td>
<td>Hl @ 100°C (atm/mole frac)</td>
</tr>
<tr>
<td>----------------------------------------------</td>
<td>---------------------------</td>
<td>----------------------------</td>
</tr>
<tr>
<td>51 Ethylene dibromide</td>
<td>3.61e+01</td>
<td>5.15e+02</td>
</tr>
<tr>
<td>52 Ethylene dichloride (1,2-Dichloroethane)</td>
<td>6.54e+01</td>
<td>5.06e+02</td>
</tr>
<tr>
<td>54 Ethylene oxide</td>
<td>1.32e+01</td>
<td>9.03e+01</td>
</tr>
<tr>
<td>55 Ethylene dichloride (1,1-Dichloroethane)</td>
<td>3.12e+02</td>
<td>2.92e+03</td>
</tr>
<tr>
<td>57 Ethylene glycol dimethyl ether</td>
<td>1.95e+00</td>
<td>4.12e+01</td>
</tr>
<tr>
<td>60 Ethylene glycol monoethyl ether acetate</td>
<td>9.86e-02</td>
<td>6.03e+00</td>
</tr>
<tr>
<td>62 Ethylene glycol monomethyl ether acetate</td>
<td>1.22e-01</td>
<td>6.93e+00</td>
</tr>
<tr>
<td>64 Diethylene glycol dimethyl ether</td>
<td>8.38e-02</td>
<td>4.69e+00</td>
</tr>
<tr>
<td>65 Diethylene glycol diethyl ether</td>
<td>1.19e-01</td>
<td>7.71e+00</td>
</tr>
<tr>
<td>72 Ethylene glycol monobutyl ether acetate</td>
<td>2.75e-01</td>
<td>2.50e+01</td>
</tr>
<tr>
<td>73 Hexachlorobenzene</td>
<td>9.45e+01</td>
<td>2.57e+04</td>
</tr>
<tr>
<td>74 Hexachlorobutadiene</td>
<td>5.72e+02</td>
<td>6.92e+03</td>
</tr>
<tr>
<td>75 Hexachloroethane</td>
<td>4.64e+02</td>
<td>7.49e+04</td>
</tr>
<tr>
<td>76 Hexane</td>
<td>4.27e+04</td>
<td>9.44e+04</td>
</tr>
<tr>
<td>78 Isophorone</td>
<td>3.68e-01</td>
<td>1.68e+01</td>
</tr>
<tr>
<td>80 Methanol</td>
<td>2.89e-01</td>
<td>7.73e+00</td>
</tr>
<tr>
<td>81 Methyl bromide (Bromomethane)</td>
<td>3.81e+02</td>
<td>2.12e+03</td>
</tr>
<tr>
<td>82 Methyl chloride (Chloromethane)</td>
<td>4.90e+02</td>
<td>2.84e+03</td>
</tr>
<tr>
<td>83 Methyl chlorofluoromethane (1,1,1-Trichloroethane)</td>
<td>9.67e+02</td>
<td>5.73e+03</td>
</tr>
<tr>
<td>84 Methyl ethyl ketone (2-Butanone)</td>
<td>7.22e+00</td>
<td>5.92e+01</td>
</tr>
<tr>
<td>86 Methyl isobutyl ketone (Hexone)</td>
<td>2.17e+01</td>
<td>3.72e+02</td>
</tr>
<tr>
<td>88 Methyl methacrylate</td>
<td>7.83e+00</td>
<td>9.15e+01</td>
</tr>
<tr>
<td>89 Methyl tert-butyl ether</td>
<td>3.08e+01</td>
<td>2.67e+02</td>
</tr>
<tr>
<td>90 Methylene chloride (Dichloromethane)</td>
<td>1.64e+02</td>
<td>9.15e+02</td>
</tr>
<tr>
<td>93 Naphthalene</td>
<td>2.68e+01</td>
<td>7.10e+02</td>
</tr>
<tr>
<td>94 Nitrobenzene</td>
<td>1.33e+00</td>
<td>2.80e+01</td>
</tr>
<tr>
<td>96 2-Nitropropane</td>
<td>6.61e+00</td>
<td>8.76e+01</td>
</tr>
<tr>
<td>99 Phosgene</td>
<td>7.80e+02</td>
<td>3.51e+03</td>
</tr>
<tr>
<td>102 Propionaldehyde</td>
<td>3.32e+00</td>
<td>1.42e+02</td>
</tr>
<tr>
<td>103 Propylene dichloride</td>
<td>1.59e+01</td>
<td>1.27e+03</td>
</tr>
<tr>
<td>104 Propylene oxide</td>
<td>1.98e+01</td>
<td>1.84e+02</td>
</tr>
<tr>
<td>106 Styrene</td>
<td>1.45e+02</td>
<td>1.72e+03</td>
</tr>
<tr>
<td>107 1,1,2,2-Tetrachloroethane</td>
<td>1.39e+01</td>
<td>1.99e+02</td>
</tr>
<tr>
<td>108 Tetrachloroethylene (Perchloroethylene)</td>
<td>9.83e+02</td>
<td>1.84e+04</td>
</tr>
<tr>
<td>109 Toluene</td>
<td>3.57e+02</td>
<td>2.10e+03</td>
</tr>
<tr>
<td>112 o-Toluidine</td>
<td>1.34e+01</td>
<td>1.15e+01</td>
</tr>
<tr>
<td>113 1,2,4-Trichlorobenzene</td>
<td>1.07e+02</td>
<td>1.04e+03</td>
</tr>
<tr>
<td>114 1,1,2-Trichloroethane</td>
<td>4.58e+01</td>
<td>5.86e+02</td>
</tr>
<tr>
<td>115 Trichloroethylene</td>
<td>5.67e+02</td>
<td>7.66e+03</td>
</tr>
<tr>
<td>116 2,4,5-Trichlorophenol</td>
<td>4.84e+01</td>
<td>6.27e+01</td>
</tr>
<tr>
<td>117 Triethylamine</td>
<td>6.94e+00</td>
<td>2.57e+02</td>
</tr>
<tr>
<td>118 2,2,4-Trimethylpentane</td>
<td>1.85e+05</td>
<td>9.74e+05</td>
</tr>
<tr>
<td>119 Vinyl acetate</td>
<td>2.82e+01</td>
<td>2.80e+02</td>
</tr>
<tr>
<td>120 Vinyl chloride</td>
<td>1.47e+03</td>
<td>6.45e+03</td>
</tr>
<tr>
<td>121 Vinyl chloride (1,1-Dichloroethene)</td>
<td>1.44e+03</td>
<td>1.40e+04</td>
</tr>
<tr>
<td>123 m-Xylene</td>
<td>4.13e+02</td>
<td>3.25e+03</td>
</tr>
<tr>
<td>124 o-Xylene</td>
<td>2.71e+02</td>
<td>2.55e+03</td>
</tr>
<tr>
<td>125 p-Xylene</td>
<td>4.13e+02</td>
<td>3.20e+03</td>
</tr>
</tbody>
</table>
Figure 1. ALTERNATIVE EXPERIMENTAL METHODS FOR DETERMINING THE FRACTION OF ORGANIC COMPOUND BIODEGRADED (Fbio) IN A BIOLOGICAL TREATMENT UNIT
Figure 2. Example Aerated Draft Tube Reactor
Figure 3. Example Sealed Draft Tube Reactor
### DATA FORM FOR THE ESTIMATION OF THE EPA METHOD 304B FIRST ORDER BIORATE CONSTANT

<table>
<thead>
<tr>
<th>NAME OF THE FACILITY for site specific biorate determination</th>
<th>Example</th>
</tr>
</thead>
<tbody>
<tr>
<td>COMPOUND for site specific biorate determination</td>
<td>METHANOL</td>
</tr>
<tr>
<td>INLET CONCENTRATION used in EPA METHOD 304B</td>
<td>78</td>
</tr>
<tr>
<td>EXIT CONCENTRATION measured by EPA METHOD 304B</td>
<td>6</td>
</tr>
<tr>
<td>BIOMASS (g/L) This is the dried solids that are obtained from the mixed liquor suspended solids in the bench scale bioreactor.</td>
<td>0.075</td>
</tr>
<tr>
<td>TEMPERATURE OF BIOREACTOR (deg. C)</td>
<td>35</td>
</tr>
<tr>
<td>VOLUME of EPA METHOD 304B bench scale bioreactor (L)</td>
<td>6</td>
</tr>
<tr>
<td>FLOW RATE of waste treated in the bench scale bioreactor (L/hr)</td>
<td>0.140</td>
</tr>
</tbody>
</table>

### CALCULATIONS FROM EPA METHOD 304B DATA MEASUREMENTS

| RESIDENCE TIME (hr) Divide the number on line 5 by the number on line 6 and enter the results here. | 41.10 |
| Concentration Decrease (g/m³). Subtract the number on line 2 from the number on line 1 and enter the results here. | 72.00 |
| BIORATE (g/m³-hr). Divide the number on line 8 by the number on line 7 and enter the results here. | 1.75  |
| Product of concentration and biomass. Multiply the number on line 2 by the number on line 3 and enter the results here. | 0.45  |
| BIORATE K1 (L/g bio-hr) Divide the number on line 9 by the number on line 10 and enter the results here | 3.89  |
| Temperature adjustment. Subtract 25 deg. C from the number on line 4 and enter the results here. | 10    |
| Temperature adjustment factor. 1.046 is the default temperature adjustment factor. Enter the temperature adjustment factor here. | 1.046 |
| Biorate temperature ratio. Raise the number on line 13 to the power of the number on line 12. | 1.567 |
| BIORATE K1 at 25 deg. C (L/g MLVSS-hr) Divide the number on line 11 by the number on line 14 and enter the results here. | 2.48  |

**Note:** With Monod kinetics, use Kmax=1000 to convert the Monod kinetics to first order. If a different temperature adjustment factor than the default is entered on line 13, make sure that the adjustment factor used in the calculations agrees with the value entered on line 13.
<table>
<thead>
<tr>
<th>UNIT</th>
<th>PROCEDURE TO FOLLOW</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Use the quiescent impoundment model to determine KL. Use Kq as KL as determined from Form VII</td>
</tr>
<tr>
<td>2</td>
<td>Use the quiescent impoundment model to determine KL for the quiescent zone, Form VII. Use the aerated impoundment model to determine KL for the agitated surface, Form VIII.</td>
</tr>
<tr>
<td>3</td>
<td>Use the quiescent impoundment model to determine Kq for the quiescent zone, Form VII. Use the aerated impoundment model to determine KL for the agitated surface, Form VIII. The total system KL is the sum of the KL from Form VIII and the equivalent KL from Form V. Use the submerged air rate as the vent rate in Form V.</td>
</tr>
<tr>
<td>4</td>
<td>Use the aerated impoundment model to determine KL if the surface is agitated. Use the quiescent impoundment model if the surface is not agitated. KL includes the effect of volatilization in the air discharge. See section 5.6.1 in AIR EMISSIONS MODELS FOR WASTE AND WASTEWATER (EPA-453/R-94-080A). The total system KL is the sum of the KL from Form VIII and the equivalent KL from Form V. Use the submerged air rate as the vent rate in Form V.</td>
</tr>
<tr>
<td>5</td>
<td>KL for the surface is assumed to be equal zero. Determine equivalent KL based upon air discharge. Use Form V for EPA Method 304A or if the concentration in the vent is not measured. Use Form V-A if the concentration in the vent is measured.</td>
</tr>
</tbody>
</table>

Estimate of KL obtained from above procedures (m/s)

6
Form II-A

PROCEDURES FORM FOR THE
ESTIMATION OF THE KL FROM WATER 7

<table>
<thead>
<tr>
<th>NAME OF THE FACILITY for site specific biorate determination</th>
</tr>
</thead>
<tbody>
<tr>
<td>NAME OF UNIT for site specific biorate determination</td>
</tr>
<tr>
<td>NAME OF COMPOUND</td>
</tr>
<tr>
<td>HENRY’S LAW COMPOUND</td>
</tr>
</tbody>
</table>

IDENTIFY THE TYPE OF UNIT (check one box below)

| Quiescent impoundment               | 1 |
| Surface agitated impoundment        | 2 |
| Surface agitated impoundment with submerged air | 3 |
| Unit agitated by submerged aeration gas | 4 |
| Covered unit, UNOX system, bench scale reactor | 5 |

PROCEDURES BASED UPON THE TYPE OF UNIT

<table>
<thead>
<tr>
<th>unit</th>
<th>procedure to follow</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Use the quiescent impoundment model to determine KL.</td>
</tr>
<tr>
<td>2</td>
<td>Use the aerated impoundment model to determine KL for the combined agitated surfaces and quiescent surfaces.</td>
</tr>
<tr>
<td>3</td>
<td>Use the aerated impoundment model to determine KL for the combined agitated surfaces and quiescent surfaces.</td>
</tr>
<tr>
<td>4</td>
<td>Use the aerated impoundment model to determine KL if the surface is agitated. Use the quiescent impoundment model if the surface is not agitated. KL includes the effect of volatilization in the air discharge. See section 5.6.1 in AIR EMISSIONS MODELS FOR WASTE AND WASTEWATER (EPA-453/R-94-080A).</td>
</tr>
<tr>
<td>5</td>
<td>KL for the surface is assumed to equal zero. Select the covered unit option with the aerated impoundment model.</td>
</tr>
<tr>
<td>Form III</td>
<td>DATA FORM FOR THE ESTIMATION OF THE COMPOUND FRACTION BIODEGRADED AND AIR EMISSIONS</td>
</tr>
<tr>
<td>----------</td>
<td>-------------------------------------------------------------------------------------</td>
</tr>
<tr>
<td>NAME OF THE FACILITY for site specific biorate determination</td>
<td>example</td>
</tr>
<tr>
<td>COMPOUND for site specific biorate determination</td>
<td>methanol</td>
</tr>
<tr>
<td>ESTIMATE OF K1 from Form I line 11, Form V line 15, Form V-A line 15, Form IV line 14, Form VI line 13, or Form XII line 9 (L/g MLVSS-hr)</td>
<td>1</td>
</tr>
<tr>
<td>BIOMASS (g/L) This is the dried solids that are obtained from the mixed liquor suspended solids in the full-scale bioreactor</td>
<td>2</td>
</tr>
<tr>
<td>VOLUME of full-scale system (cubic meters)</td>
<td>3</td>
</tr>
<tr>
<td>AREA of the liquid surface of the full-scale system (square meters)</td>
<td>4</td>
</tr>
<tr>
<td>ESTIMATE OF KL from Form II, II-A, IV, V, V-A, or V-B (m/s)</td>
<td>5</td>
</tr>
<tr>
<td>FLOW RATE of waste treated in full-scale bioreactor (m³/s)</td>
<td>6</td>
</tr>
<tr>
<td>CALCULATIONS FROM ESTIMATES OF K1 AND KL</td>
<td></td>
</tr>
<tr>
<td>BIORATE (m³/s) Multiply the numbers on lines 1, 2, and 3 together and divide the results by 3600. Enter the results here</td>
<td>7</td>
</tr>
<tr>
<td>AIR STRIPPING (m³/s). Multiply the numbers on lines 4 and 5 together. Enter the results here.</td>
<td>8</td>
</tr>
<tr>
<td>EFFLUENT DISCHARGE (m³/s). Enter the number on line 6 here.</td>
<td>9</td>
</tr>
<tr>
<td>TOTAL of the three loss mechanisms. Add the numbers on lines 7, 8, and 9. Enter the results here</td>
<td>10</td>
</tr>
<tr>
<td>Fraction biodegraded: Divide the number on line 7 by the number on line 10 and enter the results here</td>
<td>11</td>
</tr>
<tr>
<td>Fraction air emissions: Divide the number on line 8 by the number on line 10 and enter the results here</td>
<td>12</td>
</tr>
<tr>
<td>Fraction remaining in unit effluent: Divide the number on line 9 by the number on line 10 and enter the results here</td>
<td>13</td>
</tr>
<tr>
<td>Total: add the numbers on lines 11, 12, and 13. The sum should equal 1.0</td>
<td>14</td>
</tr>
</tbody>
</table>
### DATA FORM FOR THE ESTIMATION OF K1 AND KL FROM FULL SCALE UNIT DATA WITH AND WITHOUT BIODEGRADATION

For a general discussion of this approach, see Air Emissions Models for Waste and Wastewater, EPA-453/R-94-080A, Chapter 5, November 1994.

<table>
<thead>
<tr>
<th><strong>NAME OF THE FACILITY for site specific bioreactor determination</strong></th>
<th>example</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>COMPOUND for site specific bioreactor determination</strong></td>
<td>methanol</td>
</tr>
<tr>
<td><strong>BIOMASS (g/L) This is the dried solids that are obtained from the mixed liquor suspended solids in the full-scale bioreactor.</strong></td>
<td>1</td>
</tr>
<tr>
<td><strong>VOLUME of full-scale system (cubic meters)</strong></td>
<td>2</td>
</tr>
<tr>
<td><strong>AREA of the liquid surface of the full-scale system (square meters)</strong></td>
<td>3</td>
</tr>
<tr>
<td><strong>INLET CONCENTRATION of compound (g/m² or ppmw)</strong></td>
<td>4</td>
</tr>
<tr>
<td><strong>EXIT CONCENTRATION of compound (g/m² or ppmw)</strong></td>
<td>5</td>
</tr>
<tr>
<td><strong>EXIT CONCENTRATION (NO BIODEGRADATION) of compound (g/m² or ppmw)</strong></td>
<td>6</td>
</tr>
<tr>
<td><strong>FLOW RATE of waste treated in the full-scale bioreactor (m²/s)</strong></td>
<td>7</td>
</tr>
</tbody>
</table>

### ESTIMATES OF K1 AND KL FROM FIELD DATA WITH AND WITHOUT BIODEGRADATION

| **REMOVAL WITH BIODEGRADATION (g/s) Subtract the number on line 5 from the number on line 4 and multiply the results by the number on line 7. Enter the results here.** | 8 | 19.238545 |
| **REMOVAL WITHOUT BIODEGRADATION (g/s) Subtract the number on line 6 from the number on line 4 and multiply the results by the number on line 7. Enter the results here.** | 9 | 0.078250 |
| **K1 A ESTIMATE (m²/s) Divide the number on line 9 by the number on line 6. Enter the results here.** | 10 | 0.000588 |
| **K1 B V + K1A ESTIMATE (m²/s) Divide the number on line 8 by the number on line 5. Enter the results here.** | 11 | 1.820108 |
| **K1 B V ESTIMATE (m²/s) Subtract the number on line 10 from the number on line 11. Enter the results here.** | 12 | 1.819520 |
| **Product of B and V. Multiply the number on line 1 by the number on line 2 and enter the results here.** | 13 | 6480 |
| **K1 ESTIMATE (L/gMLVSS-hr) Divide the number on line 12 by the number on line 13 and multiply by 3600 s/hr. Enter the results here.** | 14 | 1.010844 |
| **KL ESTIMATE (m/s) Divide the number on line 10 by the number on line 3. Enter the results here.** | 15 | 0.0000004 |
**Environmental Protection Agency**  
**Pt. 63, App. C**

<table>
<thead>
<tr>
<th>Form V</th>
<th>DATA FORM FOR THE ESTIMATION OF K1 FOR EPA METHOD 304A OR FROM A COVERED, VENTED BIODEGRADATION UNIT.</th>
</tr>
</thead>
</table>

For a general discussion of this approach, see Air Emissions Models for Waste and Wastewater, EPA-453/R-94-080A, Chapter 5, November 1994.

<table>
<thead>
<tr>
<th>NAME OF THE FACILITY for site specific bioreactor determination</th>
<th>example</th>
</tr>
</thead>
<tbody>
<tr>
<td>COMPOUND for site specific bioreactor determination</td>
<td>methanol</td>
</tr>
</tbody>
</table>

| BIOMASS (g/L) This is the dried solids that are obtained from the mixed liquor suspended solids in the unit | 1 | 0.075 |
| VENT RATE of total gas leaving the unit (G, m³/s) | 2 | 1 |
| TEMPERATURE of the liquid in the unit (deg. C) | 3 | 25 |
| INLET CONCENTRATION of compound (g/m³ or ppmw) | 4 | 100 |
| EXIT CONCENTRATION of compound (g/m³ or ppmw) | 5 | 5 |

| ESTIMATE OF Henry's law constant (H, g/m³ in gas / g/m³ in liquid). Obtained from Form IX | 6 | 0.00021 |
| AREA OF REACTOR (m²) | 7 | 3400 |
| VOLUME OF REACTOR (m³) | 8 | 10000 |
| FLOW RATE of waste treated in the unit (m³/s) | 9 | 0.146 |

| CALCULATION OF THE ESTIMATE OF K1 |
| TOTAL REMOVAL (g/s) Subtract the number on line 5 from the number on line 4 and multiply the result by the number on line 9. Enter the results here. | 10 | 13.870000 |

| [H G] ESTIMATE (m³/s) Multiply the number on line 2 by the number on line 6. Enter the results here. | 11 | 0.000021 |

| [K1 B V] [H G] (m³/s) Divide the number on line 10 by the number on line 5. Enter the results here. | 12 | 2.774000 |

| [K1 B V] ESTIMATE (m³/s) Subtract the number on line 11 from the number on line 12. Enter the results here. | 13 | 2.773979 |

If the number on line 11 is greater than the number on line 13, this procedure cannot be used to demonstrate that the compound is biodegradable. Do not complete lines 14 and 15.

| Product of B and V. Multiply the number on line 1 by the number on line 8 and enter the results here. | 14 | 750.00000 |

| K1 ESTIMATE (L/g MLVSS-hr) Divide the number on line 13 by the number on line 14 and multiply by 3600 s/hr. Enter the results here. | 15 | 13.315099 |

| EQUIVALENT KL Divide the number on line 11 by the number on line 7. Enter the results on line 16. | 16 | 6.18e-09 |

This form may be used to estimate the Equivalent KL with input data for lines 2, 6, and 7.
Form V-A  DATA FORM FOR THE CALCULATION OF KI FROM A COVERED, VENTED BIODREDGATION UNIT. THE VENT CONCENTRATION IS MEASURED

For a general discussion of this approach, see Air Emissions Models for Waste and Wastewater, EPA-453/R-94-080A, Chapter 5, November 1994.

| NAME OF THE FACILITY for site specific biorate determination | example |
| COMPOUND for site specific biorate determination | methanol |
| BIOMASS (g/L) This is the dried solids that are obtained from the mixed liquor suspended solids in the unit. | 1 | 0.075 |
| VENT RATE of total gas leaving the unit (G, m³/s) | 2 | 1 |
| TEMPERATURE of the liquid in the unit (deg. C) | 3 | 25 |
| INLET CONCENTRATION of compound (Ci, g/m³ or ppmw) | 4 | 100 |
| EXIT CONCENTRATION of compound (Ce, g/m³ or ppmw) | 5 | 5 |
| VENT CONCENTRATION of compound (Cv, g/m³ or ppmw) | 6 | 0.101 |
| AREA OF REACTOR SURFACE (m²) | 7 | 3400 |
| VOLUME OF REACTOR (m³) | 8 | 10000 |
| FLOW RATE of waste treated in the unit (m³/s) | 9 | 0.146 |

**CALCULATION OF THE ESTIMATE OF KI**

| TOTAL REMOVAL (g/s) Subtract the number on line 5 from the number on line 4 and multiply the results by the number on line 9. Enter the results here. | 10 | 13.87 |

\[ \frac{G}{C_v/C_e} \] ESTIMATE (m³/s) Multiply the number on line 2 by the number on line 6 and divide by the number on line 5. Enter the results here.

\[ [K_iBv + G/Cv/Ce] \] (m³/s) Divide the number on line 10 by the number on line 5. Enter the results here.

\[ [K_iBv] \] ESTIMATE (m³/s) Subtract the number on line 11 from the number on line 12. Enter the results here.

If the number on line 11 is greater than the number on line 13, this procedure cannot be used to demonstrate that the compound is biodegradable. Do not complete lines 14 and 15.

Product of B and V. Multiply the number on line 1 by the number on line 8 and enter the results here.

K1 ESTIMATE (L/g MLVSS-hr) Divide the number on line 13 by the number on line 14 and multiply by 3600 s/hr. Enter the results here.

EQUIVALENT KL. Divide the number on line 11 by the number on line 7. Enter the results here.

This form may be used to calculate the Equivalent KL with input data for lines 2, 5, 6, and 7.
Form V-B  DATA FORM FOR THE CALCULATION OF EQUIVALENT KL
FROM A VENTED BIODEGRADATIN UNIT WITH AN AIR SUPPORTED COVER.
THE VENT CONCENTRATION IS MEASURED.

<table>
<thead>
<tr>
<th>NAME OF THE FACILITY for site specific biorate determination</th>
<th>example</th>
</tr>
</thead>
<tbody>
<tr>
<td>COMPOUND for site specific biorate determination</td>
<td>methanol</td>
</tr>
<tr>
<td>Vent rate of total gas entering the cover (m³/s)</td>
<td>1</td>
</tr>
<tr>
<td>Vent rate of total gas leaving the cover transferred to a control device (m³/s)</td>
<td>2</td>
</tr>
<tr>
<td>TEMPERATURE of the liquid in the unit (deg. C)</td>
<td>3</td>
</tr>
<tr>
<td>Area of air supported cover (m²)</td>
<td>4</td>
</tr>
<tr>
<td>Permeability through the cover (cm/s)</td>
<td>5</td>
</tr>
<tr>
<td>VENT CONCENTRATION of compound (g/m³)</td>
<td>6</td>
</tr>
<tr>
<td>EXIT CONCENTRATION of compound (g/m³ or ppmw)</td>
<td>7</td>
</tr>
<tr>
<td>AREA OF REACTOR SURFACE (m²)</td>
<td>8</td>
</tr>
<tr>
<td>Performance of vent control device (% control)</td>
<td>9</td>
</tr>
</tbody>
</table>

CALCULATION OF THE ESTIMATE OF EQUIVALENT KL

| Loss of forced air in the cover due to leakage. (m³/s) Subtract the number on line 2 from the number on line 1. Enter the results here. | 10 | 20 |
| Loss of compound in forced air (g/s) Multiply the number on line 10 by the number on line 6. Enter the results here. | 11 | 0.044 |
| Loss of compound by permeation through cover (g/s). Line 4 times line 5, line 6, and divide by 100. Enter the results here. | 12 | 0 |
| Loss of compound by permeation through vent (g/s). Line 2 times line 6. Enter the results here. | 13 | 0.22 |
| Treatment of compound in control device (g/s). Line 13 times line 9, divided by 100. Enter the results here. | 14 | 0.209 |
| Total removal from air phase (g/s) Sum of 11, 12, and 13. | 15 | 0.264 |
| Total treatment effectiveness (%) Line 14 divided by 15 times 100. | 16 | 79.1666 |
| [G.Cv/Cc] ESTIMATE (m³/s) Divide line 15 by line 7. | 17 | 0.025 |
| EQUIVALENT KL. Divide the number on line 17 by line 8. | 18 | 1.676-05 |

The permeability is the ratio of the flux (g/cm²) to the gas concentration (g/cm³).
If the gas is generated by the unit, the gas entering the cover may be estimated from an estimate of the cover leak rate and the total gas transferred to the control device.
<table>
<thead>
<tr>
<th>Form VI</th>
<th>DATA FORM FOR THE ESTIMATION OF K1 FROM FULL SCALE UNIT DATA WITH BIODEGRADATION</th>
</tr>
</thead>
<tbody>
<tr>
<td>NAME OF THE FACILITY for site specific biorate determination</td>
<td>example</td>
</tr>
<tr>
<td>COMPOUND for site specific biorate determination</td>
<td>methanol</td>
</tr>
<tr>
<td>BIOMASS (g/L) This is the dried solids that are obtained from the mixed liquor suspended solids in the full-scale bioreactor.</td>
<td>1</td>
</tr>
<tr>
<td>VOLUME of full-scale system (cubic meters)</td>
<td>2</td>
</tr>
<tr>
<td>AREA of the liquid surface of the full-scale system (square meters)</td>
<td>3</td>
</tr>
<tr>
<td>INLET CONCENTRATION of compound (g/m³ or ppmw)</td>
<td>4</td>
</tr>
<tr>
<td>EXIT CONCENTRATION of compound (g/m³ or ppmw)</td>
<td>5</td>
</tr>
<tr>
<td>ESTIMATE OF KL from Form II (m/s)</td>
<td>6</td>
</tr>
<tr>
<td>FLOW RATE of waste treated in the full-scale bioreactor (m³/s)</td>
<td>7</td>
</tr>
<tr>
<td>CALCULATION OF THE ESTIMATE OF K1 FROM FIELD DATA</td>
<td></td>
</tr>
<tr>
<td>REMOVAL WITH BIODEGRADATION (g/s) Subtract the number on line 5 from the number on line 4 and multiply the results by the number on line 7. Enter the results here</td>
<td>8</td>
</tr>
<tr>
<td>[KL A] ESTIMATE (m³/s) Multiply the number on line 3 by the number on line 6. Enter the results here.</td>
<td>9</td>
</tr>
<tr>
<td>[K1 B V + KL A] (m³/s) Divide the number on line 8 by the number on line 5. Enter the results here.</td>
<td>10</td>
</tr>
<tr>
<td>[K1 B V] ESTIMATE (m³/s) Subtract the number on line 9 from the number on line 10. Enter the results here.</td>
<td>11</td>
</tr>
<tr>
<td>Product of B and V. Multiply the number on line 1 by the number on line 2 and enter the results here.</td>
<td>12</td>
</tr>
<tr>
<td>K1 ESTIMATE (L/g MLVSS-hr) Divide the number on line 11 by the number on line 12 and multiply by 3600 s/hr. Enter the results here.</td>
<td>13</td>
</tr>
</tbody>
</table>
FORM VII
DATA FORM FOR CALCULATING THE
MASS TRANSFER COEFFICIENT FOR A QUIESCENT SURFACE IMPOUNDMENT

Facility Name: ____________________________________________________________

Waste Stream Compound: ________________________________________________

Enter the following:

- F - Impoundment fetch (m)
- D - Impoundment depth (m)
- U_{10} - Windspeed 10 m above liquid surface (m/s)
- D_w - Diffusivity of compound in water (cm^2/s)
- D_{sw} - Diffusivity of ether in water (cm^2/s)
- \mu_0 - Viscosity of air, (g/cm-s)
- \rho_a - Density of air, (g/cm^3)
- D - Diffusivity of compound in air, (cm^2/s)
- A - Area of impoundment, (m^2)
- H - Henry's law constant, (atm-m^3/g mol)
- R - Universal gas constant, (atm-m^3/g mol K)
- \mu_w - Viscosity of water, (g/cm-s)
- \rho_l - Density of liquid, (g/cm^3)
- T - Impoundment temperature, (°C)

Calculate the following:

Calculate F/D:

A. Calculate the liquid phase mass transfer coefficient, k_l, using one of the following procedures, (m/s)

1. Where F/D < 14 and U_{10} > 3.25 m/s, use the following procedure from MacKay and Yuen:

   Calculate the Schmidt number on the liquid side, S_{Sc}, as follows:
   S_{Sc} = \mu_w/\rho_l D_w

   Calculate the friction velocity, U', as follows, (m/s):
   U' = 0.01 \times U_{10} \times (6.1 + 0.63 U_{10})^{0.5}

   Where U' > 0.3, calculate k_l as follows:
   k_l = (1.0 \times 10^{-6}) + (54.1 \times 10^{-6}) U' \times S_{Sc}^{0.5}

   Where U' < 0.3, calculate k_l as follows:
   k_l = (1.0 \times 10^{-6}) + (144 \times 10^{-6}) U'^2 \times S_{Sc}^{0.5}

2. For all other values of F/D and U_{10}, calculate k_l using the following procedure from Springer.3

Where \( U_{in} \) is < 3.25 m/s, calculate \( k_e \) as follows:

\[
k_e = 2.78 \times 10^4 \left( \frac{D_e}{D_{th}} \right)^{0.23}
\]

Where \( U_{in} \) is > 3.25 and \( 14 < F/D < 51 \) 2. Calculate \( k_e \) as follows:

\[
k_e = \left[ 2.605 \times 10^3 \left( \frac{F}{D} \right) + 1.277 \times 10^4 \right] \left( \frac{U_{in}}{D_{th}} \right)^{0.23}
\]

Where \( U_{in} > 3.25 \) m/s and \( F/D > 51 \) 2, calculate \( k_e \) as follows:

\[
k_e = \left( 2.611 \times 10^7 \right) \left( \frac{U_{in}}{D_{th}} \right)^{0.23}
\]

B. Calculate the gas phase mass transfer coefficient, \( k_g \), using the following procedure from MacKay and Matsasug. (m/s):\(^2\)

Calculate the Schmidt number on the gas side, \( Sc_g \), as follows: \( Sc_g = \mu_g / \rho_g D_g \)

Calculate the effective diameter of the impoundment, \( d_e \), as follows, (m):

\[
d_e = \left( \frac{4 \pi \rho_g}{\mu_g} \right)^{0.5}
\]

Calculate \( k_g \), as follows, (m/s): \( k_g = 4.82 \times 10^3 U_{in} \cdot \nu \cdot Sc_g^{0.47} d_e^{0.17} \)

C. Calculate the partition coefficient, \( K_{eq} \), as follows: \( K_{eq} = H[R(T+273)] \)

D. Calculate the overall mass transfer coefficient, \( K_{eq} \), as follows, (m/s):

\[
1 / K_{eq} = 1 / k_e + 1 / K_{eq} / k_g
\]

Where the total impoundment surface is quiescent:

\[
KL = K_g
\]

Where a portion of the impoundment surface is turbulent, continue with Form VIII.

---

FORM VIII

DATA FORM FOR CALCULATING THE
MASS TRANSFER COEFFICIENT FOR AN AERATED SURFACE IMPOUNDMENT

Facility Name: 

Waste Stream Compound: 

Enter the following:

- $J$ - Oxygen transfer rate of surface aerator, (lb O₂/hr-hp)
- $POWR$ - Total power to aerators, (hp)
- $T$ - Water temperature, ($°$C)
- $O_T$ - Oxygen transfer correction factor
- $MW_L$ - Molecular weight of liquid
- $A_T$ - Turbulent surface area of impoundment, (ft²)
  (If unknown, use values from Table 1)
- $A$ - Total surface area of impoundment, (ft²)
- $\rho_L$ - Density of liquid, (lb/ft³)
- $D_L$ - Diffusivity of constituent in water, (cm²/s)
- $D_{O₂,w}$ - Diffusivity of oxygen in water, (cm²/s)
- $d$ - Impeller diameter, (cm)
- $w$ - Rotational speed of impeller, (rad/s)
- $\rho_A$ - Density of air, (gm/cm³)
- $N$ - Number of aerators
- $g_T$ - Gravitation constant, (lb. ft/s²/lb)
- $d'$ - Impeller diameter, (ft)
- $D_A$ - Diffusivity of constituent in air, (cm²/s)
- $MW_A$ - Molecular weight of air
- $R$ - Universal gas constant, (atm·m³/g mol. °C)
- $H$ - Henry's law constant, (atm·m³/g mol)

Calculate the following:

A. Calculate the liquid phase mass transfer coefficient, $k_L$, using the following Equation from
Thibodeaux: 1, 2

$$k_L = [8.22 \times 10^9 J (POWR) (1.024)^{7.29} O_T 10^6 MW_L (VA_T \rho_L) (D_L D_{O₂,w})^{0.4} ]$$ (m/s)


B. Calculate the gas phase mass transfer coefficient, \( k_{\text{g}} \), using the following procedure from Reinhardt.\(^5\),\(^6\)

Calculate the viscosity of air, \( \mu_{\text{a}} \), as follows, (g/cm·s):
\[
\mu_{\text{a}} = 4.568 \times 10^{-5} \ T + 1.7209 \times 10^{-5}
\]

Calculate the Reynolds number as follows:
\[
R_e = d \omega \rho_{\text{a}} / \mu_{\text{a}}
\]

Calculate power to impeller, \( P_i \), as follows, (ft·lb/s):
\[
P_i = 0.85 \times \text{(POWER) 550}/N
\]

Calculate the power number, \( p \), as follows:
\[
p = P_i \rho_{\text{a}} / (\rho_{\text{a}} d^3 \omega^3)
\]

Calculate the Schmidt number, \( S_{\text{Sc}} \), as follows:
\[
S_{\text{Sc}} = \mu_{\text{a}} / \rho_{\text{a}} D_{\text{a}}
\]

Calculate the Froude number, \( F_r \), as follows:
\[
F_r = d \omega^2 / g_{\text{a}}
\]

Calculate \( k_{\text{g}} \) as follows:
\[
k_{\text{g}} = 1.35 \times 10^{-6} \ R_e^{0.62} \rho_{\text{a}}^{0.3} S_{\text{Sc}}^{0.13} F_r^{-0.21} D_{\text{a}} \rho_{\text{a}} / d, \text{ (m/s)}
\]

C. Calculate the partition coefficient, \( K_{\text{eq}} \), as follows:
\[
K_{\text{eq}} = \frac{H[R(T+273)]}{H[R(T+273)]}
\]

D. Calculate the overall turbulent mass transfer coefficient, \( K_{\text{t}} \), as follows, (m/s):
\[
1/K_{\text{t}} = 1/k_{\text{g}} + 1/K_{\text{eq}} k_{\text{g}}
\]

E. Calculate the quiescent mass transfer coefficient, \( K_{\text{q}} \), for the impoundment using Form VII.

F. Calculate the overall mass transfer coefficient, \( K_L \), for the impoundment as follows:
\[
K_L = K_{\text{g}} (A - A_j) + K_{\text{a}} A_j
\]


Table 1. Turbulent Areas and Volumes for Surface Agitators*

<table>
<thead>
<tr>
<th>Motor horsepower, hp</th>
<th>$A_T$, Turbulent area, ft$^2$</th>
<th>Effective depth, ft</th>
<th>$V$, Agitated volume, ft$^3$</th>
<th>$a_{av}$, Area per volume ft$^3$/ft$^3$</th>
</tr>
</thead>
<tbody>
<tr>
<td>5</td>
<td>177</td>
<td>16.4</td>
<td>10</td>
<td>1,767</td>
</tr>
<tr>
<td>7.5</td>
<td>201</td>
<td>18.7</td>
<td>10</td>
<td>2,010</td>
</tr>
<tr>
<td>10</td>
<td>227</td>
<td>21</td>
<td>10.5</td>
<td>2,383</td>
</tr>
<tr>
<td>15</td>
<td>284</td>
<td>26.4</td>
<td>11</td>
<td>3,119</td>
</tr>
<tr>
<td>20</td>
<td>346</td>
<td>32.1</td>
<td>11.5</td>
<td>3,983</td>
</tr>
<tr>
<td>25</td>
<td>415</td>
<td>38.6</td>
<td>12</td>
<td>4,986</td>
</tr>
<tr>
<td>30</td>
<td>491</td>
<td>45.7</td>
<td>12</td>
<td>5,890</td>
</tr>
<tr>
<td>40</td>
<td>661</td>
<td>61.4</td>
<td>13</td>
<td>8,587</td>
</tr>
<tr>
<td>50</td>
<td>855</td>
<td>79.5</td>
<td>14</td>
<td>11,970</td>
</tr>
<tr>
<td>60</td>
<td>1,075</td>
<td>100</td>
<td>15</td>
<td>16,130</td>
</tr>
<tr>
<td>75</td>
<td>1,452</td>
<td>135</td>
<td>16</td>
<td>23,240</td>
</tr>
<tr>
<td>100</td>
<td>2,206</td>
<td>205</td>
<td>18</td>
<td>39,710</td>
</tr>
</tbody>
</table>

*Data for a high speed (1,200) rpm aerator with 60 cm propeller diameter (d).
## DATA FORM FOR THE ESTIMATION OF THE HENRY'S LAW CONSTANT FOR A COMPOUND IN THE BIOLOGICAL TREATMENT UNIT

<table>
<thead>
<tr>
<th>Name of the Facility for site specific biorate determination</th>
<th>Example</th>
</tr>
</thead>
<tbody>
<tr>
<td>Compound for site specific biorate determination</td>
<td>Methanol</td>
</tr>
<tr>
<td>Listed Henry's Law Value at 25 degrees Celsius. (Table 1, ratio of mol fraction in gas to mole fraction in water)</td>
<td>1.0</td>
</tr>
<tr>
<td>Temperature of the liquid in the unit (deg C)</td>
<td>2.0</td>
</tr>
<tr>
<td>Calculation of K</td>
<td></td>
</tr>
<tr>
<td>Temperature adjusted Henry's law value (equals the value on line 1 if the temperature on line 2 is 25)</td>
<td>3.0</td>
</tr>
<tr>
<td>Discuss basis of temperature adjustment</td>
<td></td>
</tr>
</tbody>
</table>

| Temperature in degrees Kelvin. Add 273.16 to the number on line 2. Enter the results here. | 4.0   | 298.1600  |
| Temperature ratio. Divide 273.16 by the number on line 4. Enter the results here.            | 5.0   | 0.9162    |
| Henry's Law adjustment factor. Multiply the number on line 5 by 0.804 and enter the results here. | 6.0   | 0.7366    |
| Henry's Law value (g/m^3 gas per g/m^3 liquid). Multiply the number on line 3 by the number on line 6 and divide the results by 1000. Enter the results here and on Form V line 6. | 7.0   | 0.000213  |
| Henry's Law value (atm m^3 per mol). Divide the number on line 3 by 55555 and enter the results here. | 8.0   | 0.000005  |
Form X
DATA FORM FOR THE CALCULATION OF
THE HENRY'S LAW CONSTANT FOR A COMPOUND IN A SEALED BATCH TEST

<table>
<thead>
<tr>
<th>NAME OF THE FACILITY for site specific borate determination</th>
<th>example</th>
</tr>
</thead>
<tbody>
<tr>
<td>COMPOUND for site specific borate determination</td>
<td>methanol</td>
</tr>
<tr>
<td>REACTOR HEADSPACE VOLUME (L)</td>
<td>1</td>
</tr>
<tr>
<td>REACTOR LIQUID VOLUME (L)</td>
<td>2</td>
</tr>
<tr>
<td>TEMPERATURE of the liquid in the unit (deg C)</td>
<td>3</td>
</tr>
</tbody>
</table>

Wastewater compounds are biodegraded by biomass in a sealed batch test. For the compound listed above, a data set of liquid and gas concentrations is measured at four different times during the sealed batch test. The data are entered below, and the ratio of the concentrations for each data set is entered in column E.

<table>
<thead>
<tr>
<th>A</th>
<th>B</th>
<th>C</th>
<th>D</th>
<th>E</th>
</tr>
</thead>
<tbody>
<tr>
<td>Data set</td>
<td>Time (hr)</td>
<td>Liquid Conc. (mg/L)</td>
<td>Gas Conc. (mg/L)</td>
<td>$K_w$ D/C</td>
</tr>
<tr>
<td>1</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>2</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>3</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>4</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Temperature in degrees Kelvin. Add 273.16 to the number on line 3. Enter the results here

Molar ratio. Multiply the number on line 4 by 4.555. Enter the results on line 5

Henry's law value (mg/L gas per mg/L liquid). Enter the average value in column E above on line 6.

Henry's law value (mole fraction gas per mole fraction liquid) Multiply the number on line 6 by the number on line 5. Enter the results on line 7.

Expected Henry's law value. Enter the number from Form IX line 3.

Precision: Discuss any variability of the numbers in column E.
Accuracy: Discuss any difference between the numbers on line 7 and line 8. Identify which value will be used for evaluating the biodegradation rate data. Divide the Henry's law value by the number on line 8 and enter the results on line 9.

$K_w$ value (mg/L gas per mg/L liquid)

HEADSPACE CORRECTION FACTOR. Divide the number on line 2 by the sum of the number on line 2 and the product of the numbers on line 9 and line 1. Enter the result on line 10.

The headspace correction factor should equal approximately 1 if the headspace is relatively small. Reducing the headspace volume may improve the test data quality if the headspace correction factor is substantially less than one.
Form XI

| NAME OF THE FACILITY for site specific biorate determination | example |
| Concentration basis (liquid or gas) | gas |
| TEMPERATURE of the liquid in the unit (deg C) | 1 | 25 |
| GAS FLOW RATE (L/hr) | 2 | 1 |
| LIQUID VOLUME (L) | 3 | 10 |
| Co concentration measurement at time=0 (mg/L) | 4 |

<table>
<thead>
<tr>
<th>A</th>
<th>B</th>
<th>C</th>
<th>D</th>
<th>E</th>
</tr>
</thead>
<tbody>
<tr>
<td>data point</td>
<td>time (hr)</td>
<td>Concentration, C (mg/L)</td>
<td>C/Co</td>
<td>-ln(C/Co)</td>
</tr>
<tr>
<td>1</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>2</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>3</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>4</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>5</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

CALCULATIONS. Use additional lines as needed in an expansion of the above table. Plot the values in column E (y axis) vs the data in column B (x axis). Reject outliers. Curve fit with a straight line. Calculate the slope and enter the slope on line 7. Attach the plot and table to this form.

| Temperature in degrees Kelvin. Add 273.16 to the number on line 1. Enter the results here. | 5 | 298.16 |
| MOLAR RATIO Multiply the number on line 5 by 4.555. Enter the results on line 6. | 6 | 1,358.12 |
| Slope of the plot of -ln(C/Co) vs time (per hour) | 7 | 2.10e-05 |
| Calculated K_w value (mg/L gas per mg/L liquid) Divide the number on line 7 by the number on line 2 and multiply the results by the number 10. Enter the results on line 8. | 8 | 0.000210 |
| Expected K_w value. Divide the number from Form IX line 3 by the number on line 6 and enter the results on line 9. | 9 | 0.000212 |

Discuss any differences between the numbers on line 8 and line 9. Identify which value will be used for the evaluation of the stripping constant (line 10). Problems can sometimes be resolved by system redesign, changing the bubble size, or confirming the experimental value of K_w by using Form X.

| K_w value (mg/L gas per mg/L liquid) | 10 | 0.000210 |
| STRIPPING CONSTANT (per hour). Divide the number on line 10 by number on line 3 and multiply by the number on line 2. Enter the final result on line 11. | 11 | 0.000021 |

The headspace correction factor equals one for an aerated batch test.
<table>
<thead>
<tr>
<th>A</th>
<th>B</th>
<th>C</th>
<th>D</th>
<th>E</th>
<th>F</th>
<th>G</th>
</tr>
</thead>
<tbody>
<tr>
<td>concentration (mg/L)</td>
<td>time (hr)</td>
<td>Rate for interval (mg/L-hr)</td>
<td>Log Mean S for interval (mg/L)</td>
<td>Ratio of rate to S (hr)</td>
<td>Adjusted rate (hr)</td>
<td>Reciprocal of adj. rate (hr)</td>
</tr>
<tr>
<td>1</td>
<td>2</td>
<td>3</td>
<td>4</td>
<td>5</td>
<td>6</td>
<td>7</td>
</tr>
</tbody>
</table>

Continue table on attached sheet as needed. Plot values in column G on y axis, values in column D on x axis. Extrapolate the trend of data points to the y intercept (S=0). Attach the plot to the form.

Slope of line near intercept (hr-L/mg) = 4.4845
Y intercept from plot (hr) = 5.1938
First order rate constant K1 (or Qm/Ks, L/g-hr) The number 1.00 divided by the products of the values on line 5, line 2, and line 3. = 2.000026
Zero order rate constant (Qm, hr). The number 1.00 divided by the products of the values on line 4, line 2, and line 3. = 8.001104
Concentration applicable to full-scale unit. Enter on line 8. = 5
Effective biorate K1 ESTIMATE (L/g MLVSS-hr)* = 0.9606

*Match the concentration on line 8 to the values in Column D and look up the equivalent rate in Column F. Divide the result with both the biomass concentration (line 2) and the headspace correction factor (line 3). Enter this value on line 9. Do not use this method to estimate K1 for line 9 if the data quality is poor in Column F. The number on line 9 is multiplied by the biomass and the system concentration to estimate the full scale biorate. Alternatively, the Monod model parameters may be used.

1. Applicability
This procedure is to be applied exclusively to Environmental Protection Agency methods developed by the Office of Water and the Office of Solid Waste. Alternative methods developed by any other group or agency shall be validated according to the procedures in Sections 5.1 and 5.3 of Test Method 301, 40 CFR Part 63, Appendix A. For the purposes of this appendix, “waste” means waste and wastewater.

2. Procedure
This procedure shall be applied once for each waste matrix. Waste matrix in the context of this procedure refers to the target compound mixture in the waste as well as the formulation of the medium in which the target compounds are suspended. The owner or operator shall prepare a sampling plan. Wastewater samples shall be collected using sampling procedures which minimize loss of organic compounds during sample collection and analysis and maintain sample integrity. The sample plan shall include procedures for determining recovery efficiency of the relevant compounds regulated in the applicable subpart. An example of an acceptable sampling plan would be one that incorporates similar sampling and sample handling requirements to those of Method 25D of 40 CFR part 60, appendix A.

2.1. Sampling and Analysis

2.1.1. For each waste matrix, collect twice the number of samples required by the applicable regulation. Designate and label half the sample vials the “spiked” sample set, and the other half the “unspiked” sample set. Immediately before or immediately after sampling (immediately after in the context of this procedure means after placing the sample into the sample vial, but before the sample is capped, cooled, and shipped to the laboratory for analysis), inject, either individually or as a solution, all the target compounds into each spiked sample.

2.1.2. The mass of each spiked compound shall be 40 to 60 percent of the mass expected to be present in the waste matrix. If the concentration of the target compounds in the waste are not known, the mass of each spiked compound shall be 40 to 60 percent of the limit allowed in the applicable regulation. Analyze both sets of samples (spiked and unspiked) with the chosen method.

3. Calculations
For each pair of spiked and unspiked samples, determine the fraction of spiked compound recovered (R) using the following equations.

where:
\[ m_r = \text{mass spiked compound measured (µg)} \]
\[ m_s = \text{total mass of compound measured in spiked sample (µg)} \]
\[ m_u = \text{total mass of compound measured in unspiked sample (µg)} \]

where:
\[ S = \text{theoretical mass of compound spiked into spiked sample (µg)} \]

3.1. Method Evaluation
In order for the chosen method to be acceptable for a compound, 0.70 ≤ R ≤ 1.30 (R in this case is an average value of all the spiked and unspiked sample set R values). If the average R value does not meet this criterion for a target compound, the chosen method is not acceptable for that compound, and therefore another method shall be evaluated for acceptance (by repeating the procedures outlined above with another method).

3.2. Records and Reports
Report the average R value in the test report and correct all reported measurements made with the method with the calculated R value for that compound by using the following equation:

\[ \text{Reported Result} = \frac{\text{Measured Mass of Compound}}{R \text{ for that compound}} \]

3.3. Optional Correction Step
If the applicable regulation allows for correction of the mass of the compound in the waste by a published \( f_m \) value, multiply the reported result calculated above with the appropriate \( f_m \) value for that compound.

[61 FR 34200, July 1, 1996]
A list of CFR titles, subtitles, chapters, subchapters and parts and an alphabetical list of agencies publishing in the CFR are included in the CFR Index and Finding Aids volume to the Code of Federal Regulations which is published separately and revised annually.

Material Approved for Incorporation by Reference
Table of CFR Titles and Chapters
Alphabetical List of Agencies Appearing in the CFR
List of CFR Sections Affected
Material Approved for Incorporation by Reference
(Revised as of July 1, 1999)

The Director of the Federal Register has approved under 5 U.S.C. 552(a) and 1 CFR Part 51 the incorporation by reference of the following publications. This list contains only those incorporations by reference effective as of the revision date of this volume. Incorporations by reference found within a regulation are effective upon the effective date of that regulation. For more information on incorporation by reference, see the preliminary pages of this volume.

40 CFR (63.1200 TO END)
ENVIRONMENTAL PROTECTION AGENCY

American Petroleum Institute
1220 L Street, NW., Washington, DC 20005–4070; Telephone: (202) 682–8000

American Society for Testing and Materials
100 Barr Harbor Drive, West Conshohocken, PA 19428–2959; Telephone: (610) 832–9585, FAX: (610) 832–9555
ASTM D 1193–77, Standard Specification for Reagent Water ................ Par. 4.1.1 and par. 4.4.2 of Appendix A to Part 63
ASTM D 1331–89, Standard Test Methods for Surface and Interfacial Tension of Solutions of Surface Active Agents. Par. 3.1 and par. 4.2 of Appendix A to Part 63

National Institute of Standards and Technology
Springfield, VA 22161
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List of CFR Sections Affected

All changes in this volume of the Code of Federal Regulations which were made by documents published in the Federal Register since January 1, 1986, are enumerated in the following list. Entries indicate the nature of the changes effected. Page numbers refer to Federal Register pages. The user should consult the entries for chapters and parts as well as sections for revisions.

Title 40 was established at 36 FR 12213, June 29, 1971. For the period before January 1, 1986, see the "List of CFR Sections Affected, 1964-1972, and 1973-1985," published in seven separate volumes.

1986—1991
(No Regulations Published)

1992
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