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The general provisions reference	That addresses	And applies to subpart WWWW of part 63	Subject to the following additional information
§63.13 §63.14	control agencies and EPA Re- gional Offices. Incorporations by reference	Yes.	
§63.15	Availability of information and con- fidentiality.	Yes.	

APPENDIX A TO SUBPART WWWW OF PART 63—TEST METHOD FOR DETER-MINING VAPOR SUPPRESSANT EFFEC-TIVENESS

#### 1. Scope and Application

1.1 Applicability. If a facility is using vapor suppressants to reduce hazardous air pollutant (HAP) emissions, the organic HAP emission factor equations in Table 1 to this subpart require that the vapor suppressant effectiveness factor be determined. The vapor suppressant effectiveness factor is then used as one of the inputs into the appropriate organic HAP emission factor equation. The vapor suppressant effectiveness factor test is not intended to quantify overall volatile emissions from a resin, nor to be used as a stand-alone test for emissions determination. This test is designed to evaluate the performance of film forming vapor suppressant resin additives. The results of this test are used only in combination with the organic HAP emissions factor equations in Table 1 to this subpart to generate emission factors.

1.1.1 The open molding process consists of application of resin and reinforcements to the mold surface, followed by a manual rollout process to consolidate the laminate, and the curing stage where the laminate surface is not disturbed. Emission studies have shown that approximately 50 percent to 55 percent of the emissions occur while the resin is being applied to the mold. Vapor suppressants have little effect during this portion of the lamination process, but can have a significant effect during the curing stage. Therefore, if a suppressant is 100 percent effective, the overall emissions from the process would be reduced by 45 percent to 50 percent, representing the emissions generated during the curing stage. In actual practice, vapor suppressant effectiveness will be less than 100 percent and the test results determine the specific effectiveness in terms of the vapor suppressant effectiveness factor. This factor represents the effectiveness of a specific combination of suppressant additive and resin formulation

1.1.2 A resin manufacturer may supply a molder with a vapor-suppressed resin, and employ this test to provide the molder with the vapor suppressant effectiveness factor for that combination of resin and vapor sup-

pressant. The factor qualifies the effectiveness of the vapor suppressant when the resin is tested in the specific formulation supplied to the molder. The addition of fillers or other diluents by the molder may impact the effectiveness of the vapor suppressant. The formulation, including resin/glass ratio and filler content, used in the test should be similar to the formulation to be used in production. The premise of this method is to compare laminate samples made with vapor suppressant additive and made without the additive. The difference in emissions between the two yields the vapor suppressant effectiveness factor.

1.1.3 The method uses a mass balance determination to establish the relative loss of the volatile component from unsaturated polyester or vinyl ester resins, with and without vapor suppressant additives. The effectiveness of a specific vapor suppressant and resin mixture is determined by comparing the relative volatile weight losses from vapor suppressed and non-suppressed resins. The volatile species are not separately analyzed. While the species contained in the volatile component are not determined, an extended listing of potential monomer that may be contained in unsaturated polvester or vinvl ester resins is provided in Table 1.1. However, most polyester and vinyl ester resin formulations presently used by the composites industry only contain styrene monomer.

TABLE 1.1—L	ST OF MONOMERS POTENTIALLY
PRESENT IN	UNSATURATED POLYESTER/VINYL
ESTER RESIN	S

Monomer	CAS No.
Styrene	100-42-5.
Vinyl toluene	25013-15-4.
Methyl methacrylate	80-62-6.
Alpha methyl styrene	98-83-9.
Para methyl styrene	Vinyl toluene isomer.
Chlorostyrene	1331-28-8.
Diallyl phthalate	131–17–9.
Other volatile monomers	Various.

#### 2. Summary of Method

2.1 Differences in specific resin and suppressant additive chemistry affect the performance of a vapor suppressant. The purpose of this method is to quantify the effectiveness of a specific combination of vapor

suppressant and unsaturated polyester or vinyl ester resin as they are to be used in production. This comparative test quantifies the loss of volatiles from a fiberglass reinforced laminate during the roll-out and curing emission phases, for resins formulated with and without a suppressant additive. A criterion for this method is the testing of a non-vapor suppressed resin system and testing the same resin with a vapor suppressant. The two resins are as identical as possible with the exception of the addition of the suppressant to one. The exact formulation used for the test will be determined by the in-use production requirements. Each formulation of resin, glass, fillers, and additives is developed to meet particular customer and or performance specifications.

2.2 The result of this test is used as an input factor in the organic HAP emissions factor equations in Table 1 to this subpart, which allows these equations to predict emissions from a specific combination of resin and suppressant. This test does not provide an emission rate for the entire lamination process.

3. Definitions and Acronyms

3.1 Definitions

3.1.1 Vapor suppressant. An additive that inhibits the evaporation of volatile components in unsaturated polyester or vinyl ester resins.

3.1.2 Unsaturated polyester resin. A thermosetting resin commonly used in composites molding.

3.1.3 Unsaturated vinyl ester resin. A thermosetting resin used in composites molding for corrosion resistant and high performance applications.

3.1.4 Laminate. A combination of fiber reinforcement and a thermoset resin.

3.1.5 *Chopped strand mat.* Glass fiber reinforcement with random fiber orientation.

3.1.6 *Initiator*. A curing agent added to an unsaturated polyester or vinyl ester resin.

3.1.7 *Resin application roller*. A tool used to saturate and compact a wet laminate.

3.1.8 *Gel time*. The time from the addition of initiator to a resin to the state of resin gelation.

3.1.9 Filled resin system. A resin, which includes the addition of inert organic or inorganic materials to modify the resin properties, extend the volume and to lower the cost. Fillers include, but are not limited to; mineral particulates; microspheres; or organic particulates. This test is not intended to be used to determine the vapor suppressant effectiveness of a filler.

3.1.10 Material safety data sheet. Data supplied by the manufacturer of a chemical product, listing hazardous chemical components, safety precautions, and required personal protection equipment for a specific product.

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3.1.11 *Tare(ed)*. Reset a balance to zero after a container or object is placed on the balance; that is to subtract the weight of a container or object from the balance reading so as to weigh only the material placed in the container or on the object.

3.1.12 *Percent glass.* The specified glass fiber weight content in a laminate. It is usually determined by engineering requirements for the laminate.

3.2 Acronyms:

3.2.1 VS—vapor suppressed or vapor suppressant.

3.2.2 NVS—non-vapor suppressed.

3.2.3 VSE—vapor suppressant effectiveness.

3.2.4 VSE Factor—vapor suppressant effectiveness, factor used in the equations in Table 1 to this subpart.

3.2.5 CSM—chopped strand mat.

3.2.6 MSDS—material safety data sheet.

#### 4. Interferences

There are no identified interferences which affect the results of this test.

#### 5. Safety

Standard laboratory safety procedures should be used when conducting this test. Refer to specific MSDS for handling precautions.

#### 6. Equipment and Supplies

NOTE: Mention of trade names or specific products or suppliers does not constitute an endorsement by the Environmental Protection Agency.

6.1 Required Equipment.

6.1.1 Balance enclosure.<sup>1</sup>

6.1.2 Two (2) laboratory balances—accurate to  $\pm 0.01$ g.<sup>2</sup>

6.1.3 Stop watch or balance data recording output to data logger with accuracy  $\pm 1$  second.^3

6.1.4 Thermometer—accurate to  $\pm 2.0$   $^\circ F(\pm 1.0\ ^\circ C).^4$ 

 $6.1.5\,$  A lipped pan large enough to hold the cut glass without coming into contact

with the vertical sides, e.g. a pizza pan.<sup>5</sup> 6.1.6 Mylar film sufficient to cover the

bottom of the pan.<sup>6</sup> 6.1.7 Tape to keep the Mylar from shifting

in the bottom of the pan.<sup>7</sup> 6.1.8 Plastic tri-corner beakers of equiva-

lent-250 ml to 400 ml capacity.8

6.1.9 Eye dropper or pipette.<sup>9</sup>

6.1.10 Disposable resin application roller,  $\frac{3}{16''-34''}$  diameter  $\times 3''-6''$  roller length.<sup>10</sup>

6.1.11 Hygrometer or psychrometer<sup>11</sup> accurate to ±5 percent

6.1.12 Insulating board, (Teflon, cardboard, foam board etc.) to prevent the balance from becoming a heat sink.^{12}

6.2 Optional Equipment.

6.2.1 Laboratory balance—accurate to  $\pm.01g$  with digital output, such as an RS-232

bi-directional interface  $^{13}$  for use with automatic data recording devices.

6.2.2 Computer with recording software configured to link to balance digital output. Must be programmed to record data at the minimum intervals required for manual data acquisition.

6.3 Supplies.

6.3.1 Chopped strand mat-1.5 oz/ft.2 14

#### 7. Reagents and Standards

7.1 *Initiator.* The initiator type, brand, and concentration will be specified by resin manufacturer, or as required by production operation.

7.2 Polyester or vinyl ester resin.

7.3 Vapor suppressant additive.

#### 8. Sample Collection, Preservation, and Storage

This test method involves the immediate recording of data during the roll out and curing phases of the lamination process during each test run. Samples are neither collected, preserved, nor stored.

#### 9. Quality Control

Careful attention to the prescribed test procedure, routing equipment calibration, and replicate testing are the quality control activities for this test method. Refer to the procedures in section 11. A minimum of six test runs of a resin system without a suppressant and six test runs of the same resin with a suppressant shall be performed for each resin and suppressant test combination.

#### 10. Calibration and Standardization

10.1 The laboratory balances, stopwatch, hygrometer and thermometer shall be maintained in a state of calibration prior to testing and thereafter on a scheduled basis as determined by the testing laboratory. This shall be accomplished by using certified calibration standards.

10.2 Calibration records shall be maintained for a period of 3 years.

#### 11. Test Procedure

11.1 Test Set-up.

11.1.1 The laboratory balance is located in an enclosure to prevent fluctuations in balance readings due to localized air movement. The front of enclosure is open to permit work activity, but positioned so that local airflow will not effect balance readings. The ambient temperature is determined by suspending the thermometer at a point inside the enclosure.

11.1.2 The bottom of the aluminum pan is covered with the Mylar film. The film is held in position with tape or by friction between the pan and the film.

11.1.3 The resin and pan are brought to room temperature. This test temperature must be between 70 °F and 80 °F. The testing temperature cannot vary more than  $\pm 2$  °F

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during the measurement of test runs. Temperature shall be recorded at the same time weight is recorded on suppressed and nonsuppressed test data sheets, shown in Table 17.1.

11.1.4 The relative humidity may not change more than  $\pm 15$  percent during the test runs. This is determined by recording the relative humidity in the vicinity of the test chamber at the beginning and end of an individual test run. This data is recorded on the test data sheets shown in Table 17.1.

11.1.5 Two plies of nominal 1.5 oz/ft<sup>2</sup> chopped strand mat (CSM) are cut into a square or rectangle with the minimum surface area of 60 square inches (*i.e.* a square with a side dimension of 7.75 inches).

11.1.6 The appropriate resin application roller is readily available.

11.2 Resin Gel Time/Initiator Percentage

11.2.1 Previous testing has indicated that resin gel time influences the emissions from composite production. The testing indicated that longer the gel times led to higher emissions. There are a number of factors that influence gel time including initiator type, initiator brand, initiator level, temperature and resin additives. Under actual usage conditions a molder will adjust the initiator to meet a gel time requirement. In this test procedure, the vapor suppressed and nonvapor suppressed resin systems will be adjusted to the same gel time by selecting the appropriate initiator level for each.

11.2.2 All test runs within a test will be processed in a manner that produces the same resin gel time ±2 minutes. To facilitate the resin mixing procedure, master batches of resin and resin plus vapor suppressant of resin are prepared. These resin master batches will have all of the required ingredients except initiator; this includes filler for filled systems. The gel times for the tests are conducted using the master batch and adjustments to meet gel time requirements shall be made to the master batch before emission testing is conducted. Test temperatures must be maintained within the required range, during gel time testing. Further gel time testing is not required after the non-vapor suppressed and vapor suppressed master batches are established with gel times within +2 minutes. A sufficient quantity of each resin should be prepared to allow for additional test specimens in the event one or more test fails to meet the data acceptance criteria discussed in Section 11.5 and shown in Table 17.2

11.2.3 The specific brand of initiator and the nominal percentage level recommended by the resin manufacturer will be indicated on the resin certificate of analysis<sup>15</sup>; or, if a unique gel time is required in a production laminate, initiator brand and percentage will be determined by that specific requirement.

11.2.4 Examples:

11.2.4.1 The resin for a test run is specified as having a 15-minute cup gel time at 77 °F using Brand X initiator at 1.5 percent by weight. The non-suppressed control resin has a 15-minute gel time. The suppressed resin has a gel time of 17-minutes. An initiator level of 1.5 percent would be selected for the both the non-suppressed and the suppressed test samples.

11.2.4.2 Based on a specific production requirement, a resin is processed in production using 2.25 percent of Brand Y initiator, which produces a 20-minute gel time. This initiator at level of 2.25 percent produces a 20 minute gel time for the non-suppressed control resin, but yields a 25-minute gel time for the suppressed resin sample. The suppressed resin is retested at 2.50 percent initiator and produces a 21-minute gel time. The initiator levels of 2.25 percent and 2.50 percent respectively would yield gel times within ±2 minutes.

11.3 Test Run Procedure for Unfilled Resin (see the data sheet shown in Table 17.1).

11.3.1 The insulating board is placed on the balance.

11.3.2 The aluminum pan with attached Mylar film is placed on the balance, and the balance is tared (weight reading set to zero with the plate on the balance.)

11.3.3 Place two plies of 1.5 oz. CSM on the balance and record the weight (glass weight). 11.3.4 The resin beaker and stirring rod

are put on the second balance and tared.

11.3.5 The required resin weight and initiator weight are calculated (refer to calculation formulas in 12.2).

11.3.6 The disposable resin application roller is placed on the edge of the plate.

11.3.7 The balance is tared, with the aluminum pan, Mylar film, glass mat, and resin application roller on the balance pan.

11.3.8 Resin is weighed into a beaker, as calculated, using the second balance. The mixing stick should be tared with the beaker weight.

11.3.9 Initiator is weighed into the resin, as calculated, using an eyedropper or a pipette, and the combination is mixed.

11.3.10 Initiated resin is poured on chopped strand mat in a pe-determined pattern (see Figure 11.6).

11.3.11 A stopwatch is started from zero.

 $11.3.12\,$  The initial laminate weight is recorded.

11.3.13 The plate is removed from balance to enable roll-out of the laminate.

11.3.14 The wet laminate is rolled with the resin application roller to completely distribute the resin, saturate the chopped strand mat, and eliminate air voids. Roll-out time should be in the range of 2 to  $3^{16}$  minutes and vary less than ±10 percent of the average time required for the complete set of six suppressed and six non-suppressed runs.

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11.3.15 Record the rollout end time (time from start to completion of rollout).

11.3.16 Place the resin application roller on the edge of the plate when rollout is completed.

11.3.17 Place the plate back on the balance pan. Immediately record the weight.

11.3.18 For the first test in a series of six tests, weight is recorded every 5-minute interval (suppressed and non-suppressed). The end of the test occurs when three consecutive equal weights are recorded or a weight gain is observed (the last weight before the increased weight is the end of test weight). For the remaining five tests in the series, after the initial weights are taken, the next weight is recorded 30 minutes before the end of the test, as suggested by the results from the first test. It is likely that the time to reach the end point of a suppressed resin test will be shorter than the time required to complete a non-suppressed test. Therefore, the time to start taking data manually may be different for suppressed and non-suppressed resins.

11.4 Test Run Procedures for Filled Resin Systems<sup>17</sup> Note that the procedure for filled systems differs from the procedure for unfilled systems. With filled systems, resin is applied to one ply of the CSM and the second ply is placed on top of the resin.

11.4.1 The insulating board is placed on the balance.

11.4.2 The aluminum pan with attached Mylar film is placed on the balance, and the balance is tared (weight reading set to zero with the plate on the balance.)

11.4.3 Place two plies of 1.5 oz. CSM on the balance and record the weight (glass weight).

11.4.4 Remove the top ply of fiberglass and record its weight (weight of 1st layer of glass).

11.4.5 The required resin weight and initiator weight are calculated (refer to calculation formulas in 12.2). Calculate the weight of filled resin and initiator based on the 2 layers of fiberglass.

11.4.6 The resin beaker and stirring rod are put on the second balance and tared.

11.4.7 A disposable resin application roller is placed on the edge of the plate.

11.4.8 The balance is tared, with the aluminum pan, Mylar film, glass mat, and resin application roller on the balance pan.

11.4.9 Resin is weighed into the beaker, as calculated, using the second balance. The mixing stick should be tared with the beaker weight.

11.4.10 Initiator is weighed into the resin, as calculated, using an eyedropper or a pipette, and the combination is mixed.

11.4.11 Initiated resin is poured on the single ply of CSM in a pre-determined pattern. Refer to Figure 11.6.

11.4.12 A stopwatch is started from zero. 11.4.13 Record the weight of the resin ans

11.4.13 Record the weight of the resin ans single ply of CSM  $(L_1)$ . The initial laminate

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weight equals  $L_1$  plus the weight of second glass layer.

11.4.14 Replace the second layer of fiberglass.

11.4.15 Remove the plate from the balance to allow roll-out of the laminate.

11.4.16 Roll the wet laminate with the resin application roller to completely distribute the resin, saturate the chopped strand mat, and eliminate air voids. Roll-out time should be in the range of 2 to  $3^{16}$  minutes and vary less than ±10 percent of the average time required for the complete set of six suppressed and six non-suppressed runs.

11.4.17 Record the roll-out end time (time from start to completion of rollout).

11.4.18 Place the resin application roller on the edge of the plate when rollout is completed.

11.4.19 Place the plate back on the balance pan. The initial weight is recorded immediately.

11.4.20 For the first test run in a series of six, weight is recorded at every 5-minute interval (suppressed and non-suppressed). The end of the test occurs when three consecutive equal weights are recorded or a weight gain is observed (the last weight before the increased weight is the end of test weight). For the remaining five tests in the series. after the initial weights are taken, the next weight is recorded 30 minutes before the end of the test, as suggested by the results from the first test. It is likely that the time to reach the end point of a suppressed resin test will be shorter than the time required to complete a non-suppressed test. Therefore, the time to start taking data manually may be different for suppressed and non-suppressed resins.

11.5 Data Acceptance Criteria:

11.5.1 A test set is designed as twelve individual test runs using the same resin,

initiator, and gel time, six of the test runs use the resin non-vapor suppressed and the other six use it vapor suppressed.

11.5.2 If a test run falls outside any of the time, temperature, weight or humidity variation requirements, it must be discarded and run again.

11.5.3 The laminate roll out time for each individual test run must vary less than  $\pm 10$  percent of the average time required for the complete set of six suppressed and six non-suppressed runs.

11.5.4 Test temperature for each test run must be maintained within  $\pm 2$  °F and the average must be between 70° and 80 °F. Refer to 11.1.3.

11.5.5 The difference in the amount of resin for each run must be within  $\pm 10$  percent of the average weight for the complete set of six suppressed and six non-suppressed runs.

11.5.6 The relative humidity from each test run must be within  $\pm 15$  percent of the average humidity for the complete set of six suppressed and six non-suppressed tests. Refer to 11.1.4

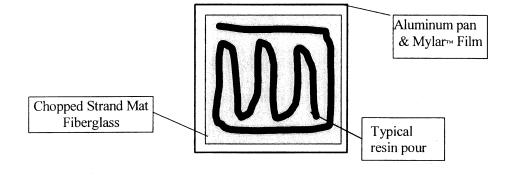
11.5.7 The glass content for each test set must be within  $\pm 10$  percent of the average resin-to-/glass ratio for the complete set of six suppressed and six non-suppressed runs. Refer to 12.2).

11.5.8 The filler content for each test of a test set must be within  $\pm 5$  percent of the average filler content for the complete set of six suppressed and six non-suppressed runs. Refer to 12.2.

11.6 Resin Application Pour Pattern:

11.6.1 To facilitate the distribution of resin across the chopped strand mat, and to provide consistency from test to test, a uniform pour pattern should be used. A typical pour pattern is shown below:

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#### Figure 11.6 Resin Distribution Diagram

11.6.2 The resin is to be evenly distributed across the entire surface of the chopped strand mat using the resin application roller to achieve a wet look across the surface of the laminate. Pushing excess resin off the reinforcement and onto the Mylar sheet should be avoided. No resin is to be pushed more than  $\frac{1}{2}$  inch beyond the edge of the glass mat. If excess resin is pushed further from the glass mat, it will void the test run. As part of this process, typical visible air voids are to be eliminated by the rollout process. If the pour pattern is different from the above, it must be recorded and attached to test data sheet 17.1.

#### 12. Data Analysis and Calculations

12.1 Data Analysis:

This test method requires a simple mass balance calculation, no special data analysis is necessary.

12.2 Calculations:

12.2.1 The target glass content (percent) for unfilled resin systems is determined from the specific production parameters being evaluated. In absence of any specific production requirements the target may be set at the tester's discretion.

 $12.2.2\,$  Glass content determination (expressed as a per cent):

% Glass = Glass wt(g)/(Glass wt(g) + Resin weight (g))

12.2.3 Weight of resin required:

Resin weight required = (Glass wt (g)/% glass)—Glass wt (g)

12.2.4 Filled resin formulation determination for filled resin systems (e.g. >30 percent filler by weight for a particulate filler, or >1 percent by weight for a lightweight filler, such as hollow microspheres):

% Resin content = resin

weight(g)/(resin weight(g) + glass

weight(g) + filler weight(g))

% Glass content = glass

weight(g)/(resin weight(g) + glass

weight(g) + filler weight(g))

Filler content = filler

weight(g)/(resin weight(g) + glass

weight(g) + filler weight(g))

12.2.5 Initiator weight determination:

Initiator weight (g) = Resin weight(g)  $\times$  Initiator %

12.2.6 Emission weight loss determination:

Emissions weight loss (g) = Initial resin weight (g) - Final resin weight (g)

12.2.7 % Emission weight loss:

% Emission Weight Loss = (Emission weight loss (g) Initial resin weight (g)  $\times 100$ 

12.2.8 Average % Emission Weight Loss (assuming six test runs):

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## Average % Emission Weight Loss = $\sum_{i}^{N=6} (\% \text{ Emission Weight Loss}_i)/6$

#### 12.2.9 VSE Factor calculation:

VSE Factor = 1 -(Average % VS Emission Weight Loss/Average NVS Emission Weight Loss)

TABLE	12.1 -	-EXAMPLE	CALCULATION
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Test #	% VS weight loss	% NVS weight loss
1	6.87	10.86
2	6.76	11.23
3	5.80	12.02
4	5.34	11.70
5	6.11	11.91
6	6.61	10.63
Average Weight Loss	6.25	11.39
VSE Factor		0.4

VSE Factor = 0.45

VSE Factor is used as input into the appropriate equation in Table 1 to this subpart. Example from Table 1 to this subpart:

Manual Resin Application, 35 percent HAP resin, VSE Factor of 0.45

HAP Emissions with vapor suppresants =  $((0.286 \times \% HAP) - 0.0529) \times 2000 \times (1 - (0.5 \times$ VSE factor))

HAP Emissions with vapor suppresants =  $((0.286 \times .35) - 0.0529) \times 2000 \times (1 - (0.5 \times .45))$ 

HAP Emissions with vapor suppresants = 73pounds of HAP emissions per ton of resin.

#### 13. Method Performance

13.1 Bias:

The bias of this test method has not been determined.

13.2 Precision Testing

13.2.1 Subsequent to the initial development of this test protocol by the Composites Fabricators Association, a series of tests were conducted in three different laboratory facilities. The purpose of this round robin testing was to verify the precision of the test method in various laboratories. Each laboratory received a sample of an orthophthalic polyester resin from the same production batch, containing 48 per cent styrene by weight. Each testing site was also provided with the same vapor suppressant additive. The suppressant manufacturer specified the percentage level of suppressant additive. The resin manufacturer specified the type and level of initiator required to produce a 20 minute gel time. The target glass content was 30 percent by weight.

13.2.2 Each laboratory independently conducted the VSE test according to this method. A summary of the results is included in Table 13.1.

TABLE 13.1—ROUND ROBIN TESTING RESULTS

	Test	Lab 1	Test I	Lab 2	Test L	.ab 3
	NVS	VS	NVS	S	NVS	VS
Average percent WT Loss Standard Deviation VSE Factor	4.24 0.095	1.15 0.060 0.730	4.69 0.002	1.84 0.002 0.607	5.73 0.020	1.61 0.003 0.720

13.3 Comparison to EPA Reference Methods This test has no corresponding EPA reference method.

#### 14. Pollution Prevention

The sample size used in this method produces a negligible emission of HAP, and has an insignificant impact upon the atmosphere.

#### 15. Waste Management

The spent and waste materials generated during this test are disposed according to required facility procedures, and waste management recommendations on the corresponding material safety data sheets.

#### 16. References and footnotes

#### 16.1 Footnotes:

<sup>1</sup>Balance Enclosure—The purpose of the balance enclosure is to prevent localized airflow from adversely affecting the laboratory balance. The enclosure may be a simple three-sided box with a top and an open face. The configuration of the enclosure is secondary to the purpose of providing a stable and steady balance reading, free from the effects of airflow, for accurate measurements. The enclosure can be fabricated locally. A typical enclosure is shown in Figure 17.1.

<sup>2</sup>Laboratory Balance-Ohaus Precision Standard Series P/N TS400D or equivalent-Paul N. Gardner Co. 316 NE 1st St. Pompano Beach, FL 33060 or other suppliers.

<sup>3</sup>Stop Watch—Local supply.

<sup>4</sup>Thermometer—Mercury thermometer— ASTM No. 21C or equivalent; Digital thermometer—P/N TH-33033 or equivalent—Paul N. Gardner Co. 316 NE 1st St. Pompano Beach, FL 33060 or other suppliers.

<sup>5</sup>Aluminum Pan—Local supply.

<sup>6</sup>Mylar—Local supply.

<sup>7</sup>Double Sided Tape—3M Double Stick Tape or equivalent, local supply.

<sup>8</sup>Laboratory Beakers—250 to 400ml capacity—Local laboratory supply.

<sup>9</sup>Eye Dropper or Pipette—Local laboratory supply.

<sup>10</sup>Disposable Resin Application Roller Source—Wire Handle Roller P/N 205-050-300 or Plastic Handle Roller P/N 215-050-300 or equivalent; ES Manufacturing Inc., 2500 26st Ave. North, St. Petersburg, FL 33713, www.esmfg.com, or other source. Refer to Figure 17.3.

<sup>11</sup>Hygrometer or Psychrometer—Model# THWD-1, or equivalent—Part # 975765 by Amprobe Instrument, 630 Merrick Road, P.O. Box 329, Lynbrook, NY 11563, 516-593-5600

<sup>12</sup>Insulating Board (Teflon, cardboard, foam board etc.)—Local supply.

<sup>13</sup>Laboratory Balance With Digital Output—Ohaus Precision Standard Series P/N TS120S or equivalent—Paul N. Gardner Co. 316 NE 1st St. Pompano Beach, FL 33060 or other suppliers.

<sup>14</sup>Chopped Strand Mat—1.5 oz/ft<sup>2</sup> Sources: Owens Corning Fiberglas—Fiberglas M-723; PPG Industries—ABM HTX; Vetrotex America—M-127 or equivalent.

 $^{15}$  Certificate of Analysis: Resin gel time, as recorded on the resin certificate of analysis, is measured using a laboratory standard gel time procedure. This procedure typically uses a 100 gram cup sample at 77 °F (25 °C),

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a specific type of initiator and a specified percentage.

<sup>16</sup>Roll-out times may vary with resin viscosity or resin additive. The important aspect of this step is to produce the same rollout time for both the suppressed and nonsuppressed samples.

<sup>17</sup>While this test can be used with filled resin systems, the test is not designed to determine the effect of the filler on emissions, but rather to measure the effect of the suppressant additive in the resin system. When evaluating a filled system both the nonvapor suppressed and vapor suppressed samples should be formulated with the same type and level of filler.

16.2 References

1. Phase 1—Baseline Study Hand Lay-up, CFA, 1996

2. CFA Vapor Suppressant Effectiveness Test Development, 4/3/98, correspondence with Dr. Madeleine Strum, EPA, OAQPS

3. CFA Vapor Suppressant Effectiveness Screening Tests, 4/4/98

4. Styrene Suppressant Systems Study, Reichhold Chemical, 11/30/98

5. Evaluation of the CFA's New Proposed Vapor Suppressant Effectiveness Test, Technical Service Request #: ED-01-98, BYK Chemie, 6/3/98

6. Second Evaluation of the CFA's New Proposed Vapor Suppressant Effectiveness Test, Technical Service Request #: ED-02-98, BYK Chemie, 1/26/99

#### 17. Data Sheets and Figures

17.1 This data sheet, or a similar data sheet, is used to record the test data for filled, unfilled, suppressed and non-suppressed tests. If additional time is required, the data sheet may be extended.

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Table 17.1 Test Data Sheet

<u>T</u>	est Number			<u>Test Type</u>		
			VS (_	)	NVS ()	
Resin			Filled (	)	Unfilled ()	
Initiator				Initiator, %		
Vapor Sup	pressant			VS, %		
Weight of 2 layers of glass, g		Weight of 1 <sup>st</sup> glass layer, g		Weight of 2 <sup>nd</sup> glass layer, g		
Initial R Weight,(g			Time (Min.)	Weight g	Temp °F	
Glass con	tent, (%)		55			
Initial Temperature <sup>0</sup> F:			60 £			
Initial Humidity %			65			
Resin Ini Level,%	tiator		70			
Resin gel time, (min.)			75			
Resin filler content, %			80			
Roll out (min.)	time,		85			
Time, (min.)	Weight, g	Temp, <sup>°</sup> F	90			

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Initial			95		
			100		
0			105		
5			110		
10			115		
15			120		
20			125		
25			130		
30			135		
35			140		
40			145		
45			150		
50			155		
Final Time, min.	Final Wei	ght, g.	Final Temp, °F	Final Humid	ity, %

17.2 Data Acceptance Criteria Worksheet: The following worksheet is used to determine the quality of collected data (*i.e.* insure

the data collected all meets acceptance criteria)

Test No.	u W	Temperature	Delta	Laminate roll out time, min	Relative h Initial	Relative humidity. % Initial Final	Resin weight, (g)	Resin weight, Glass content, %	Resin distribution	Meets criteria V/N
12 Criteria	Average   ±2 ∘F	±10% of Average	±15 of Av- erade	±15 of Average	±10% of Avg.	±10% of Avg.	<1/2 inch off mat	All Y		

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17.3 VSE Factor Calculation

TABLE 17.3—CALCULATIONS WORKSHEET

Vapor suppressed		Non-vapor suppressed		
Test #	% Weight loss	Test #	% Weight loss	
Average Weight Loss				
VSE Fa	actor			

VSE Factor = 1—(% Average Weight Loss  $_{\rm VS}$  / % Average Weight Loss  $_{\rm NVS})$ 

17.4 Figures

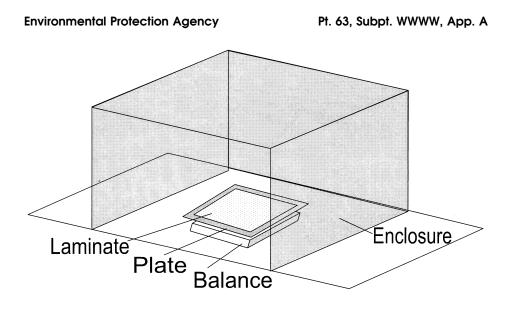


Figure 17.1. Typical Balance Enclosure

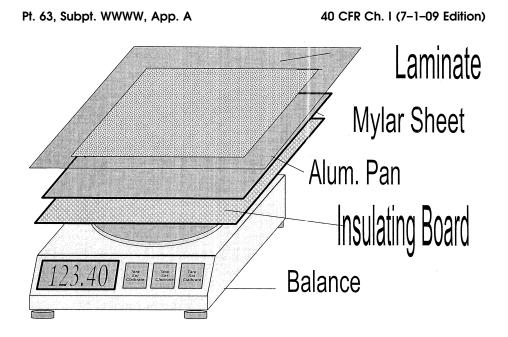
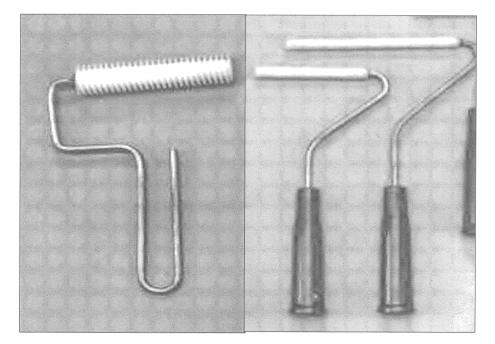


Figure 17.2. Scale, Plate, Insulating Board, Mylar, Laminate Order

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# **FRP** Rollers

#### Figure 17.3. Typical FRP Rollers

#### Subpart XXXX—National Emissions Standards for Hazardous Air Pollutants: Rubber Tire Manufacturing

SOURCE:  $67\,$  FR 45598, July 9, 2002, unless otherwise noted.

WHAT THIS SUBPART COVERS

## §63.5980 What is the purpose of this subpart?

This subpart establishes national emission standards for hazardous air pollutants (NESHAP) for rubber tire manufacturing. This subpart also establishes requirements to demonstrate