by the power absorption unit. The dynamometer is driven above the test speed range. The device used to drive the dynamometer is then disengaged from the dynamometer and the roll(s) is (are) allowed to coast down. The kinetic energy of the system is dissipated by the dynamometer. This method neglects the variations in roll bearing friction due to the drive axle weight of the vehicle. In the case of dynamometers with paired rolls, the inertia and power absorption of the free (rear) roll may be neglected if its inertia is less than 3.0 percent of the total equivalent inertia required for vehicle testing.

(1) Devise a method to determine the speed of the roll(s) to be measured for power absorption. A fifth wheel, revolution pickup, or other suitable means may be used.

(2) Place a vehicle on the dynamometer or devise another method of driving the dynamometer.

(3) If the dynamometer is capable of simulating more than a single inertia mass, engage the inertial flywheel or other inertial simulation system for the most common vehicle mass category for which the dynamometer is used. In addition, other vehicle mass categories may be calibrated, if desired.

(4) Drive the dynamometer up to 50 mph (80.5 km/hr).

(5) Record indicated road power.

(6) Drive the dynamometer up to 60 mph (96.9 km/hr).

(7) Disengage the device used to drive the dynamometer.

(8) Record the time for the dynamometer roll(s) to coastdown from 55.0 mph (88.5 km/h) to 45.0 mph (72.4 km/hr).

(9) Adjust the power absorption unit to a different level.

(10) Repeat steps (4) to (8) above sufficient times to cover the range of road power used.

(11) Calculate absorbed road power (\(HP_d\)). (See paragraph (c) of this section.)

(12) Plot indicated road load power at 50 mph (80.5 km/hr) versus road load power at 50 mph (80.5 km/hr).

(b) The performance check consists of conducting a dynamometer coastdown and comparing the coastdown time to that recorded during the last calibration. If the coastdown times differ by more than 1 second or by 5 percent of the time recorded during the last calibration, whichever is greater, a new calibration is required.

(c) Calculations. The road load power actually absorbed by each roll assembly (or roll-inertia weight assembly) of the dynamometer is calculated from the following equation:

\[
HP_d = \frac{1}{2} \left( \frac{W}{32.2} \right) (V_1^2 - V_2^2) / 550t
\]

Where:

\(HP_d\) = Power, horsepower (kilowatts)

\(W\) = Equivalent inertia, lb (kg)

\(V_1\) = Initial velocity, ft/s (m/s) (55 mph = 88.5 km/h = 80.67 ft/s = 24.58 m/s)

\(V_2\) = Final velocity, ft/s (m/s) (45 mph = 72.4 km/h = 66 ft/s = 20.11 m/s)

\(t\) = Elapsed time for rolls to coast from 55 mph to 45 mph (88.5 to 72.4 km/hr).

(Expressions in parenthesis are for SI units).

When the coastdown is from 55 to 45 mph (88.5 to 72.4 km/hr) the above equation reduces to:

\[
HP_d = 0.06073 \left( \frac{W}{t} \right)
\]

For SI units:

\[
HP_d = 0.09984 \left( \frac{W}{t} \right)
\]

The total road load power actually absorbed by the dynamometer is the sum of the absorbed road load power of each roll assembly.
(1) Follow the manufacturer’s instructions or good engineering practice for instrument startup and basic operating adjustment using the appropriate FID fuel and zero-grade air.

(2) Optimize on the most common operating range. Introduce into the analyzer a propane (or methane as appropriate) in air mixture with a propane (or methane as appropriate) concentration equal to approximately 90 percent of the most common operating range.

(3) Select an operating FID fuel flow rate that will give near maximum response and least variation in response with minor fuel flow variations.

(4) To determine the optimum air flow, use the FID fuel flow setting determined above and vary air flow.

(5) After the optimum flow rates have been determined, record them for future reference.

(b) Initial and periodic calibration. Prior to its introduction into service and monthly thereafter the FID hydrocarbon analyzer shall be calibrated on all normally used instrument ranges, and, if applicable, the methanol response factor shall be determined (paragraph (c) of this section). Use the same flow rate as when analyzing sample.

(1) Adjust analyzer to optimize performance.

(2) Zero the hydrocarbon analyzer with zero-grade air.

(c) FID response factor to methanol. When the FID analyzer is to be used for the analysis of hydrocarbon samples containing methanol, the methanol response factor of the analyzer shall be established. The methanol response factor shall be determined at several concentrations in the range of concentrations in the exhaust sample, using either bag samples or gas bottles meeting the requirements of §86.114.

(1) The bag sample of methanol for analysis in the FID, if used, shall be prepared using the apparatus shown in Figure M90–1. A known volume of methanol is injected, using a microliter syringe, into the heated mixing zone (250 °F (121 °C) of the apparatus. The methanol is vaporized and swept into the sample bag with a known volume of zero grade air measured by a gas flow meter with an accuracy of ±2 percent.
(2) The bag sample is analyzed using the FID.

(3) The FID response factor, r, is calculated as follows:

\[ r = \frac{\text{FID ppm}}{\text{SAM ppm}} \]

Where:

(i) \( r \) = FID response factor.

(ii) \( F\) = FID ppm

(iii) \( S\) = SAM ppm

**FIGURE M90-1 APPARATUS FOR PREPARATION OF FID METHANOL RESPONSE CALIBRATION MIX**
(ii) \( \text{FID}_{\text{ppm}} = \text{FID reading in ppmC} \).

(iii) \( \text{SAMppm} = \text{methanol concentration in the sample bag, or gas bottle, in ppmC} \). \( \text{SAMppm} \) for sample bags:

\[
0.02406 \times \text{Fuel injected} \times \text{Fuel density} = \text{Air volume} \times \text{Mol. Wt. CH}_3\text{OH}
\]

Where:

(iv) \( 0.02406 = \text{Volume of one mole at 29.92 in Hg and 68 °F, m}^3 \).

(v) \( \text{Fuel injected} = \text{Volume of methanol injected, ml} \).

(vi) \( \text{Fuel density} = \text{Density of methanol, 0.7914 g/ml} \).

(vii) \( \text{Air volume} = \text{Volume of zero grade air, m}^3 \).

(viii) \( \text{Mol. Wt. CH}_3\text{OH} = 32.04 \).

(d) The gas chromatograph used in the analysis of methanol samples shall be calibrated at least monthly following manufacturers’ recommended procedures (certain equipment may require more frequent calibration based on use and good engineering judgment).

(e) \( \text{FID response factor to methane} \). When the FID analyzer to be used for the analysis of natural gas-fueled vehicle hydrocarbon samples has been calibrated using propane, the methane response factor of the analyzer shall be established. To determine the total hydrocarbon FID response to methane, known methane in air concentrations traceable to National Institute of Standards and Technology (NIST) shall be analyzed by the FID. Several methane concentrations shall be analyzed by the FID in the range of concentrations in the exhaust sample. The total hydrocarbon FID response to methane is calculated as follows:

\[
\text{r}_{\text{CH}_4} = \frac{\text{FIDppm}}{\text{SAMppm}}
\]

Where:

(1) \( \text{r}_{\text{CH}_4} = \text{FID response factor to methane} \).

(2) \( \text{FIDppm} = \text{FID reading in ppmC} \).

(3) \( \text{SAMppm} = \text{the known methane concentration in ppmC} \).

[54 FR 14566, Apr. 11, 1989, as amended at 59 FR 48523, Sept. 21, 1994; 60 FR 34361, June 30, 1995]

§ 86.1228–85 Calibration of other equipment.

Other test equipment used for testing shall be calibrated as often as required by the manufacturer or as necessary according to good practice.

§ 86.1227–96 Test procedures; overview.

(a) The overall test consists of prescribed sequences of fueling, parking, and operating conditions. Vehicles are tested only for evaporative emissions.

(b) The evaporative emission test (gasoline-fueled, natural gas-fueled, liquefied petroleum gas-fueled, and methanol-fueled vehicles) is designed to determine hydrocarbon and/or methanol evaporative emissions as a consequence of diurnal temperature fluctuation urban driving and hot soaks during engine-off periods. It is associated with a series of events representative of heavy-duty vehicle operation, which result in hydrocarbon and/or methanol vapor losses. The test procedure is designed to measure:

(1) Diurnal emissions resulting from daily temperature changes (as well as relatively constant resting losses), measured by the enclosure technique (see §86.1233);

(2) Running losses resulting from a simulated trip on a chassis dynamometer, measured by the enclosure or point-source technique (see §86.1234; this test is not required for gaseous-fueled vehicles); and

(3) Hot soak losses, which result when the vehicle is parked and the hot engine is turned off, measured by the enclosure technique (see §86.1238).

(c) Background concentrations are measured for all species for which emissions measurements are made. For evaporative testing, this requires measuring initial concentrations. (When testing methanol-fueled vehicles, manufacturers may choose not to measure background concentrations of methanol, and then assume that the concentrations are zero during calculations.)

[58 FR 16952, Mar. 24, 1993, as amended at 59 FR 48523, Sept. 21, 1994; 60 FR 34363, June 30, 1995]

§ 86.1228–85 Transmissions.

(a) All test conditions, except as noted, shall be run in a manner representative of in-use operation, and where appropriate, according to the