§ 91.417 Fuel flow measurement specifications.

(a) Fuel flow measurement is required only for raw testing but is allowed for dilute testing.

(b) The fuel flow rate measurement instrument must have a minimum accuracy of ±2 percent of full-scale flow rate for each measurement range used.

§91.418 Data evaluation for gaseous emissions.

For the evaluation of the gaseous emissions recording, record the last two minutes of each mode and determine the average values for HC, CO, CO_2 , and NO_X during each mode from the average concentration readings determined from the corresponding calibration data.

§91.419 Raw emission sampling calculations.

(a) Derive the final test results through the steps described in this section.

(b) Air and fuel flow method. If both air and fuel flow mass rates are measured, the following equations are used to determine the weighted emission values for the test engine:

$$\begin{aligned} W_{\text{NO}_{\text{X}}} &= \left(G_{\text{AIRD}} + G_{\text{FUEL}}\right) \times \frac{M_{\text{NO}_{2}}}{M_{\text{exh}}} \times \text{WNO}_{\text{X}} \times K_{\text{H}} \times \frac{1}{10^{6}} \\ W_{\text{HC}} &= \left(G_{\text{AIRD}} + G_{\text{FUEL}}\right) \times \frac{M_{\text{HC}_{\text{exh}}}}{M_{\text{exh}}} \times \text{WHC} \times \frac{1}{10^{6}} \\ W_{\text{CO}} &= \left(G_{\text{AIRD}} + G_{\text{FUEL}}\right) \times \frac{M_{\text{CO}}}{M_{\text{exh}}} \times \text{WCO} \times \frac{1}{10^{2}} \end{aligned}$$

Where:

W_{HC} = Mass rate of HC in exhaust [g/hr],

G_{AIRD} = Intake air mass flow rate on dry basis [g/hr],

G_{FUEL} = Fuel mass flow rate [g/hr],

 M_{HCexh} = Molecular weight of hydrocarbons in the exhaust; see the following equation:

 $M_{HCexh} = 12.01 + 1.008 \times \alpha$

Where:

 α =Hydrocarbon/carbon atomic ratio of the fuel.

M_{exh}=Molecular weight of the total exhaust; see the following equation:

$$\begin{split} \mathbf{M}_{\text{exh}} &= \frac{\mathbf{M}_{\text{HC}_{\text{exh}}} \times \text{WHC}}{10^6} + \frac{28.01 \times \text{WCO}}{10^2} + \frac{44.1 \times \text{WCO}_2}{10^2} \\ &+ \frac{46.01 \times \text{WNO}_x}{10^6} + \frac{2.016 \times \text{WH}_2}{10^2} + 18.01 \times (1 - \text{K}) \\ &+ 28.01 \times \underbrace{\left[100 - \frac{\text{WHC}}{10^4} - \text{WCO} - \text{WCO}_2 - \frac{\text{WNO}_x}{10^4} - \text{WH}_2 - 100 \times (1 - \text{K}) \right]}_{10^2} \end{split}$$

Where:

 $\label{eq:WHC} \mbox{WHC = HC volume concentration in exhaust,} \\ \mbox{ppmC wet}$

WCO = CO percent concentration in the exhaust, wet

DCO = CO percent concentration in the exhaust, dry

 $WCO_2 = CO_2$ percent concentration in the exhaust, wet

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 $DCO_2 = CO_2$ percent concentration in the exhaust, dry

 $WNO_X = NO$ volume concentration in exhaust, ppm wet

 $WH_2 = H_2$ percent concentration in exhaust, wet

K = correction factor to be used when converting dry measurements to a wet basis. Therefore, wet concentration = dry concentration $\times K$, where K is:

$$\frac{1}{1+0.005\times(DCO+DCO_2)\times\alpha-0.01\times DH_2}$$

 $DH_2 = H_2$ percent concentration in exhaust, dry, calculated from the following equation:

$$DH_2 = \frac{0.5 \times \alpha \times DCO \times (DCO + DCO_2)}{DCO + (3 \times DCO_2)}$$

 W_{CO} = Mass rate of CO in exhaust, [g/hr]

 $\rm M_{\rm CO} = Molecular$ weight of CO = 28.01

 W_{NOx} = Mass rate of NO_X in exhaust, [g/hr]

 $M_{\rm NO2}$ = Molecular weight of NO_2 = 46.01

 K_H = Factor for correcting the effects of humidity on NO_2 formation for four-stroke gasoline engines; see the equation below:

$$K_{H} = \frac{1}{1 - 0.0329 \times (H - 10.71)}$$

Where:

 H = specific humidity of the intake air in grams of moisture per kilogram of dry air.
For two-stroke gasoline engines, KH should be set to 1.

(c) Fuel flow method. The following equations are to be used when fuel flow is selected as the basis for mass emission calculations using the raw gas method.

$$\begin{split} W_{HC} &= \frac{G_{FUEL}}{TC} \times \frac{WHC}{10^4} \\ W_{CO} &= \frac{M_{CO}}{M_F} \times \frac{G_{FUEL}}{TC} \times WCO \\ W_{NO_X} &= \frac{M_{NO_X}}{M_F} \times \frac{G_{FUEL}}{TC} \times \frac{WNO_X}{10^4} \times K_H \end{split}$$

Where:

 W_{HC} = Mass rate of HC in exhaust, [g/hr] M_F = Molecular weight of test fuel; see following equation:

$$M_F = 12.01 + 1.008 \times \alpha$$

G_{FUEL} = Fuel mass flow rate, [g/hr] TC = Total carbon; see following equation:

$$TC = WCO + WCO_2 + \frac{WHC}{10^4}$$

WHC = HC volume concentration in exhaust, ppmC wet

WCO = CO percent concentration in the exhaust, wet

DCO = CO percent concentration in the exhaust, dry

WCO₂ = CO₂ percent concentration in the exhaust, wet

 $DCO_2 = CO_2$ percent concentration in the exhaust, dry

 WNO_X = NO volume concentration in exhaust, ppm wet

 $WH2 = \overline{H_2}$ percent concentration in exhaust, wet

K = correction factor to be used when converting dry measurements to a wet basis. Therefore, wet concentration = dry concentration × K, where K is:

$$K = \frac{1}{1 + 0.005 \times (DCO + DCO_2) \times \alpha - 0.01 \times DH_2}$$

 $DH_2 = H_2$ percent concentration in exhaust, dry, calculated from the following equation:

$$DH_2 = \frac{0.5 \times \alpha \times DCO \times (DCO + DCO_2)}{DCO + (3 \times DCO_2)}$$

 W_{CO} = Mass rate of CO in exhaust, [g/hr]

 M_{CO} = Molecular weight of CO = 28.01

 $W_{\rm NOx}$ = Mass rate of NOx in exhaust, [g/hr]

 $M_{NO2} = Molecular$ weight of $NO_2 = 46.01$

 K_H = Factor for correcting the effects of humidity on NO_2 formation for four-stroke gasoline engines; see the equation below:

$$K_{H} = \frac{1}{1 - 0.0329 \times (H - 10.71)}$$

Where:

 H = specific humidity of the intake air in grams of moisture per kilogram of dry air.
For two-stroke gasoline engines, KH should be set to 1.

(d) The final reported emission test results must be computed by using the following formula for each individual gas component:

$$Y_{wm} = \frac{\sum (W_i \times f_i)}{\sum (P_i \times f_i)}$$

Where:

 Y_{wm} = Weighted mass emission level (HC, CO, NO_X) for a test [g/kW-hr].

 W_i = Average mass flow rate (W_{HC} , W_{CO} , W_{NOx}) of an emission from the test engine during mode i, [g/hr].

 f_i = Weighting factors for each mode according to $\S 91.410(a)$

P_i = Average power measured during mode i, [kW], calculated according to the formula given in §91.423(b). Power for the idle mode shall always be zero for this calculation.

(e) The final reported weighted brake-specific fuel consumption (WBSFC) shall be computed by use of the following formula:

WBSFC =
$$\frac{\sum (F_i \times f_i)}{\sum (P_i \times f_i)}$$

Where:

WBSFC = Weighted brake-specific fuel consumption in grams of fuel per kilowatthour (g/kW-hr).

 F_i = Fuel mass flow rate of the engine during mode i, [g/hr].

 f_i = Weighting factors for each mode according to $\S91.410(a)$

P_i = Average power measured during mode i, [kW], calculated according to the formula given in §91.423(b). Power for the idle mode shall always be zero for this calculation.

[61 FR 52102, Oct. 4, 1996, as amended at 67 FR 68340, Nov. 8, 2002; 70 FR 40452, July 13, 2005]

§91.420 CVS concept of exhaust gas sampling system.

(a) A dilute exhaust sampling system is designed to directly measure the true mass of emissions in engine exhaust without the necessity of measuring either fuel flow or intake air flow. This is accomplished by diluting the exhaust produced by an engine under test with ambient background air and measuring the total diluted exhaust flow rate and the concentration of emissions within the dilute flow. Total mass flow of an emission is then easily calculated.

(b) A constant volume sampler (CVS) is typically used to control the total amount of dilute flow through the system. As the name implies, a CVS restricts flow to a known value dependent only on the dilute exhaust temperature and pressure.

(c) For the testing described in this subpart, a CVS must consist of: A mixing tunnel into which the engine exhaust and dilutant (background) air are dumped; a dilute exhaust flow metering system; a dilute exhaust sample port; a background sample port; a dilute exhaust sampling system; and a background sampling system.

(1) Mixing tunnel. The mixing tunnel must be constructed such that complete mixing of the engine exhaust and background air is assured prior to the sampling probe.

(2) Exhaust flow metering system. A dilute exhaust flow metering system must be used to control the total flow